



HAL
open science

Methodology for sizing and optimising a Blended Wing-Body with distributed electric ducted fans

Alessandro Sgueglia

► **To cite this version:**

Alessandro Sgueglia. Methodology for sizing and optimising a Blended Wing-Body with distributed electric ducted fans. Mechanical engineering [physics.class-ph]. ISAE - Institut Supérieur de l'Aéronautique et de l'Espace, 2019. English. NNT : . tel-02487044

HAL Id: tel-02487044

<https://hal.science/tel-02487044v1>

Submitted on 21 Feb 2020

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



THÈSE

En vue de l'obtention du

DOCTORAT DE L'UNIVERSITÉ DE TOULOUSE

Délivré par : *l'Institut Supérieur de l'Aéronautique et de l'Espace (ISAE)*

Présentée et soutenue le *10/12/2019* par :

Alessandro SGUEGLIA

Methodology for sizing and optimising a Blended Wing-Body with distributed electric ducted fans

JURY

YVES GOURINAT	ISAE-Supaero	President
DIMITRI MAVRIS	Georgia Institute of Technology	External referee
TREVOR M. YOUNG	University of Limerick	External referee
CHRISTIAN BES	Université Paul Sabatier	Examiner
FABRIZIO NICOLSI	Università degli Studi di Napoli "Federico II"	Examiner
ROELOF VOS	Technische Universiteit Delft	Examiner
JOSEPH MORLIER	ISAE-Supaero	Advisor
NATHALIE BARTOLI	ONERA	Co-Advisor

École doctorale et spécialité :

AA : Aéronautique et Astronautique

Unité de Recherche :

Equipe MOIS – Modélisation et Ingénierie des Systèmes – ISAE & ONERA

Directeur(s) de Thèse :

Joseph MORLIER et Nathalie BARTOLI

Rapporteurs :

Dimitri MAVRIS et Trevor M. YOUNG

*“Considerate la vostra semenza:
fatti non foste per viver come bruti
ma per seguir virtute e canoscenza.”*

*[“Consider well the seed that gave you birth:
you were not made to live as brutes,
but to follow virtue and knowledge.”]*

*Dante Alighieri
La Divina Commedia, Inferno, XXVI, 118–120*

Contents

Acknowledgements	vii
Summary	ix
Nomenclature	xiii
Acronyms	xvii
List of figures	xix
List of tables	xxvii
Introduction	1
1 Advanced aircraft design process: a technology review	5
1.1 The environmental context	9
1.2 Aircraft conceptual design cycle	11
1.3 Key innovative aircraft technologies	15
1.4 The research problem	38
2 Development of an optimisation framework for conceptual aircraft design	45
2.1 Introduction	49
2.2 The sizing tool FAST	49
2.3 OpenMDAO – a multidisciplinary optimisation platform	70

2.4	The integrated platform FAST and OpenMDAO	73
2.5	Conclusion	88
3	Design methodology and exploration of hybrid aircraft	91
3.1	Introduction	95
3.2	Presentation of the proposed concept	96
3.3	Definition of a hybrid propulsive chain	98
3.4	Methodology for the sizing of hybrid aircraft	115
3.5	Exploration of hybrid aircraft with distributed electric propulsion	122
3.6	Conclusion	149
4	Design methodology and exploration of the Blended Wing-Body concept	153
4.1	Introduction	157
4.2	Development of models tailored to Blended Wing-Body sizing	158
4.3	Methodology for the Blended Wing-Body sizing	191
4.4	The Blended Wing-Body featuring conventional propulsion	195
4.5	The Blended Wing-Body with distributed electric propulsion	201
4.6	Conclusions	215
	Conclusions and perspectives	221
	Bibliography	226
	Appendix A FAST I/O file structure	255
	Appendix B Review of MDO architecture	257
B.1	An introduction to the MDO	257
B.2	A survey of monolithic architectures	260
	Appendix C Polynomial Chaos Expansion method for global sensitivity analysis	267

Appendix D Plot of sensitivity analysis results	271
D.1 2035 assessment – fixed battery case	271
D.2 2035 assessment – battery resizing	274
D.3 Tube-and-wing with distributed electric propulsion case	276

Acknowledgments

And so, as every journey, this one comes to an end too. A journey started 3 years ago, a morning of january 2017: it is incredible that 3 years have already been passed since then. During this time a lot of people supported me: tenth of pages will not be enough to mention all, but I am in duty to thanks some of them in these short lines.

First of all, special mention to my Ph.D. directors and supervisors: Nathalie Bartoli, Peter Schmollgruber, Emmanuel Benard and Joseph Morlier. Without you, this achievement would have never seen an end. I hope that you had a great time as I did working with you.

Thanks to Prof. Dimitri Mavris and Dr. Trevor Young, who reviewed the work, and to the jury members, who joined the Ph.D. viva: Prof. Yves Gourinat, Prof. Christian Bes, Dr. Roelof Vos, and Prof. Fabrizio Nicolosi.

Thanks to all the colleagues from DTIS department at ONERA, who take part to the Ph.D. with their suggestions and advice: in particular, I would like to mention Sebastien Defoort, Jean Hermetz, Michael Ridel, David Donjat, Rémi Lafage, Julie Gauvrit-Ledogar, Jean Hermetz, Sylvain Dubreuil.

Thanks to Serge Bonnet, Marylène Duffau and Guillame Gallant from AIRBUS, for their collaboration in the Chair CEDAR framework.

Thanks also to Prof. Martins and Dr. John Jasa for the MDO Lab. at University of Michigan, as well as Dr. Justin Gray from NASA Glenn Research Centre and Dr. John Hwang from University of California San Diego, for their contribution to the Ph.D., and a special mention to the Formation Doctorale of ISAE-Supaero who funded the visit at MDO Lab. in 2018.

My neverending gratitude to the MAE students from ISAE-Supaero I had the honour to supervise: Larissa Cristina e Cunha Lima, Diana Aboub Karhim, Luca Cerquetani, Pablo Rodriguez Otiero, Harleen Kaur, Paolo Traverso, Sessa Sai Chandini Yella. Without the work you did in the Blended Wing-Body project, this research would be surely poorer than it is.

And now, let pass to some more personal acknowledgments. At the beginning, my intention was to simply write “to me”, meaning that this achievement was due to myself, but

none is so far from reality. If I arrived at this point, it is mainly because of my friends, who have always been from my side. First, thanks to all the people from ONERA: Morgane Menz, Gabriel Sarazin, Rémy Priem, Tiphaine Sabatier, Marco Saporito, Joan Mas Colomer, Lynda Ait Oubelli, Maxime El Masri, Gaspard Berthelin and Vincenzo Palladino. You were more than colleagues, you were friends.

To Alessia, who did not hesitate to take a plane to be here with me in this day: you are really special, and you do not stop to show me that, day by day.

To Nicola and Alex: our friendship last since our childhood, and despite the kilometers that divide us they will never end to stay close with me.

To my beloved Antonella, one of my favourite people in the world, as a source of unlimited suggestions and comfort. And thank also for saving me during your imaginary apocalypses, soon or later I will appreciate that. . .

Last, but absolutely not least, to Sara, who is the demonstration that sometimes sisterhood is a matter of heart and not blood: thank you for have never given up on me, and trusted me even when I did not. This is for you.

Finally, to whom has been and always will be with me: my parents and my brother.

Well now, was that all of them? Who knows. . . Only one thing is certain, the best is yet to come.

Abstract — The increase of air traffic in the last decades and its projections pose a key challenge towards the carbon neutral growth objective. To cope with this societal goal, there is a need for disruptive air transport aircraft concepts featuring new technologies with low environmental impact. Such future air vehicle relies on the various interactions between systems, disciplines and components. This Ph.D. research thus focuses on the development of a methodology dedicated to the exploration and performance evaluation of unconventional configurations using innovative propulsion concepts. The use case to be considered is the optimisation at conceptual level of a Blended Wing-Body with distributed electric propulsion, a promising concept which combines high aerodynamic performances and benefits from electric propulsion.

The optimisation process based on FAST, the ISAE-SUPAERO / ONERA aircraft sizing tool, has been implemented within OpenMDAO, the NASA open-source multidisciplinary analysis and optimisation framework. With the idea of a progressive enhancement of the multidisciplinary design analysis and a better capture of the different effects, the two pioneering elements have been studied separately. First, the classical process has been revised to take into account the new hybrid powerplant. Second, a methodology has been revised to consider a radically new airframe design. Last, a design process featuring both innovative aspects has been developed to investigate a Blended Wing Body concept with distributed electric propulsion.

Concerning the design process, results show that the use of gradients in the optimisation procedure speeds up the process against a gradient-free method up to 70%. This is an important gain in time that facilitates designer's tasks. For the disruptive concept performances, results have been compared to the ones obtained for a conventional A320 type aircraft based on the same top level requirements and technological horizon. Overall, the hybrid electric propulsion concept is interesting as it allows zero emissions for Landing/Take-Off operations, improving the environmental footprint of the aircraft: fuel can be saved for missions below a certain range. This limitation is associated to the presence of batteries: indeed they introduce indeed a relevant penalty in weight that cannot be countered by benefits of electrification for longer range. Additional simulations indicate that a Blended Wing-Body concept based on a turbo-electric only architecture is constantly performing better than the baseline within the limits of the assumptions.

Keywords: Aircraft design, Multidisciplinary design optimisation, Blended Wing-Body, distributed electric propulsion

Résumé — L’augmentation du trafic aérien au cours des dernières décennies et ses prévisions constituent un défi majeur pour arriver à une croissance neutre en carbone. Pour atteindre cet objectif sociétal, il est nécessaire de définir, en rupture avec les configurations actuelles, des concepts d’avion de transport intégrant de nouvelles technologies avec au final un impact minimal sur l’environnement. Ces futurs véhicules aériens reposent entre autres sur diverses interactions entre systèmes, disciplines et composants. Aussi, ces travaux de recherche se focalisent sur le développement d’une méthodologie dédiée à l’exploration et à l’évaluation des performances de configurations non conventionnelles utilisant des concepts de propulsion innovants. Le cas d’utilisation à considérer est l’optimisation au niveau conceptuel d’une aile volante à propulsion électrique distribuée, un concept prometteur combinant des performances aérodynamiques élevées et les avantages de la propulsion électrique.

Le processus d’optimisation qui se base sur FAST, l’outil de dimensionnement avion ISAE-SUPAERO/ONERA, a été mis en œuvre dans OpenMDAO, l’environnement d’analyse et d’optimisation multidisciplinaire Open Source de la NASA. Avec l’idée d’une complexité croissante de l’analyse de conception multidisciplinaire et d’une meilleure identification des différents effets, les deux éléments innovants ont été étudiés séparément. Premièrement, le processus classique a été révisé pour tenir compte des systèmes de propulsion hybride. Deuxièmement, une méthode a été appliquée pour estimer le dimensionnement d’une cellule avion radicalement innovante. Enfin, un processus de conception intégrant ces deux aspects inédits a été mis au point pour étudier un concept d’aile volante à propulsion électrique distribuée.

En ce qui concerne le processus de conception, les résultats montrent que l’utilisation de gradients dans la procédure d’optimisation réduit les temps de calcul par rapport à une méthode sans gradient d’environ 70%. Ce gain en temps est un avantage important au niveau du processus avant-projet qui facilite les tâches du concepteur. Pour les performances au niveau avion, les résultats ont été comparés à ceux obtenus pour un avion de type A320 classique, fondés sur les mêmes exigences de haut niveau et le même horizon technologique. Globalement, le concept de propulsion électrique hybride est intéressant car il permet des opérations à proximité du sol (atterrissage, décollage) sans émission et d’économiser du carburant pour les missions situées en dessous d’une certaine distance franchissable. Cette limitation est associée à la présence de batteries : elles introduisent en effet une pénalité de masse significative qui ne peut être annulée par les avantages de l’électrification pour de longues distances. Des simulations supplémentaires indiquent qu’un concept d’aile volante fondé sur une architecture uniquement turbo-électrique consomme toujours moins de carburant que l’avion de référence dans les limites des hypothèses prises en compte.

Mots clés : Avant-projet des avions, optimisation multi-disciplinaire, aile volante, propulsion électrique distribuée

Nomenclature

Symbols

a_∞	=	Speed of sound
α	=	Angle of attack or parameter varying between 0 and 1
AR	=	Aspect ratio
b	=	Span
BPR	=	By-pass ratio
\bar{c}	=	Mean aerodynamic chord
$\underline{c}(\underline{x})$	=	Generic design constraint function
\underline{c}_{CCM}	=	Vector containing the certification specifications
C_l	=	2D lift coefficient
C_L	=	3D lift coefficient
$C_{L\alpha}$	=	Slope of the $C_L - \alpha$ curve
C_d	=	2D drag coefficient
C_D	=	3D drag coefficient
C_{D_i}	=	Induced drag coefficient
C_{D_f}	=	Friction drag coefficient
C_{D_w}	=	Wave drag coefficient, for transonic regime
C_m	=	2D pitching moment coefficient
$C_{M_{ac}}$	=	3D pitching moment coefficient, referred to the aerodynamic center
$C_{M_{cg}}$	=	3D pitching moment coefficient, referred to the center of gravity
C_H	=	Hinge moment coefficient
δ	=	Power rate
δ_e	=	Elevon's deflection angle
E_c	=	Energy consumption
$E[X]$	=	Statistical average value of a set of values X
$f(\underline{x})$	=	Generic objective function
FPR	=	Fan pressure ratio
g	=	Acceleration of gravity, in SI 9.806 m s^{-2}
γ	=	Climb angle
$\gamma\%$	=	Climb rate, in percentage
γ_a	=	Heat coefficient ratio for the air, 1.4
Δh	=	Total specific enthalpy variation
λ	=	Taper ratio

Λ_{LE}	=	Sweep angle, computed at leading edge
Λ_{TE}	=	Sweep angle, computed at trailing edge
Λ_{25}	=	Sweep angle, computed at 25% of the chord
μ	=	Mean value
\mathcal{M}	=	Generic numerical solver
$\mathcal{M}_{takeoff}$	=	Pitch moment generated at takeoff
\mathcal{M}_H	=	Hinge moment for the control surface
N_b	=	Number of batteries
N_{EM}	=	Number of electric motors
N_{GT}	=	Number of gas turbine
N_{pass}	=	Number of passengers
\mathcal{N}	=	Yaw moment
m_f	=	Fuel burn
m_{fmax}	=	Maximum fuel mass that can be stored in the wing
\dot{m}_f	=	Fuel flow
m_L	=	Maximum landing mass
m_{TO}	=	Maximum takeoff mass
m_e	=	Operating empty mass
m_{PL}	=	Payload mass
m_{PLmax}	=	Maximum payload
P	=	Power
PSFC	=	Power specific fuel consumption
P_{400}	=	Power required at 400 ft
r_f	=	Fan radius
\bar{r}_f	=	Fan radius-to-chord ratio
R	=	Range
R_g	=	Gas constant, in SI its value is $287 \text{ J kg}^{-1} \text{ K}^{-1}$
σ	=	Variance
σ^*	=	Coefficient of variation
s_i	=	First order Sobol index of the parameter x_i
s_{T_i}	=	Total Sobol index of the parameter x_i
S	=	Surface
SFC	=	Specific fuel consumption
SM	=	Static margin
SoC	=	State of charge
t	=	Time
T	=	Thrust
τ	=	Volume
$(\frac{t}{c})$	=	Thickness-to-chord ratio
V_∞	=	Free stream velocity
w	=	Width
W	=	Weight
x_{cg}	=	Center of gravity position
x_n	=	Neutral point position

\underline{x} = Design variables vector
 \underline{y} = State variables vector

Subscripts

app = Approach
 b = Battery
 cab = Cable
 cb = Centerbody
 $core$ = Core, also said bus or power management unit PMU
 cs = Cooling system
 g = Generator
 EM = Electric motor
 fin = Final value
 GT = Gas turbine
 HT = Horizontal tail
 IC = Inverter/converter
 max = Maximum value
 out = Outer wing
 toc = Top of climb
 tod = Top of descent
 tr = Transition zone
 VT = Vertical tail
 w = Wing

Superscript

(0) = Initial value
 $*$ = Final value
 t = Target variable

Acronyms

AEO	All Engine Operative
BLI	Boundary Layer Ingestion
BWB	Blended Wing-Body
CFD	Computational Fluid-Dynamics
DP	Distributed Propulsion
DEP	Distributed Electric Propulsion
DOC	Direct Operating Cost
EIS	Entry Into Service
ESAR	Energy Specific Air Range
FAST	Fixed-wing Aircraft Sizing Tool
FEM	Finite Element Model
FPR	Fan pressure ratio
HBPR	High By-Pass Ratio
ICE	Internal Combustion Engine
ISAE	Institut Supérieur de l’Aéronautique et de l’Espace
LAR	Least Angle Regression
LPA	Large Passenger Aircraft
LoD	Lift over Drag ratio
MAC	Mean Aerodynamic Chord
MEA	More Electric Aircraft
MDA	Multidisciplinary Design Analysis

MDF	Multidisciplinary Feasible
MDO	Multidisciplinary Design Optimisation
MDAO	Multidisciplinary Design Analysis and Optimisation
MFW	Maximum Fuel Weight
MLG	Main Landing Gear
MLW	Maximum Landing Weight
MTOW	Maximum Takeoff Weight
MSE	Mean Square Error
MZFW	Maximum Zero Fuel Weight
NASA	National Aeronautics and Space Administration
OAD	Overall Aircraft Design
OCI	One Core Inoperative
OEI	One Engine Inoperative
ONERA	Office National d'Études et de Recherches Aérospatiales
OWE	Operating Weight Empty
HE	Hybrid-Electric
ICE	Internal Combustion Engine
PCE	Polynomial Chaos Expansion
PMU	Power Management Unit
PFEE	Payload Fuel Energy Efficiency
PL	Payload
PMU	Power Management Unit
RoC	Rate of Climb
SAR	Specific Air Range
SUGAR	Subsonic Ultra-Green Aircraft
TAW	Tube-and-wing
TLAR	Top Level Aircraft Requirements
xDSM	eXtended Design Structure Matrix
XML	eXtensible Markup Language

List of Figures

1.1	Aviation environmental footprint perspectives according to NASA ARMD Strategic Thrust [CW16].	9
1.2	Percentage of CO ₂ emission per type of aircraft [Bra18].	10
1.3	Example of possible configurations explored in the conceptual design of civil transport aircraft [Ray11].	12
1.4	Preliminary design process, using the xDSM standard presented by Lambe and Martins [LM12].	13
1.5	Different electric propulsion architectures [Mad+16].	17
1.6	Mass specific energy vs. volume specific energy for different energy storage systems [Hep12].	19
1.7	Comparison between the Airbus A320 (right) and the new A320 Neo (left) mounting the innovative LEAP engine.	20
1.8	DRAGON concept, proposed by ONERA [Sch+19].	21
1.9	NASA SCEPTOR X-57 concept [Bor+16].	22
1.10	AMPERE concept, proposed by ONERA [HRD16].	23
1.11	Illustration showing the difference in the engine sizing to meet the OEI condition for 2 and 4 motors [Ste+12b].	24
1.12	STARC-ABL concept, proposed by NASA [WF16].	26
1.13	CENTRELINE concept, proposed by the CENTRELINE European consortium [Sei+18].	27
1.14	Main milestones in the Blended Wing-Body concept.	28
1.15	Different load distributions due to pressurization in a circular (left) and non-circular (right) cabin.	29

1.16	Rendering of the BWB Ascent 1000, announced by DZYNE and expected to fly in the near future [PSY18].	30
1.17	Integrated cabin structure design.	31
1.18	Segregated cabin structure design.	32
1.19	Oval cabin structure design.	32
1.20	Blended Wing-Body cabin design, according to Bradley [Bra04]	33
1.21	Aerodynamic tradeoff for a BWB, from the work of Qin et al. [Qin+04].	36
1.22	Shape and planform design variables considered in the work of Lyu and Martins, for the BWB optimisation [LM14].	37
1.23	NASA N3-X concept [KBF08].	39
1.24	Ph.D. roadmap, representing the two separated steps to finally converge toward the Blended Wing-Body with distributed electric propulsion configuration.	43
2.1	Diagram of FAST, using the xDSM standard [LM12].	52
2.2	CERAS engine reference deck [CER15].	54
2.3	xDSM diagram of the geometry analysis coded in FAST [LM12].	56
2.4	Compressibility drag coefficient as function of Mach and lift coefficient. Curves are obtained considering $\Lambda_{25_w}=28$ deg and $(\frac{t}{c})_w=0.12$	60
2.5	xDSM diagram for the time step performance analysis.	63
2.6	Different mission profiles [BD11].	64
2.7	xDSM diagram climb and cruise phase performance, to highlight the iterative procedure used in FAST.	65
2.8	Some of the outputs of FAST, related to the A320 validation test case, with the TLAR reported in Table. 2.4. Continuous line represents the trajectory, meanwhile dashed line is the true air speed or the lift coefficient, according to the flight phase.	69
2.9	Comparison between gradient-free and gradient-based methods on the required number of iterations [Mar14].	71
2.10	Relations between the OpenMDAO four basic classes: <code>Component</code> , <code>Group</code> , <code>Driver</code> and <code>Problem</code> [Gra+19].	72

2.11	xDSM diagram for the integrated version of FAST, obtained by the coupling with OpenMDAO.	75
2.12	xDSM diagram for the geometry module of integrated version FAST and OpenMDAO.	77
2.13	Payload-Range diagram, for the A320 CERAS test case, baseline and optimised aircraft.	84
2.14	Convergence history for optimisation problem of A320 CERAS test case. . . .	84
2.15	Fuel consumption as a function of design range for the A320 baseline and the optimised aircraft, resized to match EIS2035. TLAR are reported in Table 2.14.	87
3.1	Typical evolution of atmospheric boundary layer during the day. Convective boundary layer extension is shown [Li+14]	97
3.2	Classical TAW configuration featuring distributed electric propulsion concept, as modeled in OpenVSP [Ope18b].	97
3.3	General scheme of hybrid electric distributed propulsive chain architecture considered in this reseach. Case of 40 electric motors distributed along the wing.	99
3.4	Ragone plot for different types of batteries, 2008 technology state of the art [SG08].	101
3.5	Typical battery discharge curve voltage vs capacity; with the three characteristic regions identified [TD09].	102
3.6	Turboshaft model, as in GSP software [NLR00].	104
3.7	Scheme of anular motor, which integrates electric motors and ducted fan [Eic+06].	106
3.8	Scheme of a ducted fan for the model presented	110
3.9	Fan radius (in blue) and required power (dashed line) as function of FPR, $c_T = 9.86 \times 10^{-2}$, $M_0 = 0.78$ and $h=35000$ ft.	112
3.10	Allowable region for the velocity at the tip of fan blade. The shaded region represents a non feasible space.	113
3.11	FAST xDSM scheme for the version tailored to hybrid aircraft featuring distributed electric propulsion, shown in Fig. 3.2.	116
3.12	Scheme of ducted fan for the wetted surface estimation.	117
3.13	Blowing surface visualisation: here the region interested is indicated by the red colour.	118

3.14	xDSM diagram for the integrated version of FAST, tailored to optimisation of hybrid aircraft with distributed electric propulsion.	121
3.15	Effects on OWE m_e and energy consumption E_c of battery technology parameters. Fixed battery case.	126
3.16	Fuel consumption as function of design range, comparison between the baseline and the hybrid aircraft with distributed propulsion.	131
3.17	Energy consumption as function of design range, comparison between the baseline and the hybrid aircraft with distributed propulsion.	132
3.18	PFEE, defined in Eq. (1.3) as function of design range, comparison between the baseline and the hybrid aircraft with distributed propulsion.	132
3.19	Electric motors' mass as function of number of electric cores for the hybrid aircraft concept, $N_{EM} = 32$, $R = 900$ nmi.	134
3.20	Fuel consumption as function of design range, comparison between the optimised baseline and hybrid aircraft with distributed electric propulsion.	141
3.21	Energy consumption as function of design range, comparison between the optimised baseline and the hybrid aircraft with distributed electric propulsion.	141
3.22	PFEE, defined in Eq. (1.3) as function of design range, comparison between the optimised baseline and the hybrid aircraft with distributed electric propulsion.	142
3.23	Exploration points using NSGA-II, for the multiobjective optimisation of hybrid aircraft, $N_{EM} = 32$ and $R = 900$ nmi. 20000 points considered.	147
3.24	Comparison between the Pareto frontier obtained with NSGA-II and SNOPT, through the composite function in Eq. (3.55). Hybrid aircraft case, $N_{EM} = 32$ and $R = 900$ nmi.	148
3.25	Comparison between three different configurations, chosen within the Pareto frontier for $\alpha = 0$, $\alpha = 0.5$ and $\alpha = 1$ in Eq. (3.55).	149
4.1	ISAE-Supaero and ONERA Blended Wing-Body reference geometry.	158
4.2	Detail of the Blended Wing-Body mesh around the body.	160
4.3	Convergence history example for CFD simulation, $\alpha = -3$ deg, $M = 0.78$ and $h = 35000$ ft.	161
4.4	$C_L - \alpha$ curve, comparison between SU2, FAST and OpenVSP. RANS simulation case, $M = 0.78$ and $h = 35000$ ft.	162

4.5	$C_D - C_L$ curve, comparison between SU2, FAST and OpenVSP. RANS simulation case $M=0.78$ and $h=35000$ ft.	163
4.6	Lift-over-drag ratio curve, comparison between SU2, FAST and OpenVSP. RANS simulation case. $M=0.78$ and $h=35000$ ft.	164
4.7	$C_D - M$ curve, $\alpha=1.5$ deg and $h=35000$ ft. Drag divergence point marked in black.	164
4.8	Aircraft diagram scheme, noting the angle of attack α , the flight path angle γ and the line for indices [de 15a].	166
4.9	The 6 control surfaces configurations proposed for the BWB reference geometry for the purpose of this research activity.	167
4.10	Elevon deflection δ_e for the 6 BWB configurations of Fig. 4.9, as function of demanded angle of attack.	169
4.11	Maximum hinge moment for the 6 BWB configurations of Fig. 4.9, as function of demanded angle of attack.	170
4.12	Peak power for the 6 BWB configurations of Fig. 4.9, as function of demanded angle of attack.	171
4.13	Sensitivity analysis of trimmed condition with respect to the static margin. Quantities of interest considered are the angle of attack α , the elevon's deflection δ_e and the variation of LoD value between trimmed and non trimmed condition $\Delta\left(\frac{L}{D}\right)$	173
4.14	BWB geometry visualisation; ribs have been omitted for clarity purposes. . .	174
4.15	Static analysis results for the BWB reference geometry design.	176
4.16	Structural components mass breakdown for the static analysis of BWB reference geometry.	177
4.17	BWB reference geometry, together with integrated nacelle, at the symmetry section.	179
4.18	Detail of the optimised nacelle, mounted on the BWB.	180
4.19	Performance comparison between the non optimised and optimised nacelle geometry using MSES.	180
4.20	Displacement thickness and kinetic energy thickness comparison between the integrated geometry and the isolated body geometry.	181
4.21	Planform scheme for the Blended Wing-Body sizing.	183

4.22	Seats arrangements for a three class BWB configurations.	184
4.23	Final rendering of Blended Wing-Body with distributed propulsion.	187
4.24	Seats arrangement and boarding doors position assumption for the BWB geometry.	188
4.25	Blended Wing-Body with distributed propulsion rendering, detail of subsystems allocation.	190
4.26	MDA loop tailored for the Blended Wing-Body sizing with conventional propulsion.	192
4.27	Constraint diagram for the BWB with conventional propulsion.	194
4.28	Comparison between the LoD curve for the reference aircraft and the BWB with conventional propulsion. Shading identifies the region where models are not accurate anymore, since the wave drag is not well predicted at high C_L	197
4.29	Visualization of the airfoils used in the BWB concept depicted in Fig. ?? at different sections, in real scale.	198
4.30	$C_{M_{cg}}$ vs. α curve around the cruise point for the BWB concept obtained.	198
4.31	Mass breakdown for the BWB featuring conventional propulsion, with TLAR reported in Table 2.4. Mass norm is the reference French 2001/D, used in FAST [DGA84].	199
4.32	Comparison between the reference aircraft and the BWB with conventional propulsion for different operational ranges.	199
4.33	Payload-Range comparison between the reference aircraft and the BWB with conventional propulsion, considering the two cases with auxiliary tanks and not.	200
4.34	Fuel consumption as function of design range, comparison between the optimised baseline and the BWB with distributed electric propulsion. Three configurations have been analysed, corresponding to $N_{EM} = 16, 32, 48$	207
4.35	Energy consumption as function of design range, comparison between the optimised baseline and the BWB with distributed electric propulsion. Three configurations have been analysed, corresponding to $N_{EM} = 16, 32, 48$	207
4.36	PFEE, defined in Eq. (1.3) as function of design range, comparison between the optimised baseline and the BWB with distributed electric propulsion. Three configurations have been analysed, corresponding to $N_{EM} = 16, 32, 48$	208
4.37	Mass breakdown for the BWB with distributed electric propulsion, $N_{EM} = 32$, R=900 nmi. Mass norm is the revised French 2001/D for hybrid architectures, used in FAST [DGA84].	210

4.38	Exploration points using NSGA-II, for the multiobjective optimisation of BWB with distributed electric propulsion, $N_{EM} = 32$ and $R = 900$ nmi. 50000 points considered.	212
4.39	Comparison between the Pareto frontier obtained with NSGA-II and SNOPT, through the auxiliary function in Eq. (3.55). BWB with DEP case, $N_{EM} = 32$ and $R = 900$ nmi.	212
4.40	Fuel consumption as function of design range, comparison between the optimised baseline and the BWB with DEP, where the electric propulsion is obtained by turbogenerators solely.	214
B.1	Comparison between the relative error using different MDO architectures on a given design problem [TM10].	258
B.2	xDSM diagram for the AAO problem.	261
B.3	xDSM diagram for the SAND architecture.	261
B.4	xDSM diagram for the IDF architecture.	262
B.5	xDSM diagram for the MDF architecture.	263
B.6	Summary of MDO architectures [ML13].	265
D.1	Effects on OWE m_e and energy consumption E_c of battery technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Fixed battery case.	271
D.2	Effects on OWE m_e and energy consumption E_c of gas turbine and generator technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Fixed battery case.	272
D.3	Effects on OWE m_e and energy consumption E_c of electric motor and cooling system technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Fixed battery case.	272
D.4	Effects on OWE m_e and energy consumption E_c of inverter/converter and electric core technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Fixed battery case.	273
D.5	Effects on OWE m_e and energy consumption E_c of battery technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Battery's resizing case.	274

D.6	Effects on OWE m_e and energy consumption E_c of gas turbine and generator technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Battery's resizing case.	274
D.7	Effects on OWE m_e and energy consumption E_c of electric motor and cooling system technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Battery's resizing case.	275
D.8	Effects on OWE m_e and energy consumption E_c of inverter/converter and electric core technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Battery's resizing case.	275
D.9	Effect of wing parameters over energy consumption E_c , OWE m_e and maximum LoD for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$	276
D.10	Effect of HT parameters over energy consumption E_c , OWE m_e and maximum LoD for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$	276
D.11	Effect of VT parameters over energy consumption E_c , OWE m_e and maximum LoD for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$	277
D.12	Effect of FPR over energy consumption E_c , OWE m_e and maximum LoD for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$	277

List of Tables

1.1	NASA ARMD Strategic Thrust table of objectives, for the subsonic transport aircraft [CW16]. Variation are intended with respect to 2005 best in class configuration.	10
1.2	Classification of electric propulsion architectures, based on the degree of hybridization.	18
1.3	Decision matrix for the three BWB cabin concepts proposed in literature. Values are assigned as follow: +1 if there is a good improvement, 0 if it may be an issue, but not relevant and -1 if it introduces a penalty.	33
1.4	Structural masses for different BWB concepts available in literature. Adapted from [vV14].	33
1.5	Comparison of performance for the different target distributions examined in the work of Qin et al. [Qin+04], related to a BWB configuration.	37
2.1	Input parameters to properly size each geometrical component, according to the formulation used in FAST [DC12].	55
2.2	Mass breakdown standard, according to the French norm 2001/B [DGA84] and implemented in FAST.	61
2.3	CATPOL [EAS12] and CS-25 [EAS17] rules explanation, considered in the CCM module of FAST. V_z represents vertical speed, meanwhile $\gamma\%$ the gradient flight.	66
2.4	Top level requirements for the A320 CERAS validation case used in FAST.	67
2.5	Geometrical inputs for the A320 CERAS validation case.	67
2.6	Thrust rate definition for each mission segment for the A320 CERAS validation case.	67
2.7	Comparison between the results obtained in FAST and the A320 CERAS data [Sch+17a].	68

2.8	CCM results for the A320 CERAS validation case.	68
2.9	Optimisation problem definition for the A320 CERAS case. Variables' limits come from literature review on single aisle type aircraft [Ros05b].	80
2.10	Set-up for the A320 CERAS optimisation problem, using gradient based method.	81
2.11	Comparison between quantities of interest for the baseline and the optimised aircraft, A320 CERAS test case. Top level requirements are reported in Table 2.4.	82
2.12	Comparison between design variables for the A320 CERAS test case baseline and optimised. Geometric inputs for the baseline are in agreement with Table 2.5.	82
2.13	Objective function and norm constraints, defined as in Eq. (2.22), for the 10 optimisation runs carried out for A320 CERAS test case baseline.	83
2.14	Top level requirements for the resized A320, considering EIS2035.	85
2.15	Impact of new technologies on airframe mass estimation according to IATA [IAT13b], considering EIS2035.	85
2.16	Impact of new technologies on aerodynamics according to IATA [IAT13b], considering EIS2035.	86
2.17	Quantities of interest for the A320 case baseline, resized to match EIS2035 with TLAR reported in Table 2.14 and geometrical inputs as in Table 2.5. . .	88
2.18	Quantities of interest for the A320 case optimised, resized to match EIS2035 with TLAR reported in Table 2.14.	88
3.1	Top level requirements for the proposed TAW configuration featuring distributed electric propulsion, shown in Fig. 3.2.	97
3.2	Design point for the gas turbine modeled in GSP.	105
3.3	Center of gravity location of the different electric components, belonging to the propulsive system shown in Fig. 3.3.	118
3.4	Proposed addendum to mass breakdown standard [DGA84] to include electric components mass.	119
3.5	Design space exploration for technological parameters, in 2035 perspectives, according to bibliographic review. In bold the value with biggest uncertainty.	122
3.6	Mean first order indices related to key parameters m_e , E_c and SoC_f ; in bold are marked the most relevant parameters. Fixed battery case.	125
3.7	Coefficient of variation σ^* of Sobol indices related to key parameters m_e , E_c and SoC_f . Fixed battery case.	125

3.8	Mean value and coefficient of variation of MSE on training set for key parameters considered. Fixed battery case.	125
3.9	Mean first order indices related to key parameters m_e , E_c and τ_b ; in bold are marked the most relevant parameters. Battery resizing case.	127
3.10	Coefficient of variation σ^* of Sobol indices related to key parameters m_e , E_c and τ_b . Battery resizing case.	127
3.11	Mean value and coefficient of variation of MSE on training set for key parameters considered. Battery resizing case.	128
3.12	Technological parameters chosen for the design of hybrid aircraft, EIS 2035.	129
3.13	Propulsive system top level parameters for the hybrid aircraft with distributed propulsion performance evaluations.	130
3.14	Mission profile definition for the hybrid aircraft case, through the battery and gas turbine power rates defined in Eq. (3.1).	131
3.15	Kerosene properties [Edw02].	131
3.16	Quantities of interest for the hybrid aircraft with distributed electric ducted fan, associated to TLAR of Table 3.1, $N_{EM}=32$	133
3.17	Fuel breakdown for the R = 900 nmi mission, comparison between the conventional and the hybrid aircraft.	133
3.18	Optimisation problem definition for the hybrid aircraft with distributed propulsion case.	136
3.19	First order Sobol indices mean value μ key output variables with respect to inputs, hybrid distributed propulsion case. Most relevant parameters for each output are written in bold.	137
3.20	First order Sobol indices coefficient of variation σ^* for key output variables, with respect to inputs, hybrid distributed propulsion aircraft case. An asterisk identifies the case in which the mean value μ is zero and σ^* is replaced by convention with its variance σ	138
3.21	Mean value μ and coefficient of variation σ^* of the relative MSE on validation set for the sensitivity analysis of Table 3.19.	139
3.22	Quantities of interest for the optimised hybrid aircraft with distributed electric ducted fan, $N_{EM}=16$	142
3.23	Quantities of interest for the optimised hybrid aircraft with distributed electric ducted fan, $N_{EM}=32$	143

3.24	Quantities of interest for the optimised hybrid aircraft with distributed electric ducted fan, $N_{EM}=48$	143
3.25	Optimisation problem definition for the mission profile, hybrid aircraft case, $N_{EM} = 32$, $R = 900$ nmi.	145
3.26	Comparison between the baseline and the optimised mission profile for the hybrid aircraft with distributed propulsion, $N_{EM} = 32$, $R = 900$ nmi.	145
3.27	\mathcal{L}_2 -norm calculation between the final objective function and design variables vector. The subscript identifies the method.	148
4.1	TLAR and main parameters for the ISAE-Supaero and ONERA Blended Wing-Body reference geometry.	159
4.2	Set up of CFD RANS simulations in SU2 for the BWB reference geometry aerodynamic study.	160
4.3	Comparison of the slope C_{L_α} estimated by SU2, VSP and FAST. RANS simulation case, $M=0.78$ and $h=35000$ ft.	162
4.4	Comparison of the Oswald coefficient e , estimated by SU2, FAST and OpenVSP. RANS simulation case. $M=0.78$ and $h=35000$ ft.	162
4.5	Geometrical and aerodynamic coefficients for the BWB reference geometry, for longitudinal control surface purposes.	167
4.6	$C_{L_{\delta_e}}$ and $C_{M_{\delta_e}}$ coefficients for the 6 configurations shown in Fig. 4.9. They are computed using VLM technique [MIT18a].	168
4.7	Hinge moment coefficients to define the model of Eq. (4.8) for the 6 different configurations shown in Fig. 4.9.	168
4.8	Aluminium alloy 7075 properties [Meg12].	175
4.9	Loads applied on the BWB geometry for the FEM analysis considered.	175
4.10	Structural components thickness for the static analysis of BWB reference geometry, case of maximum load factor $n = 2.5$	176
4.11	Comparison between the FEM analysis and the surrogate model for centerbody and outer wing, for the BWB reference geometry case. Aluminium alloy 7075 is used as material.	177
4.12	Comparison between the FEM analysis and the surrogate model for centerbody and outer wing, for the BWB reference geometry case. CFRM material is used in the centerbody.	178

4.13	Condition for the study of nacelle effect in MSES.	179
4.14	Sum up of geometrical entries for the BWB parametrization.	187
4.15	Boarding time for the BWB and the A320 reference aircraft with and without handbags, 150 passengers. Simulation carried out using PAXelerate [Sch+16].	189
4.16	Geometrical inputs for the BWB with conventional propulsion sizing case. . .	195
4.17	Comparison between the A320 resized to match EIS2035 and the BWB, with the TLAR reported in Table 2.4.	196
4.18	Optimisation problem definition for the BWB aircraft with distributed electric propulsion case.	202
4.19	First order Sobol indices mean value μ for key output variables with respect to inputs, BWB with distributed electric propulsion case. Most relevant parameters for each output are written in bold.	203
4.20	First order Sobol indices coefficient of variation σ^* for key output variables, with respect to inputs, BWB with distributed electric propulsion case. An asterisk identifies the case in which the mean value μ is zero and σ^* is replaced by convention with its variance σ	204
4.21	Mean value μ and coefficient of variation σ^* of the relative MSE on validation set for the sensitivity analysis of Table 4.19.	205
4.22	Objective function and norm constraints, defined as in Eq. (2.22), for the 10 optimisation runs carried out for the BWB with distributed electric propulsion, $N_{EM} = 32$, $R = 900$ nmi.	206
4.23	Quantities of interest for the optimised BWB with distributed electric ducted fan, $N_{EM} = 16$	208
4.24	Quantities of interest for the optimised BWB with distributed electric ducted fan, $N_{EM} = 32$	209
4.25	Quantities of interest for the optimised BWB with distributed electric ducted fan, $N_{EM} = 48$	209
4.26	Comparison between the two BWB with DEP optimisation problems, considering the CCM lower limit as specified in the CS-25 [EAS17] and equals to the A320 2005 version, reported in Table 2.8. $N_{EM} = 32$, $R = 900$ nmi case. . . .	211
4.27	\mathcal{L}_2 -norm calculation between the final objective function and design variable vectors. The subscript identifies the method.	213
4.28	Quantities of interest for the BWB with distributed electric ducted fan, power supplied by turbogenerators solely, $N_{EM} = 16$	215

4.29	Quantities of interest for the BWB with distributed electric ducted fan, power supplied by turbogenerators solely, $N_{EM} = 32$	215
4.30	Quantities of interest for the BWB with distributed electric ducted fan, power supplied by turbogenerators solely, $N_{EM} = 48$	216
B.1	Mathematical notation for MDO problem formulations, given by Martins and Lambe [ML13].	259

Introduction

Since its birth in '30s, air transport sector has been continuously growing each year. In last decade, thanks to the entry of new commercial area, such as south America or western Asia, the trend has become exponential. According to perspective from Boeing and Airbus, the two main leaders in the sector, the number of aircraft flying will be increased of about 39000 units in 20 years.

This growth poses a key problem when looking at the emission level. According to 2015 data, aviation contribution to total CO_x and NO_x emissions is below other sectors, such as industry or electricity generation. Nonetheless, without any action taken, predictions indicate that this percentage will reach values between 30 and 50% in a 20 years horizon. To avoid such scenario, a sustainable growth must be found.

Several consortia and agencies, spreaded between America and Europe, have published their objectives for emission reduction in near and long term, up to 2050 horizon. All these perspectives are very aggressive, and it is commonly recognised that they cannot be achieved through the incremental approach that has been used so far in aviation. The classical “tube-and-wing” (TAW) configuration has been indeed developed for more than 70 years, and it offers only small potential gains. It is then necessary to introduce a new paradigm in aircraft design, a disruptive concept, based on innovative technologies, to drastically reduce emission. The study of a disruptive concept takes place at conceptual design level, where different configurations are defined and sized in order to downselect the most promising ones for further developments. Thus this Ph.D. proposes to develop a Multidisciplinary Design and Optimisation (MDAO) process tailored to the design of an unconventional configuration that would match stringent environmental goals.

In literature, two main areas of research have been considered: technologies at airframe level, focusing on more aerodynamically efficient architectures, and technologies at propulsive level, deploying hybrid and electric propulsive chain. Given the objectives, a most likely viable aircraft must benefit from a combination of both technologies, leading to an optimised overall configuration including hybrid powerplant. The main problem when dealing with such innovative concepts concerns the models: the classical methods proposed by aircraft design handbooks are well suited for a conventional configuration, but lose their validity when the concept is drastically different, as in the case of hybrid propulsion or integrated airframe concepts. From this consideration the main problem to be solved can be stated as

following: **“How can unconventional configurations be investigated at conceptual design level”?** This dissertation proposes an answer to this question in 4 steps.

Chapter 1 reviews the state of the art, focusing on the works of major interest for this research. After a brief introduction to better frame the environmental context, the conceptual aircraft design procedure is presented. Then, innovative key technologies are explored: one of the most promising technology found in literature is the electric and hybrid propulsion. This technology, which has been applied at automotive industry and on some general aviation aircraft, enables a total or partial mission electrification, greening the air and the reduction of emission. Also, such propulsion concepts enable the increase of propulsive and aerodynamic efficiency, through distribution of thrust and/or boundary layer ingestion.. Both these aspects will be detailed. At airframe level, the Blended Wing-Body (BWB) is identified as a promising concept with high aerodynamic efficiency. At the end of the review, a promising integrated concept is identified in the Blended Wing-Body (BWB) with distributed electric propulsion. Following the statement of the research problem, it is found that aircraft design must go towards a Multidisciplinary Design Optimisation approach, since it provides the necessary tools to establish a tradeoff for unconventional configuration, without neglecting any of the possible key interactions.

Chapter 2 presents the development of an aircraft optimisation sizing platform, based on the integration of the code FAST within OpenMDAO. FAST, which stands for Fixed-wing Aircraft Sizing Tool, is a code developed at ONERA and ISAE-Supaero for the preliminary design of large passenger aircraft. OpenMDAO, instead, is an MDAO platform, developed at NASA Glenn Research Center, which has been used for a large variety of MDO problems in aeronautics. After a presentation of both tools, with features and drawbacks, the integration of FAST and OpenMDAO is described. A suitable MDO architecture for aircraft design problem is identified, and the process carried out in the integration is detailed. The developed code is used for the optimisation of the Airbus A320 test case, so that gains of the optimisation process would be highlighted. Subsequently, the code has been used to define a set of reference aircraft, considering entry into service 2035. Results will be used later to evaluate performance of the proposed disruptive concept.

The BWB with distributed electric propulsion concept is based on the integration of two different innovative technologies: a new hybrid powerplant at propulsive level and a non conventional architecture at airframe level. To better quantify the impact of each of these aspects on the overall design, they are individually treated considering a conventional tube-and-wing aircraft featuring distributed electric propulsion and a BWB mounting conventional air-breathing engines. The coupling between the two finally leads to the proposed concept of BWB with distributed electric propulsion. The following two chapters reflects this approach.

Chapter 3 is dedicated to the methodology and the exploration of the first concept, tube-and-wing aircraft with distributed electric propulsion. The first part of the chapter focuses on the methodology: the overall propulsive chain is defined at system level, and then models related to each electric component are presented. Afterwards, these models are integrated within the conceptual design loop and required modifications to the disciplines are detailed. Finally, the revised sizing process is included in the MDO formulation defined in Chapter 2,

to finally converge towards an optimisation sizing framework for an hybrid aircraft. The second part of the chapter presents the sizing results for this concept: at first only the sizing loop is applied, to assess its quality in dealing with the innovative powerplant. Afterwards, optimisation results are presented, varying also the number of engines, in order to establish a possible tradeoff. Aircraft performances are evaluated against the reference aircraft, defined in Chapter 2. A Pareto frontier is also generated, comparing two different optimisation algorithms, one gradient-based and another one gradient-free, in order to assess the reduction in computational cost due to the utilisation of derivatives in the optimisation process.

Chapter 4 presents the methods that have been implemented for the conceptual design of Blended Wing-Body concept. First, the research strategy is detailed: in order to tackle the lack of reference data for the BWB architecture, a multi-fidelity analysis is carried out at disciplinary level, so that fast but reliable methods can be identified and used in the conceptual design stage. Once more, revised models are integrated within the sizing loop, and the resulting procedure is included in the MDO formulation. Finally an MDAO framework tailored to BWB with DEP is obtained. The first part of the results relates only to application of the sizing loop, considering conventional engines, in order to assess the benefits coming solely from the BWB architecture. Afterwards, the powerplant modeled in Chapter 3 is combined with this architecture, and the BWB with distributed electric propulsion is explored. In this case too, performances are evaluated against the reference aircraft EIS 2035. A Pareto frontier is also obtained, to establish tradeoff for the proposed disruptive concept.

This dissertation is concluded with an overall review of the work and possible further development to be made on the Multidisciplinary Design Analysis and Optimisation process.

Chapter 1

Advanced aircraft design process: a technology review

Résumé

Ce chapitre est le premier de cette thèse et a l'objectif de présenter des notions introductives au problème. Le contexte de cette recherche est lié aux défis de l'aviation pour les années à venir: la réduction des émissions est en effet un des enjeux des clés grands sociétaux. En particulier, selon les perspectives données par Boeing et Airbus, ces deux principaux constructeurs aéronautiques estiment que plus de 20 000 appareils voleront dans les 20 prochaines années, dans le segment des courtes et moyennes distances, ce qui deviendra alors le facteur décisif pour répondre aux objectifs environnementaux. Malheureusement, ces objectifs peuvent difficilement être atteints avec une configuration conventionnelle (tube-and-wing), car celle-ci est développée depuis plus de 70 ans et offre encore de faibles gains potentiels. Ainsi, un concept de rupture doit être introduit, au niveau de la conception, afin de trouver une solution prometteuse pour réduire l'empreinte environnementale de l'aviation.

Pour mieux cerner le problème, la boucle de conception conceptuelle utilisée jusqu'à présent est détaillée. Ensuite, les technologies innovantes clés étudiées au cours des dernières années sont explorées. L'innovation peut être principalement apportée à deux niveaux: modification de la cellule (géométrie) ou modification du système propulsif. En ce qui concerne la dernière catégorie, la propulsion hybride/électrique a suscité beaucoup d'intérêt: elle a été appliquée avec succès dans l'industrie automobile et les avions de petite taille et, au cours des prochaines années, différentes organisations souhaitent étendre son application au cas des avions de grande capacité. La principale caractéristique de la propulsion hybride/électrique est qu'elle permet aux nouveaux appareils de tirer parti de l'intégration entre propulsion et aérodynamique. Par exemple dans un système qui

considère la propulsion électrique distribuée conjointement avec un dispositif d'ingestion de couche limite (BLI), les effets provenant du souffle et du flux ingérant sont renforcés. La discussion va plus loin: dans plusieurs ouvrages, il a été souligné que la BLI fonctionnait mieux pour des grandes cordes, ce qui met l'accent sur la recherche de l'architecture la plus appropriée pour l'intégration d'un tel système. La réponse est donnée par l'aile volante, qui intègre la charge utile et la structure et offre à la fois de grandes surfaces et un volume important pour l'attribution de sous-systèmes; de plus, elle est naturellement très efficace d'un point de vue aérodynamique.

Sur la base de ces considérations, il a été décidé d'étudier comme configuration l'aile volante à propulsion électrique distribuée. En effet, ce concept a déjà été étudié par la NASA dans le cadre de son programme N3-X, mais leurs travaux portent principalement sur la modélisation des différentes disciplines impliquées. Dans cette recherche, l'objectif est plutôt de mettre en place une procédure pour son étude au niveau conceptuel, avec une entrée en service prévue en 2035. La question qui guide cette recherche peut être formulée comme suit: "Comment le processus de conception avion peut-il être modifié pour l'étude d'une configuration non conventionnelle dotée d'un groupe électrogène hybride innovant?" La réponse peut être exprimée en trois points:

- La définition de nouveaux modèles afin de prendre en compte l'impact de l'architecture innovante sur la géométrie, la structure, l'aérodynamique et l'évaluation des performances;
- L'application d'une approche haute fidélité pour calibrer les méthodes de conception du niveau conceptuel avec des simulations plus précises;
- La définition d'une procédure de dimensionnement basée sur l'optimisation multidisciplinaire, en raison de sa capacité à établir un compromis tenant compte de toutes les interactions entre les disciplines, particulièrement pertinente pour les aéronefs non conventionnels.

Il est à noter que le cas test considéré introduit deux innovations clés: une au niveau de la cellule (architecture aile volante) et une autre au niveau de la propulsion (utilisation de la propulsion hybride). Afin de mieux évaluer les avantages découlant de chacun de ces deux aspects, ils ont été étudiés séparément: un aéronef conventionnel à propulsion électrique répartie est d'abord pris en compte, puis un concept d'aile volante équipé de moteurs classiques. La procédure finale provient de l'intégration de ces deux études.

Contents

1.1	The environmental context	9
1.2	Aircraft conceptual design cycle	11
1.3	Key innovative aircraft technologies	15
1.3.1	Hybrid and electric propulsion technology	16
1.3.1.1	Hybrid propulsion fundamentals	16
1.3.1.2	Distributed propulsion technology review	20
1.3.1.3	Boundary layer ingestion device	24
1.3.2	Blended Wing-Body aircraft	27
1.3.2.1	Structural design of Blended Wing-Body concept	30
1.3.2.2	Aerodynamic tradeoff for the Blended Wing-Body	34
1.4	The research problem	38
1.4.1	Towards a promising solution for aviation sustainability	38
1.4.2	Problem statement and proposed solutions	40

Outline

- Aviation challenges for upcoming years are identified, specifically about the problem of emission reduction.
- The aircraft conceptual design loop is described.
- Different solutions to match the aviation's environmental goals are explored, to converge towards a promising disruptive concept.
- Research problem is stated.

1.1 The environmental context

In last decades world is facing with a more and more relevant environmental crisis [CW16; OEC11; Bra18]: CO₂ emission are increasing year by year, and a drastic reduction of these emissions in the upcoming years is a duty, for human sustainability.

On this scenario, aviation plays a key role too. Although its environmental footprint accounts much less than other sectors (estimated around 3%) [IAT13a; ICA16], the increasing number of aircraft flying every day, which is doubled in 15 years [Air19], plus the more accessibility to this conveyance, make the trend growing rapidly, as shown in Fig. 1.1. The

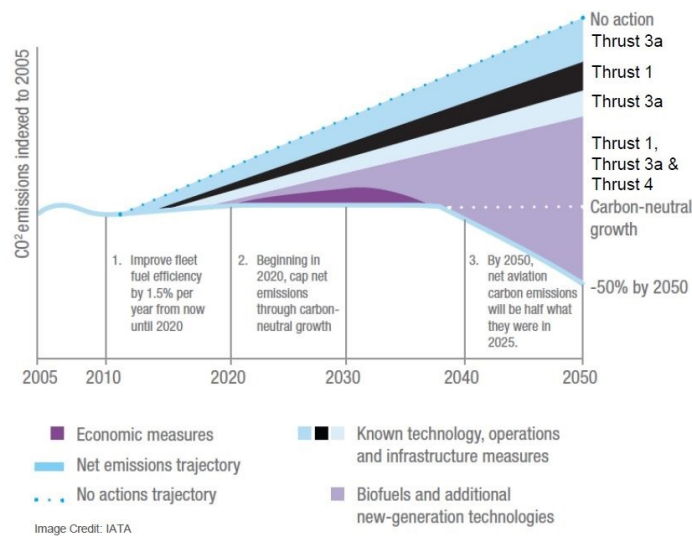


Figure 1.1: Aviation environmental footprint perspectives according to NASA ARMD Strategic Thrust [CW16].

image, taken from the NASA ARMD Strategic Thrust [CW16], shows the aviation impact perspectives in different scenarios. Without any action, its contribution to global emission will be soon unsustainable; the best target is to reduce CO₂ release up to 50%, to maintain a sustainable level. The 50% reduction goal is shared by other associations and projects in Europe too: both ATAG [ATA16] and ACARE [ACA15] presented their objectives, in line with the NASA studies.

According to a study, conducted by Boeing, the most critical segment is the one of large passenger aircraft (single and twin aisle) [Bra18]: their contribution is estimated to be around 93%, as shown in the breakdown of Fig. 1.2. Nowadays, with current electric technology, small regional aircraft are already being electrified, but from this analysis it is clear that the major efforts in next years will be to go on large passenger aircraft.

Besides the emissions, which remain the most important issue, also the noise and the energy consumption are relevant aspects to be reduced. All the goals can be summed up with a technological table, an example is given in Table 1.1, where the short, mid and long term goals are well identified. These are the objectives of NASA N+3 project [Fol+11], started in

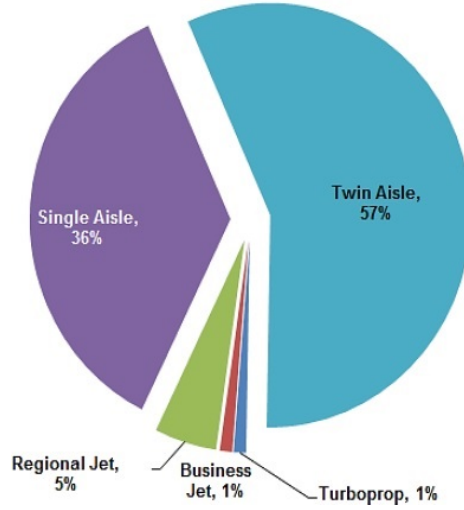


Figure 1.2: Percentage of CO₂ emission per type of aircraft [Bra18].

2011 and still on-going: despite they seems to be very aggressive, they represent the target for the aviation's sustainability.

Technology benefits	Technology generations		
	Near term 2015–2025	Mid term 2025–2035	Far term beyond 2035
Noise	22–32 dB	32–42 dB	42–52 dB
LTO NO _x emission	70–75%	80%	>80%
Cruise NO _x emission	65–70%	80%	>80%
Aircraft fuel/energy consumption	45–50%	50–60%	60–80%

Table 1.1: NASA ARMD Strategic Thrust table of objectives, for the subsonic transport aircraft [CW16]. Variation are intended with respect to 2005 best in class configuration.

To accomplish the aviation's goals, the classical tube-and-wing (TAW) configuration is not sufficient anymore: it has been developed over the last 7 decades, and it still has small potential gains. A disruptive configuration needs to be introduced, focusing on new and innovative configuration that features advanced technologies. This innovative aircraft must be introduced at conceptual design level, which is the phase of aircraft design where different configurations are studied in order to assess their performance and choose the most promising one. For this reason, before going through a bibliographic review about new promising technologies for future aircraft, next section will detail this phase, in order to understand how the conceptual design has been done until now.

1.2 Aircraft conceptual design cycle

Aircraft design is a discipline over a century old and it has evolved during the years, from the first flight in 1903 to nowadays. Thanks to the experience gained during the decades, design methods are well assessed for a conventional TAW architecture, and surrogate or statistical models take the place of numerical methods (*i.e.* for the aerodynamics calculation) [And10; Ray18].

The aircraft design process may be divided into three main steps [Sch18]:

1. Conceptual design phase, when a new concept is studied using reliable models, low or high fidelity according to the needs, to downselect the most promising concept.
2. Preliminary design phase, where new levels of details are added to the design in order to assess the results coming from the conceptual design phase.
3. Detailed design phase, where the overall configuration is well assessed and the focus is on the sizing of individual components and subsystems.

Once the configuration is adequately assessed at detailed phase, a new program is launched, entering in the aircraft development. From this point forward in this dissertation only conceptual design is considered, since it is the only one of interest for the research here presented.

As listed above, the main purpose of conceptual design phase is the downselection of the most promising configuration for a given set of top level aircraft requirements (TLAR). This phase involves a few number of people, working for about one year. The rapidity is one of the main required feature in this phase, in order to analyse as many configurations as possible: for this reason, mainly low fidelity methods, *i.e.* semiempirical or surrogate models, are used, but this is not a rule since when required also high fidelity methods can be employed to study a particular phenomenon [McD16]. One of the reference works for the methods to use is the book series from Roskam [Ros05a], which collects the most common methods used in the preliminary design process, still used nowadays; other milestones are the published book by Raymer [Ray18] and Anderson [And10]. Nicolai suggest to use in this phase some figures of merit, to assess the advantages of a configuration with respect to another one [Nic16].

At this stage multiple configurations can be analysed and advantages and drawbacks are discussed; after a debriefing it is possible to reduce the problem and choose a limited number of promising new configurations. As example, Fig. 1.3 shows all the innovative configurations studied in the first phase of the NASA N+3 project [Ray11]: the benefit of each configuration has been quantified considering the estimated gain in fuel and energy reduction; at the end of the downsizing procedure the design exploration is reduced at only two promising configurations.

As first step, the constraint analysis approach is applied to define the design domain and estimate the necessary thrust [Ros05a]; on the basis of this value the engine is chosen, also considering the available technology in the foreseen EIS [Ros05b]. Then, weight estimation

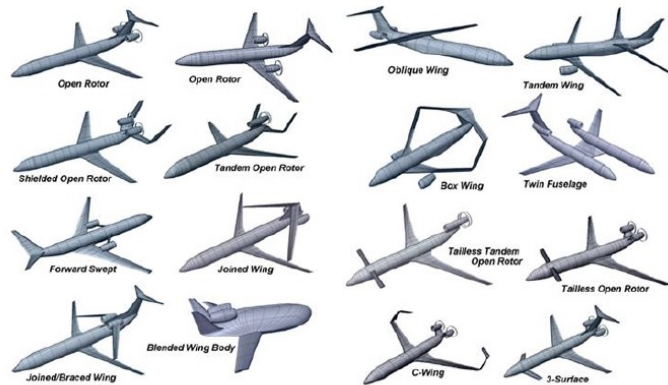


Figure 1.3: Example of possible configurations explored in the conceptual design of civil transport aircraft [Ray11].

and aerodynamics can be evaluated on the basis of surrogate models, that often use few key parameters, like the wetted surfaces [Ros05e; Ros05f]. As first estimate, cruise performance is often evaluated using the Breguet equation [And12; RL97; Phi10]. More accurate methods consist in integrating the set of ordinary differential equations describing the flight dynamics [Ros08] using a time step integration [Sfo14], based on the Euler or higher degree methods like the Runge-Kutta scheme [LeV07].

The aircraft design problem involves multiple disciplines, coupled each others (*e.g.* aerodynamics provides the loads for structural sizing), and thus it may be considered as a Multi-disciplinary Design Analysis (MDA). The MDA is defined as a “non linear system of equations obtained by the non-intuitive coupling of disciplinary solvers involved in complex engineering systems” [ML13; Gra+19], specifically for this case the conceptual design problem, whereas each discipline provide a set of equations that is coupled with other disciplines. The generic sizing procedure is given by Schmollgruber in his Ph.D. work [Sch18]; the scheme is presented in Fig. 1.4, using the xDSM standard [LM12]. Since this standard will be used throughout all this manuscript, it is a important to get familiar with it. In this notation the purple circular block represents the optimiser, meanwhile the orange one refers to a MDA loop. Green blocks represent the analysis, numbered according to the order of processing, and pink rectangles represent the functions. The main workflow is identified by the black line; gray lines represent instead the data sharing. Analyses outputs are indicated with a grey block, and finally I/O data are identified with a white block: inputs are at the top row, as outputs are at the left column. For what it concerns the notations, \underline{x} represents the design variables vector, \underline{y} the state variables, apex (0) indicates an initial guess, t a target variable (that is, a variable that is a copy of a previous output) and $(*)$ the final value. Algorithm 1 reports the description of analyses, with the numbering that refers to what are used in Fig. 1.4. For a more detailed description refers to the already mentioned work [Sch18].

In the illustrated case, engine is initialised outside the loop: one of the finding for the designers is to search for an existing engine that matches the fuel consumption targets, or to design a tailored one [MHP02; Rou05]. The iterative loop calls all the key disciplines involved

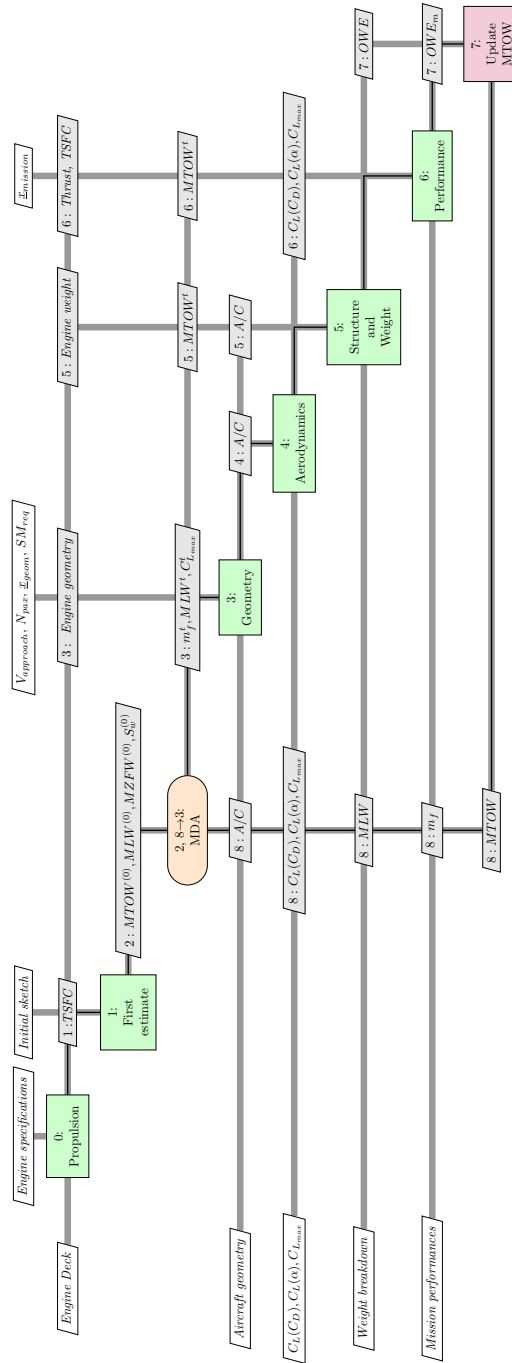


Figure 1.4: Preliminary design process, using the xDSM standard presented by Lambe and Martins [LM12].

in aircraft design: geometry, aerodynamics, structures and performance. Convergence is driven by the operating weight empty OWE: process is over when the value computed by structural analysis (step 5) is equal to the value computed by performance analysis (state

Algorithm 1 Preliminary design process algorithm. Numbering is referred to the xDSM presented in Fig. 1.4.

Require: Initial design parameters (TLAR)

Ensure: Sized aircraft, drag polars, masses, design mission trajectory

0: Engine initialization.

1: Compute the initial sizing point (first estimation of wing area S_w , Maximum Takeoff Weight MTOW, ...)

2: Initialise the loop.

repeat

3: Get the aircraft geometry.

4: Compute the aerodynamics.

5: Perform the structure analysis and get the weight of all the aircraft's components.

6: Compute performance.

7: Update the MTOW value.

8: Check the convergence: if the tolerance is below the desired threshold, return the sized aircraft, otherwise proceed to next iteration.

until 8 \rightarrow 3: MDA has converged

6). It must be noted that disciplines share variables, and thus are coupled each others; *i.e.* structures and weight depend on the aerodynamic results, and the improvement in one of these two disciplines can lead to a degradation in the other one. At the end more design choices can be made on the final layout, considering also the subsystems [Ros05c; Ros05d].

It is evident that the aircraft design is a matter of choosing the best compromise between the disciplines that can be considered during this phase or later (*i.e.* acoustic, aeroelasticity, ...). After having sized the aircraft according to given requirements, it is also worthy to study its performance on a set of operational missions, different from the design one: in general, during its life aircraft needs to supply a huge variety of missions, rarely equal to the design one [Ros05h]. Tradeoff studies regarding stability or control have low priority in conceptual design phase, but can be included with very easy models, to have a first estimation before the preliminary design phase [Ros05g]. The Digital Datcom tool [PDA17] is a powerful tool to estimate stability derivatives with the help of the USAF manual [Fin60]: data results come from statistical data on commercial aircraft and allow to size with limited approximation wing and tails [Sfo14]. Despite the advantages, this tool is limited to conventional configuration, and is not reliable when the aircraft architecture differs from a TAW configuration.

Clearly, at this point there are some uncertainties, associated to both the methods used and the perspective on the available technologies for the EIS considered; a good practice to approach this issue is through the use of some corrective factors [Kir02], to assess the sensitivity with respect to technological parameters. The choice of the preferred configuration can be guided also by other considerations, like a preliminary cost assessment [Ros05h]. Once that a configuration is chosen, it is possible to proceed through the preliminary design phase, aimed to study with more detailed models to better understand if the proposed aircraft can fulfill the customer requirements with a reasonable given cost.

To conclude this paragraph, the conceptual design methods are well assessed for conventional configuration, but may be unable to deal with innovative concepts; however they represent the state of the art today and the starting point for future development.

Next section reports a bibliographic review on the most promising technologies for next generation aircraft, which will be helpful in defining a promising concept to cope with environmental goals.

1.3 Key innovative aircraft technologies

One of the *leitmotiv* of aviation has always been the reduction of fuel consumption, related to emission and costs for airlines. For this reason, the research of innovative technologies has always been a priority in aircraft design, and with the rise of environmental constraint the works about this subject have been multiplied year by year.

Innovation can be brought at mainly two levels: architecture and propulsion [IS14; BCM17]. To the first category belong all the configurations deploying new technologies to increase the aerodynamic efficiency (expressed by the lift-to-drag ratio LoD), *e.g.* the strut braced wing [Gur+10] or the active flow control [IAT13a; IAT13b]. To the second category, instead, belong the aircraft that presents innovation at propulsive level, *e.g.* the Airbus Neo generation which mount high by-pass ratio (BPR) engines [Hug09], or proposed concept whereas the propulsive plant has been completely modified to go towards electric/hybrid propulsion [PI15; Cam03; Lam+16].

The last case is one of the most interesting from an environmental point of view, since the possibility to employ electric source for propulsion may allow the desired emission reduction [Hep12; Van15]. Fostered by promising results in automotive industry, some manufacturers have already entered in the commerce with small electric aircraft; in particular it is worth noting the experience of Pipistrel [Pip16; Pip11] and Lange Aviation [Lan03; Cos11].

In practice, the challenges of designing aircraft with new propulsive systems require a cross-disciplinary effort that focuses on: feasible propulsion system, reduced fuel consumption, aviation safety and reliability, noise reduction, and optimised aircraft design to achieve desirable performance [Liu+18]. Starting from the very basic performance, even the Breguet equation loses its validity for this category of aircraft, and must be reformulated [Hep12; Mar+17]. The definition of a proper powerplant is not a trivial aspect [Isi+12], and also acceptance to passengers is of relevance in the introduction of such disruptive concept [Hor+13]. Nevertheless, many authors, such as Freeman et al. [Fre+14] or Seitz et al. [Sei+12], note that new propulsive system based on hybrid/electric technologies opens new and still unexplored scenarios that may potentially be beneficial from a performance point of view. Campbell in its work identifies hybrid/electric propulsion as the most promising solution for revolutionary propulsion [Cam03].

It is to note that the electric aircraft already flying today are within the segment of small

aircraft (two or four seater), whereas the most critical segment on which an action is needed is the single and twin aisle large passenger aircraft, as shown also in the breakdown of Fig. 1.2. In particular, both Boeing and Airbus [Air19; Boe16] identify the single aisle aircraft as the segment with the major growth in 20 years perspective, and it is then the one of relevance for this research. Conceptual studies to cover this segment are available in literature; next section will survey some of them to understand their impact and possible benefit.

1.3.1 Hybrid and electric propulsion technology

This section focuses more on the concept, proposed in literature, to match the environmental goals of Table 1.1, and thus have a long-term entry into service, except for the NASA X-57. The study of large passenger aircraft featuring hybrid and electric (HE) propulsion has started in last decade within the NASA funded projects, as the N+3 [Fol+11] and the SUGAR [BD12; BD15], the Aurora D8 program [Dre11], the PEGASUS concept [AC17], the ECO-150 aircraft [SF16; FS19], or the CE-Liner proposed by Bauhaus [Hor+13; Ste+12b], just to give some examples.

The key aspect in these studies is the perspectives of available technologies in long-term: nowadays the exploration of the superconducting devices has started, and they show better performance than the non cryogenic technologies [Dev+15; Mad+16]. The great advantage of the superconductors theory is that it eliminates the thermal management unit, which represents one of the most relevant weight penalties, and a main aspect in the sizing of electric aircraft, that can not be neglected [Fre+14].

Among the possibilities introduced by the hybrid/electric propulsion, two main features have been identified: distributed propulsion [Goh14] and Boundary Layer Ingestion device [SR47]. They have been noted because of their interest in terms of aero-propulsive integration and propulsive efficiency, confirmed by different authors [Bor+16; Wel+17], and thus they are reviewed more in detail; before going through these topics, some notions on hybrid/electric architecture are introduced in next paragraph.

1.3.1.1 Hybrid propulsion fundamentals

A dual-energy source aircraft can be categorised using the degree of hybridization, initially defined by Isikveren et al. [Isi+14]. The degree of hybridization is a figure of merit of the aircraft hybridization, that can be related to the power or the energy. It is defined as the power/energy demanded by the secondary source over the total:

$$H_P = \frac{P_{elec}}{P_{tot}} \quad (1.1a)$$

$$H_E = \frac{E_{elec}}{E_{tot}} \quad (1.1b)$$

It is to remark that the H_P and H_E are referred to a dual-energy source aircraft, but they do not depend by the type of sources: electric power can be delivered by batteries such as other devices, without losing any generality. By definition, a conventional aircraft has $H_P = H_E = 0$. With the help of these definitions, four types of aircraft can be recognised, the scheme of which is shown in Fig. 1.5:

- All electric aircraft, that use exclusively electric energy and power (Fig. 1.5a).
- Turboelectric aircraft, that use combustibile fuel for energy storage but electric power to drive the propulsors (Fig. 1.5b).
- Series hybrid aircraft, where electrical power is supplied by the two sources that work together and are connected through an electrical node, called bus (Fig 1.5c).
- Parallel hybrid aircraft, where the engine provides power to propulsors mechanically. Combustion engine may use electrical power to reduce the fuel flow [BD15], or clutch-off to allow full electric segments [AA12] (Fig. 1.5d).

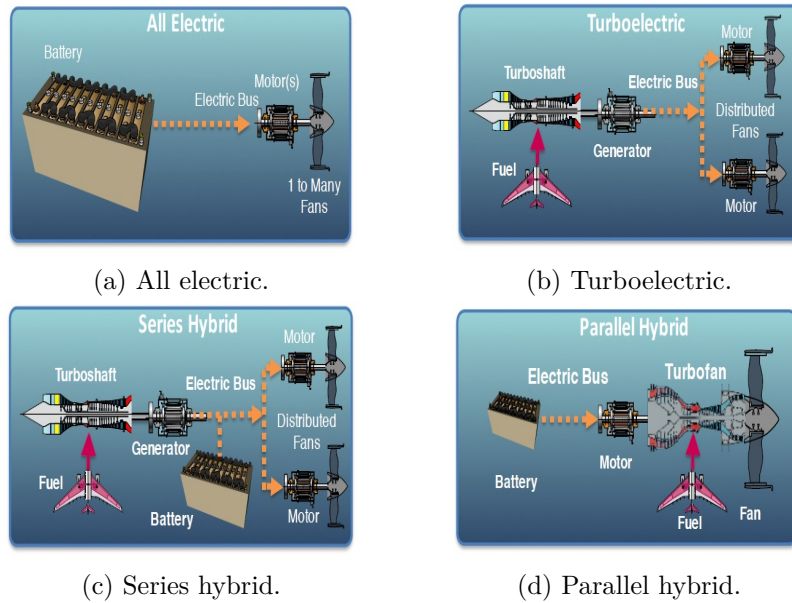


Figure 1.5: Different electric propulsion architectures [Mad+16].

The categories just described are classified according to the degree of hybridization as in Table 1.2: the classification is clear recalling the definition of H_P and H_E .

In an hybrid electric architecture the key points for the sizing are the power and the energy requirements: each component needs to supply a certain amount of power. For this reason, when evaluating this kind of concept, the two most important technological parameters, for each device, are the specific power and the specific energy [Fra15; NAE16], defined respectively as the power or energy per unit of mass. Specific energy content is particularly valuable for batteries design, since these elements must store a certain amount of energy, meanwhile

	H_P	H_E
Conventional	0	0
All-electric	1	1
Turboelectric	>0	0
Series hybrid	1	<1
Parallel hybrid	<1	<1

Table 1.2: Classification of electric propulsion architectures, based on the degree of hybridization.

specific power is the key design parameter for electric components that must deliver certain amount of power. Following the examples of Pernet et al. [Por+14b; Por15] and Brelje and Martins [BM18b], the notation here adopted uses the lowercase to represent specific quantities of the extensive quantity: *i.e.*, e indicated the specific energy density and p the specific power density.

Together with the specific quantities, also the volumetric densities are relevant, since the volume available constrains the integration of the electronic systems. Specific and volumetric densities are related through the physical density:

$$\rho_E = \rho e \quad (1.2a)$$

$$\rho_P = \rho p \quad (1.2b)$$

where ρ_E and ρ_P are the energy and power volumetric content, and ρ the physical density.

The main challenge facing HE aircraft is that batteries specific energy content is 50 times lower than that of fuel: *i.e.*, for the fuel $e_f=11900 \text{ kW h kg}^{-1}$, meanwhile for a classical Lithium-Ion battery $e_b=200 \text{ kW h kg}^{-1}$, for today's technology [RL16]. This is also shown in Fig. 1.6, that presents the energy characteristics for different energy storage systems.

From the diagram emerges that hydrogen has a very large specific energy, even larger than the kerosene, but at standard pressure the volume content is poor, and thus it requires large volumes for the allocation. The problem can be avoided pressurizing the hydrogen, or using it at liquid state with a cryogenic technology, but difficulties in the identification of a sustainable production, storage and delivery system make this technology unfeasible for aviation, considering today's technological capabilities [RSG14].

The problem of mounting and dismounting batteries' package has been addressed by Plötner et al. [Pl13] in the case of CE-Liner, and in their work they showed that integration of batteries in airframe, as well as airport operations (mounting/dismounting) do not present particular issue, for today's technology. Among the different types, LiOH batteries are the most performing, with the highest energy and volume content, that allow to have a certain amount of energy still with a feasible volume that can be mounted on aircraft. However, the huge difference with respect to kerosene characteristics limits the range of application: batteries introduce in fact a weight penalty, resulting in a bigger MTOW for HE aircraft. As a consequence, this concept is not feasible for long range distances, where the effect of carrying

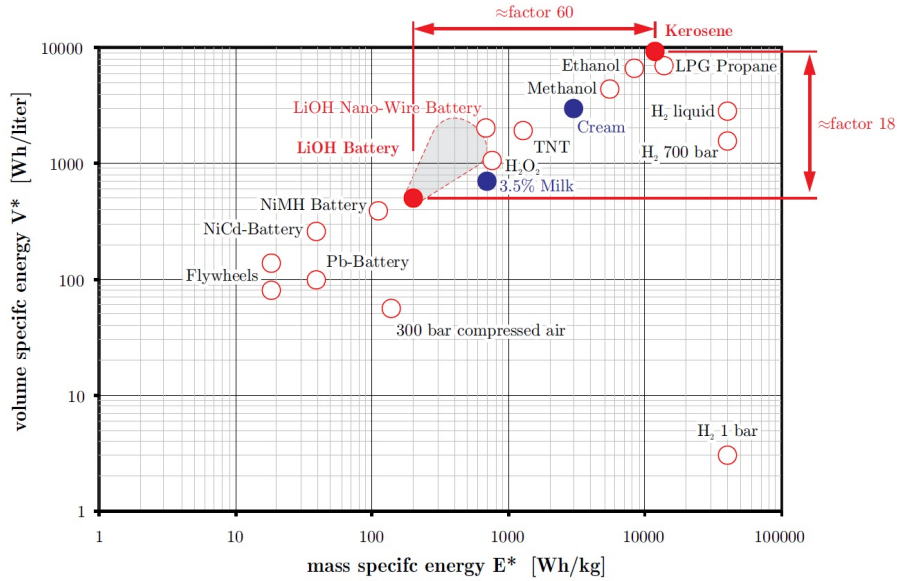


Figure 1.6: Mass specific energy vs. volume specific energy for different energy storage systems [Hep12].

heavy batteries outweighs the total energy advantage coming from the hybridization: its major interest is within the short and medium range segment.

Finally, to conclude this overview on the hybrid and electric aircraft fundamentals, a metric to assess the “goodness” of the hybrid/electric concept must be defined. Some of the parameters used for conventional aircraft work fine also for the hybrid electric architecture [BM18b], *e.g.* the fuel burn or the MTOW [Ros05h; Tho13].

Acquisition and direct costs are also relevant as metrics, specially for airlines. Pernet et al. presented new models for the cost evaluation, that consider the substitution of an internal combustion engine (ICE) with new hybrid power plant [PKG14].

Then, literature proposes other metrics: among all the possibilities, for hybrid electric aircraft are particularly relevant the energy specific air range ESAR [PKG14; Plo+13] and the payload fuel energy efficiency PFEE [Hil+08], plus some other metrics for propulsion system performance evaluation, that prescind to the propulsive system itself and can be applied for conventional, hybrid and electric aircraft [SH13]. The ESAR quantifies the distance flown per unit of energy, and it is directly derived from the specific air range SAR (distance flown per mass of fuel). Higher the ESAR, better is the aircraft.

The disadvantage of the ESAR, as similar metrics, is that it does not consider the payload: according to the ESAR, an aircraft that is not carrying any payload results more efficient than a loaded aircraft, when in reality the first one is not useful, since the main scope of the aircraft is to carry a certain payload from one point to another. To include also the useful carried weight, Hileman [Hil+08] defined the PFEE as the range-payload per unit of energy

consumed:

$$PFEE = \frac{Rm_{PL}}{E_c} \quad (1.3)$$

This metric identifies an efficient aircraft as that one able to carry for longer distances a certain payload, with less energy, so it includes all the key aspects in the aircraft design. Unified propulsion system performance metrics proposed by Schmitz can be applied to all types of propulsion, but they do not consider the integration within the overall design and they are tailored purely to evaluate propulsive performance. PFEE, instead, represents the most complete figure of merit to assess the validity of the hybrid concept.

1.3.1.2 Distributed propulsion technology review

The distributed propulsion architecture addresses the problem of how to improve propulsive efficiency η_p . This quantity depends on the fan pressure ratio (FPR) as follow [FKB09]:

$$\eta_p = 0.98 - 0.08(\text{FPR} - 1) \quad (1.4)$$

Engine's manufacturers have been working for years to reduce the FPR and increase η_p , but the procedure presents a relevant drawback: to keep the same thrust level, a reduced FPR requires a bigger mass flow rate passing through the fan. This reflects on greater fan dimensions [Sch+19]. As example, Fig. 1.7 shows a comparison between the engine's dimension of the A320 and its evolved configuration, the A320Neo, mounting the new LEAP engine [CFM16]. It is clear that it is not possible to continuously reduce the FPR, because



Figure 1.7: Comparison between the Airbus A320 (right) and the new A320 Neo (left) mounting the innovative LEAP engine.

the advantages of having a better propulsive efficiency will be counterbalanced by the augmentation in drag due to the bigger wetted surfaces.

In this context, the distributed propulsion (DP) has a major interest, since it allows to

distribute thrust on a given set of engines, with a smaller power requirement than the classical two engine configurations [KSM03; Kir15; Sch+19]. So with the help of DP it is still possible to reduce the FPR, keeping dimensions limited.

As seen in previous section, the DP represents a key technology that has been massively explored in recent years. Gohardani is one of the pioneer of the DP, and collected in a single paper all the milestones of such system, from early years to today [GDS11], and opened perspectives for its application in the electric aircraft. It is to underline that the DP technology is applied without considering the devices that generate thrust: they can be propellers, ducted fans, moved by turboshafts or electric motors. Strictly speaking, this technology is related to how the total thrust can be distributed, no matter how it is produced. The interest to integrate the DP with an electric propulsive system is that the electric components can be downscaled, reducing the weight [KPA18]. To differentiate the two cases, the acronym DP is used to talk about the concept, as DEP (distributed electric propulsion) is linked with the particular application of DP to electric propulsion.

One of the main example of DEP application to improve the propulsive efficiency is provided by DRAGON, a concept presented by ONERA [Sch+19] and shown in Fig. 1.8. In this



Figure 1.8: DRAGON concept, proposed by ONERA [Sch+19].

concept two turboshafts provide electric power to the motors, mounted on the wing lower surface. This concept is represented of the downsizing due to the distributed propulsion, and represents a practical application of DEP applied to the segment of major interest in this research. Tradeoff studies on this configuration are promising and identify potential gains with respect to reference conventional aircraft. Also, this work addresses the problem of the mass variation due to the presence of a distributed propulsion system: in theory, the distributed weight along the wing relax the bending moment at the wing root, resulting in a possible less stiffened structure. In practice, the authors explain that this analysis does not include the torsion moment generated by the engines, and some preliminary analyses show that there is an increase in weight due to this effect [Sch+19]. Kim et al. further developed the propulsive and weight aspects, adding some knowledge to the aforementioned work of Gohardany [Kim10; KPA18]: they proposed a benchmark of typical weights and aircraft parameters featuring DEP.

Moreover, the potentiality introduced by DEP are not only limited to a better propulsive efficiency: indeed, the idea is 60 years old and dates back to 1924, when Manzel considered the possibility of distributing propellers over a row [Man24]. He had an intuition that in this system aerodynamics and propulsive aspects are correlated; in some experimental work he detected that the region interested by the presence of distributed fan is subject to a blowing, which energises the flow. In this condition it is possible to potentially have laminar flow with increased lift, resulting in a reduced takeoff and landing length; unfortunately the project has been abandoned for lack of knowledge. His idea was further developed at the beginning of the VTOL concepts [Mal74], and it has been further developed up to today; even the basic idea was the same of Manzel, his concept has been brought on a new level, thanks to the knowledge gained in over 80 years [Goh14].

The state of the art for the DP application is the NASA SCEPTOR X-57 demonstrator [Bor+16] shown in Fig. 1.9. It is a small aircraft, based on the existing Tecnam P2006T



Figure 1.9: NASA SCEPTOR X-57 concept [Bor+16].

aircraft, that proposes to use two wingtip propellers, to reduce induced drag, and a certain number of smaller distributed propellers, to take advantages of distributed propulsion through the blowing effect to increase the maximum C_L [Dee+17b]. High-lift devices are not needed anymore, leading to an easier and lighter wing structure; however, the distributed propellers require an accurate wing design [Dee+17a]. To avoid problem in cruise, where the blowing worsens the handling qualities, the small propellers are used only for takeoff and landing, then they are feathered and only the two wingtip propellers are used. The electric version of the NASA X-57, sometimes referred as NASA X-57 Maxwell, mounts Lithium-Ion batteries to supply electric power. Thermal [Sch+17b] and control aspects [Cla+17] of this configuration have been studied, then the batteries and the propellers have been optimised with respect to the mission requirements [HN18]: it is possible to say that the work on the NASA X-57 is the most comprehensive and represents the best example of electric integration benefits. It is also a milestone in the distributed propulsion effects on performance and sizing [MN18].

Another interesting concept, in the same segment as the X-57, is AMPERE [HRD16], developed at ONERA and depicted in Fig. 1.10. Instead of having distributed propellers, the propulsion is obtained with a set of ducted fans, distributed along the wing. Differently

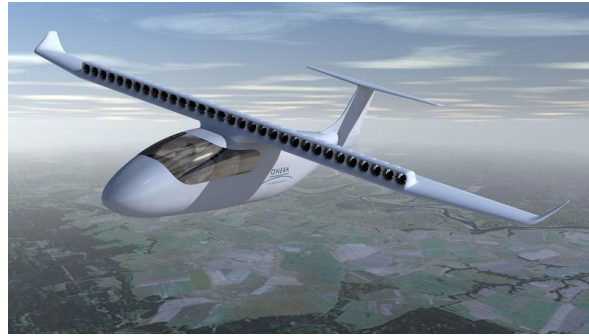


Figure 1.10: AMPERE concept, proposed by ONERA [HRD16].

from the previous example, the blowing effect is acting in all the mission phases, and thus to understand how it impacts on the handling qualities wing tunnel tests and simulations have been carried out [Dil+18].

Nevertheless, blowing phenomenon is just one of the aerodynamic effects introduced by DP: Manzel already mentioned the possibility of a laminar flow over the wing, and in recent years Borer et al. [Bor+17], for the case of NASA X-57, showed that indeed laminarity is obtained and assessed the related aerodynamic improvement. However, the benefits strongly depend on the engines' position: Wick et al. [Wic+15] considered three different configurations, with engines over the wing, integrated within the structure and under the wing, and it has been seen that the aerodynamics strongly depends on how the engines are distributed. The embedded configurations are even harder to analyse, due to the strong coupling between the aerodynamics and the propulsion, as well as the structural side of building wing with propulsors integrated in the airframe [Khe15]. Hoogref et al. [Hoo+19], on the contrary, concluded showing that the DP must be rediscussed, because the advantages can not be so marked as the literature may suggest. At this stage, further analyses have to be conducted to select the most promising disposition to benefit of DP.

Another non trivial feature of DP is linked to the possibility of engines downsizing. Generally, one of the main requirements to meet in aircraft design is the case of one engine inoperative (OEI) [Ros05a]. This condition in a DP system becomes less stringent: in fact, in case one engine is out, to get the same thrust level the other engines must provide less thrust *i.e.* in case of 4 engines deployed than 2 [Ste+12b]. This concept is better illustrated in Fig. 1.11. Of course, a lower installed thrust is directly linked to a smaller engines; it is to mention that on a safety point of view the DP may be considered safer than the classical one, since it intrinsically adds redundancy.

Safety aspects of the DP are treated by Papathakis et al. [Pap+17], but so far a full comprehension of all the issues related to security is still a remarkable challenge. At this stage, research is still far to define a preferable arrangement for the engines, to maximise aerodynamics' benefit; also, due to the strong integration between different disciplines, so far the works are limited by the use of high fidelity tools, and thus the DP effects in the overall design process have not been considered yet. A clear and shared DP terminology is

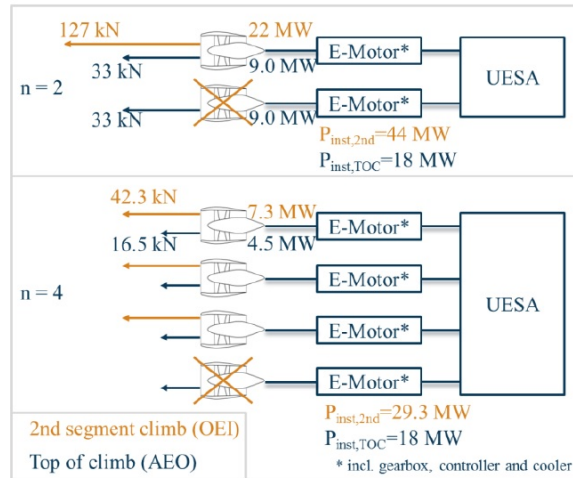


Figure 1.11: Illustration showing the difference in the engine sizing to meet the OEI condition for 2 and 4 motors [Ste+12b].

desireable in the future to permit to better discuss this emerging technology. Then, more detailed studies are needed to identify an optimised framework, involving weight, number of propulsion units, and other top level aircraft parameters, to meet a commercial configuration capable to go through a sustainable civil aviation.

Distributed electric propulsion is only one of the two features identified for hybrid/electric technology, the other one is the BLI, which enhances the advantages of DEP and viceversa, as it will be better detailed in the following section.

1.3.1.3 Boundary layer ingestion device

The second aspect identified for hybrid and electric configurations is the Boundary Layer Ingestion (BLI) device: it is one of the core technologies that may impact the distributed propulsion technology. The BLI idea arose at the beginning for marine applications [Par+05; RW98] and has been lately applied to aircraft [TPP05; OAG08; AO06; Pei+16], mainly in subsonic configurations, but some examples on supersonic jet can be found too [KST92].

A non negligible part of the total drag around a body in a flow comes from the boundary layer [MS98b]; the BLI is a device that reduces this contribution by partially ingesting the boundary layer [Smi93]. As for the DEP, this technology is not recent: one of the early application comes from the work of Smith and Roberts [SR47] in 1947. In their work, they compared a conventional turbojet configuration with one having installed boundary layer suction devices within some slots in the wing. They assessed a 30% improvement in fuel efficiency and a 7% higher optimum cruise speed due to the suction of the boundary layer; also they demonstrated that BLI increases the lift-to-drag ratio, reduces takeoff length and contributes to enhance control characteristics. Again, its development has been stopped because of lack of knowledge needed, but the improvement since then allows to consider such

device for today's applications.

The main challenge in dealing with the BLI lies in a proper formulation to assess the benefits: since it includes the boundary layer aspects, a fully RANS model needs to be used. The most important phenomenon related to BLI is that the flow field results changed: streamlines are not parallel to the body anymore and distortion occurs at the inlet entrance. Considering only this effect may neglect important phenomena in the evaluation of the BLI benefits; Plas et al. [Pla+07] report all the physical phenomena that occur in BLI and need to be considered:

- State of the boundary layer coming into the intake;
- Inlet design, both outside and inside;
- Evolution of the non-uniform inlet flow from intake entrance to engine face;
- Distortion transfer across the fan;
- Response of the fan to the distortion, which may impact operability and aeromechanics;
- Evolution of the flow downstream of the fan;
- Duct losses, which shows a high sensitivity because of low FPR;
- Potential flow separation and unsteadiness of the flow field.

So far, the most common way to treat the BLI is with the help of a RANS model: Gray et al. presented an approach in which these equations are coupled with the propulsion, and the geometry is optimised to maximize the benefits of the BLI in the STARC-ABL concept [Gra+18b]. The same authors optimised the overall turboelectric propulsion system featuring the BLI [Gra+18a]. NASA presented an easier modelling, yet using high fidelity, based on the entropy calculation and successfully used in the N+3 concept studies [Gre+10a; Gre+10b]; ONERA reported a similar approach, but based on the exergy more than the entropy [Arn+14]. De la Rosa Blanco et al. considered the BLI as basis for a silent aircraft engine, noting the advantages in noise reduction; they also assessed a gain of about 4% with respect to the best in class with the BLI [EdC07]. There is no evidence of surrogate models, or semi-empirical equations, capable to deal with this phenomenon at low fidelity, and this may be understandable because of the large number of phenomena to be considered.

Another issue is the definition of a figure of merit to evaluate performance; different authors use the power saving coefficient PSC, defined as below [Smi93]:

$$\text{PSC} = \frac{P_{ref} - P_{BLI}}{P_{ref}} \quad (1.5)$$

In the equation above, P_{ref} is the reference power of a non-BLI propulsor and P_{BLI} the power required by the propulsors in case the BLI is mounted: as such, PSC quantifies the

reduction in the power needed, on a common configuration, with and without the boundary layer suction. It is clear that the BLI represents a key feature and may be beneficial for the emission' reduction, despite the huge number of challenges that it poses.

The most interesting application of BLI is the STARC-ABL [WF16], shown in Fig. 1.12. This concept was born because the NASA wanted to develop a concept feasible in the nearer term, overcoming the high technological barrier set by N+3 program [BD15]. In the STARC-

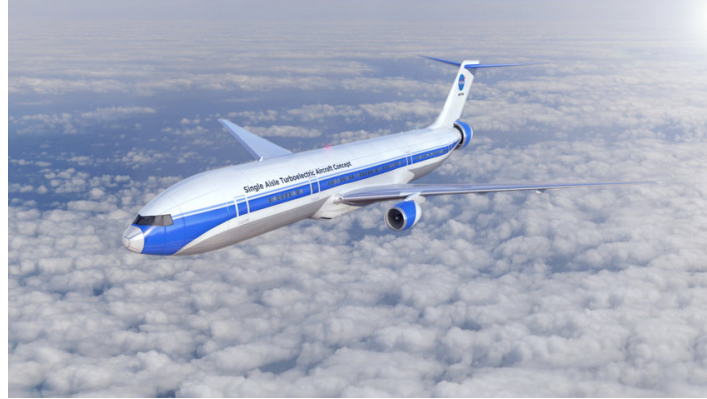


Figure 1.12: STARC-ABL concept, proposed by NASA [WF16].

ABL a tailcone propulsor is mounted on a conventional TAW fuselage, and it works coupled with two downsized turbofans, which provide power needed [Yoo+19]. The tail-cone propulsor is integrated within the fuselage and mounts a BLI device, capable to ingest around 60% of the fuselage boundary layer [Wel+17]. The performance assessment shows a 10-12% fuel burn reduction thanks to the BLI. Another interesting study concerns the dynamic behaviour of the propulsive system, analysed in one of the latest work on STARC-ABL [KT19]: the dynamic of electric system is indeed an aspect that cannot be neglected during the design of powerplant components; but the level of detail is already higher than that required at conceptual design. The program is still active and more studies are foreseen in the next years.

On European side, the CENTRELINE consortium is investigating a concept similar to the STARC-ABL, with propulsive fuselage, called CENTRELINE [Sei+18; Hab+18; BSH18; Gor+18]. The aircraft is depicted in Fig. 1.13; an entry into service 2035 is foreseen for the concept. Works on the CENTRELINE confirm the potential benefits coming from a propulsive fuselage with a BLI devices, already seen in the STARC-ABL. A major point of interest is the design of the powerplant, based on turboelectric configuration, and the technologies adopted [BSH18].

So far, two different potential technologies to be used in the hybrid and electric frame have been addressed: the DEP and the BLI, which seem to be the most promising features of such a kind of aircraft. Actually, these two aspects are not separated, but the DEP is synergistic with BLI, since each one enhances the effect of the other [Goh14]. Indeed, each element of a distributed propulsion can be equipped with a BLI device, and enlarging the distribution over the spanwise dimensions increase the portion of area subject to the ingestion, improving the aerodynamics. In addition, the BLI has an effect on the thrust requirement [SR47], which



Figure 1.13: CENTRELINE concept, proposed by the CENTRELINE European consortium [Sei+18].

indirectly impact the fan size.

The main question is: which is the best geometry to be considered, to maximize the benefits coming from the DEP coupled with BLI? From the experience of the STARC-ABL, the BLI operates better when the reference length is higher: in configurations like the DRAGON one, its effects can be neglected because of the reduced chord length in the wing. This has been confirmed by another study on the Nautilus concept [WN18], and others [Arn+14; Pla+07].

Possible candidate to answer the question is the Blended Wing-Body [LPR98], in which the whole body is a lifting surface, and the reference length is large enough to take the maximum benefits from a possible integration with DEP and BLI [Bis+18; KL13]. Besides this aspect, the BWB concept offers more space to locate distributed propulsion, maximizing the area subject to the combined effect of blowing and BLI. Last but not least, the BWB is a concept designed to maximise the aerodynamic, and thus it shows higher lift-to-drag ratio (values of 22-23 or above are foreseen): it has the potentiality to combine a morphological efficient architecture with enhancement benefits coming from the distributed propulsion, since it offers large span and chords to benefit of DEP and BLI features, explained above.

Hence, seen the very promising perspectives offered by the BWB, next section investigates more profoundly this configuration, to understand the basic aspects and problems, in order to prepare the field for the discussion regarding a possible integration with hybrid propulsion.

1.3.2 Blended Wing-Body aircraft

On a classical TAW configuration, the fuselage is only aimed to carry passengers and baggage, but it is solely a source of drag, being a non lifting component. To generate lift in a more efficiency way, it would be better to have all the components generating lift: this is the idea behind the Blended Wing-Body (BWB) concept, where even the passengers' cabin is aerodynamically shaped to contribute to the total aircraft lift.

The first evidence of an integrated concept can be found in the delta wing aircraft [NW96], as *i.e.* the Northrop YB-49 aircraft [Rob47; AK89]. These concepts have been mainly developed for military applications, and they are considered as the precursor of the modern BWB concept. McDonnell & Douglas company was the first to think at the utilisation of BWB for civil transport in 1994, and the outcomes of this work were published by Liebeck in 1998 [LPR98]. Boeing followed their example and proposed a configuration for 450 passengers [Lie04]: these two examples represent a milestone in the development of this configuration, and they are both shown in Fig. 1.14.

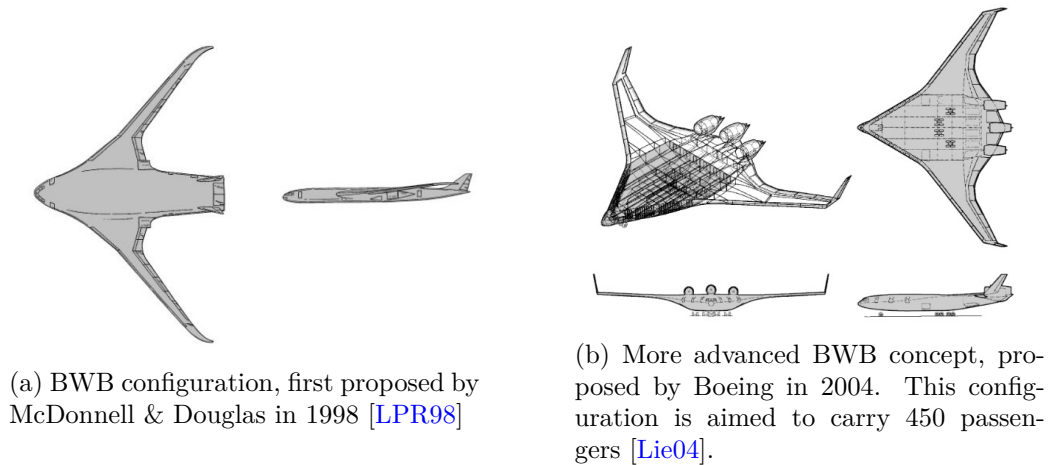


Figure 1.14: Main milestones in the Blended Wing-Body concept.

The gain in the global lift-to-drag ratio comes mainly from the wetted area reduction: the integration of payload, lift, control surfaces and propulsion in an airfoil shaped centerbody helps to reduce the wetted area of about 30% [LPR98], resulting in a lower friction coefficient and a better efficiency. The maximum lift-to-drag ratio is estimated to be likely around 27 [Tor91]. Apart from the aerodynamic aspects, BWB shows also an improved structural efficiency, coming from the lower wing loading and large inertia relief [Lie04]. Some studies also confirm that it has reduced the noise, relevant aspect close to ground, *i.e.* during takeoff and landing [Gre+10a]. Also, the BWB has more available volume to be used for the freight and the subsystem allocations, allowing more flexibility in the center of gravity positioning.

Despite these advantages, several challenges arise in its design:

- Since the cabin it is not cylindrical anymore, the pressurization generates a non-linear stress constraint which varies quadratically with the cabin's width (see Fig. 1.15), resulting in a more complex structural design [LPR98; Muk+04; Muk05]. Of course this leads to an increase in mass, compared to a conventional fuselage: the challenge is to design a shell to efficiently carry the pressurization loads, saving weight.
- The BWB is a tailless configuration, so the airfoil design is a key point to obtain a longitudinally stable aircraft [NW96], otherwise fly-by-wire systems for the active control have to be inserted, with penalties in weight.

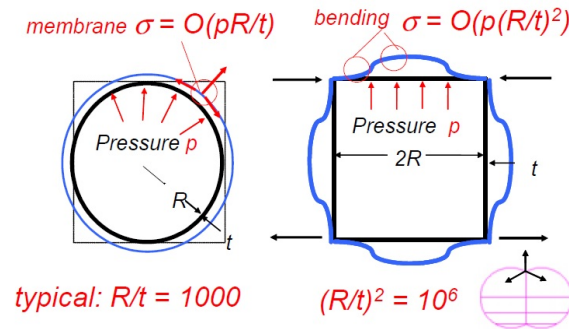


Figure 1.15: Different load distributions due to pressurization in a circular (left) and non-circular (right) cabin.

- Generally, the centerbody trailing edge is used to trim the aircraft at low speed: there is less place for high lift devices and thus $C_{L_{\max}}$ is reduced with respect to a conventional aircraft.
- Because of the airfoil-shaped centerbody, the landing gears positioning may represent an issue. In order to have enough space available for this component, the relative thickness must be oversized, and this aspect is more critical especially for small BWB (short and medium range).

These drawbacks make the interest in this concept being lost, because of the high commercial risk; however, it has emerged again in past years. Nickol et al. [NH16] considered the BWB as the most promising concept for the aviation environmental sustainability; in the N+3 project the BWB has been deeply studied to assess its performance: the final report from NASA represents a milestone because it provides a comprehensive study of different aspects [Gre+10a], together with an appendix with all the models [Gre+10b]. Centracchio et al. [CRI18] got almost the same results as Nickol, comparing a BWB concept with long range best-in-class aircraft. TU Delft presented two works, one related to the cabin design [VGH12], and the second one about the parametrization and low fidelity models for evaluate the weights [BV18]; ONERA [Def+18] proposed an OAD procedure for its sizing within the CICA project; AGILE project studies the definition of an OAD procedure for the BWB sizing, in their paradigm [Pra+18; Ani+18], ISAE-Supaero, together with Airbus, mainly addressed with two Ph.D. projects the problem of the handling qualities [Sau13; Den16]. Also, it is to mention the study of Bonet, who analysed a scaled BWB geometry in wind tunnel [Bon18], to confirm numerical results, and the X-48 demonstrator [NAS13], built from Boeing and NASA on the basis of Liebeck's work [Lie04] to study control within a flight test campaign, and the experimental work of Cranfield University for the VULCAN concept [PMP60]. Finally, DZYNE (a company based in California, USA) presented a new concept [PSY18], based on an innovative landing gear sizing, which opens this concept for small size, without the drawback of the oversized thickness-to-chord ratio. They announced the construction of a BWB for an entry into service in the next decade, covering different segments, from the business to long range. They called it ASCENT, and a visualisation of this concept is provided in Fig. 1.16, taken from the work of Page et al. [PSY18].



Figure 1.16: Rendering of the BWB Ascent 1000, announced by DZYNE and expected to fly in the near future [PSY18].

The examples above indicate how large is the interest in this concept, nevertheless, they are not exhaustive of the whole literature on the topic: a more expanded review on the development of this concept throughout the years can be found in the work of Okonokwo and Smith [OS16], Ordoukhanian and Madni [OM14], or in the lecture note from prof. Scholz [Sch06]. Most of cited works cover only structural and aerodynamic aspects, using high fidelity; a minor part is instead deputed to handling qualities and control laws. At this stage there are only two evidences in literature of a revised sizing process for the BWB: NASA has implemented surrogate model for the cabin design, with aerodynamic correction, in its in-house code called FLOPS [Bra04], but its development has been stopped [BM18b]. Van Dommelen and Vos [vV14] presented a conceptual tool for the BWB design, based on classical methods that can be found in Roskam's books [Ros05a].

Another difficulty is that there is no availability of public reference data, to build surrogate models to use in preliminary design, with some exceptions as the FLOPS code, the aforementioned work of Van Dommelen and Vos [vV14], and the database of NACA for the Northrop YB-49 aircraft [Rob47; AK89]. In the following two paragraphs, the problem of structural and aerodynamic design for a BWB is addressed, to prepare the field for a possible modelling approach, to be integrated in the conceptual design cycle.

1.3.2.1 Structural design of Blended Wing-Body concept

The cabin structure is the most challenging aspect in designing the BWB: it must carry passengers (and eventually payload) and sustain both pressurization and aerodynamic loads. In literature it is possible to find three main propositions: integrated, segregated and oval structure. The first two were proposed by Liebeck [LPR98], the third one has been explored by Vos et al. [VGH12]. They also suggest the following element to be considered when analyzing the cabin design:

- Design simplicity;

- Passenger evacuation;
- Passenger comfort;
- Structural efficiency;
- Aerodynamic efficiency.

The three cabin concepts have been considered by different authors dealing with structural design [Muk+04; Muk05; QA18; HHH08], essential features of each of them is listed below.

- **Integrated structure.**

This concept consists on a unique skin which carries out the aerodynamics and the pressurization loads. The aerodynamisc envelop is divided by several walls to increase the stiffness. The skin is optimized with respect to aero loads, which entails the skin is not optimized for the pressure. Indeed, this configuration is very simple and mimics conventional fuselages, both for the integrating vessel and the passengers' evacuation. The main issue is in the pressure load distribution: the pressure cabin is interrupted by structural elements which impacts negatively the passengers comfort. However, educing them to improve the comfort reduces the structural efficiency too, so a compromise has to be found.

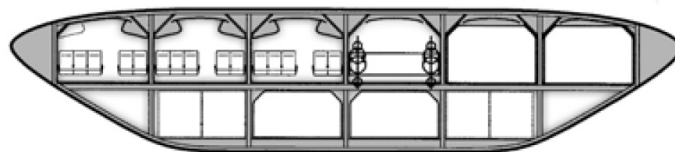


Figure 1.17: Integrated cabin structure design.

- **Segregated structure.**

This concept consists on a separation of the pressurization loads from all others. The structure is formed with two skins: the external skin which carries out the aerodynamics and the load transferring; and the internal one which only carries out the pressure load. Thus, the external skin is optimized with respect to aerodynamics and the internal one is formed by intersecting circular tubes which are connected with vertical shells. This solution is very efficient both aerodynamically and structurally, and it increases passengers comfort, but the double shell adds complexity in the overall design, with consequently penalties in weight. Also, the evacuation can be an issue, since the exit has to penetrate both the shells, a stiffener may be needed.

- **Oval structure.**

Compared to the previous two, this configuration is the more complex: in every design phase a compromise between structural, aerodynamic efficiency and payload integration has to be found. It has shown the largest amount of pressurized space, introducing

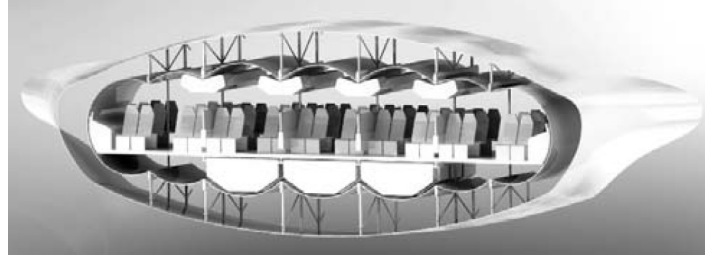


Figure 1.18: Segregated cabin structure design.

penalties in weight and in the aerodynamics design, which is compromised by structural requirements. The major interest of this configuration lies in the passengers comfort: they have an uninterrupted view in the pressure cabin which enhances their orientation and acceptance; it also allows natural light throughout the cabin. On this side, the oval configuration is the closest possible to a conventional fuselage. The evacuation is done in the same way as in the integrating concept, with cutaways in the outer shell.

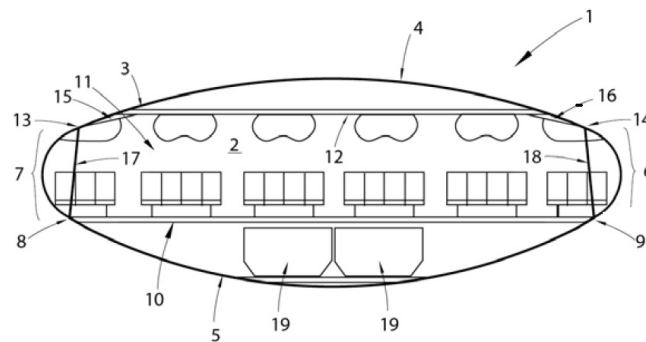


Figure 1.19: Oval cabin structure design.

From these elements, it is possible to make a decision matrix to understand which is the most promising solution. This is done in Table 1.3, where a value of +1 is assigned whereas there is an advantage using a certain concept, 0 if an aspect may be an issue, but no relevant and -1 whereas a concept introduces a penalty.

Table 1.3 shows that the most interesting concept is the integrated one, since it conjugates a non complex design with acceptable passenger comfort and evacuation and good structural and aerodynamic efficiency: indeed, it has been largely used in different studies on the BWB structural design [Pit+11; Kaw11; Hil+10; Bra04; Che12]. These works use finite element method, with a detailed structure, to get an estimation of the structural mass of BWB: van Dommelen and Vos collected the available data from literature in their work [vV14]; Table 1.4 sums up their review. It is to note that no less than 215 passengers are considered. In general, the more complex structure introduces a penalty in weight: for comparison, the structural mass of the Airbus A321, designed for 236 passengers, is 48.5 t, which is lighter than the data of Table 1.4, except for the BWB-250 which uses very aggressive hypothesis for the

	Integrated	Segregated	Oval
Design complexity	+1	-1	-1
Passenger evacuation	+1	-1	+1
Passenger comfort	0	+1	+1
Structural efficiency	0	+1	+1
Aerodynamic efficiency	+1	+1	0

Table 1.3: Decision matrix for the three BWB cabin concepts proposed in literature. Values are assigned as follow: +1 if there is a good improvement, 0 if it may be an issue, but not relevant and -1 if it introduces a penalty.

Aircraft	Ref.	Number of passengers	Structural mass [t]
OREIO	[Pit+11]	224	54.9
N2A	[Kaw11]	262	51.6
SAX-40	[Hil+10]	215–236	47.6
BWB-250	[Bra04]	250	38.3
BWB-450	[Bra04]	450	68.9

Table 1.4: Structural masses for different BWB concepts available in literature. Adapted from [vV14].

material. However, this comparison is only indicative, since a lot of information about the detailed design adopted are missing, but it gives in any case an idea about the expected order of magnitude.

Bradley was the only one to try to get a surrogate model, for an easy application in preliminary design phase [Bra04]. In his work, he considered different BWB configurations, varying from 200 to 450 passengers, all of them shown in Fig. 1.20. The concept for the cabin

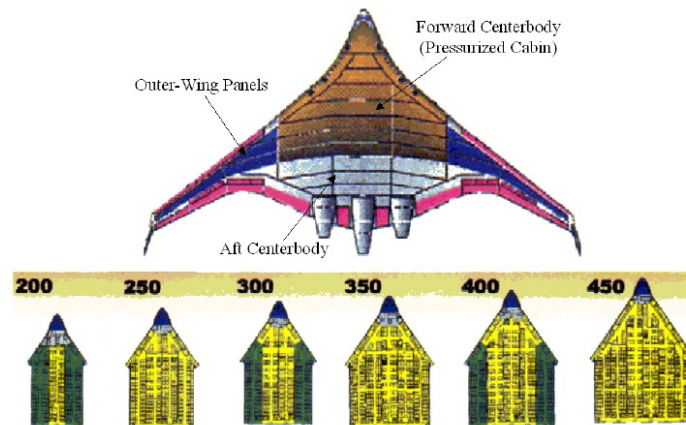


Figure 1.20: Blended Wing-Body cabin design, according to Bradley [Bra04]

is the integrated one: he assumed that the cabin is divided into bays by the ribs, and each bay can allocate a single aisle with two column of passengers. Then, he built the models and ran FEM analyses, for different configurations, to estimate the cabin mass. With the

data obtained, he aimed to find a surrogate model, where the cabin mass formula takes the following shape:

$$m_{cabin} = a (m_{TO})^b (S_{cabin})^c \quad (1.6)$$

where m_{cabin} is the mass of the cabin, m_{TO} the maximum takeoff weight, S_{cabin} the planform surface of the centerbody (including the area behind the cabin) and a , b , c some constants to be determined.

Using the regression analysis, the three constants may be determined, finally having

$$m_{cabin} = k_s 0.316422 (m_{TO})^{0.166552} (S_{cabin})^{1.061158} \quad (1.7)$$

where k_s is a scaling factor to consider different technologies, that in his work was calibrated on the Boeing data, resulting to be $k_s = 5.698865$. This model has then been implemented into FLOPS, a NASA in-house code for the preliminary design, to size a BWB, but as already said it has been abandoned and no further development came out.

The main limiting factor of the model proposed by Bradley is that it uses very aggressive hypothesis on the composite material, and it considers also one load case, with reference values from Liebeck [Lie04]; also, it does not consider the effect of the cabin thickness. Despite these drawbacks, it has been successfully applied in other projects [LHF17] and still remains a good starting point for further development of a conceptual tool for the BWB.

Some authors carried out also a dynamic structural analysis for the BWB, in order to capture the vibration modes [YWS15; WC10; SSP13; Car04]. Despite the research on this field is very limited, results show that a BWB configuration suffers less of flutter problem, due to stiffer structure, but torsional and bending moment are more critical. The most complete work is the one presented by Stettner and Voss [SV02], who included also handling qualities together with aeroelasticity analysis, showing that the trim problem is not trivial. Their main conclusion is that the BWB configuration needs more control surfaces than conventional aircraft to ensure stability and controllability, especially at low speed condition, where the bending and torsional moments are more relevant.

1.3.2.2 Aerodynamic tradeoff for the Blended Wing-Body

The BWB design is mainly done for improving aerodynamic performances, achieved by having a single lifting body and a reduced wetted area [LPR98]. The airfoil design is then a priority for the aerodynamic design, in particular for the cabin section, in which the thickness has to be large enough to allocate the passengers.

The BWB design is highly influenced by equilibrium and stability constraints: for longitudinal equilibrium, the center of gravity should be aft of the neutral point, defined as the ultimate point the center of gravity can assume to have neutral static stability (corresponding to $C_{M_\alpha} = 0$) [And12]. This location, however, implies a statically unstable aircraft. Herein, classical notation for aircraft stability is considered: moment is positive when it is clockwise, that is when it tends to pitch up the nose of the aircraft [RL97; Ros08]. In conventional

aircraft a horizontal tail is designed to make the aircraft statically stable, but being the BWB a tailless concept, the stability criterion must be met in other ways [Den16]. The goal is to have a small positive moment coefficient around the center of gravity $C_{M_{cg}}$, at the cruise angle of attack, which represents the best condition. Most of the airfoils, instead, are designed to obtain a negative C_m [Av59], the only exception is represented by the reflex airfoil. These types of airfoils have a trailing edge camber line lifted upward, generating a positive C_m , and this effect makes them perfect for the BWB design [Ale14; Wan12]. The most common reflex airfoil family is represented by the NACA 5-digit series [Av59], but other families have been developed, like the MH family, deputed for the use on tailless aircraft [Hep18; Hep90].

However, using a reflex airfoil could compromise the transonic behaviour [Sar+10]: due to three-dimensionality, most of the centerbody lift is generated at the front. For a reflex airfoil, this zone needs more curvature to counteract the lose of lift in the afterward part. As such, the critical and drag divergence Mach numbers are lower than that of a conventional airfoil, with potentially issue in the transonic regime. To limit the contribution to compressibility, as general rule, the thickness-to-chord ratio for the centerbody must not exceed 18% [KS15; Ike06].

The path just described helps the section design, but on a global point of view the aerodynamic load and the target C_l distribution drive the design [And12]. It is to recall that the aerodynamic load is a lumped quantity, associated to the lift distribution as follow

$$\gamma(\eta) = \frac{c(\eta) C_l(\eta)}{2b} \quad (1.8)$$

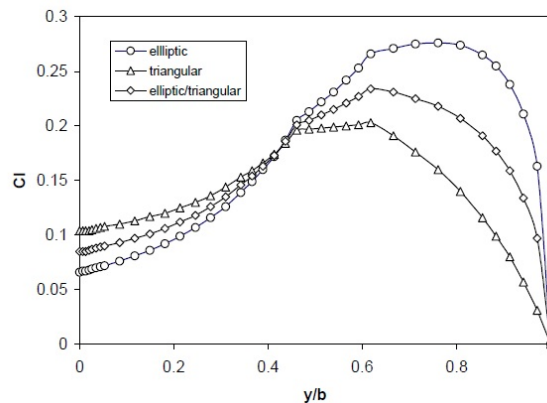
where $\eta = \frac{y}{b}$ is the non dimensional coordinate in the spanwise direction, c and C_l the local chord and lift coefficient, and b the wing span. Integrating this quantity over the span the global C_L is obtained

$$C_L = AR \int_0^{\frac{b}{2}} \gamma(\eta) d\eta \quad (1.9)$$

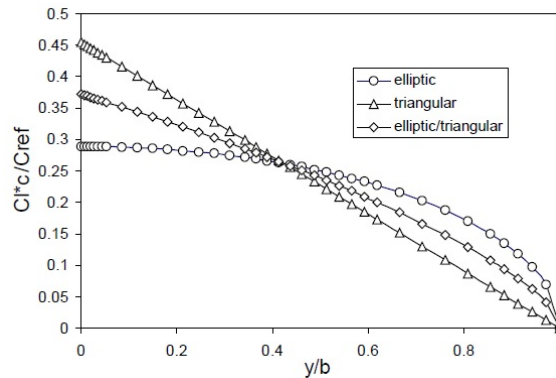
with AR being the aspect ratio.

On a conventional aircraft, with an aspect ratio above 5-6, the Prandtl theory gives results with a good accuracy; the reduced aspect ratio of the BWB, however, suggests that the Prandtl theory is not valid anymore, but the Jones theory may be more indicated [de15b]. This theory states that, in case of a low and untwisted aspect ratio wing, the aerodynamic load follows the elliptical distribution, and then from one hand the induced drag is minimised, but from the other hand it shows high C_l at the wing tip for untwisted configuration, with consequently issues for the transonic performance and controllability because of the impossibility to use ailerons. Qin et al. [Qin+04] studied the load distribution on a BWB configuration, using RANS methods, and confirmed that the elliptical distribution is obtained with an untwisted wing. To balance the induced drag and the transonic performance, they added a twist distribution, using the inverse design technique, and found that the best load is obtained averaging and elliptical load with a triangular one. The inverse design is done using a low fidelity method (panel method); the results are then assessed on a set of points with high fidelity (RANS method). Their results are presented in Fig. 1.21a and Fig. 1.21b,

as well as in Table 1.5. With the average load, the lift coefficient at the tip is not as high as the elliptical case, avoiding stall and compressibility problems, but it is not as low as the triangular distribution, avoiding to increase the angle of attack to find the right lift. The elliptical-triangular distribution has a lower global C_L , but the difference is small (around 2%); from Table 1.5 it can also be noted that, even if for an elliptical distribution the induced drag is lower, the wave drag is instead higher and in the end the global C_D is higher, confirming that it is not the global optimal distribution, but only with respect to the induced drag.



(a) Target lift distribution as a function of non dimensional span, for the case examined by Qin et al. [Qin+04].



(b) Target aerodynamic load distribution as a function of non dimensional span, for the case examined by Qin et al. [Qin+04].

Figure 1.21: Aerodynamic tradeoff for a BWB, from the work of Qin et al. [Qin+04].

The work just described is interesting for two main reasons: it confirms that the Jones theory can be applied on a BWB, and it is the first evidence of a strategy in which the low fidelity is used to design a BWB, with the results being lately assessed using high fidelity. For what has been extensively said in Section 1.2, at conceptual design is a key point to have fast and reliable methods, and Qin suggested a first path to follow in the conceptual aerodynamic

Table 1.5: Comparison of performance for the different target distributions examined in the work of Qin et al. [Qin+04], related to a BWB configuration.

Twist distribution	C_L	C_D	C_{D_i}	C_{D_f}	C_{D_w}
Baseline	0.4136	0.03268	0.02504	0.00764	0.00407
Elliptic	0.4102	0.02837	0.02031	0.00806	0.00209
Averaged	0.4090	0.02783	0.02008	0.00774	0.00180
Triangular	0.4071	0.02866	0.02083	0.00783	0.00161

design of the BWB.

Beside this work, the other major references about the BWB aerodynamics used RANS method for the design: the design point is chosen, based on the target C_L , and then the configuration is resized until it matches the requirement. This approach has the drawback that there are no information about the other operating points at which the BWB flies [Li+12].

In the past year, fostered in the progress made in the MDO techniques [ML13], different authors used optimisation algorithm for the geometry design, included the airfoil. The first ones were Mader and Martins [MM13], who tested on a flying wing this approach. Later Lyu and Martins set up an optimisation routine for a BWB, based again on a RANS solver [LM14]. They defined a total of 273 design variables, regarding the twist distribution, the airfoil shape, the local sweep and chord, and the span, as shown in Fig. 1.22. They investigated the impact of the various constraints and design variables on optimised BWB: trim and static stability were investigated both for the design and off design conditions. As a result, it was possible to find the best combination of wing twist and airfoil reflex to maximize the efficiency, satisfying at the same time trim and stability constraints.

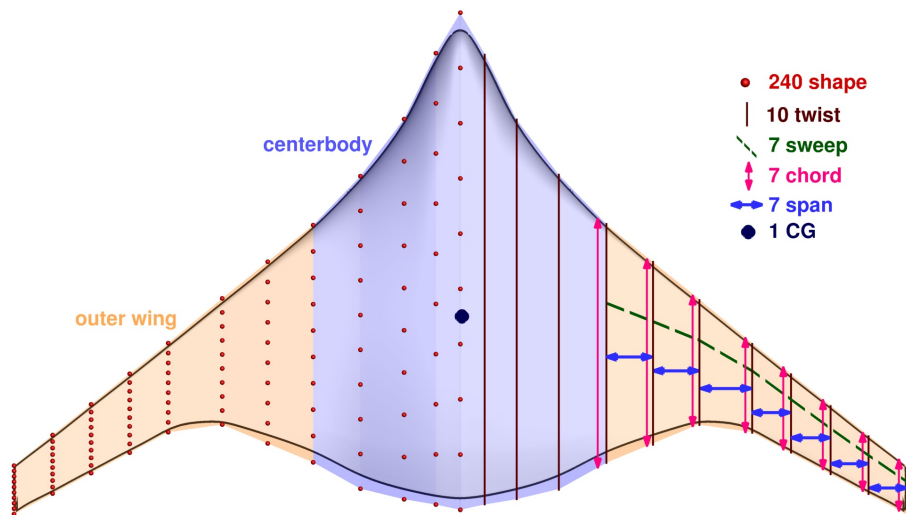


Figure 1.22: Shape and planform design variables considered in the work of Lyu and Martins, for the BWB optimisation [LM14].

Liou et al. [LKL16; Lio+17] carried out a similar work, including also the engine integra-

tion within the airframe, on a NASA hybrid configuration. Through all these works, that do not cover all the bibliography for the subject, the RANS-based aerodynamics shape optimisation method has been well assessed: they demonstrated that is a practical tool for the BWB aerodynamic design. The main drawback is the computational cost: it is unfeasible to carry out such simulations on a single processor, and then a multiprocessor architecture is needed; still, the computational cost remains high. As example, in the work of Lyu and Martins [LM14], a single optimisation converged in 10 h using 240 processors. Thus, it is unfeasible to integrate CFD analysis for aerodynamics within the conceptual design loop, but it can be used to validate low fidelity methods or to define surrogate models, based on few set of geometrical parameters.

On this direction, a first step has been done by Prince et al. [Pri+18], who tested a commercial code, based on panel method, and compared the results with a RANS solver: they reports a maximum error of 10% for the BWB configuration, which may be acceptable at conceptual design. Also, the maximum difference occurs at very high Mach number, when the compressibility effects are dominating the flow field; at low Mach numbers the agreement between the methods is much more marked.

This work and the already mentioned work of Qin et al. represent the two most interesting cases in which theory or low fidelity methods are applied for the BWB configuration; further investigation is needed to get more reliable results, or even surrogate models to replace the empirical equations suggested by Roskam and extensively used for conventional aircraft [Ros05f].

The overview on the BWB concept ends up here: the next paragraph will discuss the possible integration among the innovative technologies identified to finally converge towards a potential solution capable to match environmental goals.

1.4 The research problem

1.4.1 Towards a promising solution for aviation sustainability

The previous section reports a review of the most promising innovative technologies considered in literature, to match the aviation's environmental goal for the upcoming years. Among all the possibilities, the hybrid and electric propulsion have been identified: from the studies reported came out that this technology has been identified as the best choice for the next generation aircraft. In particular, the main feature is that it opens new and still unexplored possibilities, *e.g.* the integration with a BLI device to improve aerodynamics. Distributed propulsion is identified as a solution to take advantage of the hybrid propulsion, especially because DEP enhances the benefits coming from the BLI, and viceversa.

Then, the focus has been shifted on the best architecture for this integration: in fact, BLI to be efficient requires large chords, otherwise its impact is negligible. The solution is the Blended Wing-Body architecture, which is characterised by the integration of aerodynamic,

structure and payload. By definition, the BWB is a whole lifting surface, and offers very large chords. So, it comes almost naturally to consider the Blended Wing-Body featuring distributed electric propulsion as possible solution for next generation aircraft. In fact, it takes advantages from all the innovative aspects described above. It is to note that innovation is brought on a two different level: propulsive, with the introduction of a new power plant, and structural, with a disruptive concept mainly designed for high aerodynamic performances.

The integration of BWB with DEP is confirmed by one of the most known concept proposed by NASA, within the N+3 program: the N3-X turboelectric concept [KBF08]. This concept, shown in Fig. 1.23, has been designed to be competitor of the Boeing 777 in terms of range and payload, and it is characterised by the integration of a distributed electric propulsive system within the BWB architecture. The entry into service goal is set to 2040: technological assumptions are made in perspectives for this horizon. The propulsors are



Figure 1.23: NASA N3-X concept [KBF08].

mounted at the trailing edge, with the electric power coming from two generators, located at the wing tip; studies from Kim et al. [Kim+13] show that this configuration enables very high propulsive efficiency, thanks to the partial electrification of the engine's cycle. The N3-X has been presented for the first time in 2008: both Kim [KBF08] and Felder [FKB09] performed preliminary studies to have a first estimation of its performance. Both the works showed that N3-X offers very good performance in terms of fuel reduction; as a consequence, deeper studies were conducted to confirm the preliminary results [FTC12; Kim+14], with refined trade-off for the weights [Bro11], noise and emission [BH14]. It has been estimated that the concept requires an amount of power in the order of 50 MW: such demand makes the superconducting technology and the associated cryogenic subsystems the only possible way to satisfy the requirements. In different works Rolls-Royce and the University of Strathclyde in UK collaborated on electrical system trades [ARB12a; ARB12b; Arm+15] and the system safety analysis of such a complex architecture [Ros+14; Sha+14; Sha+15]. The assessment of performance shows a reduction of 70% in fuel burn, compared to the Boeing 777 [Fel+11], due to the partial electrification and the improved airframe; economic viability is demonstrated

too [Gol+17]. The main issue with this concept is that it uses a very aggressive technology, and thus it introduces a large amount of technological risk for an EIS2040: Jansen et al. [Jan+17] studied, for this case, the required individual technology for the electric subsystems, and they are really challenging even dealing with such a large technological horizon. Despite that, the N3-X is still a milestone for the integration of the hybrid propulsion within BWB airframe and the benchmarking for the fuel burn, noise and emission reduction.

Beside the N3-X, other authors found an interest in the BWB featuring hybrid propulsion: Rodriguez presented the benefits coming from the BLI on a reference Boeing geometry [Rod09], meanwhile Kok [KVv10] and Campbell [Cam+05] separately studied the effects of combining DEP and BLI on a BWB configuration. Finally, Ko et al. [Ko+03] set up a multidisciplinary optimisation formulation to get the optimal geometry with respect to the propulsive benefits. All these works report an improvement in the fuel efficiency above the 20-30%.

So far, the N3-X is the most complete concept, but it has been studied considering individual disciplines, with specific high fidelity tools, but no OAD process is defined. Also, it is competitor of the Boeing 777, so it is designed for long range and 450 passengers, whereas the single aisle aircraft, as *i.e.* the Airbus A320, represents the critical segment for emission (see Fig. 1.2), and in Boeing perspective it will be the segment with the major growing ratio [Boe16].

1.4.2 Problem statement and proposed solutions

This research, finally, has the objective to define an OAD process, at conceptual level, for the study of a BWB featuring DEP, in the same segment as the Airbus A320 (short/medium range, 150 passengers). An EIS 2035 is considered; to limit the risk associated to the concept, only non-cryogenic technology is considered. In fact, there is a lot of uncertainty about the cryogenic technology and its application for aviation on short term.

The research problem can be summed up in the following question:

Research problem. How can the conceptual design process be revised for the study of an unconventional configuration that features an innovative hybrid powerplant?

The answer is not obvious: conceptual design methods, described in Sec. 1.2, are well assessed for a TAW aircraft configuration, but are not valid anymore for hybrid aircraft. The example of the N3-X, as well as the X-57, the STARC-ABL and others presented in Sec. 1.3, show hybrid/electric aircraft have more interaction between disciplines than a conventional aircraft. As already remarked, even the Breguet equation does not hold yet and must be revised [Hep12; Mar+17]. The most representative case of the existing coupling is provided by aerodynamics and propulsion, that cannot be considered as separated disciplines, since each one impacts the other one. Pernet et al. [Por+14b; Por+14a] presented a preliminary sizing procedure for hybrid aircraft, and they stressed in different points that integration of a new hybrid powerplant has an impact on all disciplines. At that stage several assumptions have been

done, that limit the application. Cinar et al. [Cin+17a] arrived at same conclusion; De Vries et al. [dBV18] presented instead a revised procedure for the sizing that includes aero-propulsive interaction, demonstrating on a test case of regional aircraft that the two disciplines cannot be considered separated anymore.

More complications come considering the thermal management, which has been neglected in the three works cited above [Por+14b; Cin+17a; dBV18]: Freeman [Fre+14] and Campbell [Cam03] noted that thermal aspects cannot be neglected when considering electric architecture. Due to the large demand of power, dissipation due to Joule effect is significant, and cooling systems must be included to avoid problems related to structure's heating.

A key point, addressed by Brelje and Martins, is that the classical design procedure relies on MDA, and its capability to deal with the problem of unconventional configurations is limited [BM18b]. Research must focus more on a revised sizing procedure, based on Multidisciplinary Design optimisation (MDO) [ML13]; sometimes the notation MDAO (Multidisciplinary Design Analysis and Optimisation) is used to highlight the multidisciplinary characterization. The MDAO, as defined by Martins and Lambe [ML13], is a “field of engineering that focuses on the use of numerical optimization for the design of systems that involve a number of disciplines and subsystems”. MDO origins can be traced back to '60 years, when Haftka [Haf73; Haf+75; Haf77; Haf79] and Schmit [Sch65; ST65; Sch81; Sch84] started to extend their experience in the structural optimisation to other disciplines. In recent years, thanks to the improvements in computational science and the new resources available, MDO is become a powerful tool for aircraft design [Kro+84; Man99; AK05; HMP12; AC12] and other engineering problems [ML13]. Moreover, it is recognised as the only solution to deal with the problem of unconventional configurations [LM14; Ray18; BM18b]. Brelje and Martins demonstrated their assumption on another work [BM18a], whereas they present an MDO tool for the optimisation of small electric aircraft. Despite the limiting assumptions in models used, they concluded that performances were indeed improved compared to a conventional MDA procedure. Also, they identified the problem of a full MDO formulation for aircraft design problem as still an open issue in literature.

Finally, the answer to the research problem comes out. It can be divided into three subpoints, as follow:

Answer to research problem. The problem of sizing unconventional configurations with hybrid architecture for the thrust generation at conceptual level can be tackled through:

- The definition of new models, to consider the impact of the innovative architecture on geometry, structure, aerodynamics and performance evaluation;
- The application of detailed design for some key disciplines, to calibrate the conceptual design methods with more refined simulations;
- The definition of a sizing procedure based on Multidisciplinary Design Analysis

and Optimisation, because of its capability to establish tradeoff taking into account all the interactions between disciplines, particularly relevant for unconventional aircraft.

The definition of an MDAO formulation opens two related issues: “Which are the models to use for the discipline, to account for innovative configurations?” and “Which is the best MDO formulation for aircraft design problem?”. All these issues will be addressed in the manuscript; the two main research objectives can be summed up considering these points:

- Set up of a complete multidisciplinary design analysis process for the sizing of the innovative concept and its performance evaluation;
- Choice of the most suitable multidisciplinary design optimisation formulation, in order to carry out an optimisation loop.

It has been noted several times, and recalled here, that the test case of BWB with DEP presents two main innovations, one related to the propulsive architecture and another one to the overall configuration. To facilitate the development of a sizing procedure, the work is divided into three minor steps:

- Study of a TAW configuration featuring distributed electric propulsion,
- Study of a medium range BWB, with conventional engines,
- Merge of the two previous concepts, to finally arrive at the BWB with distributed electric propulsion.

The Ph.D. roadmap, that shows this division into intermediate steps, is shown in Fig. 1.24. The approach taken allows to study the two innovative aspects introduced separately, assessing their benefits in terms of aircraft performance individually.

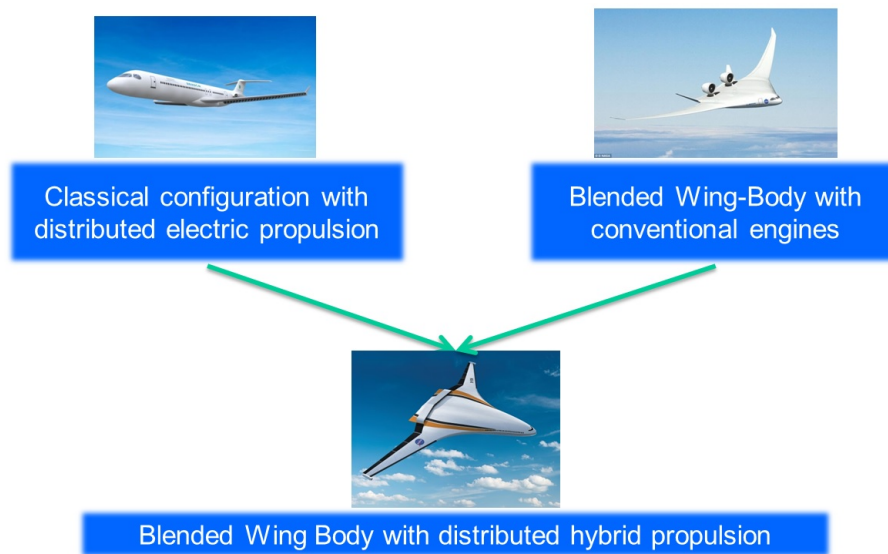


Figure 1.24: Ph.D. roadmap, representing the two separated steps to finally converge toward the Blended Wing-Body with distributed electric propulsion configuration.

Synthesis of the chapter

- Increase of emissions pose a problem for aviation: to reduce the environmental footprint, a disruptive concept must be introduced.
- The exploration of an innovative concept must be carried out at conceptual design level.
- Key technologies to match the environmental goals are explored:
 - Hybrid and electric propulsion offers new and still unexplored features.
 - Blended Wing-Body is identified as the most promising architecture for the integration with a distributed electric propulsion system.
 - Blended Wing-Body with distributed electric propulsion is chosen as test case for the research.
- Because of the strong integration among disciplines for unconventional aircraft, classical conceptual design loop based on Multidisciplinary Design Analysis may lead to misleading results: definition of an Overall Aircraft Design procedure based on Multidisciplinary Design Optimisation technique is investigated.
- The two key technologies introduced (hybrid propulsion and BWB architecture) are studied separately: final concept results from the merging between the two.

Chapter 2

Development of an optimisation framework for conceptual aircraft design

Résumé

Ce chapitre présente l'élaboration d'un cadre pour le dimensionnement et l'optimisation d'un avion de grande capacité. Le code développé repose sur l'intégration de FAST dans la plate-forme d'optimisation multidisciplinaire OpenMDAO.

FAST est un outil d'analyse de conception multidisciplinaire développé par l'ONERA et l'ISAE-Supaero pour le dimensionnement d'aéronefs conventionnels. Entièrement écrit en Python, il est basé sur les méthodes classiques du manuel de conception et sur une approche de masse ponctuelle pour l'estimation des performances. La boucle de dimensionnement regroupe toutes les disciplines clés de la conception des aéronefs: aérodynamique, structure/masse, propulsion, performances, ainsi que certains aspects liés aux spécifications de certification. Le scénario de test de validation de FAST est l'avion CERAS d'Airbus A320.

OpenMDAO est plutôt une plate-forme d'optimisation multidisciplinaire développée par la NASA Glenn Research Center. Ce intègre une grande variété d'algorithmes d'optimisation, déjà inclus dans les bibliothèques Python, dans un code créé spécifiquement pour faciliter la définition de problèmes d'optimisation de conception multidisciplinaire. Grâce à sa logique, composée de modules indépendants, le problème peut être décomposé et organisé au plus haut niveau très facilement : cette approche modulaire permet de remplacer certaines disciplines avec des modifications mineures. La principale caractéristique d'OpenMDAO est liée à MAUD, qui constitue un moyen innovant de

calculer des dérivés pour résoudre des problèmes d'optimisation. Grâce à MAUD, OpenMDAO peut calculer efficacement les dérivées, en réduisant le coût de calcul, et il est principalement adapté aux optimisations basées sur les gradients. Son succès est attesté par la grande variété de travaux faisant appel à OpenMDAO que ce soit dans le cadre de problèmes aéronautiques et aérospatiaux ou d'autres sujets.

Pour intégrer FAST dans OpenMDAO, le code doit être modifié et réorganisé: les anciennes disciplines sont décomposées en différents modules ; pour faciliter l'utilisation du gradient, chaque module correspond à une équation. À un niveau supérieur, les critères de conception, par exemple pour les surfaces d'aile et d'empennage, sont remplacés par la définition de contraintes de conception pour le problème d'optimisation, afin de permettre à l'optimiseur de trouver la meilleure solution dans l'espace de conception. Grâce aux méthodes numériques efficaces et à la logique d'OpenMDAO, le coût de calcul a été réduit de 5 minutes à environ 30 secondes pour une seule itération. Cependant, il présente l'inconvénient que la modularité a introduit 200 nouvelles fonctions, au lieu des 20 fonctions utilisés précédemment, ce qui peut compliquer la compréhension du code par un nouvel utilisateur. La formulation résultante de l'optimisation multidisciplinaire est l'architecture MDF, qui apparaît comme la plus appropriée au problème de conception d'aéronef, bien qu'elle nécessite la définition d'une boucle complète d'analyse de conception multidisciplinaire.

La version intégrée a été appliquée sur le scénario du cas test CERAS: les résultats montrent que l'optimisation entraîne une réduction de la consommation de carburant d'environ 10%, ce qui n'est pas négligeable en pourcentage. Ensuite, l'avion CERAS est redimensionné en tenant compte de différentes plages de conception et d'hypothèses technologiques pour l'horizon 2035, afin d'obtenir un ensemble d'aéronefs de référence à utiliser pour la comparaison avec les configurations non conventionnelles qui seront proposées dans les chapitres suivants.

Il est à mentionner que le travail d'intégration a été effectué en collaboration avec le MDO Lab. à l'Université du Michigan, lors d'une visite de 3 mois de janvier à avril 2018, avec le support financier de la Formation Doctorale ISAE-Supaero.

Contents

2.1	Introduction	49
2.2	The sizing tool FAST	49
2.2.1	Overview	49
2.2.2	I/O structure file	50
2.2.3	Code description	51
2.2.3.1	Propulsion	53
2.2.3.2	Geometry	54
2.2.3.3	Aerodynamics	58
2.2.3.4	Mass estimation	60
2.2.3.5	Performance	61
2.2.3.6	CCM – Certification Constraint Module	64
2.2.4	Test case: Airbus A320	67
2.3	OpenMDAO – a multidisciplinary optimisation platform	70
2.4	The integrated platform FAST and OpenMDAO	73
2.4.1	Optimisation of a turbofan aircraft with FAST under OpenMDAO	79
2.4.1.1	Problem formulation	79
2.4.1.2	Test case: A320 CERAS aircraft	81
2.4.1.3	Test case: A320 CERAS resized for EIS2035	84
2.5	Conclusion	88

Outline

- Description of FAST, the ONERA and ISAE-Supaero aircraft sizing tool, is given.
- OpenMDAO, the multidisciplinary optimisation tool from NASA Glenn Research Centre, is presented. Notions on its logic are given, to understand the development of MDO problems.
- An integrated sizing tool is obtained from the coding of FAST within the OpenMDAO platform.
- The integrated code FAST and OpenMDAO is used to optimise the Airbus A320 CERAS test case.

2.1 Introduction

This chapter presents the sizing tool developed in this research to obtain an MDO procedure, considering the test case of a conventional aircraft. It comes from the integration of FAST [Sch+17a], an in-house code developed at ONERA and ISAE-Supaero, into OpenMDAO, an optimisation platform developed at NASA Langley Research Centre [Ope18a; Gra+19].

At first, Sec. 2.2 presents a description of the original code FAST, including discipline models and validation cases. Then, Sec. 2.3 describes the multidisciplinary optimisation platform OpenMDAO, highlighting its capabilities and main features for optimisation problems. Finally, the integration of FAST into OpenMDAO is reported in Sec. 2.4, where the recoding work is detailed. This section gives also the chance to highlight differences between the MDA and the MDO approach, showing that the latest is more accurate when dealing with a large number of disciplines, thanks to the way the design constraints are defined. The new framework is then evaluated on the Airbus A320 CERAS test case [CER15], to assess the optimisation process, and is then used to define the reference aircraft, to compare with the hybrid and the BWB concept later.

It must be mentioned that the work described in this chapter has been done in collaboration with the MDO Lab., at University of Michigan, during a visit conducted from January to April 2018. The visit has been funded thanks to a grant for international exchange from *Formation Doctorale* of ISAE-Supaero.

2.2 The sizing tool FAST

2.2.1 Overview

FAST (Fixed-wing Aircraft Sizing Tool) is an in-house software, developed by ONERA and ISAE-Supaero, for aircraft sizing and analysis purposes [Sch+17a]. Fully developed in Python 2.7, in its native version, it is a multidisciplinary code, capable to carry out the preliminary sizing of a turbofan aircraft, for given top level requirements (TLAR), and evaluate its performance. The validation case is the A320 CERAS test case [Sch+18], based on the Airbus A320 data [Air18]. During the process, it considers all the key disciplines in aircraft design: aerodynamics, structure/mass estimation and propulsion. Since FAST is tailored for the conceptual design, models are based mainly on semi-empirical equations, coming from classical design handbooks [Ros05a; Ray18] and Airbus experience and collected in the ISAE-Supaero notes [DC12], which are accurate as long the conventional TAW configuration is considered.

FAST interfaces also with other softwares, that are used for aerodynamic computation: XFOIL [MIT18b] for airfoil performance and OpenVSP [Ope18b] for the low speed polars. The last one is also used for visualisation purposes at the end of the sizing procedure. An xml file (eXtensible Markup Language) is used for the flow data: it contains the initial set of

TLAR and collects the output variables of the design process. Thus the `xml` file is the I/O file for the FAST workflow.

After its first developments, FAST has been successfully used in several projects, and it is now been expanded to consider regional aircraft, ATR type [Boh+18], and to interface with a certification constraint module and full mission simulations [Sch+18; Sch18]. The next sections give an outlook to the main elements of FAST: Sec. 2.2.2 describes I/O file structure, Sec. 2.2.3 reports details of a description of all the parts of the software, and Sec. 2.2.4 reports the results for the validation test case.

2.2.2 I/O structure file

To manage the dataflow, FAST relies on an `xml` file. This format is mainly indicated for the management of a large data flow, since it facilitates the inputs and the outputs, and is well interfaced with Python, thanks to the dedicated libraries [Nag+12].

FAST uses GAMME for reading and writing [BHK13]: it is a meta-model, capable to automatically create Python dictionaries from the `xml` file. It can also handle units and their conversion, which is an added feature of relevance in aircraft design, where input data can be given following different unit systems.

The main argument of `xml` file is called `Aircraft`. Then this argument is structured in nine subparts, on different levels (from input data to output per discipline), as follows:

- **TLAR.** This section contains the top level requirements for the aircraft: aircraft type (large passenger, business jet, . . .), range, number of passengers, approach speed, cruise Mach number and maximum allowable takeoff runway length.
- **Configuration.** This section contains the parameters used to define the configuration, such as engine location or empennage type. Each of these specifications is identified by a numerical flag.
- **Mission.** This section contains the parameters to define the given mission, and, as outputs, the relative fuel breakdown, time of flight and takeoff/landing performances. This section has two sublevels: one related to the design mission, and another one to operational missions.
- **Cabin.** This section is used to define all the parameters for the internal cabin layout.
- **Geometry.** This section is dedicated to the geometry. It is divided into several sublevels, one for each geometrical component: in each sublevel there are a few sets of inputs. As outputs, all the geometrical dimensions are reported. This section is also shared with the OpenVSP visualisation tool, in order to create a 3D sketch of the aircraft at the end of the sizing loop.
- **Propulsion.** This section contains the input parameters for the engine definition, according to the chosen model, as it will be described later.

- **Aerodynamics.** This section is solely for output, and it stores global aerodynamic parameters.
- **Weight.** This section is for the mass breakdown, and it is divided into sublevels: airframe, propulsion, secondary systems, furnishings and crew. The breakdown is made according to the standard defined by the French norm AR 2001/D [DGA84].
- **Balance.** This section shows the same structure as the **Weight** section, but instead of masses it contains all the center of gravities positions, plus the global center of gravity. It is also used to define the maximum allowable CG range variation, used to satisfy stability requirements.

An example of `xml` file structure is reported in Appendix A.

Accessing a file is a costly procedure in programming, even with dedicated libraries that facilitates the reading and writing: for this reason, FAST reads the `xml` file one time at the beginning of the process, to store all the input variables. Afterwards, it accesses to the file again at the end of sizing, for output writing purposes.

Finally, it must be highlighted that `xml` format has been largely used in aircraft design: a standard, called CPACS, is defined as common language, to facilitate the data sharing [Nag+12]. To enlarge the possible utilisation of the software, FAST is provided with a CPACS converter, to switch between this standard and the native `xml` standard for FAST.

2.2.3 Code description

The code is described in Fig. 2.1, with the xDSM standard, meanwhile the detailed algorithm (with the numbering referred to the figure) is reported below in Alg. 2. The scheme shown in Fig. 2.1 highlights the multidisciplinary nature of the software: disciplines are connected each others and exchange lot of data, as indicated by the grey line.

It must be noted that the engine is initialised outside the sizing loop, using the inputs from the `xml` file. The curves of thrust and specific fuel consumption SFC are obtained and provided to the performance analysis: in other words, FAST does not include the engine sizing in the design process. Instead, it relies on a pre-existing engine deck, as will be detailed in Sec. 2.2.3.1.

The driven parameter for the MDA convergence is the operating weight empty OWE estimation. There are two estimations for this parameter; the first one is obtained at analysis 3 as sum of all the airframe, propulsion, systems and furniture masses:

$$m_{e3} = \sum_{i=1}^n m_i \quad (2.1)$$

where i represents the generic component, as in the mass standard [DGA84].

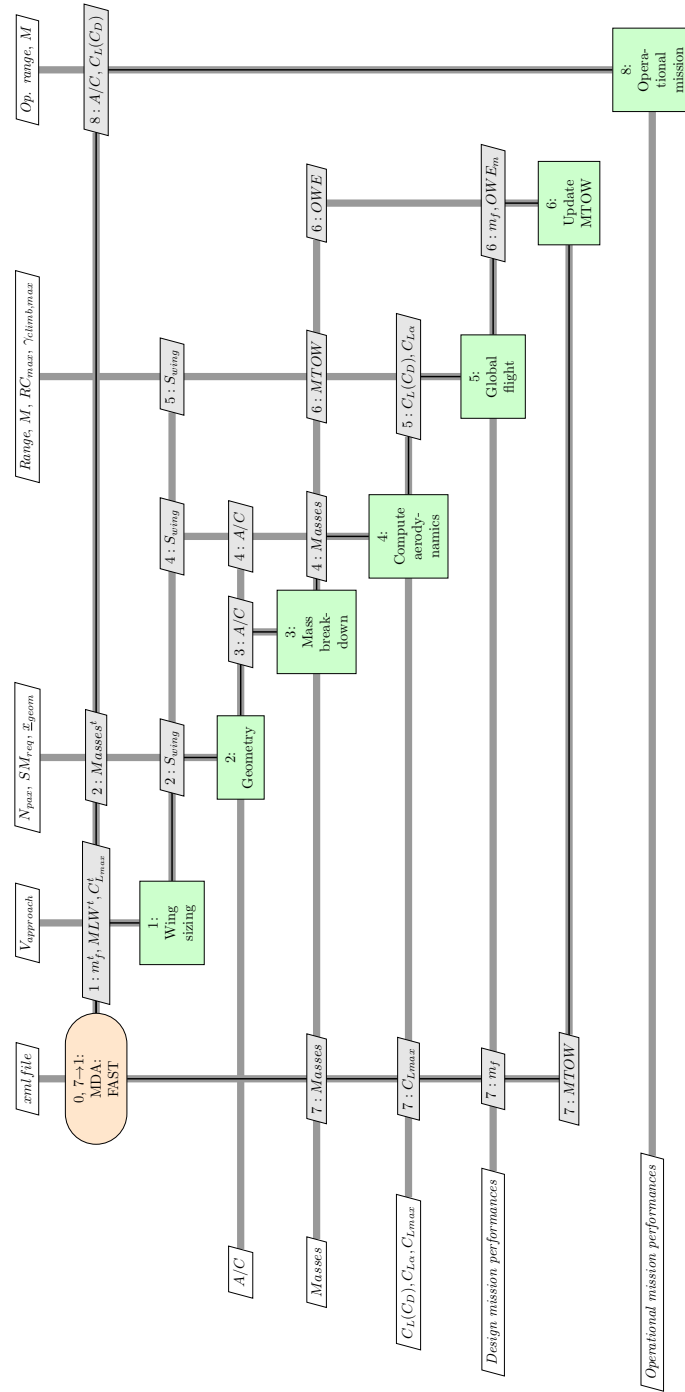


Figure 2.1: Diagram of FAST, using the xDSM standard [LM12].

The second estimation is instead provided after the performance analysis:

$$m_{e5} = m_{TO} - m_f - m_{PL} \tag{2.2}$$

Algorithm 2 FAST algorithm. Numbering is referred to diagram shown in Fig. 2.1.

Require: Initial design parameters (TLAR)

Ensure: Sized aircraft, drag polars, masses, design mission trajectory

0: Initialise the loop with a first estimate of geometry and masses, with the values from the `xml` file [DC12]. At this step engine is initialised too.

repeat

1: The wing area is obtained in order to supply enough lift in landing condition and to store all the fuel needed for the design mission.

2: The aircraft geometry is deduced through a resizing loop, to match the stability requirements.

3: Using the data coming from analysis 2, the masses and the center of gravities of each component are computed. Standard is the French norm AR 2001/D [DGA84].

4: Aerodynamic analysis is carried out, to get the polars at low and high speed.

5: Performance calculation: the trajectory is performed through the integration of the flight equations using the Euler time step approach.

6: Update the value of MTOW, with the data coming from analyses 3 and 5.

7: Check the convergence: if the tolerance is below the needed threshold, return the sized aircraft, otherwise proceed to next iteration.

until 7 → 1: MDA has converged

8: Optionally, perform an operational mission, to assess the performance on different missions than the design one.

At convergence, the two values from Eq. (2.1) and Eq. (2.2) must be the same. The convergence criterion is then that the relative difference between the two does not exceed 0.05%:

$$\left| \frac{m_{e3} - m_{e5}}{m_{e3}} \right| \leq 5 \times 10^{-4} \quad (2.3)$$

In case the error is above the value, MTOW is updated adding the difference between m_{e3} and m_{e5} :

$$m_{TO_{i+1}} = m_{TO_i} + (m_{e3} - m_{e5}) \quad (2.4)$$

In next sections more details on the disciplinary analyses are provided. Indeed since they represent the starting point for the development aimed in this research, have a clear understanding of the models and their limit of validity is a key point.

2.2.3.1 Propulsion

In FAST the engine sizing is not included into the iterative process, but the curves representing its performances are provided to the code for the trajectory analysis. There are two engine models that can be used in FAST: the first one is the engine deck used for the CERAS reference aircraft [CER15], meanwhile the second one is the so called “rubber engine” [Rou05], which represents a model for the engine sizing, based on entries as thrust at sea level or BPR.

The CERAS engine is based on the deck used for the CERAS reference aircraft [CER15].

The data are as close as possible to the Airbus A320's engine. In particular, the by-pass ratio BPR is equal to 6 and the thrust at sea level is 117.8 kN. The maps for thrust and fuel flow, as function of altitude and Mach, are provided to the performance module in FAST: according to the actual trajectory point, these parameters are evaluated through an interpolation. The maps are shown in Fig. 2.2. The main limitation of this model is that thrust and fuel flow (then specific fuel consumption SFC too) are already provided, and there is no possibility to change the engine's parameters to obtain new curves. The field of application has been enlarged thanks to the definition of some corrective factors, that can be used to calibrate thrust and SFC; on top, this approach does not give any indication on the geometry data, so the impact on aerodynamics is neglected. For a more detailed assessment a new model, that takes as input a set of engine parameters, must be defined.

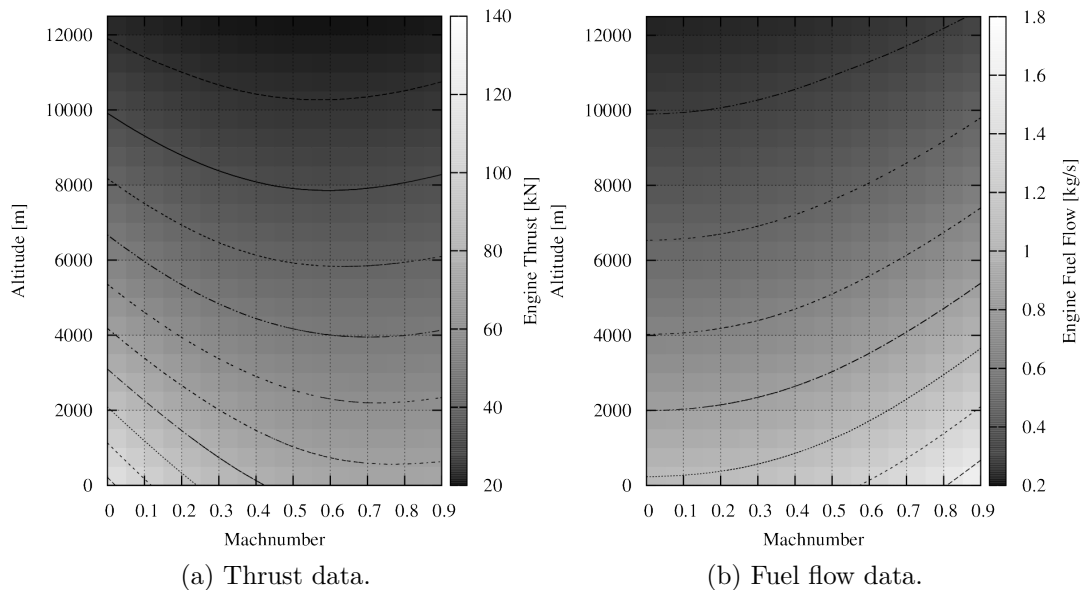


Figure 2.2: CERAS engine reference deck [CER15].

To this end, the “rubber engine” model has been developed by Roux in her Ph.D. thesis [Rou05]: she based her equations on the previous formulations of Mattingly [MHP02], Jane Taylor [Tay79], Torenbeek [Tor86] and ESDU database [ESD82]. This model fixes the limitations of the CERAS deck, providing a set of equations to create the thrust and fuel flow maps, starting from a set of parameters: BPR, thrust at sea level, operating pressure ratio and temperature at the exit of the nozzle. It also provides the dimensions, giving an estimation of the engine wetted area, to consider also the impact on the aerodynamics.

2.2.3.2 Geometry

The geometry module is one of the key analyses to carry out, as it allows the definition of a viable aircraft, that satisfies OAD requirements, including balance and stability.

Each aircraft component requires a set of input parameters from which it is possible to get

geometrical properties and mass estimation. The choice of the entry parameters is not unique, but depends on the formulation; in FAST theoretical and statistical equations are applied, following the handbook provided by Airbus [DC12]. Table 2.1 reports the set of parameters needed for each component; note that the wing needs the wing area, which is separately computed at step 2 of Fig. 2.1. Entries do not cover all the parameters needed: the remaining ones are computed starting from statistical equations that give the dependency with these entries. As example, the thickness-to-chord ratio of the wing is computed considering the cruise Mach number, to take into account that it can not be too large to avoid compressibility at high speed [DC12]; in other formulations this parameter may be considered as input too. The same logic applied for the tails' aspect ratio and sweep. This aspect will become a key point in the development of the MDO problem, as it will be shown later.

Fuselage	Wing	Tails	Engine and nacelle
Number of passengers	Wing area	Taper ratio	Thrust at sea level
Seats' dimensions	Aspect ratio	Thickness-to-chord ratio	Bypass ratio
	Sweep angle		
	Taper ratio		
	Mach number		

Table 2.1: Input parameters to properly size each geometrical component, according to the formulation used in FAST [DC12].

The geometry analysis is an iterative procedure, that needs to converge, and thus it can be expressed with the usual xDSM diagram, as done in Fig. 2.3. Corresponding algorithm is reported in Algorithm 3.

The diagram of Fig. 2.3 shows evidence of two iterative loops. The outer loop is the main one, since it describes the full resizing process and it is driven by the stability requirement: the static margin SM must be included in an allowable range, given by certification. It is to revise that SM is defined as the distance between the center of gravity and the neutral point, normalised with respect to the mean aerodynamic chord: for stability it has to be negative [And12; RL97]. However, FAST uses the opposite convention:

$$SM = \frac{x_n - x_{cg}}{\bar{c}} \quad (2.5)$$

then for stability SM must be positive. Also, it can not be too high as value, otherwise the aircraft will be too stable to be easily controlled; the allowable domain, required by certification [DC12] is that SM is included between 5 and 10%:

$$0.05 \leq SM \leq 0.10 \quad (2.6)$$

For completeness, the expression of the neutral point is reported below:

$$x_n = \frac{\bar{x}_{ac} + \frac{C_{L\alpha HT}}{C_{L\alpha}} \eta_{HT} \frac{S_{HT}}{S_w} \bar{x}_{ac HT} \left(1 - \frac{\partial \epsilon}{\partial \alpha}\right)}{1 + \frac{C_{L\alpha HT}}{C_{L\alpha}} \eta_{HT} \frac{S_{HT}}{S_w} \left(1 - \frac{\partial \epsilon}{\partial \alpha}\right)} \quad (2.7)$$

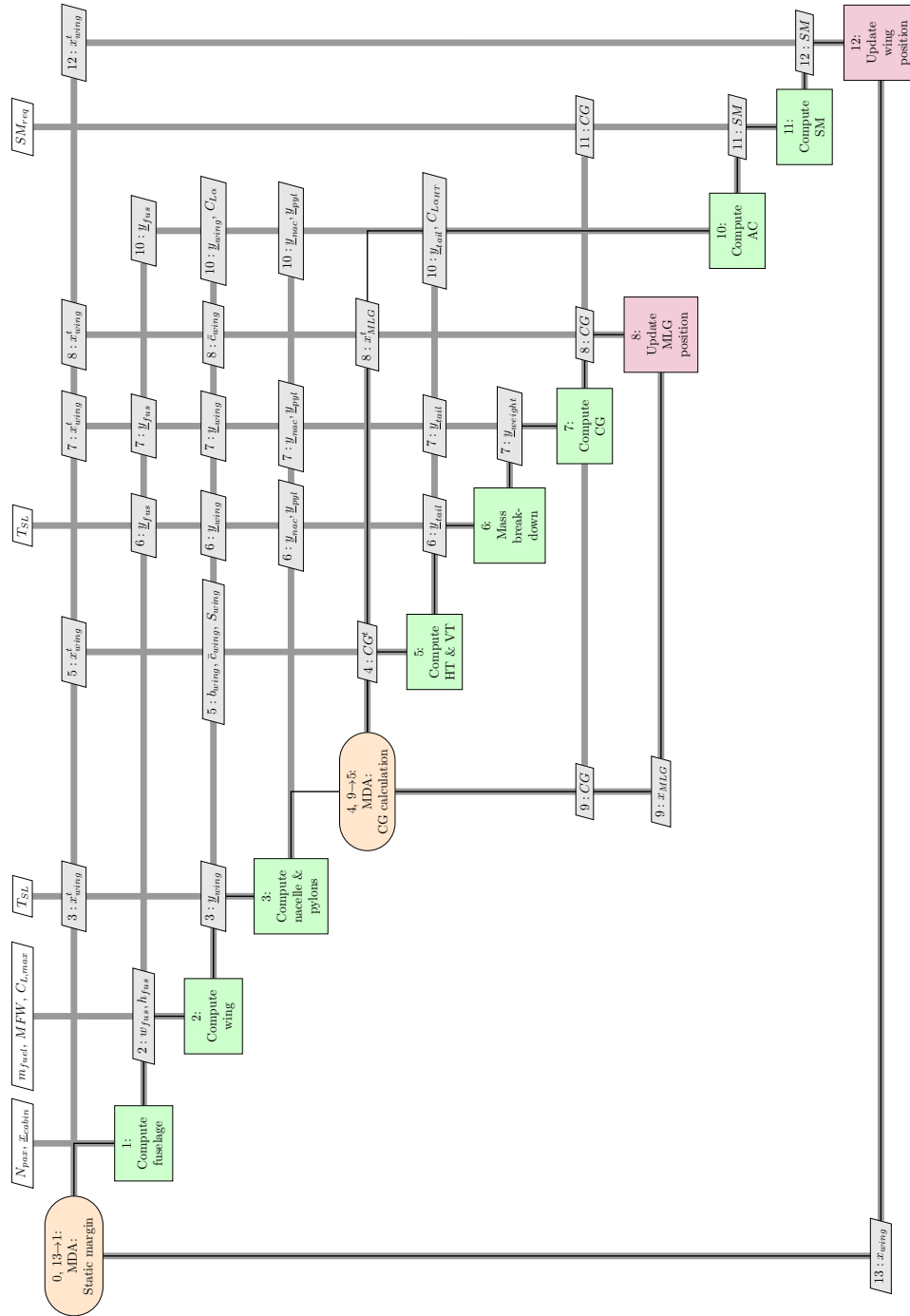


Figure 2.3: xDSM diagram of the geometry analysis coded in FAST [LM12].

In Eq. (2.7) \bar{x}_{ac} and \bar{x}_{acHT} are the normalised aerodynamic centers of wing-body and horizontal tail, placed at 25% of their MAC, η_{HT} the efficiency factor of horizontal tail (typically $\eta_{HT} = 0.9$) and $\frac{\partial \epsilon}{\partial \alpha}$ the downwash of the wing (a typical value is $\frac{\partial \epsilon}{\partial \alpha} = 0.4$).

Algorithm 3 Algorithm for the geometry module of FAST, shown in Fig. 2.3.

Require: Geometry design parameters.

Ensure: Aircraft geometry, that satisfied the required stability constraint.

0: Initialise the geometry resizing loop.

repeat

1: Compute the fuselage geometry, according to the required number of passengers and seat arrangement.

2: Compute the wing geometry, starting from the wing area information, deduced in a previous analysis.

3: Compute nacelles and pylons geometry.

4: Initialise the internal loop, to get the center of gravity.

repeat

5: Compute the empennages, horizontal and vertical tails, according to stability requirements.

6: Estimate the masses of all the components.

7: Estimation of the global center of gravity.

8: Update the main landing gear position, to get the global center of gravity.

until 9 → 5: internal loop has converged.

10: Estimate the aerodynamic center position.

11: Compute the static margin with Eq. (2.5).

12: Change the wing position, to match the static margin requirement.

until 13 → 1 MDA has converged.

From Eq. (2.5) and Eq. (2.7), static margin depends on the wing and the tails geometry, in particular their position aspect ratio and sweep, which affects the slope. Among them, only the wing position is free to vary, since the others represent geometrical entries, and it is then changed until condition expressed by the inequality (2.6) is met. Then it proceeds to next iteration.

The internal loop involves mainly the empennages and the landing gear. At step 4 it initialises the values of horizontal and vertical tails, starting from volume coefficient estimation [And12]. Then it iteratively resizes the tails to ensure that the horizontal tail provides enough lift to balance the aircraft at the maximum center of gravity forward position (in the most penalising conditions) and to respect condition given by Eq. (2.6), and the vertical tail provides enough sideforce for lateral trim in crosswinds corresponding to the 20% of takeoff speed, which is equivalent to holding with 11.5 deg at takeoff [Ray18]. These rules come from the work of Raymer [Ray18] and Kroo [Kro01]. At this point, the geometry module proceeds to the center of gravity estimation: in case it is out of the required range of variation, it updates the main landing gear position to fix it, to proceed at the next iteration, otherwise it proceeds with the SM estimation. The iterative loops give as output a viable geometry, starting from which the aerodynamics and the performances can be evaluated.

Finally, even if the wing area is computed outside this procedure, it is useful to spend some words on how it is calculated. Its estimation is done at step 2 of Fig. 2.1, according to two requirements approach speed and fuel capacity. The first condition ensures that the

wing area provides enough lift in approach, with flap and slat fully retracted, and can be represented by the lift equation as follow:

$$m_L g = \frac{1}{2} \rho V_s^2 S_{w_{app}} C_{L_{max}} \quad (2.8)$$

where m_L is the maximum landing weight, V_s the stall speed (23% lower than the approach speed V_{app}), $C_{L_{max}}$ the maximum lift coefficient with flap and slat in landing configuration, and $S_{w_{app}}$ the minimum wing area needed to satisfy the equation.

The second condition ensures that the wing is large enough to accommodate the fuel needed to complete the design mission. An estimation of wing capacity is provided by Raymer [Ray18]:

$$m_{f_{max}} = 224 S_{w_f}^{1.5} AR^{-0.4} \left[0.6 \left(\frac{t}{c} \right)_{root} + 0.4 \left(\frac{t}{c} \right)_{tip} \right] + 1570 \quad (2.9)$$

where AR is the aspect ratio, $\frac{t}{c}$ is the thickness-to-chord ratio, evaluated at the wing root and tip, and S_{w_f} the wing area. Imposing $m_{f_{max}} = m_f$ yields to an estimation of the minimum wing area needed for the fuel storage.

The final wing area must respect both Eq. (2.8) and Eq. (2.9). Thus the maximum value between the two estimations is chosen. This procedure ensures a feasible value of wing area, however it is to note that it limits the exploration of the wing area to only two values, whereas the conditions described by Eq. (2.8) and Eq. (2.9) may be written as inequalities, enlarging the values to explore that satisfy the conditions. As a conclusion, the estimated value may not be optimal, because of the limited design space, and FAST does not explore any other values but $S_{w_{app}}$ and S_{w_f} .

2.2.3.3 Aerodynamics

The aerodynamic module is devoted to the polar estimation $C_D = f(C_L)$, both for low and high speed. This analysis too is based on statistical and engineering equations [DC12], enabling extremely fast computations. The drag coefficient is composed of three terms: friction drag C_{D_0} , induced drag C_{D_i} and compressibility drag C_{D_c} .

Friction drag is the term due to the form, generally it does not depend by the flight condition and then is considered constant with the lift coefficient. The formulation used in FAST depends solely on the wetted areas. First the friction coefficient is computed, with the Prandtl-Schlichting correlation [Mon53]:

$$c_f = \frac{0.455}{(1 + 0.126 M^2) (\log_{10} Re)^{2.58}} \quad (2.10)$$

where M is the actual Mach number, Re the Reynolds number. Then, the C_{D_0} is computed

as the sum of friction coefficients for each component:

$$C_{D_0} = \sum_i c_{f_i} k_{f_i} \frac{S_{i_{wet}}}{S_w} \quad (2.11)$$

where c_{f_i} is the local friction coefficient, $S_{i_{wet}}$ the wetted surface of i -th component, and k_{f_i} a corrective factor, to consider secondary aspects, such as the sweep effect. Note that the Reynolds number used in Eq. (2.10) is not constant, but varies for each component, since the reference length is different. The value of C_{D_0} is corrected, to include a parasite drag effect, with a corrective factor depending on the total wetted area.

The second term of the induced drag depends on the square lift coefficient, in agreement with Prandtl theory [de 15b; And11], and it represents the greater contribution in the drag breakdown. It is computed as

$$C_{D_i} = \frac{C_L^2}{\pi (AR)_w e} \quad (2.12)$$

where e is the Oswald factor, depending solely on the wing geometry and the Mach number, estimated using the method proposed by Niță and Scholz [NS12].

The induced drag is associated to the energy dissipated by the vortex at the wing trailing edge. These vortex generate a downwash, which must be taken into account in the drag calculation, and as well as in the needed deflection to trim the aircraft. This last effect generates a new source of drag, associated to trim, that is added to the induced drag and, at first instance, is computed as

$$C_{D_{trim}} = 5.89 \times 10^{-4} C_L \quad (2.13)$$

Finally, the last term C_{D_c} is associated to the presence of compressibility phenomena and shock wave on the wing. At low speed, it can be neglected, but in the transonic regime it is crucial to have a proper estimation of this term. Unfortunately, it is not an easy task to find a simple suited model, as it depends on multiple factors: Mach number, lift coefficient, wing geometry, but also flow properties. A good correlation is found in the Airbus notes, in which C_{D_c} depends solely on the Mach number and C_L , as shown in Fig. 2.4, for a wing sweep of 28 deg and a thickness-to-chord ratio of 12%. It must be noted that the tendencies vary from aircraft to aircraft; however, in the zone of interest for the flight of subsonic turbofan aircraft ($M = 0.7 - 0.8$), the term is small and near zero, and thus the approximation works fine, despite the limitations.

With all the terms are identified, the drag polar is computed as

$$C_D = k_{C_D} \left(k_{C_{D_0}} C_{D_0} + k_{C_{D_i}} C_{D_i} + k_{C_{D_c}} C_{D_c} \right) \quad (2.14)$$

The k -terms are added to consider some improvements coming from the technologies, *i.e.* the winglet design impact the induced drag, and this can be modeled using $k_{C_{D_i}}$.

Alternatively to these equations, if desired, it is possible to use OpenVSP [Ope18b] for the calculations. This code relies upon the VLM method, which is limited to incompressible

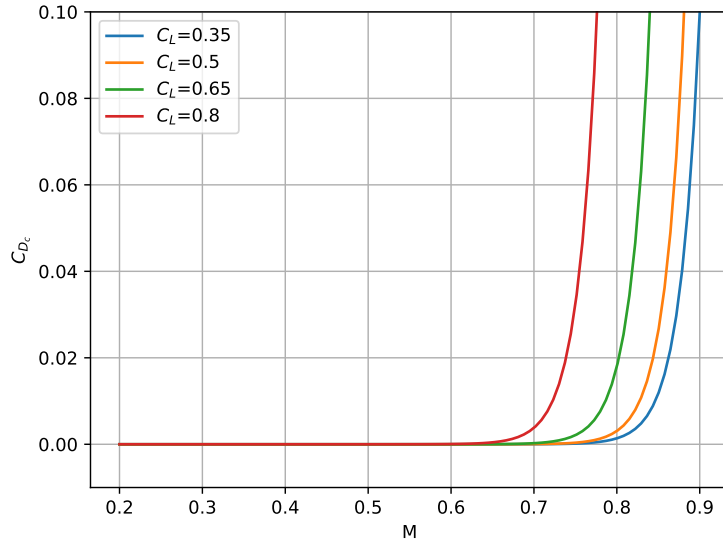


Figure 2.4: Compressibility drag coefficient as function of Mach and lift coefficient. Curves are obtained considering $\Lambda_{25_w}=28$ deg and $(\frac{t}{c})_w=0.12$.

flow, thus it is used only for low speed calculation, to get the slope C_{L_α} and the lift coefficient at zero angle of attack C_{L_0} . In real, VLM is limited to inviscid flow too, but OpenVSP offers a correction based on wetted areas. FAST interfaces also with Xfoil [MIT18b] for the airfoil aerodynamics, mainly used in the estimation of the maximum C_L at low speed. To account for the three-dimensionality introduced by the sweep, the cosine law is considered [Av59; de 15b; And11]:

$$C_{L_{\max}} = k_w C_{l_{\max}} \cos \Lambda_{25_w} \quad (2.15)$$

2.2.3.4 Mass estimation

The mass breakdown used in FAST follows the French standard 2001/B [DGA84], which is reported in Table 2.2 for sake of clarity. The OWE is divided into five parts: airframe, propulsion, systems, operational items and crew. Adding payload and fuel, the MTOW is obtained.

For parts B, C, D, and E statistical equations, reliable for standard TAW configurations, are used. The airframe part is the most complicated, since in general the components need to satisfy different critical conditions, according to certification. As example, the wing is sized to carry out the aerodynamic load, but also to limit the torsion and the bending moment and avoid aeroelasticity issues; fuselage instead needs to carry on the pressurization load, and pass the stress analyses [Meg12]. Generally, for these parts, FEM or even experimental tests are used; thanks to the experience gained throughout the years, surrogate models have been developed: they are accurate as far as the configuration does not change from the TAW.

A	Airframe
A1	Wing
A2	Fuselage
A3	Horizontal and Vertical tail
A4	Flight controls
A5	Landing gear
A6	Pylons
A7	Paint
B	Propulsion
B1	Engines
B2	Fuel and oil systems
B3	Unusable oil and fuel
C	Systems and fixed installations
C1	Power systems (APU, electrical and hydraulic system)
C2	Life support systems (Pressurization, de-icing, seats, ...)
C3	Instrument and navigation
C4	Transmissions
C5	Fixed operational systems (radar, cargo bay hold mechanization)
C6	Flight kit
D	Operational items
D1	Cargo bay equipment
D2	Passenger seats
D3	Catering equipment
D4	Passenger safety equipment
D5	Cabin toilet equipment
E	Crew
F	Fuel
G	Payload

Table 2.2: Mass breakdown standard, according to the French norm 2001/B [DGA84] and implemented in FAST.

These models, collected in the Airbus note [DC12], are implemented in FAST.

To consider the impact of different technologies, notoriously the use of new materials like composite or advanced aluminium alloy, the same technique based on the corrective factors k is used: each element listed in Table 2.2 has its own k -factor, to model a reduction or increase in mass (in percentage), as proposed by Kirby [Kir02].

2.2.3.5 Performance

The performance analysis is based on the point mass approach: the aircraft is represented as a mass point, and the mission over the time is computed through a time step integration. For each time step, the code carries out the following analyses:

1. First, the actual atmospheric data, starting from the actual altitude, are computed using the ISO standard atmosphere.
2. Then, using the lift equation in balanced flight (load factor $n = 1$) FAST computes the actual value of C_L :

$$C_L = \frac{mg}{\frac{1}{2}\rho V^2 S_w}. \quad (2.16)$$

The drag coefficient C_D is obtained interpolating the polar data with the actual value of C_L .

3. As third step, performance analysis computes the actual propulsive data. In case of balanced longitudinal flight (that is, during the cruise leg), the thrust required is already known imposing that the aircraft has no climb angle:

$$\begin{cases} L = mg \\ D = T \end{cases} \quad (2.17)$$

In case of non balanced flight (that is, when the aircraft is climbing or descending), the thrust is obtained interpolating the engine deck on a given thrust rate, and the climb angle is computed solving the non balanced longitudinal flight equations:

$$\begin{cases} L \cos \gamma = mg \\ D = T + L \sin \gamma \end{cases} \quad (2.18)$$

In both cases, the SFC is calculated, to consider the mass variation. It is to highlight that the set of Eq. (2.18) assumes steady, non-accelerating climb, and they are then a simplified version. However, several authors suggest their use for the mechanics of flight [And12; RL97; Phi10], as the vertical acceleration can be neglected.

4. Finally, FAST updates the state vector recomputing the new value of velocity and mass

$$m_{i+1} = m_i - T(\text{SFC})\Delta t \quad (2.19)$$

and proceeds to next iteration, using the new state vector as initial point of the following time step.

This process can be represented using an xDSM diagram, as shown in Fig. 2.5.

This routine allows to get a detailed trajectory. The mission is made up by takeoff, initial climb up to 1500 ft, climb to reach the cruise altitude, cruise, descent, an alternate flight plus holding phase to consider reserve calculation, and finally landing. The cruise altitude is found imposing that the initial point corresponds to the maximum lift-to-drag ratio: in practice this is obtained introducing the condition that the climb phase ends up when the aircraft reaches the design Mach and $C_L = C_{L_{opt}}$, where $C_{L_{opt}}$ indicates the lift coefficient at maximum LoD. At the top climb a check is also performed, to verify that the reserve of vertical speed is above 300 ftmin^{-1} , as demanded by operational requirements [Ros05a; EAS12]. In case the condition is not met, the code iterates the value of cruise altitude until

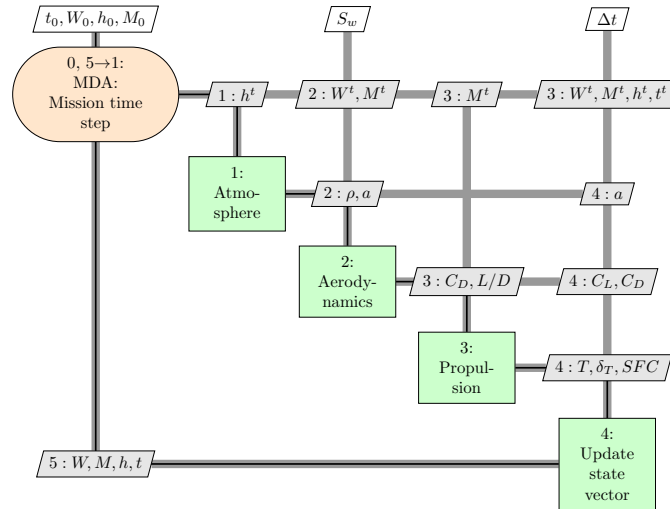


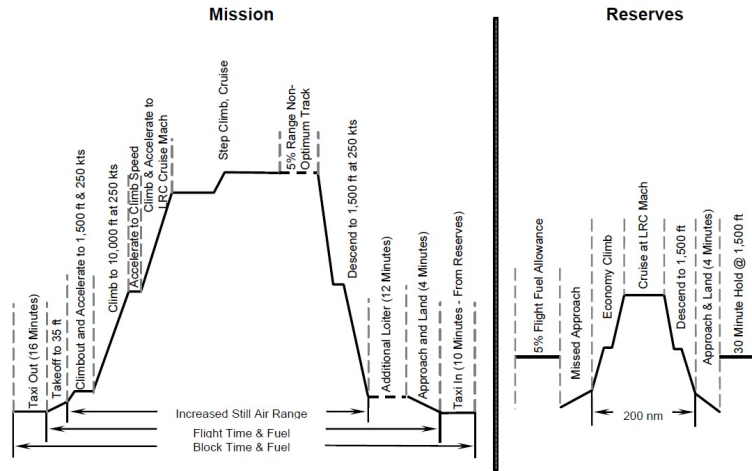
Figure 2.5: xDSM diagram for the time step performance analysis.

the criterion is satisfied, it may happen that to satisfy this criterion the cruise point does not correspond to the one of maximum LoD. The condition represents the only exception to the assumption of a cruise at maximum LoD.

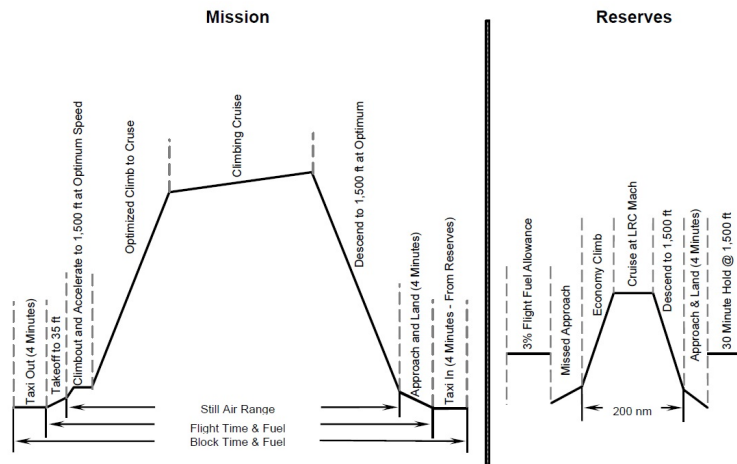
There are two modality for the cruise phase: a conventional step climb and a cruise climb approach. They are shown in Fig. 2.6.

The step climb approach recalls the real aircraft trajectory, for which it is mandatory to fly on predefined flight level according to the air traffic management rules [Eur10]. The step climb is done only if it advantageous for fuel saving, otherwise the aircraft continues on the same level. However, according to NASA perspectives [BD11], the cruise climb option will replace the step climb, since it saves fuel having the aircraft always flying at its maximum lift-to-drag ratio point. This new mission is also included as one of the most innovative aspects in the new air traffic management rules for a more sustainable aviation [BD11]. From a coding point to view, the cruise climb approach is less time consuming than the step cruise, since at each iteration the code does not need to check if it is advantageous to perform a climb of 2000 ft.

When in the cruise leg, the descent function is called at each time step, to know the total distance travelled: in case this value is below the range, it proceeds to a new time step. This algorithm is not efficient, as the descent function is called many times (about 1000). This point is identified as an area of improvement for FAST. The procedure is also shown in Fig. 2.7 and described in Algorithm 4, to better highlight the point. For clarity, only the two iterative loops, to find the cruise altitude and to cover the range, are shown; a complete diagram must include ground operation before the climb and reserve calculation after the descent.



(a) Step climb mission.



(b) Cruise climb mission.

Figure 2.6: Different mission profiles [BD11].

2.2.3.6 CCM – Certification Constraint Module

The Certification Constraints Module, abbreviated as CCM by now, is the module developed by Schmollgruber during his Ph.D. [Sch+18; Sch18]. The scope of the CCM is to check if certification specifications are respected: indeed, it is not sufficient that the aircraft is viable, but it must comply with the EASA/FAA rules.

The module works outside the sizing loop: it limits to control if the aircraft complies with certifications, but in case one of the rules is not satisfied, it does not proceed by itself to any correction. It is up to the user to go back manually and change the design parameter to get the certifications satisfied. However, it may be integrated within an optimisation loop, where the conditions are design constraints, and the algorithm may find the optimum design that satisfies all the rules above. This procedure has been set by Schmollgruber, who used Scipy

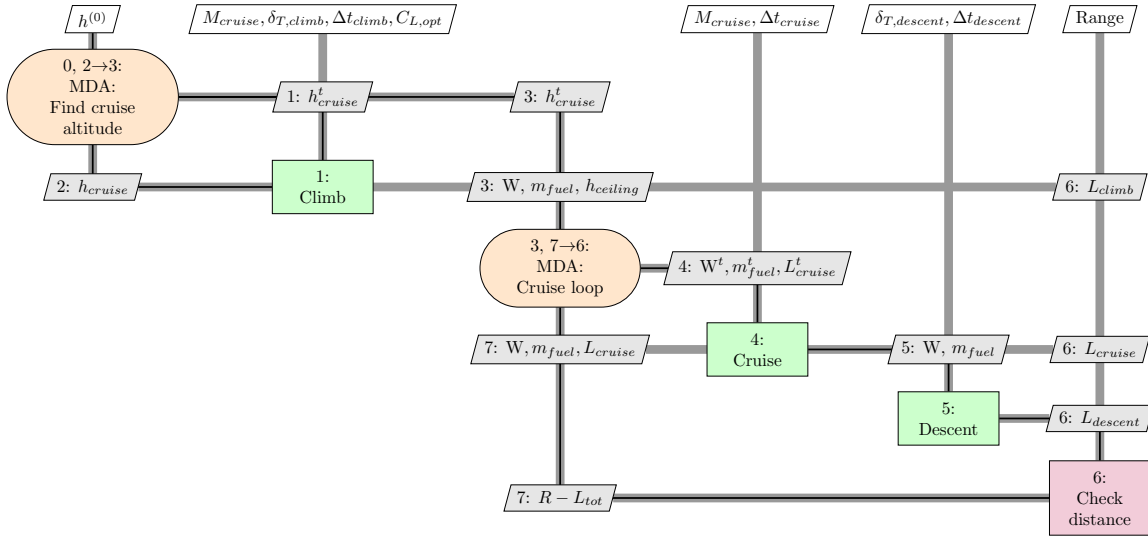


Figure 2.7: xDSM diagram climb and cruise phase performance, to highlight the iterative procedure used in FAST.

Algorithm 4 Algorithm for climb and cruise phase performance, with reference to xDSM diagram shown in Fig. 2.7.

Require: MTOW and polar.

Ensure: Detailed trajectory calculation.

0: Initialise the climb loop.

repeat

1: Compute the climb and check if the final altitude corresponds to the maximum lift-to-drag ratio.

2: If the final climb altitude does not correspond to that of maximum lift-to-drag ratio, compute a new value, otherwise proceed to next iteration.

until 2 → 1: initial cruise altitude is found.

repeat

3: Initialise the state vector for the cruise phase.

4: Perform a time step of cruise leg.

5: Compute the descent leg.

6: Compute the difference between the required range and the total distance travelled.

7: Check if the difference of step 6 is equal to zero: if not, proceed to a new time step.

until 7 → 1 total required range is covered.

libraries to carry out an optimisation based on certifications [Sch18].

The CCM module relies upon a `xml` file, which contains the prescribed conditions to check, using the meta-model GAMME as for the I/O file [BHK13]. The document considered is the CS-25 [EAS17], which is related to large passenger aircraft and prescribe the conditions to be respected en-route and during takeoff and landing (the most stringent segments), with all engines operative and in case of failure. In addition, despite it is not a certification, the

CAT.POL document [EAS12] is also taken into account, since it prescribes the requirements an aircraft must met during its operations (specifically in cruise). For each case, the CCM solves the flight equations using the Python function `fsolve`. The details of rules are listed below in relation with a single-aisle twin-engine aircraft (A320 type) which is the reference case for FAST; for shortness the acronym AEO is used to indicate the condition of all engine operative, and OEI to indicate the one engine inoperative condition.

- **CAT.POL.A.410(a)**. This paragraph of the CATPOL document [EAS12] prescribes that, in en-route condition with all the engines operative, at the top of climb (1) and top of descent (2) the aircraft must preserve a reserve of vertical speed not below than 300 ft/min.
- **CS-25.119(a)**. This rule, from CS-25 specifications for large passenger aircraft [EAS17], requires that in landing condition with AEO, the steady gradient flight must not be less than 3.2%.
- **CS-25.121(a)**. This rule requires that, during takeoff with landing gear extracted and OEI condition, the steady gradient flight must be positive.
- **CS-25.121(b)**. This rule requires that, during takeoff and OEI condition, at the point of flight path when the landing gears are fully retracted (400 ft), the steady gradient flight must not be less than 2.4%.
- **CS-25.121(c)**. This rule requires that, in en-route configuration at the end of takeoff and in OEI condition, the steady gradient flight must not be less than 1.2%.
- **CS-25.121(d)**. This rule requires that, in approach configuration with AEO condition, the steady gradient flight must not be less than 2.1%.

Table 2.3 sums up the rules, together with the flight path specified and the minimum value of parameters required. The notation V_z indicates the vertical speed, meanwhile $\gamma\%$ the steady gradient flight in percentace.

Reference document	Phase	Condition	Parameter	Min. value
CAT.POL.A.410(a)-1	Top of climb	AEO	V_z	300 ft/min
CAT.POL.A.410(a)-2	Top of descent	AEO	V_z	300 ft/min
CS-25.119(a)	Landing	AEO	$\gamma\%$	3.2 %
CS-25.121(a)	Takeoff	OEI	$\gamma\%$	0 %
CS-25.121(b)	400 ft	OEI	$\gamma\%$	2.4 %
CS-25.121(c)	End of takeoff	OEI	$\gamma\%$	1.2 %
CS-25.121(d)	Approach	AEO	$\gamma\%$	2.1 %

Table 2.3: CATPOL [EAS12] and CS-25 [EAS17] rules explanation, considered in the CCM module of FAST. V_z represents vertical speed, meanwhile $\gamma\%$ the gradient flight.

2.2.4 Test case: Airbus A320

FAST has been developed for designing large passenger aircraft, using turbofan as engine. The validation case, presented by Schmollgruber et al. [Sch+17a], is the Airbus A320 [Air18], with the top level requirements reported in Table 2.4. The geometrical inputs required are instead reported in Table 2.5, following the list presented in Table 2.1. Finally, Table 2.6 reports the thrust rate for each mission segment. Actually, even if the Airbus A320 specification manual

Range	2750	nmi
Number of passengers	150	
Approach speed	132	kn
Design payload	13608	kg

Table 2.4: Top level requirements for the A320 CERAS validation case used in FAST.

AR_w	9.5	
Λ_{25_w}	25	deg
λ_w	0.38	
λ_{HT}	0.4	
$\left(\frac{t}{c}\right)$	0.1	
λ_{VT}	0.3	
$\left(\frac{t}{c}\right)$	0.13	

Table 2.5: Geometrical inputs for the A320 CERAS validation case.

Segment	δ_T
Taxi	0.3
Takeoff	1.0
Climb	0.93
Cruise	Computed
Descent	0.55
Alternate climb	0.93
Alternate cruise	Computed
Alternate descent	0.55
Hold	Computed
Landing	0.03

Table 2.6: Thrust rate definition for each mission segment for the A320 CERAS validation case.

contains many geometrical information, as well as cargo bay disposition, it does not have any information regarding the mass breakdown, performance and the engine map. Thus, in FAST, the CERAS data are considered for comparison [CER15], since it emulates the Airbus A320 aircraft; engine model is directly taken from the website. All the performances of this reference aircraft are available, and thus are used for the comparison.

The results of FAST, for the A320, are shown in Fig. 2.8: the climb and descent profile are depicted in Fig. 2.8a and Fig. 2.8b, meanwhile the global profile, using both the step cruise and the cruise climb, are shown in Fig. 2.8c and Fig. 2.8d. The drag polar is reported in Fig. 2.8e, while the payload range diagram of Fig. 2.8f ends the set of output available. Note that the mission profile is very detailed and mimics a real aircraft trajectory, according to the air traffic rules [Eur10]. The climb profile is made of three different segments: a first climb at CAS=250 kt up to 10 kft, then acceleration from CAS=250 to CAS=300 kt, and a climb at constant CAS up to cruise altitude, which corresponds to the point $M=0.78$ and $C_L = C_{L_{opt}}$. The descent profile is also made up by three segments, that mirror the climb profile.

Table 2.7 reports the comparison between FAST, using both the step climb and the cruise climb approach, and the reference aircraft: it can be seen that the results are consistent, since the maximum difference is always less than 1%. It must be highlighted that the step cruise and the cruise climb results are similar, but the computational cost of the second approach is reduced, because it does not need to check if it is convenient or not to perform a step of 2000 ft. For this reason, only this approach will be used for the future simulations.

		Step climb	Cruise climb	A320 CERAS
MTOW	[kg]	74168.96	74562.82	74102.34
OWE	[kg]	42200.58	42190.71	42120.22
Wing area	[m ²]	122.74	122.68	122.41
Mission fuel	[kg]	18799.11	18798.85	18678.12

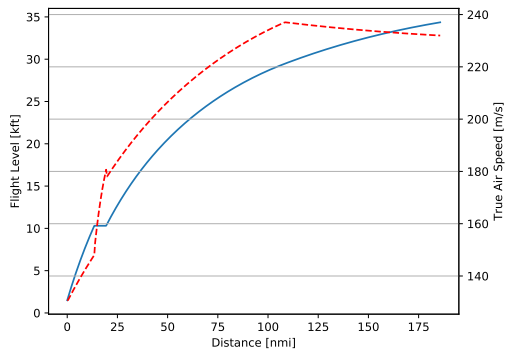
Table 2.7: Comparison between the results obtained in FAST and the A320 CERAS data [Sch+17a].

The CCM results are instead presented in Table 2.8: the aircraft is compliant with both CATPOL and CS-25 specifications, with a safe margin for all the parameters. The margin is taken to consider the case of hot day, with airport at high altitude (for the Airbus A320, La Paz airport is considered, which is 2000 m above the sea level).

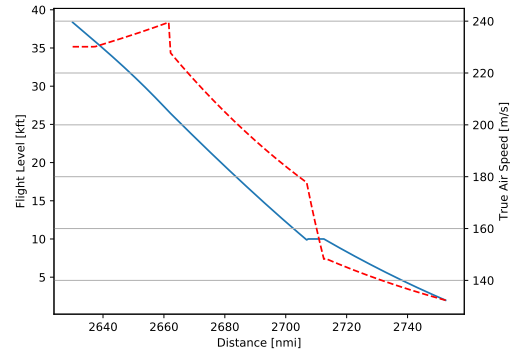
CAT.POL.A.410(a)-1	964.69	ft/min
CAT.POL.A.410(a)-2	1031.82	ft/min
CS-25.119(a)	19.46	%
CS-25.121(a)	1.61	%
CS-25.121(b)	3.43	%
CS-25.121(c)	5.56	%
CS-25.121(d)	7.19	%

Table 2.8: CCM results for the A320 CERAS validation case.

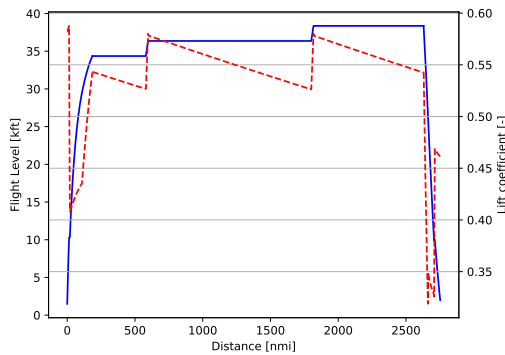
Finally, some remarks on the computational time: the idea at the basis of FAST is to have a reliable code capable to deal with multidisciplinary of aircraft design process and to have a result in a short time. The complete sizing process is done in 15-30 minutes, with the variation being associated with various TLAR and CPU performance level. For the specific case of the reference Airbus A320 aircraft, the code runs for 25 minutes using the step climb



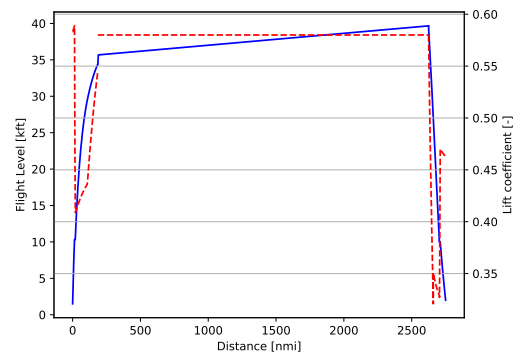
(a) Climb profile.



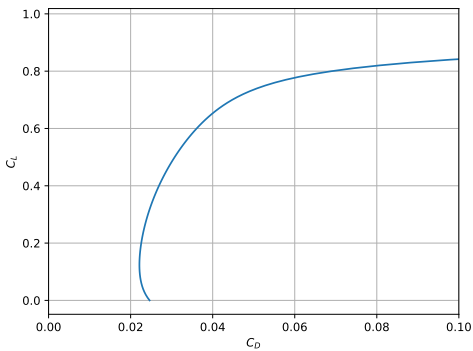
(b) Descent profile.



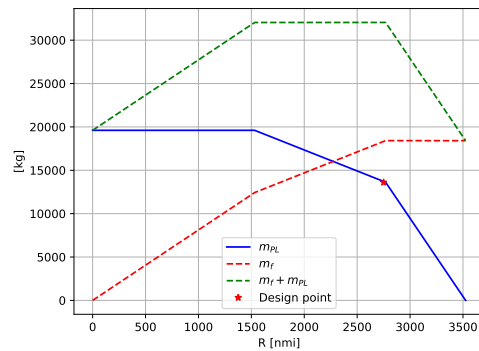
(c) Step cruise profile.



(d) Cruise climb profile.



(e) Drag polar.



(f) Payload-Range diagram.

Figure 2.8: Some of the outputs of FAST, related to the A320 validation test case, with the TLAR reported in Table. 2.4. Continuous line represents the trajectory, meanwhile dashed line is the true air speed or the lift coefficient, according to the flight phase.

approach and 20 minutes using the cruise climb approach. Preliminary tests indicated that the recoding of the cruise segment, as stated in Sec. 2.2.3.5, could lead to a reduction of CPU time of 5 to 10 minutes.

2.3 OpenMDAO – a multidisciplinary optimisation platform

OpenMDAO has been created because of the need of NASA to have its own MDAO framework, in 2012, when v1.0 was released [HG12; Gra+14]. The code has been continuously developed throughout the years; this research considers the version 2.4, released in August 2018. [Ope18a]. OpenMDAO has been coded in Python, to facilitate the scripting, but also because the `Scipyoptimisation` python library already includes several optimisation algorithms, both gradient-free and gradient-based [Oli07; MA01], that can be inherited as class by OpenMDAO. It also provides a class to use the `pyOptSparse` library [PJM12], which extends the gradient-based algorithms choice.

The first feature of OpenMDAO is that it uses distributed memory and high performance computing to speed up the serial computation, as well as it enables efficient parallel execution [Bal+02; HM15]. Although OpenMDAO can use also algorithms not based on derivatives, the major feature of this framework is the possibility to compute total derivatives very efficiently: OpenMDAO, indeed, relies upon the unified theory MAUD developed by Hwang and Martins for the gradient calculation [MH13; HM18]. Users can choose among finite differences method, complex step or analytic derivatives, making the code very flexible. In the first two cases the code automatically computes derivatives, meanwhile in the last one the user needs to define analytic expressions within the process. At first a large effort in the set-up is required, but analytic derivatives speed up the process significantly. Several authors benchmark algorithms that use derivatives against gradient-free algorithms, and all of them show the number of iterations is reduced by several order of magnitude when considering derivatives [ML13; Yu+18; TM10]. Also, as general rule, the required number of iterations for gradient-free methods grow quadratically with the number of design variables, whereas the trend is linear for gradient-based methods, as also remarked in Fig. 2.9, which represents the required number of iterations as function of design variables number for different methods.

The total derivatives compose a non linear system of equations which can be solved by an adjoint or a direct method. The solution of this system gives the path towards the function minimum. The usage of unified theory makes OpenMDAO perfect for large-scale problems, since it conjugates computational efficiency and multidisciplinary design [Hwa15]. Also, as a consequence, the computational cost is kept low even increasing the number of disciplines in coupled high-fidelity problems [MAR05]. This is a key in the design of new technologies, such as BLI, since it enables to establish tradeoff in acceptable time.

Starting from v2.4 the usage of sparse matrix has been implemented, reducing the computational cost to solve the non linear system of derivatives. Sparse matrices also allow to use a direct method, instead of a numerical one, in order to find the solution of the non linear system, making the code stable and easy to use by a user who does not have enough background on numerical methods, which is a non-trivial aspect.

The success of OpenMDAO as a reliable and efficient multidisciplinary optimisation platform is demonstrated by its large users community. Problems concerning the aero-structural optimisation [JHM18b], topology optimisation [JHM18a], on-demand mobility [HN18], small

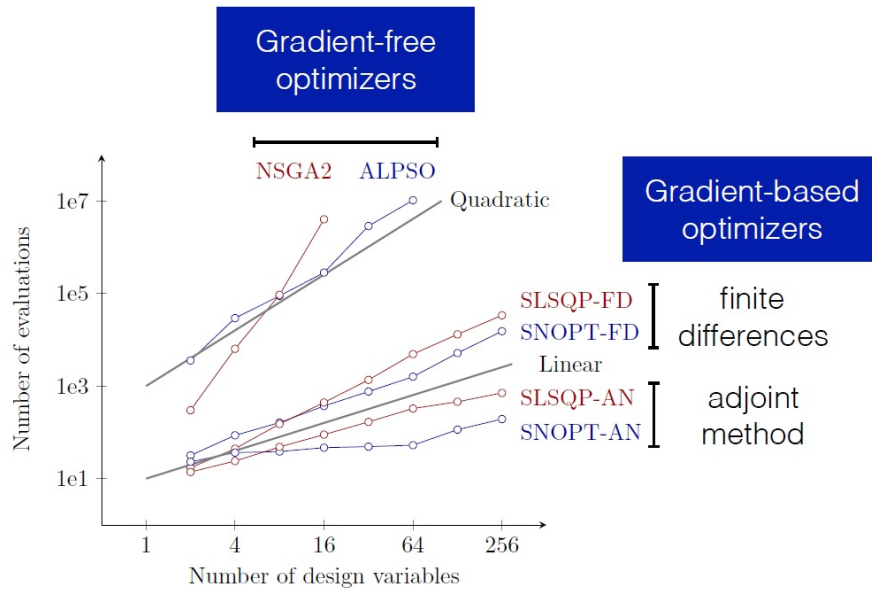


Figure 2.9: Comparison between gradient-free and gradient-based methods on the required number of iterations [Mar14].

satellite design [Hwa+14], trajectory optimisation with cost analysis [Chu+16], wind turbine blade shape optimisation [Bar+16] and boundary layer ingestion optimisation using high fidelity [Gra+18b] are successfully solved with this framework.

In the following paragraphs, a brief description on how to use OpenMDAO is provided. In this manner, the integration of FAST can be better illustrated: more details about its structure, as well as the theory behind the solvers used and their implementation in the framework are given. OpenMDAO uses the object-oriented programming paradigm, which is facilitated by Python scripting, and an object composition design pattern. Just four classes are defined in OpenMDAO: `Component`, `Group`, `Driver`, and `Problem`. They are detailed below.

- **Component** class. Components in OpenMDAO replace the classical definition of “discipline” in a MDO process. They can represent a whole discipline, or a sub-set of it. Components share a common interface that allows them to be integrated to form larger problems: thus, they are the fundamental bricks in OpenMDAO to build the process. There are no specification about the component’s instance: it simply maps a set of inputs to give a desired set of outputs, no matter if the outputs are provided with equations or a call to an external software, potentially written in a different language. The `Component` class can be further divided into `ExplicitComponent` and `ImplicitComponent`: as the name suggests, the first uses explicit formulation in which the outputs are direct function of inputs; on the contrary in the second instance outputs are implicit function of inputs, and they are found through an iterative procedure that drives the function’s residuals (defined by the user) to zero.

- **Group** class. The **Group** instance contains the components, other groups, or a mix of both. The relationship between groups and components forms a hierarchy tree, where a top-level group contains other groups. In turn, these groups contain other groups and so on; the bottom-level contains only components. There are no limit on the hierarchy level that can be defined. **Group** instances are used mainly to package sets of components together, to create better organised namespaces (since all the components are named based on their ancestors on the tree) and to facilitate the use of hierarchical nonlinear and linear solvers. The ensemble of all the groups basically forms the model.
- **Driver** class. The **Driver** instance defines a set of algorithms which iteratively call the model. The algorithms are not only limited to optimisation, but can be also defined to execute other functionalities, *i.e.* a sensitivity analysis or design of experiments. As said previously, **Driver** class already instances the **Scipyoptimisation** and the **pyOptSparse** classes, but a user can code its own class, which can be later instantiated in OpenMDAO. In case of optimisation, design variables are a subset of models' inputs, objective function and eventually constraints are a subset of models' outputs.
- **Problem** class. This class has the function of top-level container, which includes all the objects defined. A **Problem** instance contains all the hierarchical structure, defined by groups and components, and a single driver instance. Aside of serving as a container, **Problem** class provides also the user interface for setup and execution.

The relationship between the four OpenMDAO classes is illustrated in Fig. 2.10. Following the same definition given by Gray et al. [Gra+19], “partial derivative” refers to the derivatives of component outputs with respect to inputs, meanwhile “total derivative” refers to derivatives of model outputs with respect to model inputs.

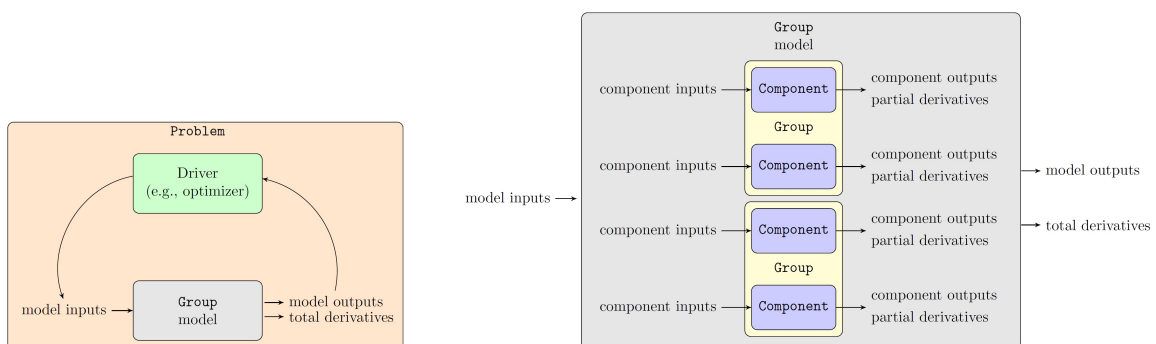


Figure 2.10: Relations between the OpenMDAO four basic classes: **Component**, **Group**, **Driver** and **Problem** [Gra+19].

Following this overview of OpenMDAO, the next step consists in detailing the integration of FAST within this optimisation platform.

2.4 The integrated platform FAST and OpenMDAO

To proceed with the integration of FAST and OpenMDAO, the disciplines must be rewritten in the OpenMDAO language, using components and groups. For clarity, from now on the original version of FAST is referred as “original version” meanwhile the new one within the OpenMDAO platform is referred as “integrated version”. One important difference is that under OpenMDAO, the integrated version carries out aircraft optimisation, starting from the same set of TLAR as the original version. It must be noted that the optimisation can be carried out in other ways than using OpenMDAO, *i.e.* using the gradient-free algorithms available in the SciPy library, or a global algorithm as SEGOMOE, jointly developed by ONERA and ISAE-Supaero [Bar+19]. These solutions are more intuitive and in some way simpler to implement than the complete OpenMDAO process. In this Ph.D., the choice has been to go with the recoding in OpenMDAO because of its various advantages, especially when dealing with derivatives, as seen from the description of previous section and the works that use OpenMDAO [Gra+19]. The use of derivatives has a major interest because the high efficiency of gradient-based methods, remarked also in Fig. 2.9.

For this reason it has been chosen to develop the integrated version of FAST considering derivatives information for aircraft optimisation. This choice led to an important set-up time dedicated in the recoding of FAST under the OpenMDAO language. Because of this fully recoding, it has been decided to move from Python 2.7 to Python 3.7, which is a more recent and stable Python version.

The starting point is then to convert all the disciplines as they are into `ExplicitComponent` or `ImplicitComponent`, according to their nature. Derivatives can be then computed with finite difference method. However, this is not the most efficient choice: except for some specific modules that call XFOIL or OpenVSP, FAST is based on mathematical expressions: it is possible to have analytic derivatives, better in terms of required iterations (see again Fig. 2.9). To facilitate their computation, each discipline has then been broken into small components, basically one `Component` instance (explicit or implicit) for each equation; subsequently all these elements have been regrouped again to form groups, each group representing a discipline, in agreement with the schema of Fig. 2.1.

At this stage of the process development, it is necessary to choose the MDO architecture: in fact the outputs definition depends on the architecture. Among all the possibilities, listed in the work of Martins and Lambe [ML13] and reported in Appendix B, it has been decided to proceed with a Multidisciplinary Feasible (MDF) architecture, for several reasons, detailed here after:

- It is the most intuitive to implement in the case of FAST, since the MDA loop is already defined. Also, since a recoding is necessary for the MDA, it allows to reduce the time dedicated to this phase, because it simply requires to add an optimiser at architecture top level;
- The main drawback of the MDF is that it requires a full MDA to be solved at each

iteration [ML13]. However, because of the low CPU time for a sizing loop, this issue is not limiting;

- It requires the minor number of outputs definitions, since consistency constraints and residuals are not required;
- In case of optimisation failure before the convergence, it ensures consistency at each iteration, that is the aircraft is always consistent, albeit it may not be feasible from a constraints point of view. This feature may be useful for designers, because it is still possible to establish a tradeoff with design variables even if the optimisation fails, and facilitate the correction of the starting point.

The xDSM diagram for the integrated version is shown in Fig. 2.11, where the MDA loop within the MDF architecture is clearly identified. The equivalent algorithm is reported in Algorithm 5. In this schema, the engine deck initialization is explicated in this diagram (step 1). The `xml` file is still used as I/O, but since the parameters need to be defined in

Algorithm 5 Integrated version of FAST and OpenMDAO algorithm description, tailored to perform an optimisation of a conventional turbofan aircraft (integrated version).

Require: Initial design parameters (TLAR), design variables initial vector $\underline{x}^{(0)}$

Ensure: Sized aircraft, drag polars, masses, performance, \underline{x}^*

0: Initialise the optimisation loop: initial values are read from the `xml` file.

repeat

1: Initialise the engine deck, using one of the models available, starting from the thrust at sea level.

2: Initialise the MDA (used to get a viable aircraft).

repeat

3: Compute MTOW.

4: Compute the aircraft geometry and perform the mass breakdown, to estimate weight of all components.

5: Compute the static margin, to check later on if the stability constraint is satisfied or not.

6: Aerodynamic calculation, based on the same equations of the original version.

7: Compute the aircraft performance.

8: Check the convergence. The driving parameter is the MTOW, when the error is lower than the tolerance, convergence is reached.

until 8 → 3: MDA has converged

9: Evaluate the objective function. If a gradient based solver is used, this analysis computes also derivatives.

10: Evaluate the design constraints. If a gradient based solver is used, this analysis computes also the derivatives of each constraint.

11: Check if the optimisation has converged. If not, this analysis updates \underline{x} for the next iteration.

until 11 → 1: MDO has converged

OpenMDAO language, the meta-model GAMME is not used anymore. Instead, the dictionary

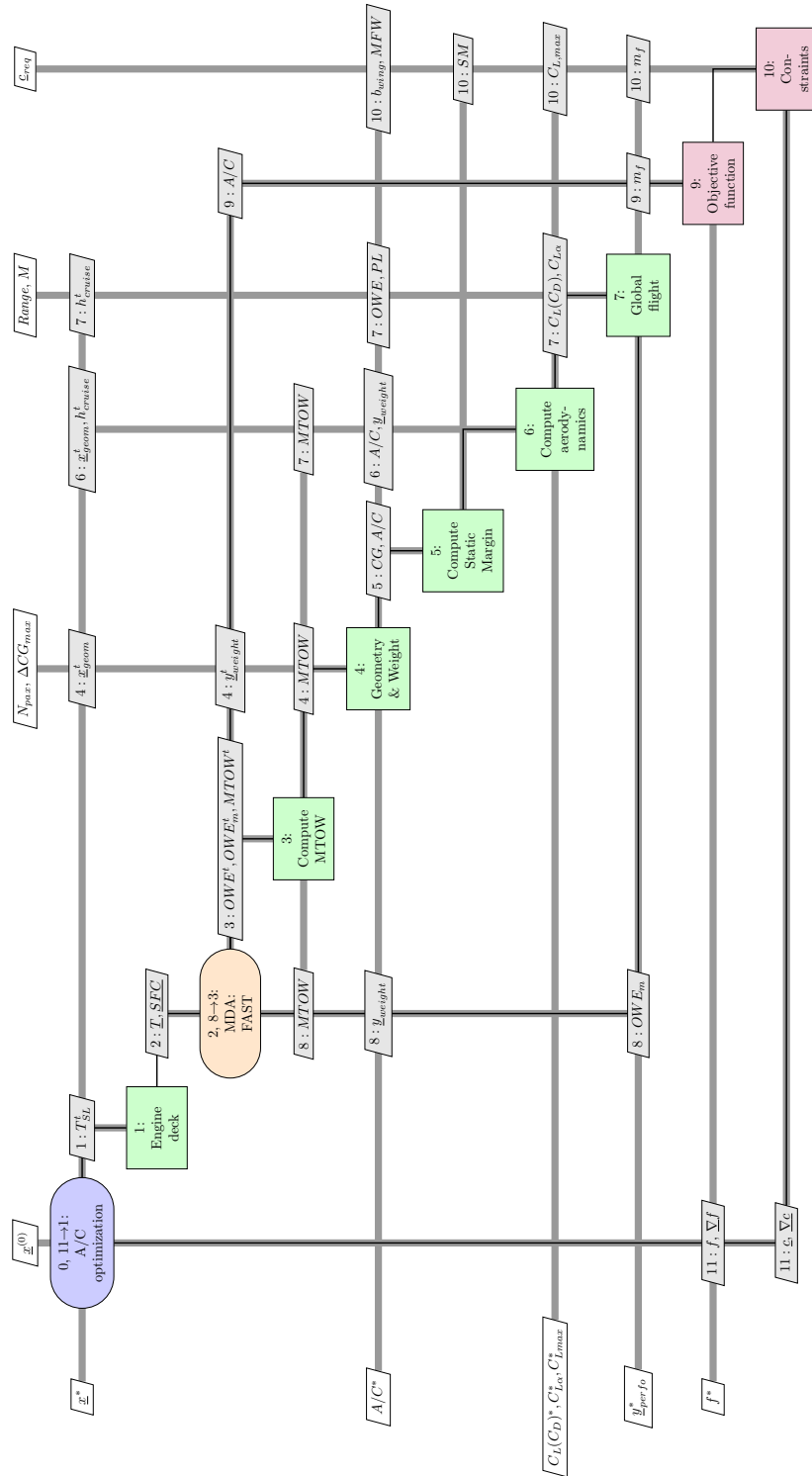


Figure 2.11: xDSM diagram for the integrated version of FAST, obtained by the coupling with OpenMDAO.

is defined in Python, then an explicit component reads the `xml` and saves the values in the OpenMDAO format.

Another consideration is that the optimisation must be “fully opened”, in the sense that any of the chosen design variables must be constrained within a component, but it must be free to vary. The clearest example of this concept is the case of the wing area: in Sec. 2.2.3.2 it has been said that two values of wing area are computed, using Eq. (2.8) and Eq. (2.9), and then the maximum between the two is considered. In this way the design space for the wing area is limited to just two values, one for each condition to satisfy, where in real wing area can assume all the values included in an acceptable domain [Ros05a]. It may be that the optimal value for wing area is not one of the two explored, but another one contained in the design space. At the root of the optimisation logic, instead, there is the idea to define a design space exploration for each design variable. Variables are then free to assume any value contained in its design space, it is up to the optimiser to find the optimal value that satisfies the design constraints.

In the example of the wing area, with this logic Eq. (2.8) and Eq. (2.9) are rewritten as inequalities:

$$\begin{cases} C_{L_{\max}} \geq \frac{m_L g}{\frac{1}{2} \rho V_s^2 S_w} \\ 224 S_w^{1.5} AR^{-0.4} \left[0.6 \left(\frac{t}{c}\right)_{root} + 0.4 \left(\frac{t}{c}\right)_{tip} \right] + 1570 \geq m_f \end{cases} \quad (2.20)$$

Afterwards, the set of Eq. (2.20) are added as design constraints, in order to let the wing area exploits all the possible values and find the optimal one that satisfies the conditions. The same approach applies also to the horizontal and vertical tails surface, as well as the wing position and the cruise altitude. In short, all the design rules that were hard coded in the original FAST, are now opened and treated as design constraints in an optimisation logic.

As a result, the integrated version features less iterative loops than the original one: specifically the geometry module does not exhibit anymore a double loop, and concerning the performance calculations, the process does not need to iterate to find the cruise altitude. This can be also seen in Fig. 2.12, which shows the xDSM diagram for the new geometry module. It is clear that now the wing position is an input that serves for the SM calculation; the optimal value is chosen to minimize the objective function and to respect the SM constraints.

Also, to fully open the problem, it has been decided to remove all the relationships between geometrical variables. As said in Sec. 2.2.3.2, in fact, a lot of geometrical parameters, like the sweep of the tails, are related to the main wing parameters through statistical equations. From a design point of view, there are no reasons to keep these relations. Thus and then all these parameters have been added as design variables, resulting in a larger design space exploration.

Regarding the performance analysis, beside the absence of the iterative loop to find the cruise altitude, the module is now more efficient because each mission segment has become an explicit component. This enables the possibility to recode the mission simulation in order to remove the issue found in the calling of descent function during the cruise leg. The integrated

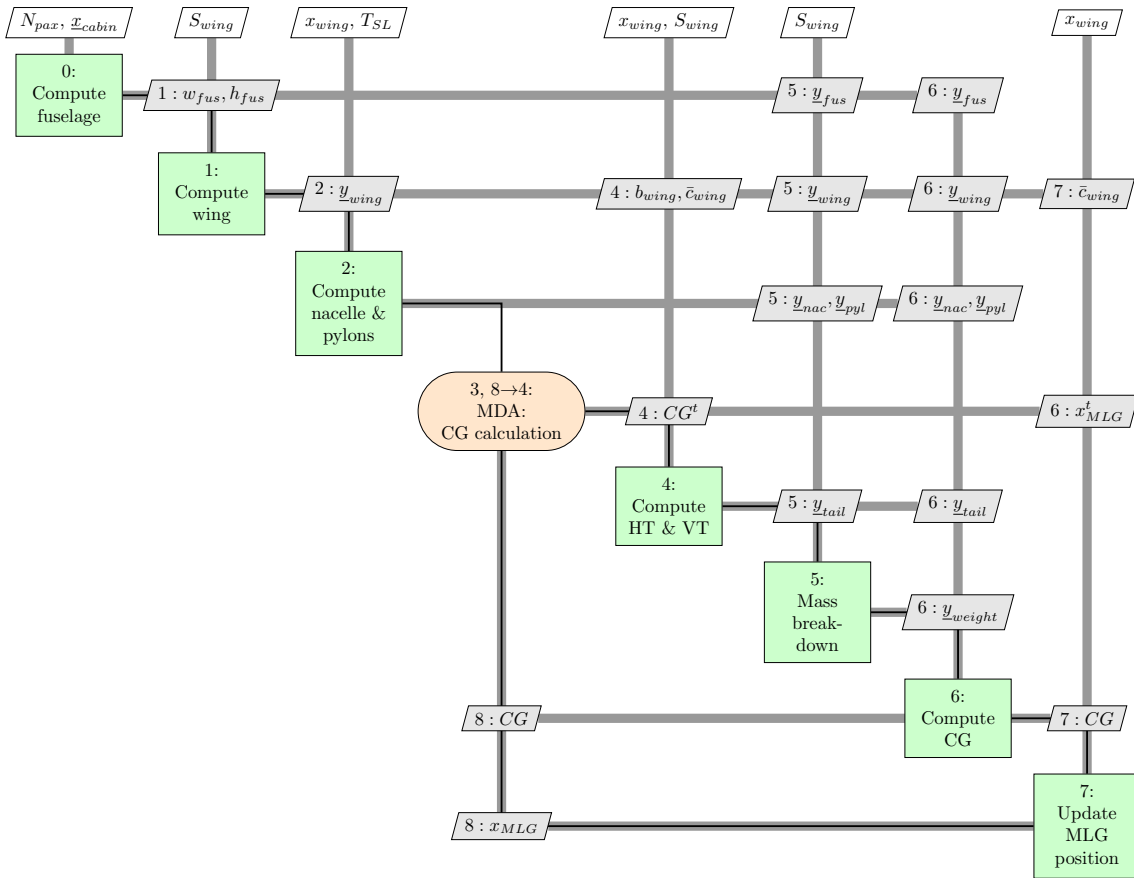


Figure 2.12: xDSM diagram for the geometry module of integrated version FAST and OpenMDAO.

version just requires an initial guess of the distance to travel in cruise. Then, this value is iteratively changed until the total distance travelled for climb, cruise and descent is equals to the required range. With this modification, the descent component is called less than 10 times over a mission. Compared to the hundred of times of original version that accounted for most of the computational cost, this change contributed strongly to the efficiency improvement of the process, with a reduction in time estimated in 5-10 minutes, as remarked at the end of Sec. 2.2.3.5.

To consider certification specifications and operational requirements, the prescribed values reported in Table 2.3 are directly computed at the flight point of interest, since the CCM can not be used directly, having being coded using GAMME. However, the two formulations are totally equivalent. These conditions are then defined as design constraints, in order to let the optimiser find the optimal set of design variables that minimize the objective function, satisfying the CATPOL and CS-25 rules.

Other minor considerations are related to the numerical schemes. In the original version, for each iterative loop, the fixed point method was used. In the integrated version it is possible

to choose between a large variety of methods, available in OpenMDAO (like the Gauss-Seidel or the Krylov methods). Also, robustness is increased: the original version needed to initialise the starting point because otherwise there was the risk to not get any results. OpenMDAO, instead, does not present any issue related to the choice of initial point; convergence is always ensured even with a bad choice of the initial point. Of course, if $\underline{x}^{(0)}$ is well chosen, the convergence is faster as the algorithm requires less iterations.

One of the possible risk of using OpenMDAO, from a user point of view, is the choice of a proper numerical scheme for convergence. In fact, a good choice can accelerate the convergence, but a background on numerical computation is needed [LeV07]. In OpenMDAO it is possible to directly solve the problem using a direct solver: it represents the easiest way since it always ensures the convergence. On the other side it is costly since it requires a full matrix inversion [Gra+19]. However, starting by the v2.4, sparse matrices have been added to help the calculation. This results that a direct solver is efficient as a numerical scheme, which is an added feature for users. Finally, always related to robustness, it is worthy to note that thanks to the absence of convergence problems, the final tolerance in the integrated version is reduced of 3 orders of magnitude, from 10^{-3} to 10^{-6} , resulting in more accurate results.

Despite these advantages, the integrated version presents a relevant drawback: in fact, there are more than 200 components to facilitate analytic gradient computation, compared to the 19 classes of the original one, making the code not user friendly to modifications by a new user, neither easy to understand and to use. Also, due to the way the process is built, it is no more possible to use the code only for sizing, since parameters as wing area, wing position and so on are now design variables subject to design constraints. In OpenMDAO, design constraints are not activated when a simple run is carried out, but they act only in an optimisation simulation.

Also, in some cases it may be of interest to perform multiobjective optimisation, but OpenMDAO is limited to single objective problems when dealing with derivatives; from v2.4 it allows the use of NSGA-II, a genetic algorithm for multiobjective optimisation [Deb+02], but it is gradient-free and thus requires long computational time. However, this issue can be handled with the definition of weighted functions [CZM13; GF15] or the development of specific algorithms [D 12]. In Sec. 3.5.3.4 and Sec. 4.5.4 examples are provided, in relations with the optimisation of the hybrid TAW and the BWB with DEP.

The next paragraph states the optimisation problem, identifying the design variables as well as the constraints, and reports some results on the A320 CERAS validation case and a set of baseline aircraft. These configurations will be use later on to assess performance of conventional configurations.

2.4.1 Optimisation of a turbofan aircraft with FAST under OpenMDAO

2.4.1.1 Problem formulation

This section presents an application of the new framework, built on the integration of FAST within OpenMDAO. At first, the problem must be defined: the main interest, for a civil transport aircraft, is to reduce the fuel consumption m_f . This parameter becomes the objective function; all the geometrical inputs are now design variables. Also the cruise altitude and the thrust at sea level belongs to the design variables vector: the first is added because, in agreement with the original version, it is desired to have the aircraft always starting the cruise at the optimal altitude. The second parameter instead allows to resize the engine according to thrust requirements. Finally, design constraint must be added. They need to ensure the feasibility of the concept, and also to comply with airport specification, top level requirements as well as certification (see Table 2.3). The various constraints are listed below, with details to better explain the OAD problem.

- The wing has to carry all the fuel needed ($\Delta m_f = \text{MFW} - m_f \geq 0$, being MFW the maximum fuel weight) and match the approach condition ($\Delta C_{L_{ldg}} = C_{L_{\max}} - C_{L_{app}} \geq 0$).
- The horizontal tail is sized to obtain rotational performance at takeoff: the longitudinal moment balance has to be larger than zero (zero at limit) for a given maximum center of gravity variation. This condition is defined by imposing that the total moment is lower than zero $\Delta \mathcal{M}_{takeoff} \leq 0$.
- The vertical tail is sized to have lateral stability in cruise: S_{VT} has to ensure good lateral trim properties. This is achieved imposing that the C_{N_β} of the aircraft is equal to a given $C_{N_\beta}^*$, which depends by the Mach number [Ros08]. In mathematical symbols it can be written as $\Delta \mathcal{N}_{cruise} \geq 0$, being \mathcal{N} the yaw moment.
- The static margin SM has to be included between the 5% and 10% of the mean aerodynamic chord, in agreement with Eq. (2.6). This condition determines the wing position x_w , which is placed to have SM in the required range.
- Wing span b_w and takeoff field length TOFL are limited by aerodrome constraints for a medium range aircraft, in agreement with ICAO rules [dW97; ICA17].
- The lift coefficient at the top of climb has to be equal to the value that maximizes the lift to drag ratio, to fly at the best altitude; in other words $\Delta C_{L_{toc}} = C_{L_{toc}} - C_{L_{opt}} = 0$.
- The CATPOL [EAS12] and CS-25 [EAS17] specifications must be satisfied as given in Table 2.3. In total, there are 6 constraints taken from the CCM; to simplify the process, these conditions have been collected in a single vector

$$\underline{c}_{CCM} = [V_{z_{toc}} - 300, V_{z_{tod}} - 300, \gamma_{\%119a} - 3.2, \gamma_{\%121a}, \gamma_{\%121b} - 2.4, \gamma_{\%121c} - 1.2, \gamma_{\%121d} - 2.1]$$

which must be greater than 0.

With these notations, the problem formulation can be finally written: it is reported in Table 2.9, following the MDO community standard (see *i.e.* the work of Jasa et al. [JHM18a]). For each design variable, lower and upper bounds are defined, and this results in prescribing a design space. Limits are chosen recalling data on a large set of commercial single-aisle aircraft [Ros05b]. The size of the problem is 13, with 1 equality and 12 inequalities design constraints.

Category	Name	Size	Lower	Upper	Equals	Units
Objective	m_f	1	–	–	–	kg
Variables	S_w	1	100	150	–	m ²
	x_w	1	15	20	–	m
	AR_w	1	8	12	–	–
	λ_w	1	0.2	0.6	–	–
	Λ_{25_w}	1	20	45	–	deg
	$(\frac{t}{c})_w$	1	0.1	0.15	–	–
	S_{HT}	1	20	60	–	m ²
	AR_{HT}	1	2	5	–	–
	λ_{HT}	1	0.2	0.6	–	–
	$\Lambda_{25_{HT}}$	1	20	45	–	deg
	$(\frac{t}{c})_{HT}$	1	0.1	0.15	–	–
	S_{VT}	1	15	50	–	m ²
	AR_{VT}	1	1	2.5	–	–
	λ_{VT}	1	0.3	1.0	–	–
	$\Lambda_{25_{VT}}$	1	25	55	–	deg
	$(\frac{t}{c})_{VT}$	1	0.13	0.18	–	–
	T_{SL}	1	90	130	–	kN
	h_{toc}	1	30 000	40 000	–	ft
	Total	18				
Constraints	Δm_f	1	0	–	–	kg
	$\Delta C_{L_{app}}$	1	0	–	–	–
	b_w	1	–	36	–	m
	$\mathcal{M}_{takeoff}$	1	–	0	–	N m
	$\Delta \mathcal{N}_{cruise}$	1	0	–	–	N m
	TOFL	1	–	2200	–	m
	$\Delta C_{L_{toc}}$	1	–	–	0	–
	SM	1	0.05	0.10	–	–
	c_{CCM}	5	0	–	–	%
		Total	13			

Table 2.9: Optimisation problem definition for the A320 CERAS case. Variables' limits come from literature review on single aisle type aircraft [Ros05b].

2.4.1.2 Test case: A320 CERAS aircraft

The first test case to be analysed is the optimisation of the A320 CERAS aircraft, already studied with the original version of FAST in Section 2.2.4, associated to TLAR reported in Table 2.4. One issue regarding gradient-based methods is that the optimum point \underline{x}^* can be a local minimum [ML13]. To increase the likelihood of convergence to the global optimum, a multistart check is performed, with 10 different initial vectors $\underline{x}^{(0)}$. If \underline{x}^* does not depend on initial value, then it is assumed as global minimum; otherwise it is reasonable to consider that the global minimum is within the obtained solutions. The 10 starting points are chosen through the creation of a Latin hypercube sampling LHS [Sac+89].

Table 2.10 reports the set-up that is used: the optimisation solver is SNOPT [GMS05], a sequential least squares programming algorithm, that derives from SLSQP algorithm [Kra+88], and included in the `pyOptSparse` library. It has been chosen because it is one of the most efficient gradient based algorithm (see also Fig. 2.9), that supports both inequalities and equalities constraints [GMS05]. Linear and non-linear solver are respectively the Gauss–Seidel and the direct solver. The utilisation of direct solver in place of a numerical method is justified by the consideration done in Sec. 2.3. Starting from OpenMDAO 2.4, the implementation of sparse matrices makes the two methods comparable in terms of performance. Direct solver facilitates the setting, since it does not require the definition of pre-conditioner or similar options, and thus it is considered in this optimisation problem. Tolerance, both for MDA and MDO, is 10^{-6} as default value.

Optimisation solver	SNOPT
Linear solver	Linear Gauss-Seidel
Non linear solver	Direct solver
MDA tolerance	10^{-6}
Optimisation tolerance	10^{-6}

Table 2.10: Set-up for the A320 CERAS optimisation problem, using gradient based method.

Table 2.11 reports a comparison between the quantities of interest for the considered test case, both for baseline and optimised aircraft, meanwhile Table 2.12 reports the design variables values. The geometrical input parameters for the baseline are the same of Table 2.5. Note that most of the variables of Table 2.12 are computed within the original version with statistical equations, meanwhile in the integrated version they are free to vary within their specified range. The mission profile is defined by using values of Table 2.6 for thrust setting.

The first point to note is that the aspect ratio is increased. The optimiser finds that the optimal path goes towards a larger wing, that uses all the span possible (36 m). As a result, the maximum lift-to-drag ratio is increased of about 8%. Also the OWE is slightly higher, because of bigger wing. However, the aerodynamic benefits overcome the penalties in weight, and the fuel consumption is reduced of about 9%. This also results in a reduced MTOW. Another difference lies in the static margin: the original version, indeed, was coded in order that the internal loop stops the first time the static margin stays within the range of

		Baseline	Optimised
MTOW	[t]	74.2	73.7
OWE	[t]	42.2	42.4
Wing area	[m ²]	122.74	123.38
Max. LoD		15.9	17.1
Static margin		0.10	0.05
Fuel mission	[t]	18.7	17.1
CAT.POL.A.410(a)-1	[ft/min]	964.69	913.17
CAT.POL.A.410(a)-2	[ft/min]	1031.82	663.85
CS-25.119(a)	[%]	19.46	17.82
CS-25.121(a)	[%]	1.61	2.01
CS-25.121(b)	[%]	3.43	2.47
CS-25.121(c)	[%]	5.56	5.30
CS-25.121(d)	[%]	7.19	6.78

Table 2.11: Comparison between quantities of interest for the baseline and the optimised aircraft, A320 CERAS test case. Top level requirements are reported in Table 2.4.

		Baseline	Optimised
S_w	[m ²]	122.74	123.38
x_w	[m]	16.61	15.94
AR_w		9.5	10.6
λ_w		0.38	0.33
$\Lambda_{25,w}$	[deg]	25	23.4
$(\frac{t}{c})_w$		0.128	0.117
S_{HT}	[m ²]	33.28	29.32
AR_{HT}		4.33	3.74
λ_{HT}		0.4	0.2
$\Lambda_{25,HT}$	[deg]	28	32.14
$(\frac{t}{c})_{HT}$		0.1	0.1
S_{VT}	[m ²]	29.53	26.23
AR_{VT}		1.74	1.2
λ_{VT}		0.3	0.3
$\Lambda_{25,VT}$	[deg]	35	35
$(\frac{t}{c})_{VT}$		0.1	0.1
T_{SL}	[kN]	117.8	108.2
h_{toc}	[ft]	34000	33248

Table 2.12: Comparison between design variables for the A320 CERAS test case baseline and optimised. Geometric inputs for the baseline are in agreement with Table 2.5.

5-10%. This means that, if the initial wing position is backwarded, the SM achieved is always 0.10. In the integrated version, instead, the optimiser finds the most forwarded position, in order to increase tail level arm and to reduce the tail size. Also, aspect ratio and sweep of the horizontal tail are optimised to move the aerodynamic center in the farthest position as possible, always to advance the wing the most allowable. Note also that, because of the lighter mass,

the cruise altitude is slightly lower (33.2 kft in place of 34).

Table 2.11 reports also the values achieved for the various certification constraints during the sizing loop. It is interesting to note that the thrust of the engine is reduced while complying with the CS-25.121(b). The reduction in thrust contributes to the increase in maximum lift-to-drag ratio too, since the engine wetted area is reduced.

These results show that the problem is well-posed, and that the optimiser goes towards the best solution. Also, it is verified that with the 10 multistart approach, there are no local minima. In order to understand the presence of more minima, the objective function value and the norm of constraints are evaluated. Considering the constraint written in the form $\underline{c} = [g_i(\underline{x}) - a_i] \leq 0$, with $i = 1, \dots, N$, this last quantity is defined as:

$$\|\underline{c}\| = \sum_{i=0}^N |g_i(\underline{x}) - a_i| \quad (2.21)$$

where

$$|g_i(\underline{x}) - a_i| = \begin{cases} 0 & g_i(\underline{x}) \leq a_i + \epsilon \\ g_i(\underline{x}) - a_i & \text{otherwise} \end{cases} \quad (2.22)$$

with ϵ being the tolerance. In other word, if a constraint is violated the norm is computed as the difference with respect to the minimum value, otherwise it is set to zero. As a consequence, a feasible point has the norm of the constraints equals to zero.

Table 2.13 reports the final objective function f^* and the norm of constraints for the 10 runs: all the points are feasible, and no local minima are detected, since the maximum difference among the 10 f^* is less of 0.4%.

	Run									
	1	2	3	4	5	6	7	8	9	10
f^*	17094	17151	17086	17092	17139	17101	17089	17128	17112	17104
$\ \underline{c}\ $	0	0	0	0	0	0	0	0	0	0

Table 2.13: Objective function and norm constraints, defined as in Eq. (2.22), for the 10 optimisation runs carried out for A320 CERAS test case baseline.

The payload-range is also computed with the integrated process: a comparison between the baseline and the optimised aircraft is shown in Fig. 2.13. Only minor differences are detected: because of the reduced MTOW, the first horizontal segment is shorter, but then better aerodynamics and larger fuel capacity make the ferry range of the aircraft higher, even if the difference is of only few nautical miles.

The code took about 35 min to reach the convergence; a total of 36 iterations, with 39 call to objective functions, have been needed to find the solution. The convergence history is shown in Fig. 2.14. The algorithm finds very soon the minimum: indeed after 20 iterations, variations are so small that the objective value can be assumed constant. Note that up to iteration 10 the objective function is smaller than the final value, but these points do not

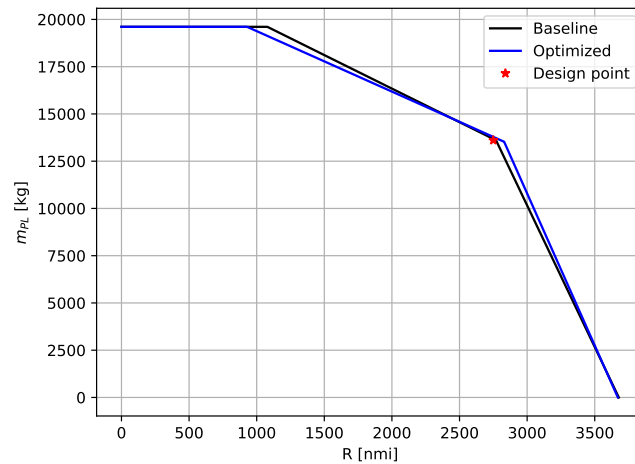


Figure 2.13: Payload-Range diagram, for the A320 CERAS test case, baseline and optimised aircraft.

respect the full set of design constraints and are not feasible.

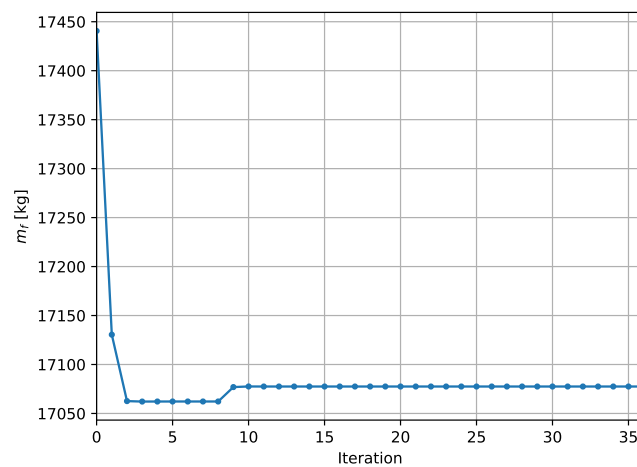


Figure 2.14: Convergence history for optimisation problem of A320 CERAS test case.

2.4.1.3 Test case: A320 CERAS resized for EIS2035

In this section, the integrated code is used to generate the baseline aircraft to be used as comparison for the assessment of unconventional configurations. The technological horizon is 2035, which means that some assumptions have to be made for the mass estimation, the engine model and aerodynamics. The TLAR are practically the same, except for the range,

that not 2750 nmi anymore. Its variation is instead limited from 600 to 1500 nmi. This choice is dictated by the marketing. According to an Airbus analysis, in fact, most of the aircraft fly in this operational range, and thus for the future can be considered to have new resized aircraft on these ranges [Air19]. For clarity, the new TLAR are reported in Table 2.14. The mission profile is still the one of the A320 CERAS reference aircraft, presented in Table 2.6.

Range	600–1500	nmi
Number of passengers	150	
Approach speed	132	kn
Design payload	13608	kg

Table 2.14: Top level requirements for the resized A320, considering EIS2035.

For the technological assumptions, the most reliable document available so far in literature is the IATA report [IAT13a; IAT13b], which states perspectives of available technologies in a 20 year period and their foreseen impact. Regarding the mass estimation, the use of innovative materials, like new alloys or composites, reduces the weight of the aircraft. The estimated impact of new technologies is reported in Table 2.15. These estimations are not the

Component	Impact on mass
Wing	-10%
Fuselage	-5%
Landing gear	-15%
Pylons	-10%
Passenger seats	-60%

Table 2.15: Impact of new technologies on airframe mass estimation according to IATA [IAT13b], considering EIS2035.

only one available in literature, however they seem to be the more reasonable in the chosen technological horizon. The gains at discipline or component level have been implemented through the corrective factors technique, as described in Section 2.2.

For aerodynamics, improvements can be foreseen thanks to the introduction of different new technologies [IAT13b]:

- **New winglet design.** A careful winglet design, with innovative and optimised shape, could lead to a reduction on the induced drag up to 10%.
- **Laminarity drag coating.** The use of a film coating on the wing can reduce the roughness in order to achieve a fully laminar flow and reduce the friction coefficient up to 20%. In practice, it is very sensitive to external condition and it is not said that the flow will be in any condition laminar.
- **Turbulent drag coating.** This technology is complementary to the previous one. A rough coating is added on the wing to induce turbulence: despite the flow results more

viscous, the turbulence avoids separation and its impact on the C_{D_0} is estimated to be of 5%. Also, it is less sensitive to external condition than the laminarity drag coating.

- **Natural laminar flow control.** An accurate wing design can be achieved to naturally have laminar flow over the wing. In practice, this solution is unfeasible for wing with sweep angles higher than 20° .
- **Shock control.** This technology uses a bump over the wing to control the shock wave geometry even in off-design conditions. It may reduce the wave drag coefficient up to 50%.
- **Morphing wing.** The idea at the back of this technology is to use smart materials that change the wing shape, in order to always adapt the geometry to external condition and increase the aerodynamic efficiency. Its reduction on the total drag coefficient is estimated to be of about 3.2%.
- **Hybrid laminarity flow control (HLFC).** In this case, laminarity is achieved through both accurate wing design and active flow control to ingest boundary layer. Its effect on the friction coefficient is about 45-50%. In practice the system introduces relevant penalties in weight, that may counterbalance the aerodynamic benefits. Also, its integration within the airframe is very challenging.

For the 2035 reference aircraft, new winglet design, shock control and morphing wing are considered. The turbulent drag coating is also taken into in spite of the laminarity drag coating, because it is less sensitive to external condition and then more reliable. A natural shock control is unfeasible because of the transonic region, which requires a swept wing. Finally, HLFC is not considered because of limited knowledge at this stage: low maturity and penalties assessment are complex to quantify and it can introduce potential risks to the design.

The final impacts on aerodynamics are reported in Table 2.16. As for the weight, variations have been implemented using corrective factors in Eq. (2.14).

Technology	Parameter	Impact
Winglet design	C_{D_i}	-10%
Turbulent drag coating	C_{D_0}	-5%
Shock control	C_{D_c}	-50%
Morphing wing	C_D	-3.2%

Table 2.16: Impact of new technologies on aerodynamics according to IATA [IAT13b], considering EIS2035.

Some assumptions at engine level have also to be made. It is reasonable to consider that engines in the future will belong to ultra by-pass ratio category, as for the LEAP engine [CFM16]: these engines have a greater BPR, to increase the thrust generated by cold flow and consequently reduce the SFC. Current technology shows a maximum BPR of 11-12.

It is foreseen that this value shall not be exceeded, to keep fan dimensions within the limits, but the engine improvements will be mainly related to a more efficient combustion process. To match 2035 assumptions, a BPR equals to 11 is taken into account, to have the effect of wetted areas, together with a reduction of SFC and an impact on the masses, due to a combined effect of larger engines and new materials.

With these assumptions, it is finally possible to proceed with the sizing of a new set of A320 type aircraft, that matches the EIS2035. Again, the optimised aircraft is compared with some baseline, obtained with the original version using the geometrical input of Table 2.5.

The fuel consumption as a function of the design range is shown in Fig. 2.15, for the baseline and the optimised aircraft. For completeness, key parameters for each configuration are reported in Table 2.17 (baseline) and Table 2.18 (optimised). The optimised configuration shows a fuel saving in the order of 10-15%; also since the slope of the curve of Fig. 2.15 is lower for optimised aircraft, it can be expected that the impact will be greater on longer range. Same considerations done for the optimum point in Section 2.4.1.2 can be retaken here. Concerning certification constraints, for shorter range aircraft it is important to note that the sizing condition for the thrust is not anymore the slope at 400 ft of altitude, corresponding to CS-25.121(b), but more the operational requirement CAT.POL.A.410(a)-2, which corresponds to the vertical speed reserve at the top of descent. This can be explained because the aircraft is more efficient, and therefore consumes less fuel. So the difference in weight between the beginning and the end of the cruise is reduced, and due to the higher mass it needs more thrust at the top of descent to match the needed V_z . On the other hand, condition CS-25.121(b), which was the most stringent condition in the case of Table 2.11, decreases with respect to range, so it can be expected that on longer range, where also the aircraft is lightened more because of the greater distance, it will be again the sizing condition for maximum thrust, in agreement with previous case.

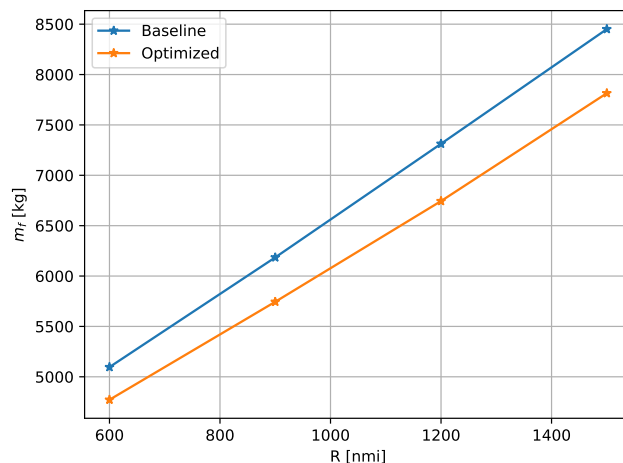


Figure 2.15: Fuel consumption as a function of design range for the A320 baseline and the optimised aircraft, resized to match EIS2035. TLAR are reported in Table 2.14.

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	58.83	60.02	61.24	62.48
OWE	[t]	40.21	40.31	40.4	40.49
Wing area	[m ²]	118.79	118.97	119.16	119.35
Max. LoD		17.44	17.44	17.43	17.43
Fuel mission	[t]	5.09	6.18	7.31	8.45
CAT.POL.A.410(a)-1	[ft/min]	932.18	929.41	928.88	927.4
CAT.POL.A.410(a)-2	[ft/min]	786.4	780.39	774.13	767.66
CS-25.119(a)	[%]	21.98	21.92	21.87	21.81
CS-25.121(a)	[%]	6.01	5.65	5.31	4.97
CS-25.121(b)	[%]	7.94	7.64	7.28	6.91
CS-25.121(c)	[%]	8.84	8.57	8.29	8.05
CS-25.121(d)	[%]	8.8	8.76	8.72	8.68

Table 2.17: Quantities of interest for the A320 case baseline, resized to match EIS2035 with TLAR reported in Table 2.14 and geometrical inputs as in Table 2.5.

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	56.76	57.89	59.01	60.14
OWE	[t]	38.58	38.71	38.79	38.84
Wing area	[m ²]	116.21	116.47	116.63	116.76
Max. LoD		18.47	18.46	18.45	18.44
Thrust @ SL	[kN]	99.5	100	100	99.75
Fuel mission	[t]	4.77	5.74	6.77	7.81
CAT.POL.A.410(a)-1	[ft/min]	905.76	905.59	904.13	904.48
CAT.POL.A.410(a)-2	[ft/min]	308.9	315.24	309.41	300.24
CS-25.119(a)	[%]	17.54	17.61	17.57	17.49
CS-25.121(a)	[%]	4.5	4.29	4.02	3.62
CS-25.121(b)	[%]	6.37	6.14	5.9	5.47
CS-25.121(c)	[%]	6.86	6.72	6.51	6.28
CS-25.121(d)	[%]	7.01	7.03	6.99	6.93

Table 2.18: Quantities of interest for the A320 case optimised, resized to match EIS2035 with TLAR reported in Table 2.14.

2.5 Conclusion

This chapter presents the first step of the PhD work and describes the development of a new version of FAST, integrated within OpenMDAO platform, to carry out aircraft design optimisation. This work has been conducted at the MDO Lab., University of Michigan, during a three months visit at the beginning of 2018, sponsored by the Formation Doctorale of ISAE-Supaero, to benefit from OpenMDAO expertises.

At first, an overlook to OpenMDAO and its structure is given, to understand how to build

an optimisation problem in this framework. Then, the integration process between FAST and OpenMDAO is described, having a focus on the problems that have been found and solved, the drawbacks as well as the new paradigm adapted. In fact, one of the key point that has been stressed out is that the optimisation must be fully opened, in the sense that the largest number of independent parameters must be free to vary, as a design variable; correlations between them are dealt more as design constraints than hard-coded relationship, to extend the design space exploration. The selected architecture used is MDF: it requires a full MDA, which was already available in FAST, and so add an optimisation solver at the top level of the iterative loop has been the most intuitive solution for the actual problem. Also, since much effort has been required for the recoding of FAST in the OpenMDAO logic, the choice helped to reduce the time spent on this phase. Finally, this new integrated version is tested on the A320 CERAS test case, to understand if the problem is well posed as well as the behaviour of the optimiser. It is then used to get a resized A320 type aircraft, considering assumptions for EIS2035, that will be later the reference case for the comparison with the unconventional configurations.

From these studies, it can be concluded that the integrated version of FAST works as expected in the case of A320 type aircraft. The process represents also the starting point to proceed towards the end of the Ph.D. It addresses indeed one of the points related to the answer to research question, stated at the end of Chapter 1, that is “Which is the most suitable MDO architecture for aircraft design purposes?”. With the MDO formulation ready, the next steps consist in adapting the MDA to the analysis of unconventional configuration. The definition of proper MDA loop to consider hybrid propulsion first and BWB configuration then, are the objectives of the following two chapters.

Synthesis of the chapter

- In order to obtain an efficient code, capable to carry out an optimisation in relatively short time, FAST has been integrated within OpenMDAO. The deployment of analytic derivatives is taken into account.
- Resulting code shows the following main features:
 - The design criteria are now considered as design constraints in the optimisation problem.
 - Multidisciplinary Feasible architecture is recognised as the most suitable for aircraft design problem: it does not ensure a feasible aircraft at each iteration, but it guarantees consistency between disciplines.
 - The problem has been decomposed in hundred of modules, to ease the analytic derivatives definition.
- The optimised A320 CERAS test case shows a 10% reduction on the design mission.
- The A320 CERAS has been resized to consider and Entry Into Service 2035 and different design ranges, to provide a baseline for comparison with unconventional configurations.

Research contribution

Collaboration with MDO Lab., University of Michigan, and NASA Glenn Research Center for the development of the integrated code FAST and OpenMDAO, during a visit from January to April 2018, funded by the Formation Doctorale of ISAE-Supaero.

Chapter 3

Design methodology and exploration of hybrid aircraft

Résumé

Ce chapitre est consacré à la mise au point d'une méthodologie pour la propulsion hybride, en considérant le cas test d'un avion conventionnel à propulsion électrique distribuée. La principale exigence est que l'avion vole de manière entièrement électrique jusqu'à 3000 pieds, afin de réduire les émissions près du sol.

La propulsion hybride est générée par deux turbines à gaz qui fonctionnent conjointement avec un ensemble de batteries. Par l'intermédiaire d'un ensemble de noyaux électriques, d'un convertisseur et d'un redresseur, l'énergie électrique générée par ces éléments est fournie à un ensemble de fans carénés, qui produisent finalement la poussée nécessaire au maintien du vol. Chaque composant est modélisé par son efficacité, sa densité de puissance spécifique et sa puissance maximale pouvant être délivrée. Seules les batteries diffèrent, car elles ont également besoin de la densité d'énergie spécifique pour estimer la quantité d'énergie pouvant être stockée. Pour des raisons de sécurité, seulement 80% de cette énergie est utilisable à des fins de propulsion. Un autre aspect important de la chaîne de propulsion est lié à la sécurité: les aéronefs doivent généralement pouvoir subir une panne moteur (condition OEI), mais dans le cas de moteurs multiples répartis le long de l'aile, ce cas n'est pas critique. Il est plus intéressant d'analyser la panne d'un noyau électrique (condition OCI): dans ce cas, un certain nombre de moteurs électriques ne seront plus disponibles, ce qui rendra plus stricte les conditions de dimensionnement. Ainsi, cette recherche propose une révision du document de certification CS-25, dans laquelle l'OEI est remplacée par l'OCI. Comme il existe deux sources d'énergie différentes, le cas d'une panne d'une batterie ou d'une turbine à gaz n'est pas pris en compte, car on peut supposer que l'autre source peut réagir pour maintenir le niveau de puissance requis.

Les modèles sont ensuite intégrés au processus de dimensionnement afin de prendre en compte dans la boucle de conception l'impact du nouveau groupe motopropulseur sur l'aérodynamique, la géométrie et les performances.

La procédure révisée est intégrée à la formulation MDO présentée au Chapitre 2, afin de disposer d'un cadre d'optimisation pour l'étude de ce concept. Les premiers résultats obtenus sur le concept concernent l'impact technologique. Du fait, il y a des nombreuses incertitudes dans la définition des paramètres pour les perspectives 2035. Une analyse de sensibilité est effectuée, pour évaluer leur impact sur la conception globale. Les résultats montrent que les batteries représentent le paramètre déterminant de la conception. Il est donc primordial de les concevoir avec soin pour réduire l'incertitude liée à leurs paramètres.

Ensuite, le problème d'optimisation est défini: il comprend 21 variables de conception soumises à 17 contraintes. La taille de l'aéronef est adaptée à différentes plages de conception, le nombre de moteurs variant de 16 à 48 afin de refléter son effet sur la conception. L'aéronef hybride est évalué par rapport à l'aéronef conventionnel de référence défini au Chapitre 2. Les résultats montrent qu'il existe une zone d'intérêt pour la conception de cet avion, qui est limitée à un rayon d'action environ 1000 nmi. Ce compromis est dû au fait que les batteries introduisent une pénalité de poids importante. En fait, sur de courtes distances, l'effet le plus important est l'avantage d'un segment entièrement électrique. Sur des distances plus longues, cependant, les pénalités en masse sont prédominantes, ce qui explique la tendance montrée. Une optimisation plus poussée montre que, du point de vue de la consommation de carburant, il est préférable de voler sans batterie, mais dans ce cas il n'est plus possible d'atteindre l'objectif de zéro émission près du sol. Les résultats montrent que le cas avec 32 moteurs est le plus performant, car il représente un équilibre entre efficacité aérodynamique et propulsion. Enfin, un diagramme de Pareto est obtenu, en tenant compte du poids à vide et de la consommation d'énergie, définis comme les deux fonctions objectif du problème. Pour cette analyse, une méthode sans gradient et une méthode basée sur le gradient sont comparées: les résultats montrent que les dérivés réduisent le coût de calcul d'environ 70%, ce qui est un élément clé pour les concepteurs.

Contents

3.1	Introduction	95
3.2	Presentation of the proposed concept	96
3.3	Definition of a hybrid propulsive chain	98
3.3.1	Battery	100
3.3.2	Gas turbine and generator	103
3.3.3	Electric motor	105
3.3.4	Inverters and converters	106
3.3.5	Power management unit PMU	107
3.3.6	Cooling system	108
3.3.7	Cables	108
3.3.8	Ducted fan	109
3.3.9	Certification constraint module	113
3.4	Methodology for the sizing of hybrid aircraft	115
3.4.1	MDA sizing loop	115
3.4.2	MDO formulation	120
3.5	Exploration of hybrid aircraft with distributed electric propulsion	122
3.5.1	2035 technology assessment	122
3.5.1.1	Sensitivity analysis – fixed battery case	124
3.5.1.2	Sensitivity analysis – battery resizing	126
3.5.2	Sizing of aircraft with distributed electric propulsion	129
3.5.3	Optimisation of aircraft with distributed electric propulsion	135
3.5.3.1	Problem formulation	135
3.5.3.2	Sensitivity analysis	137
3.5.3.3	Mono-objective optimisation	140
3.5.3.4	Pareto frontier with gradient information	145
3.6	Conclusion	149

Outline

- The hybrid propulsive chain is defined. Distributed electric propulsion is considered for the thrust generation.
- Details of the models adopted for the electric components are provided.
- Definition of a Multidisciplinary Design Analysis procedure for the sizing of a tube-and-wing aircraft featuring distributed electric propulsion.
- Definition of a Multidisciplinary Design Optimisation for the exploration of the tube-and-wing featuring distributed electric propulsion: the formulation is identical to what has been presented in Chapter 2, with the actual MDA replacing the one for conventional aircraft.
- A technological assessment is carried out, considering perspectives in 2035.
- The proposed tube-and-wing featuring distributed electric propulsion is explored. Number of electric motors is varied to capture the effects of this parameter on the overall design.

3.1 Introduction

This chapter can be divided into two main parts: in the first one, the methodology for the sizing of a TAW aircraft featuring distributed electric propulsion is described, meanwhile the second part reports the results obtained by applying the methodology. This study is key to explore the first of the two innovative aspects of this Ph.D., in agreement with the roadmap of Fig. 1.24. Also, it assesses the possibility to introduce distributed hybrid propulsion on large passenger aircraft, while recent works are mainly related to small aircraft (see *i.e.* [HRD16; Bor+16]).

In Sec. 3.2 the proposed concept is presented: it is a TAW configuration, featuring distributed electric propulsion. Sec. 3.3 presents the hybrid chain, starting from a global overview and then detailing all the components. Then, Sec. 3.4 details the integration of these models in the design loop, to consider hybrid electric aircraft. Afterwards, the resulting MDA is integrated in the MDF that describes the MDO problem for FAST, in order to finally define a tool capable to optimise hybrid aircraft featuring distributed propulsion.

The MDA is the initial step of the exploration, with results presented in Sec. 3.4.1. Its next step, the optimisation, is carried out with the integrated version of FAST; Sec. 3.4.2 details this major work. Before going through the optimisation, a sensitivity analysis is carried out to evaluate the importance of each design variable on the design: this helps to reduce the problem size, reducing thus the time analysis. Then, different objective functions are defined, and a multiobjective optimisation is carried out both to benchmark the concept and evaluate the advantages of the integrated code developed, in terms of computational cost. The reference aircraft is the A320 EIS2035, presented in Sec. 2.4.1.3: the non optimised and optimised hybrid aircraft are compared respectively with the non optimised and optimised baselines.

The research contribution of this chapter is collected into the following publications:

1. The development of the sizing process for the hybrid electric configuration and related results are collected in a paper contained in the AIAA SciTech 2018 proceedings [Sgu+18a].
2. The development and the application of a version of FAST tailored for the optimisation of this kind of concept is the subject of a journal paper [Sgu+20b], submitted to Journal of Aircraft. At this work contributed also expertises from MDO Lab., University of California San Diego and NASA Glenn Research Centre.
3. The sensitivity analysis on the technology is the subject of a book chapter regarding the uncertainty in aerospace systems [SDB20].

Also, the integrated version of FAST for hybrid aircraft has become one of the test cases for SEGO, a global optimisation algorithm developed by ONERA and ISAE-Supaero [Bar+19].

3.2 Presentation of the proposed concept

In order to study solely the effect of hybrid propulsion, it has been decided to study a classical TAW configuration, where the propulsion system is replaced by a new one, based on electric systems. There are different ways to achieve hybrid propulsion, as described in Chapter 1. The main interest of this study, however, is to explore a distributed electric propulsion architecture, featuring ducted fans, as it offers many advantages (see Sec. 1.3.1.2 for more details):

- Higher propulsive efficiency than a conventional engine at the same design point associated to the reduction in fan pressure ratio without geometrical constraints;
- General desizing components as failure conditions are less stringent because of the distributed thrust;
- Blowing as a main aeropropulsive effect, which leads to higher local C_l ;
- The possibility to combine with a boundary layer ingestion device, depending on the configuration layout;
- Distributed electric motors can partially help towards lateral control, with the consequent desizing of the vertical tailplane (VTP).

The segment of application is the small and medium range aircraft, since it account nowadays for a 36% of total emission (see also Fig. 1.2) and according to the perspectives by Airbus and Boeing it emerges it will be the one with the major growth in next years [Air19; Boe16]. At present, with available technologies, a zero-emission from gate to gate appears unfeasible [Hor+13], even in 2035 horizon, but to match the environmental goals at least the concept must be capable to green the air close to ground. This is translated into a new requirement, not present for conventional aircraft, which states that the emission must be zero at least up to 3000 ft (about 1 km). The value of altitude is not chosen by chance, but represents the mean altitude of atmospheric boundary layer [Li+14], as also shown in Fig. 3.1. Within this zone, convective effects create turbulence which mixes the air: harmful particles (CO_x , NO_x , ...) released in the region beyond 3000 ft worsen the quality of air at ground, resulting into conditions more dangerous for human being. To achieve the zero emission, a green source of energy (batteries, in specific case), must be taken into account.

The top level requirements for this large passenger aircraft (LPA), based on DEP and different energy sources, are reported in Table 3.1. They are similar to the Airbus A320 requirements, resized for 2035 and explored in Sec. 2.4.1.3; note that the zero emission requirement appears clearly as a TLAR.

A visualisation of the concept to investigate is depicted in Fig. 3.2, using OpenVSP [Ope18b]. The hybridization is obtained through a set of batteries, located in the cargo and not shown in Fig. 3.2, and two turboshafts located at the rear. Because of the rear turboshaft position, a T-tail must be used for the empennage configuration. More details on the hybrid chain and its modelisation are provided in next section. Electric motors and ducted fans are placed over

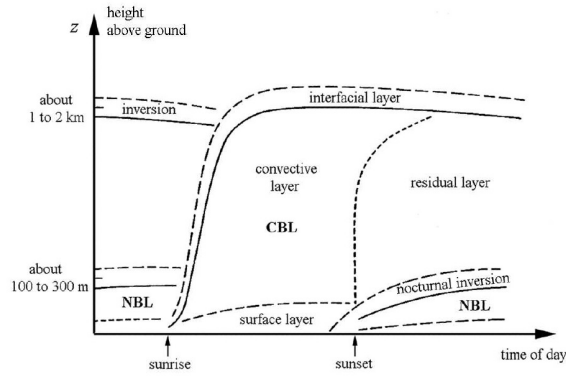


Figure 3.1: Typical evolution of atmospheric boundary layer during the day. Convective boundary layer extension is shown [Li+14]

Range	600–1500	nmi
Mach number	0.78	
Number of passengers	150	
Approach speed	132	kt
EIS	2035	
Zero emission limit	3000	ft

Table 3.1: Top level requirements for the proposed TAW configuration featuring distributed electric propulsion, shown in Fig. 3.2.

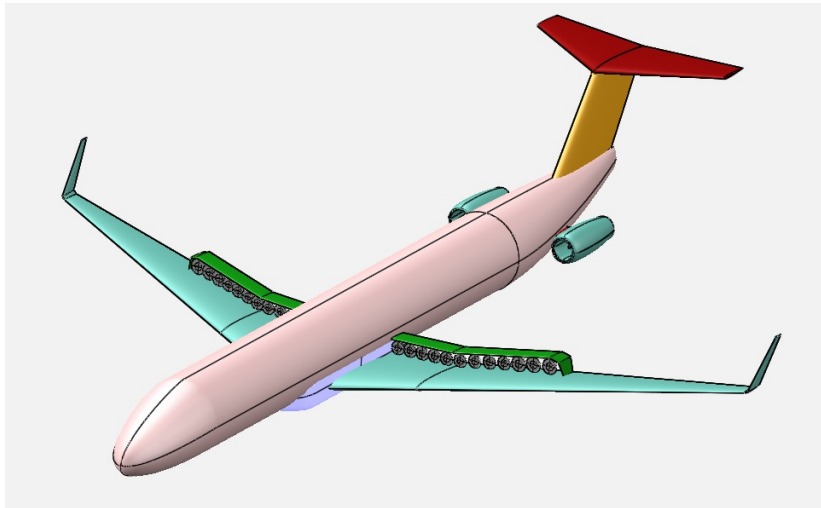


Figure 3.2: Classical TAW configuration featuring distributed electric propulsion concept, as modeled in OpenVSP [Ope18b].

the wing, to take advantage of blowing effect, especially for takeoff and landing phase [MN18; Dee+17b]. To maximise this phenomenon, a hyperdistributed configuration is considered, that is more than 15-20 ducted fans are used. Beside the blowing effect, this solution is easier to implement, compared to others (*e.g.* embedded engines), and limits the associated

risk [MOM18]. Also, it has been shown in the work of Wick et al. [Wic+15] that it does not produce wave drag divergence in transonic regime.

On this configuration, the BLI effects can be neglected because of the small chord available on the wing. Therefore, the blowing is the only aero-propulsive effect taken into account. From the AMPERE experience at ONERA [HRD16], such phenomenon produces full laminary flow on the upper surface, increasing the local 2D lift to values in the range of 4-5. As a consequence, takeoff length is reduced, the wing area is reduced, and high-lift devices are no more needed, saving weight. The blowing, however, may lead to tip-stall problem. To force the stall starting at the center of the wing, a twist law must be defined [de 15b]. The research of an appropriate twist law, however, has not been tackled in this research, which is limited to the development of an OAD procedure for the concept, and it is marked among the further developments. It is worthy to mention, however, that the twist problem is not trivial: the zone interest by the presence of electric motors have to be untwisted, in order avoid that the thrust vector has a vertical component. This means that most likely the twist angle at tip must be higher for this case than the reference aircraft, with corresponding worsening of the aerodynamics, that impacts the cruise performance. This effect is not considered in this study; in the same way also benefits coming from distributed propulsion on the polar are not considered, but the two effects tend to counterbalance and in the end this limitation is not stringent for the results.

The advantages of distributed propulsion in case of failure condition have already been discussed in Chapter 1 (see also the work of Steiner et al. [Ste+12b]). Its effect on the mass is also been discussed in Sec. 1.3.1.2 in the case of DRAGON configuration [Sch+19]. In particular, it has been remarked that from one hand distributed propulsion alleviates the aerodynamic load, but on the other hand enhances the torsion moment, leading to an increasing in wing weight.

Concerning the position of batteries, as said they are located in the cargo. This choice was mainly dictated by stability needings: batteries introduce a non negligible lumped mass that may strongly affect the center of gravity; placing them in the cargo reduces their impact since the global center of gravity is found around the wing center of gravity. Also, the cargo is the zone that offers more volume available for its allocation.

After this general overlook on the concept, next section details the propulsion system, presenting a general overlook and then the modelisation of each component.

3.3 Definition of a hybrid propulsive chain

The general scheme, in the case of 40 distributed motors, is represented in Fig. 3.3. The number of motors is chosen as it is indicative of a hyperdistributed architecture, which is considered in this work. The two turboshafts, referred also as gas turbines, are connected to a device, called generator, that converts mechanical power into electrical power. They are coupled to a set of batteries thanks to a set of electrical buses, also called power management

units PMU or electric cores. From the PMU dedicated lines start, one for each electric motor, aimed to convert electric power in mechanical power.

The current is brought in DC way, at this scope along the lines there are AC/DC and DC/AC devices to switch the current type from DC to AC and vice versa, and DC/DC devices to bring the current at the right transport voltage. Finally, breakers are installed to disconnect a line in case of failure.

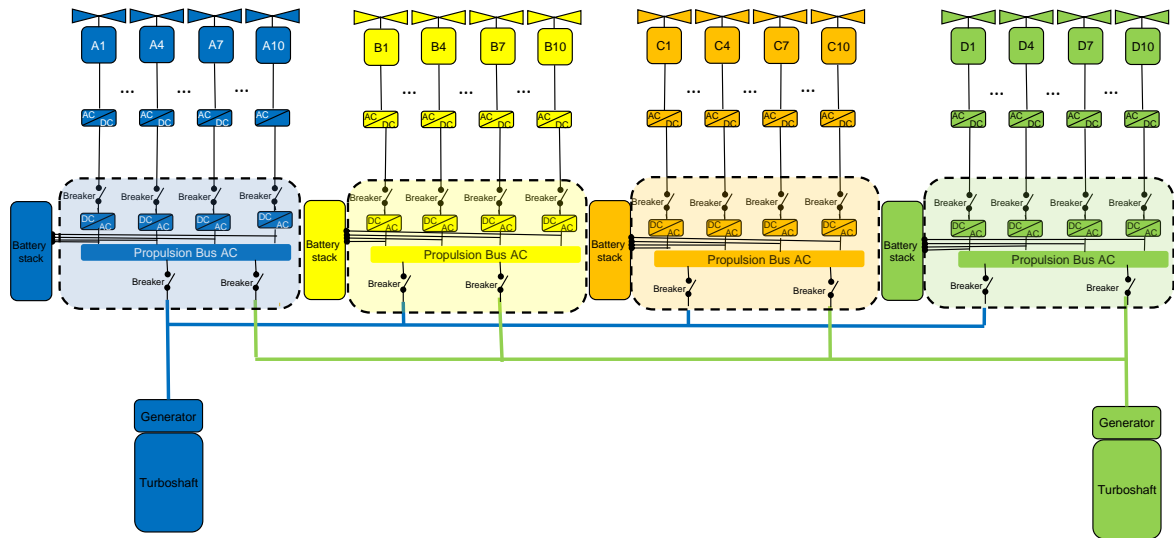


Figure 3.3: General scheme of hybrid electric distributed propulsive chain architecture considered in this research. Case of 40 electric motors distributed along the wing.

It is to note that each power source supplies power to the whole electric buses, to increase redundancy and avoid power losses in case of an electric core failure. Electric motors are directly connected through the shaft to the ducted fan, which finally converts mechanical power into thrust. From an architecture point of view, the power that arrives at the electric cores is the sum of the battery and the turboshaft power, so they work like in a serial architecture. After the electric cores, instead, power is splitted along all the lines, keeping the voltage constant, and this part of the scheme works as a parallel architecture. Therefore, the global arrangement could be defined as a mix-type architecture.

The propulsive chain is more complex than a traditional one, but it can rely on better efficiency due to the electrification, with potential reduction in fuel consumption. Still, because of the complexity and the presence of more devices, it may require more maintenance, which leads to higher maintenance cost, and thus a deeper analysis has to be carried out [PKG14].

Concerning the power management, this research proposes a different approach than the hybrid ratio used in previous work [Por+14b; Isi+14]. One of the limit of the degree of

hybridisation is the flexibility: in fact, in case of a sudden loss of power, it is still distributed between the sources at the same percentage, and the power demanded to each source is always dependent on the other. Instead, here it has been preferred to control each source separately, with a dedicated power rate defined as following:

$$\delta_b = \frac{P_b}{P_{b_{\max}}} \quad (3.1a)$$

$$\delta_{GT} = \frac{P_{GT}}{P_{GT_{\max}}} \quad (3.1b)$$

where δ_b and δ_{GT} are the battery and the turboshaft power rate respectively, P_b and P_{ts} the delivered power by battery and turboshaft, and the subscript max refers to their maximum value (as the turboshaft output depends on Mach and altitude, since it is an air breathing engine). The total power arriving at the PMU level is then

$$P_c = \delta_b \eta_b P_{b_{\max}} + \delta_{GT} \eta_g P_{GT_{\max}} \quad (3.2)$$

where η represents the efficiency of batteries and generator. In this way, power demanded to turboshafts and batteries are decorellated, and the advantage of this approach is in the flexibility that it permits in case of failure. If a sudden loss of source occurs, in fact, it is still possible to ask for more power to the other source, since the two sources can deliver their maximum power at the same time, whereas before this was not possible since an increase in the degree of hybridisation results in a major power request from one source and less from the other one.

Finally, a remark on the technological choice must be done. There are two possible solutions for the upcoming years: a non-cryogenic technology, where the components are further developed but without considering the superconductivity [Dev+15], or a cryogenic technology, where the use of superconductivity allows to drastically lighten the system without any heat dissipation [Mad+16]. The cryogenic technology has potentially much more advantages than the non-cryogenic one, however it is still under experimentation and it is unforeseen to have it ready at large power scale before the 2040 [BM18b]. Therefore, to reduce at most the risk related to the design, a more conventional non-cryogenic technology is here considered, within the 2035 perspectives.

Next sections will present the model implemented for each of the components. When dealing with electric components, the key parameters are the specific energy and the specific power density; following the notation used by Brelje and Martins [BM18b], these quantities are represented as the lower case of extensive quantities (e for specific energy density, p for specific power density).

3.3.1 Battery

Battery is a vital component of electric achitecture as it is a main source of power, while corresponding to a permanent weight penalty. Beside the power, battery is also an energy

source, and generally its overall performance is classified based both on the energy and the power content, through the use of a Ragone plot [Rag68]. This curve shows, for a given category of battery, the tradeoff between specific power and the specific energy; sometimes it is referred in equivalent way to volumetric quantities. The tradeoff between the two parameters is almost exponentially decreasing: the more powerful a battery is, the less energetic is and viceversa. The choice is then not unique but depends on the case of application, *i.e.* for small aircraft the power level is not so relevant and a more energetic battery is of more interest [Hep12], on the contrary for larger size aircraft power may become the most stringent criteria to supply [Kim+14]. An example of Ragone plot, for different types of batteries, is given in Fig. 3.4.

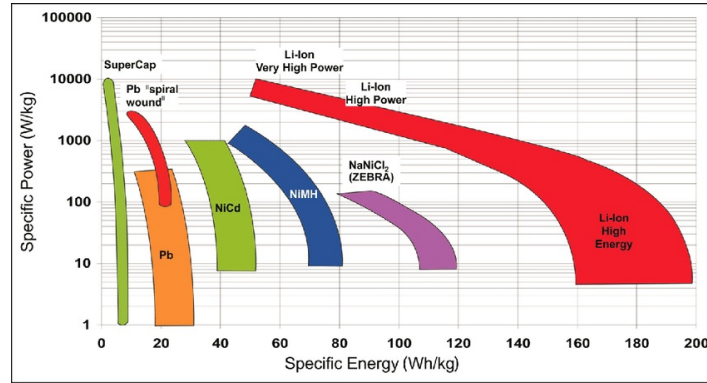


Figure 3.4: Ragone plot for different types of batteries, 2008 technology state of the art [SG08].

In recent years, research has been focusing in developing new technologies for the upcoming generation of batteries: beside the classical Lithium ones, other developments are focusing on the studying of Sulphur, Nickel, Polymer based batteries, and even a new innovative category of air-breathing batteries, the so-called Lithium-Air [Fra15; BM+13]. The research in this field, however, still corresponds to the experimentation stage and in some cases even at theoretical level; choosing such innovative aspects in the design is a significant risk. On the contrary, the actual Lithium-Ion technology is well assessed, and it covers a large variety of situations, from high power to high energy (see also Fig. 3.4) [Xue+15]. Despite the theoretical limit for these batteries is almost reached [Fra15], in this research it has been decided to use Li-Ion, in order to reduce the risk related to the design.

A battery is defined by a set of five parameters: specific energy density e_b , specific power density p_b , density ρ_b , energy density and power density [Cin+17b; LL12]. Actually, they are not independent of each others, but only three of them are necessary for a full definition. The first and most natural input is the physical density ρ_b ; the two other independent parameters can be equivalently specific energy and power density, or volumetric energy and power density, as from the Ragone plot. In this work ρ_b , e_b and p_b are given as inputs; energy and power density follow to be $\rho_b e_b$ and $\rho_b p_b$. The energy stored E_b and the maximum power P_b which can be delivered by the battery are then computed:

$$E_b = e_b m_b = e_b \rho_b \tau_b \quad (3.3)$$

$$P_b = p_b m_b = p_b \rho_b \tau_b \quad (3.4)$$

where τ_b is the battery volume and m_b is the battery mass.

Another key aspect of batteries is their dynamic: during the use, their capacity, that is the integral of current over the time, changes together with the voltage delivered. A typical battery discharge curve, representing voltage vs. capacity, is shown in Fig. 3.5. Three regions are usually identified: an exponential zone, at low capacity, that in general can be neglected, a region in which the voltage is constant, and finally a region in which voltage drops rapidly (deep discharge zone).

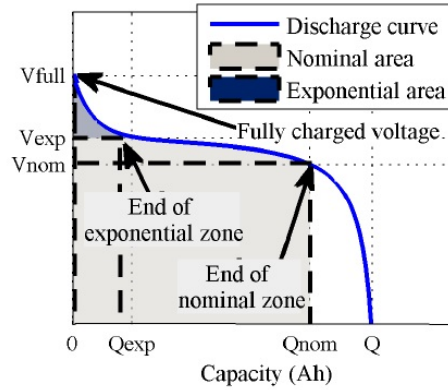


Figure 3.5: Typical battery discharge curve voltage vs. capacity; with the three characteristic regions identified [TD09].

To avoid damaging the system, a battery should not work in the deep discharge zone. To monitor the energy left the state of charge SoC , defined as the ratio between the capacity at a certain time $q(t)$ and the total capacity q_b , is used:

$$SoC(t) = 1 - \frac{q(t)}{q_b} \quad (3.5)$$

where $q(t) = \int_0^t i(s) ds$, with $i(s)$ the current intensity at time s and $q_b = q(t_f)$, with t_f the final time. To avoid the deep discharge zone, SoC can not be allowed under a certain limit, which in general depends on the battery type. For a Li-Ion battery the minimum limit for the SoC is estimated to be 20% [LL12; TD09]. Finally, the total battery energy, defined in Eq. (3.3), is also the area under the discharge curve:

$$E_b = \int_0^{V_f} q(V) dV = \int_0^{V_f} \int_0^{t_f} i(s) ds dV. \quad (3.6)$$

At conceptual design level, it is a hard work to implement the full battery dynamic into the model, due to the huge number of variables involved [TD09]. For that reason, in this work the dynamic behaviour is neglected and the hypothesis of constant voltage is made; in other words, it is assumed that the exponential zone can be neglected and the 20% limit ensures to avoid the deep discharge zone. Under this assumption, it is possible to remove dV from the

integral in Eq. (3.6):

$$E_b = \Delta V \int_0^{t_f} i(s) ds = \Delta V q_b \quad (3.7)$$

Note that in Eq. (3.7) the quantity ΔV , which is total constant voltage, appears. Finally, multiplying by ΔV both numerator and denominator in Eq. (3.5), the *SoC* at time t can be written in terms of energy:

$$SoC(t) = 1 - \frac{E_c(t)}{E_b}, \quad (3.8)$$

where $E_c(t)$ represents the energy consumption at time t . The assumptions here are not restrictive and this approach is used in this study.

The other advantage of this model is that defining a battery discharge curve the battery energy is fixed, and then the number of batteries has to be treated as design variable in an optimisation process. Since it is an integer, this quantity can not be easily included and mixed integer nonlinear programming algorithms have to be considered [Bel+13]. On the contrary, the battery volume, which defines energy and power content through Eq. (3.3) and Eq. (3.4), can be used in the equivalent way, with the advantage of being a continuous variable. This aspect will be recalled later, during the optimisation problem formulation.

For what it concerns the sizing, batteries must supply both the energy and the power requirements. The volume is then computed in order to satisfy the conditions of Eq. (3.9), N_b being the number of batteries.

$$SoC(t_f) \geq 0.20 \quad (3.9a)$$

$$N_b P_b \geq P_{ref} \quad (3.9b)$$

Eq. (3.9a) states that the state of charge at the final time must be at least 0.20, for safety issues, meanwhile Eq. (3.9b) states that the power delivered by all the batteries must be higher than a reference power, specified by the designer, *i.e.* the power at takeoff. Note that this procedure is similar to the wing sizing in the original FAST, where the wing area needs to satisfy at the same time conditions of Eq. (2.8) and Eq. (2.9).

The battery mass is simply computed by the volume information as

$$m_b = \rho_b \tau_b \quad (3.10)$$

3.3.2 Gas turbine and generator

Gas turbine is the other main of power source and it is then one of the most important element to size. It is no more than an air breathing engine, with the scope to produce power to deliver at the electric chain; its operation is similar to the turboshafts that equip regional aircraft, like the ATR 72 [Rou07], with the only difference that mechanical power is not delivered to a propeller but to a device that converts it into electric power, called generator.

In fact, its design is similar to these types of engines: after the inlet, there is a single compressor, followed by the combustion chamber, where the chemical reactions take place, and two turbines [MHP02]. The first turbine is the high speed one, which is mounted on the same shaft of compressor and moves it. The second turbine, instead, works at low speed, and it is mounted on a different shaft, where the generator is placed. Most of the power generated by the combustion is delivered to the high speed turbine; the remaining represents the useful power, which is of interest to compute performances.

The gas turbine has been developed using GSP, acronym of gas turbine Simulation Program. It is a software, developed at NLR, for the performance analysis of engines [VB00; NLR00]. Its scheme, as modeled in GSP, is shown in Fig. 3.6; it is possible to detect all the elements described above.

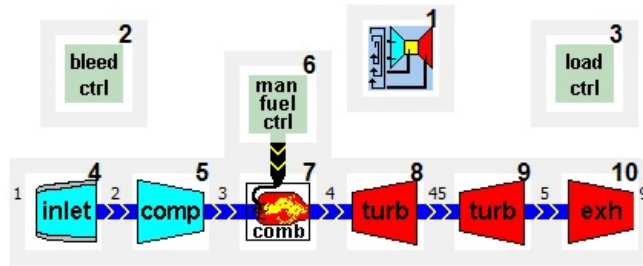


Figure 3.6: Turboshaft model, as in GSP software [NLR00].

The output of the model are the maps for power P_{GT} and fuel flow $\dot{m}_{f_{GT}}$ as function of Mach and altitude, similar to the outputs from the CERAS and the rubber engine described in Sec. 2.2.3.1. For the performance, the specific fuel consumption is replaced by the power specific fuel consumption PSFC, defined in Eq. (3.11).

$$\text{PSFC} = \frac{\dot{m}_{f_{GT}}}{P_{GT}} \quad (3.11)$$

Units for PSFC are $\text{kg kW}^{-1} \text{h}^{-1}$, a typical value is in the order of 0.22 [BB12].

Finally, the inlet diameter is computed by knowing the value of mass flow, meanwhile the total length is estimated starting from statistical equations given by Raymer [Ray18]. To consider a “rubberized” version, a scale factor is considered, defined as

$$k_{GT} = \frac{P_{GT_{des}}}{P_{GT_{ref}}} \quad (3.12)$$

where $P_{GT_{des}}$ is the needed design power and $P_{GT_{ref}}$ the reference power of the GSP model; note that the design point must be the same to ensure coherency. The power map is rescaled according to this factor. No changes are considered for the PSFC, since from Eq. (3.11) emerges that a change in power automatically impacts the PSFC.

Burguburu and Basset [BB12] give an estimation of the mass of this type of engine, considering a large number of different similar turboshaft. From this study it is possible to define a power to mass ratio, so the gas turbine mass results to be

$$m_{GT} = \frac{P_{GT_{des}}}{p_{GT}} \quad (3.13)$$

Concerning the design point, it depends on the designer choice and it may be the takeoff, the cruise or other points. In this research batteries can help the takeoff and the climb phase, but design also a hybrid cruise will result unfeasible. As a result, the cruise segment is the main segment where the gas turbine works alone, and it is preferable to have it designed for these conditions. Table 3.2 reports the design point for the GSP gas turbine; the altitude is taken in a reasonable flight level.

Mach number	0.78
Altitude	35 kft
Δ ISA	0 °C

Table 3.2: Design point for the gas turbine modeled in GSP.

3.3.3 Electric motor

Electric motors are the other main component of the hybrid propulsion, aimed to convert electrical power to mechanical power for the shaft. They are very reliable devices and can operate at very high efficiency, that, with a careful design, can reach 95-98%. Furthermore, respect to a combustion engine, their performances are not dependent from the altitude [SIH13], which represents their main advantage. Losses are mainly linked to friction of components and magnetic field, Lowry and Larminie presented a full description of all the losses that occur in an electric motor [LL12]. Despite all these features, their use has been limited by power-to-mass ratio, but advances in the last decade enabled to reach higher values, which opened their use in aircraft industry [Cam+11].

Basically, electric motors can be divided into two classes: AC and DC motors. The former are lighter than the latter, but require complex power conversion hardware to convert the DC current in AC, suitable for the motors. On the other side, DC motors tend to be larger than AC motors with the same specification, and require more maintenance. The most common DC motors are based on the permanent magnet technology: their advantage is that they do not require an excitation power source to establish a magnetic field, so they can be used as a motor and generator, but they are heavy and very expensive [Cam+11]. As a conclusion, it seems that AC motors represent the best choice to reduce penalties in weight, despite they need DC/AC converters, that are in fact present in the scheme of Fig. 3.3, one for each motor line.

For the sizing, motors are defined by their specific power; knowing the maximum power

demanded their weight results to be:

$$m_{EM} = \frac{P_{EM_{max}}}{p_{EM}} \quad (3.14)$$

The electric motor must be coupled with the ducted fan, and the rotational speed of both the elements must be matched. For this purpose, a gearbox must be added, introducing weight to the system, or a more integrated device like the annular motors can be used [Eic+06]. An example of annular motor is shown in Fig. 3.7: the fan is directly integrated within an annular fairing, and it is moved by the magnetic field generated in the external shroud.

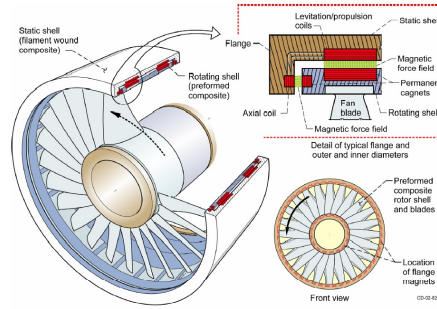


Figure 3.7: Scheme of annular motor, which integrates electric motors and ducted fan [Eic+06].

Albeit the difficulty in design and the very low power to mass ratio (in the order of 5 kW kg^{-1} according to the work of Eichenber et al. [Eic+06]), an annular motor removes the problem of coupling, since the fan rotational speed is directly controlled by the magnetic field generated. The length of the motor is computed by the ratio between length and fan radius:

$$L_{EM} = \left(\frac{L_{EM}}{r_f} \right) r_f \quad (3.15)$$

r_f being the fan radius, the sizing of which will be explained later in Sec. 3.3.8. The ratio $\left(\frac{L_{EM}}{r_f} \right)$ is function of FPR solely:

$$\left(\frac{L_{EM}}{r_f} \right) = \begin{cases} 1.25 + 0.5 (1.1 - \text{FPR}) & \text{FPR} \leq 1.1 \\ 1.75 & \text{otherwise} \end{cases} \quad (3.16)$$

The total radius includes also the external shell; its thickness is estimated to be 5% of the fan radius.

3.3.4 Inverters and converters

The DC/AC and AC/DC devices are present along all the lines, to switch from DC current, which is the type that goes in cables, to AC current, needed for the electric motors. These devices are commonly called inverters. Another type of device is the DC/DC, called converter,

that brings a DC current at the right voltage, and it is placed in the battery pack.

They are simply defined by the power specific density and the efficiency. Their sizing is similar to that already adopted for the other elements: starting from the knowledge of the maximum power they need to sustain, their mass is computed by the definition of the power specific density, as in Eq. (3.17).

$$m_{IC} = \frac{P_{IC_{\max}}}{p_{IC}} \quad (3.17)$$

The value of maximum power depends on the location at which they are placed in the chain of Fig. 3.3: the inverters before the motors need to sustain a level of maximum power equal to that of the motors, divided by their efficiency, meanwhile the inverters after the electric cores must sustain a maximum power that is greater because there were some loss due to efficiency and transport.

3.3.5 Power management unit PMU

The power management unit (PMU), sometimes referred also as electric core, is the device aimed to electrically connect the generators and the batteries. It can be schematised as an electrical node, which takes two lines and spread them to transport power to electric motors. In general, more than one of these units are located in the chain for redundancy; also, as shown in Fig. 3.3, each power source is connected to all the electric cores, in order to avoid a power loss in case of PMU failure.

They are defined by an efficiency and a power density, similar to other components their mass is estimated as:

$$m_{core} = \frac{P_{core_{\max}}}{p_{core}} \quad (3.18)$$

These devices are highly efficient, however it is to note that a loss of one of them is reflected in a set of electric motors becoming inoperative; the remaining working motors are:

$$N_{EM_{op}} = \frac{N_{core} - 1}{N_{core}} N_{EM} \quad (3.19)$$

From Eq. (3.19) it is evident that the more the propulsion is distributed, that is more electric cores are present, the less is the quantity of electric motors becoming inoperative. That is, a highly distributed propulsion system, at PMU level, helps to reduce the penalties due to the oversizing, which is the equivalent effect studied by Steiner et al. in relation to the engine failure [Ste+12b]. This aspect, together with the increased propulsive efficiency, is really the key point of interest for distributed propulsion.

3.3.6 Cooling system

Thermal aspects are of relevant importance in an hybrid architecture. Generally, electric components show a very high efficiency, with small loss. Nevertheless, due to high values of power used, in the order of megawatt, a sizable quantity of this power is dissipated into heat.

A cooling system must be added, to avoid that the temperature increases beyond the safety limit, damaging the systems within the propulsive chain or even the airframe. Of course, such system introduces a relevant penalty in weight, and thus a careful design must be carried out, to limit penalties.

A cooling system consists of two different devices: heat exchanger and air cooling systems. Heat exchangers are devices that surround the cables and artificially dissipate the power using air, meanwhile the latter are air inlets and associated ducting placed in the fuselage, in order to have cold air circulating into the system. The heat exchanger introduces a mass penalty, that can be evaluated knowing the value of power to dissipate [Ant17]:

$$m_{cs} = \frac{P_{diss}}{p_{cs}} \quad (3.20)$$

with m_{cs} cooling system mass, P_{diss} power dissipated and p_{cs} cooling system specific power. Air cooling does not introduce weight but incurs a penalty on the drag coefficient, estimated to be 5% with the equations presented by Hoerner [Hoe65].

3.3.7 Cables

The cables have to transport current from one device to another within the hybrid architecture. They are sized in order to carry a certain current, which must be below the maximum allowed threshold [Van15]. The current, and so the sizing, depends on the voltage used for the transport.

First the current which flows through a cable is computed as

$$i = \frac{P}{\Delta V} \quad (3.21)$$

Then a check has to be done in order to be sure that value is lower than the maximum current. If it is not, more cables have to be installed; the number is computed dividing the value of current with the maximum one:

$$N_{cab} = \left[\frac{i}{i_{max}} \right] \quad (3.22)$$

where the square brackets indicate the integer part of $\frac{i}{i_{max}}$. The number of cables is then doubled to consider that current can move in both directions. Finally, according to motors, generators and batteries positions, it is possible to estimate the cable length and so the weight:

$$m_{cab} = N_{cab} \left(\frac{m}{L} \right) L_{cab} \quad (3.23)$$

where $\frac{m}{L}$ is the cable linear density. Installation and Health Monitoring System have to be included in the weight calculation. Preliminary works at ONERA show an increasing in weight of 30% for the installation and of 5% for the HMS.

During the transport, a certain amount of power that is dissipated into heat due to the Joule effect [TM08]; these losses can be evaluated using the Ohm's second law:

$$P_{cab_{diss}} = R_{cab}i^2 \quad (3.24)$$

where R_c is the resistance, computed with the classical equation

$$R_{cab} = \rho_{cab} \frac{L_{cab}}{S_{cab}} \quad (3.25)$$

where ρ_{cab} is the electrical resistivity and S_{cab} the cable section area. For copper, $\rho_{cab} = 1.68 \times 10^{-8} \Omega m$ at 20 °C. The power dissipated is subtracted from the total useful power and added to the power sizing for cooling system.

A cable efficiency can be defined considering the total electric power ΔVi and the power loss of Eq. (3.24):

$$\eta_{cab} = \frac{\Delta Vi - R_{cab}i^2}{\Delta Vi} = \frac{\Delta V - R_{cab}i}{\Delta V} \quad (3.26)$$

To note that the power loss is equivalent to the loss of tension, in agreement with the Ohm's first law [TM08].

3.3.8 Ducted fan

Ducted fan is the ending point of the propulsive chain, and it is dedicated to thrust generation, starting from the mechanical power received by the shaft. It is sized to be adapted for a single point, which is typically the cruise point, corresponding to a certain altitude h and Mach number M_0 . Since it is none more than a duct with air passing through, it can be schematised as a nozzle where quasi-isentropic transformation takes place. Under this assumption, it is possible to get a sizing using thermodynamic isentropic equations [Fer38; Car09; LL87]. The model described here has been provided by Olivier Atinault, research engineer at ONERA Meudon, and published in the AIAA SciTech proceedings [Sgu+18a].

The scheme of the fan with all the sections detailed is shown in Fig. 3.8; the description that follows refers to this scheme. The main parameter that drives the design is the fan pressure ratio FPR, which represents the pressure gauge at the fan section. As remarked in Sec. 1.3.1.2, FPR impacts both the size and the thrust generated: the smaller, the bigger is the size and lower the thrust, and viceversa. The sizing starts from the thrust coefficient, defined as

$$c_T = \frac{T}{\frac{\gamma_a}{2} p_{s_0} M_0^2 S_{ref}} \quad (3.27)$$

where T is the thrust, p_{s_0} is the static pressure at the given altitude, γ_a the ratio between the specific heats for air, $\gamma_a = 1.4$ [Fer38], and S_{ref} an arbitrary reference surface.

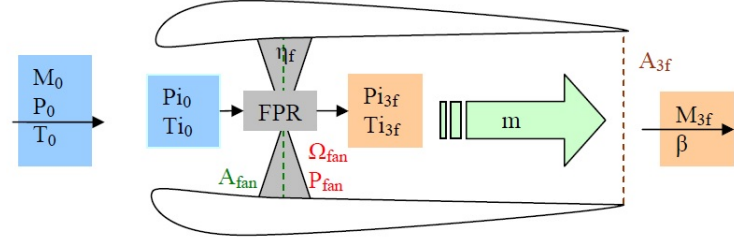


Figure 3.8: Scheme of a ducted fan for the model presented

The steps to follow are listed below.

1. The first step is to compute the total pressure and temperature at the inlet, using the de Saint-Venant relations [Car09]:

$$p_{t0} = p_{s0} \left(1 + \frac{\gamma_a - 1}{\gamma_a} M_0^2 \right)^{\frac{\gamma_a}{\gamma_a - 1}} \quad (3.28)$$

$$\theta_{t0} = \theta_{s0} \left(1 + \frac{\gamma_a - 1}{\gamma_a} M_0^2 \right) \quad (3.29)$$

with θ_{s0} representing the static temperature at the given altitude.

2. Then it is possible to compute the Mach number at the exit of the nozzle:

$$M_{3f} = \sqrt{\frac{2}{\gamma_a - 1} \left[\left(1 + \frac{\gamma_a - 1}{\gamma_a} M_0^2 \right) \text{FPR}^{\frac{\gamma_a - 1}{\gamma_a}} - 1 \right]} = f(M_0, \text{FPR}) \quad (3.30)$$

This relation is obtained considering the nozzle is adapted, that is the pressure at the exit is equal to the ambient pressure ($p_{3f} = p_{s0}$). It is also possible to compute the velocity ratio β as follows:

$$\beta = \frac{V_{3f}}{V_0} = \frac{M_{3f}}{M_0} \sqrt{\frac{\theta_{3f}}{\theta_0}} = \frac{M_{3f}}{M_0} \sqrt{\text{FPR}^{\frac{\gamma_a - 1}{\eta_f \gamma_a}} \frac{1 + \frac{\gamma_a - 1}{2} M_0^2}{1 + \frac{\gamma_a - 1}{2} M_{3f}^2}} = f(M_0, \text{FPR}) \quad (3.31)$$

η_f being the polytropic efficiency of the fan. If $\eta_f=1$ the compression is isentropic. In practice it is possible to compute the polytropic efficiency with the semiempirical relation [KSM03]:

$$\eta_f = 0.98 - 0.08 (\text{FPR} - 1) \quad (3.32)$$

3. At this stage it is possible to compute the nozzle exit area:

$$\frac{S_{3f}}{S_{ref}} = \frac{c_T}{2} \text{FPR}^{\frac{\gamma_a(1-\eta_f)-1}{\gamma_a \eta_f}} \left(\frac{1 + \frac{\gamma_a - 1}{2} M_0^2}{1 + \frac{\gamma_a - 1}{2} M_{3f}^2} \right)^{\frac{1}{\gamma_a - 1}} \frac{1}{\beta^2 - \beta} = f(M_0, \text{FPR}, c_T) \quad (3.33)$$

Finally, supposing the section circular, it is possible to deduce the exit diameter:

$$D_{3_f} = 2\sqrt{\frac{A_{3_f}}{\pi}} \quad (3.34)$$

4. At this step it is possible to compute the mass flow and then the power required by the fan. The required mass flow which enters the fan is:

$$\dot{m} = p_{3_f} M_{3_f} S_{3_f} \sqrt{\frac{\gamma_a}{R\theta_{3_f}}} = p_{3_f} M_{3_f} S_{3_f} \sqrt{\frac{\gamma_a}{R\theta_{t_{3_f}}}} \left(1 + \frac{\gamma_a - 1}{2} M_{3_f}^2\right)^{\frac{1+\gamma_a}{2(1-\gamma_a)}} \quad (3.35)$$

with $p_{t_{3_f}} = p_{t_0} \text{FPR}$ from the fan pressure ratio definition and $T_{t_{3_f}} = T_{t_0} \text{FPR}^{\frac{\gamma_a-1}{\gamma_a}}$.

The total enthalpy variation is then

$$\Delta h = c_p(\theta_{t_{3_f}} - \theta_{t_0}) = \frac{\gamma_a R}{\gamma_a - 1} \theta_{t_0} \left(\text{FPR}^{\frac{\gamma_a-1}{\gamma_a}} - 1\right) \quad (3.36)$$

and finally the power required by the fan is

$$P_f = \Delta h \dot{m} \quad (3.37)$$

5. It is finally possible to compute the fan area. For aerodynamic reasons, the Mach number at the fan section is fixed to a maximum value of 0.65 ($M_f = 0.65$); the fan area results to be

$$S_f = \frac{\dot{m}}{p_{t_0} M_f \sqrt{\frac{\gamma_a}{R\theta_{t_0}}} \left(1 + \frac{\gamma_a-1}{2} M_f^2\right)^{\frac{1+\gamma_a}{2(1-\gamma_a)}}} \quad (3.38)$$

Fan radius is obtained from the ratio between the tip and the hub radius σ :

$$r_f = \sqrt{\frac{S_f}{\pi(1 - \sigma_f^2)}} \quad (3.39)$$

The parameter σ_f depends on the technological level; at today, reasonable value based on commercial engines is between 25-30% [Rou07].

Note from Eq. (3.32) that the fan efficiency solely depends on the FPR: the lower, the more efficient is the fan, in agreement with what has been explained earlier concerning the power required. For high values of FPR the power demanded to achieve a given c_T increases; on the other hand, the fan size decreases, with a consequent improvement of the aerodynamics due to lower wetted surface. The tradeoff between size and power as function of FPR is shown in Fig. 3.9, for $c_T = 9.86 \times 10^{-2}$, $M_0 = 0.78$ and $h=35000$ ft.

Another interpretation of η_f can be given introducing the ratio between total pressure

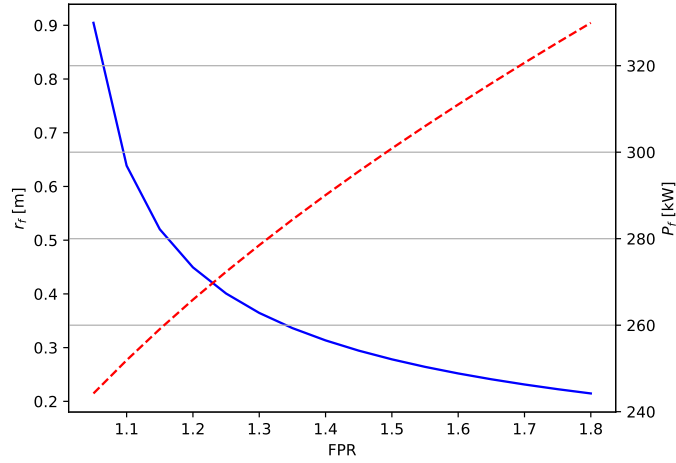


Figure 3.9: Fan radius (in blue) and required power (dashed line) as function of FPR, $c_T = 9.86 \times 10^{-2}$, $M_0 = 0.78$ and $h=35000$ ft.

and total temperature through the fan:

$$\frac{\theta_{t_{3f}}}{\theta_{t_0}} = \left(\frac{p_{t_{3f}}}{p_{t_0}} \right)^{\frac{\gamma_a - 1}{\gamma_a \eta_f}} \quad (3.40)$$

The relation described by Eq. (3.40) shows that at the fan section there is a loss of total quantities related to the polytropic transformation, which becomes more and more relevant when η_f decreases. Of course, if total quantities are lower, the energy produced is smaller and then the power required needs to be higher to keep c_T constant.

The fan size cannot prescind by local flow; the velocity at tip blade must never exceed a certain value, for aerodynamic considerations. The maximum allowable speed at the tip is not constant but depends also on the FPR; Fig. 3.10 shows the feasible design domain for this variable, indicated as V_{tip} . In case the point lies in the shaded region, which is a non feasible domain, FPR and σ_f are the variables on which it is possible to act to have proper design.

Finally, other two relevant parameters are the rotational speed Ω and the torque Θ , that can be computed as follow:

$$\Omega_f = \frac{V_{tip}}{r_f} \frac{60}{2\pi} \quad (3.41a)$$

$$\Theta_f = \frac{P_f}{\Omega_f \frac{2\pi}{60}} \quad (3.41b)$$

The units are revolution per minute for the rotational speed and Newton-second for the torque.

The process just described has an estimated error of less than 10% on the power demanded.

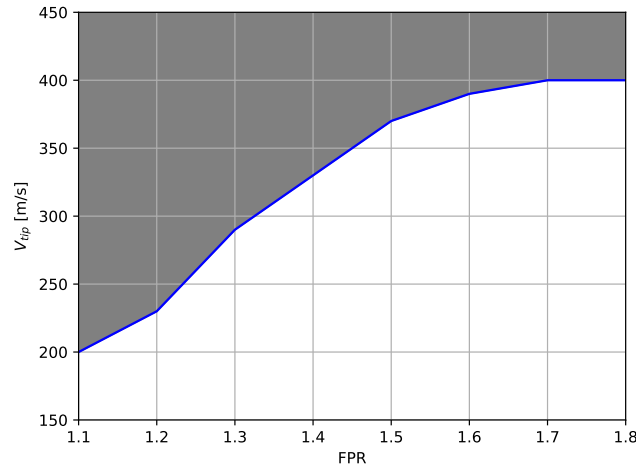


Figure 3.10: Allowable region for the velocity at the tip of fan blade. The shaded region represents a non feasible space.

As a design point, the first cruise point is the best choice. Generally the cruise is the longest segment, and thus it is good practice to have the fan adapted for that condition; the first point is also the point in which aircraft is heavier, and then it is the most stringent. In case of off design conditions, a different value of FPR which provides the same S_{3_f} has to be found. In practice, FPR variation corresponds to a different rotational speed on a real fixed-pitch fan.

3.3.9 Certification constraint module

A discussion about a new propulsive system can not avoid an overview of failure cases. Albeit the CS-25 do not include yet any rule regarding hybrid/electric aircraft, some assumptions need to be made, at least to justify the design choices and reduce risks related to the concept.

The starting point is the CS-25 [EAS17] certification and the CATPOL [EAS12] document for aircraft operations, summed up in Table 2.3. The CAT.POL.410(a)-1 and 2, as well as the CS-25.119(a) and CS-25.121(d) consider the All Engine Operative condition, and thus can be retained as they are. Issues arise with the others, where the One Engine Inoperative condition must be replaced by something different. In particular, in an hybrid architecture there are two possible scenarios to consider:

1. Electric ore failure, which corresponds to a certain number of electric motors inoperative. This condition, however, does not impact the total amount of power delivered, which is still the same.
2. One power source failure, which corresponds to a loss of total power available and, as a consequence, of thrust.

In the first case, there is no loss of power, but this power must be redistributed among the remaining motors working, computed from Eq. (3.19). So this condition, that from now on is indicated with the acronym of OCI (One Core Inoperative), defines the maximum level of power that all the components must supply in case of electric core failure, and it is then the sizing condition for the components, starting from the electric core up to electric motors.

On the contrary, the second condition corresponds to a loss of power, that is a loss of thrust available, and since the aircraft must comply with the certification the power sources must be oversized, to satisfy the certification constraint. So this condition is the sizing one for the components before the electric bus.

However, it is to note that a simultaneous failure of a gas turbine and a battery is an extremely rare case because of the high efficiency of these elements. Also, thanks to the power management adopted, see Eq. (3.2), there is a certain margin of safety in case of one power source failure, since the other one can be used. Then, in this research the OEI condition from Table 2.3 is simply replaced by a OCI, to properly find the required level of power for the electric components. This is not valid for all the hybrid configurations, but only for double source power; in case hybridization is obtained by fuel cell or gas turbine, both the failure conditions must be considered.

From previous studies, it emerges that among the three rules that consider a failure, the most critical is the CS-25.121(b) [HRD16]: indeed, in this condition the blowing has a strong impact, and the associate drag reduces the LoD ratio. To keep the desired slope, more thrust is needed, as also shown by Eq. (2.18), which explains the criticism associated to this requirement. For this reason, the condition of electric core failure at 400 ft is retained as sizing condition for the electric chain.

From Eq. (2.18) it is possible to estimate the minimum thrust needed for each fan to maintain the 2.4% of slope ($100 \tan \gamma_{400} = 2.4$) as

$$T_{400} = m_{400}g \left[0.024 + \frac{1}{\left(\frac{L}{D}\right)} \right] \frac{N_{core}}{N_{core} - 1} N_{EM} \quad (3.42)$$

where m_{400} represents the aircraft mass at 400 ft, in the condition of interest. Corresponding power to generate required thrust P_{400} is obtained from the fan model. The maximum powers to use in the sizing of electric components are then:

$$P_{EM_{max}} = \frac{P_{400}}{\eta_{EM}} \quad (3.43a)$$

$$P_{IC_{max}} = \frac{P_{400}}{\eta_{EM}\eta_{IC}\eta_{IC}} \quad (3.43b)$$

$$P_{core_{max}} = \frac{P_{400}}{\eta_{EM}\eta_{IC}\eta_{IC}\eta_{core}} \quad (3.43c)$$

Finally, since at 400 ft the aircraft must fly fully electric, P_{400} defines also the reference power to use in the battery constraint of Eq. (3.9b):

$$P_{b_{ref}} = \frac{P_{core_{max}}}{\eta_{core}\eta_{IC}\eta_b} \quad (3.44)$$

It is worth noting that the specifications applied here are related to a twin-engine aircraft, but they are different for a three or four-engine aircraft. However, since there are no indications about the rules to follow for a distributed propulsion, where the propulsive system is different from the conventional one, it has been decided to keep the same rules as in Table 2.3 since the proposed concept is in the same category as the Airbus A320, but future developments must include new specifications for hybrid aircraft.

This last remark concludes the overview on the hybrid chain; next section describes first the new MDA tailored for the proposed concept, based on the models just described, and then the resulting MDO formulation.

3.4 Methodology for the sizing of hybrid aircraft

3.4.1 MDA sizing loop

The resulting MDA loop for the hybrid electric aircraft here considered is shown in Fig. 3.11, with the detailed algorithm reported in Alg. 6. The impact of hybrid architecture on the overall loop is small: the main difference with respect to the diagram of Fig. 2.1 lies in step 2, where a new analysis is added to size the battery with respect to power and energy requirements, as described by Eq. (3.9a) and Eq. (3.9b). Similarly to wing area, it gets two values of battery volume, each one satisfying the two equality requirements, and then it takes the maximum between the two. At first step, where no information on the energy consumption are known, the battery volume is initialised with respect to the reference power in the initiator analysis.

Going deeper into the analysis, the major impacts of hybrid propulsion are in step 4 to 8. The geometry calculation needs to consider the new elements of the hybrid chain: the wetted surface is greater because of the nacelle used to contain the electric motors on the upper wing and the gas turbine nacelles at the rear. The last contribution is easily computed by knowing the overall gas turbine dimensions:

$$S_{GT_{wet}} = N_{GT}2\pi(r_{GT}L_{GT} + 1.05r_{GT}L_{GT}) \quad (3.45)$$

The first term of Eq. (3.45) represents the internal wetted surface, meanwhile the second one is the external one. The fairing thickness is assumed to be 5% of the gas turbine radius, in agreement with data on existing engines [Rou07].

For the ducted fans nacelle wetted surface the estimation is similar, a scheme of the contributions is given in Fig. 3.12. Nacelle internal surface only accounts in the wetted surface

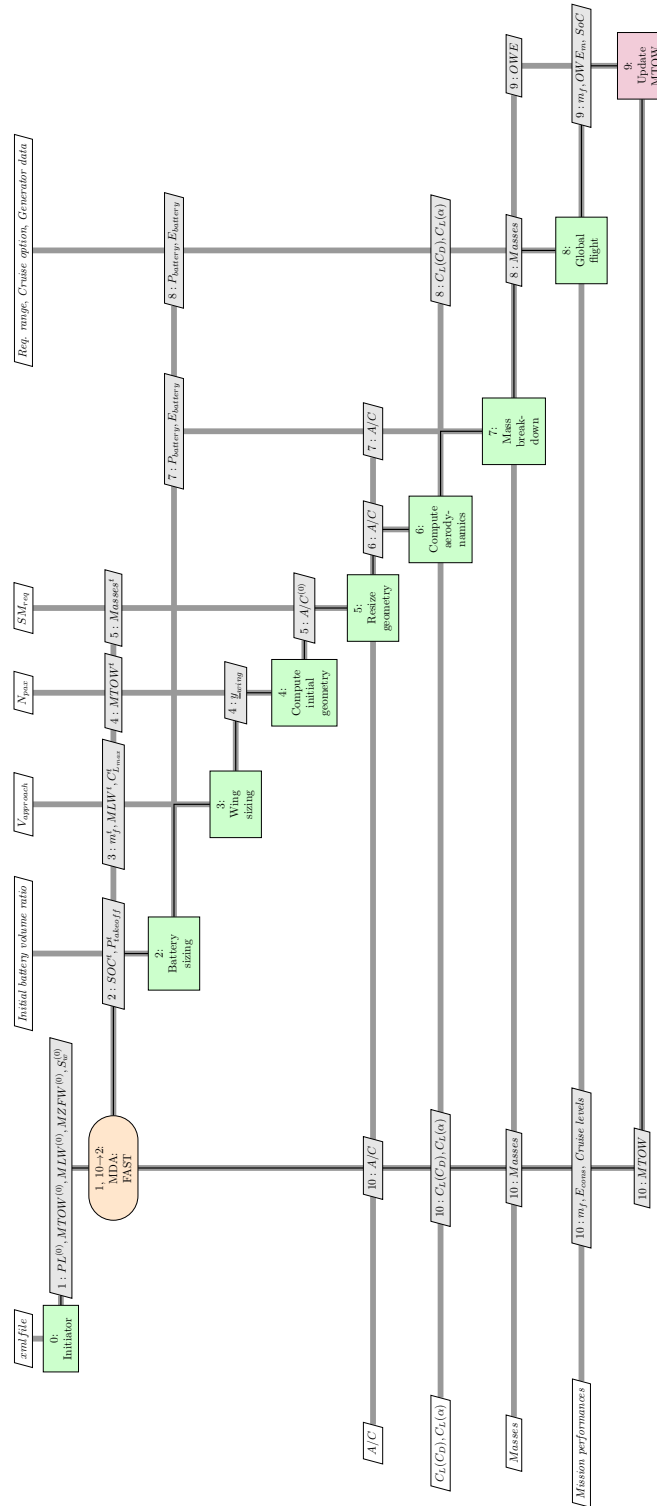


Figure 3.11: FAST xDSM scheme for the version tailored to hybrid aircraft featuring distributed electric propulsion, shown in Fig. 3.2.

Algorithm 6 FAST algorithm for the sizing of hybrid aircraft featuring distributed electric propulsion; numbering is referred to xDSM of Fig. 3.11

Require: TLAR

Ensure: Sized aircraft, drag polars, masses, design mission trajectory

0: Initialise the OAD parameters, according to rules contained in Airbus and ISAE handbook [DC12].

repeat

1: Initialise the loop.

2: Size the battery, according to Eq. (3.9a) and Eq. (3.9b).

3: Compute the wing surface, in order to respect Eq. (2.8) and Eq. (2.9).

4: Compute initial geometry.

5: Resize the geometry, to match stability constraints.

6: Aerodynamics calculation.

7: Mass breakdown calculation. The standard AR 2001/D [DGA84] is modified to include electric components.

8: Trajectory analysis. At the end, together with the fuel consumption, this analysis gives in output also the total energy consumption and the final battery SoC.

9: Update the MTOW.

10: Check if the convergence criteria is satisfied; if not, proceed to next iteration. Beside the criteria on OWE of Eq. (2.3), the condition on the state of charge described by Eq. (3.9a) is added to ensure convergence.

until 10 → 1: MDA has converged

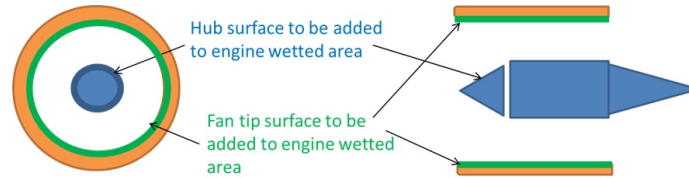


Figure 3.12: Scheme of ducted fan for the wetted surface estimation.

calculations, being the external surface contribution already included in the wing wetted area estimation, as visible in Fig. 3.13. Hub and engine lateral surface must be included, adding a relevant penalty. Motors' contribution is then:

$$S_{EM_{wet}} = N_{EM} 2\pi [r_f L_{EM} + r_h L_{EM}] \quad (3.46)$$

In Eq. (3.46) r_h represents the hub radius, equals to $\sigma_f r_f$ from the definition of σ_f , and the motor length L_{EM} is computed with Eq. (3.15) considering an annular motor. Another relevant aspect in the geometry module is the components' positioning, since they introduce point masses within the airframe, shifting the center of gravity. Table 3.3 reports the location of each electric component in the propulsive scheme considered.

The high speed aerodynamic analysis (step 6) is slightly modified: since the C_D curve is estimated from the wetted surfaces information, in agreement with Eq. (2.11), a proper

Component	CG location
Electric motors	Over the wing, trailing edge
Gas turbines and generators	Approximately 93% of the fuselage length
Batteries	Split in the front and rear cargo
Inverters and converters	In correspondance of the EMs, generators and batteries
Cooling system	In correspondance of the EMs, generators and batteries
Cables	Estimated by their mass distribution in the airframe

Table 3.3: Center of gravity location of the different electric components, belonging to the propulsive system shown in Fig. 3.3.

estimation of wetted surface at step 4 and 5 is the only thing needed to properly estimate the impact on aerodynamics. At low speed, the procedure to get the maximum lift coefficient changes, to consider the blowing effect. This phenomenon is relevant only in the region where electric motors are mounted: referring to Fig. 3.13, the region interested by blowing is the red one. The global maximum lift coefficient can be computed as

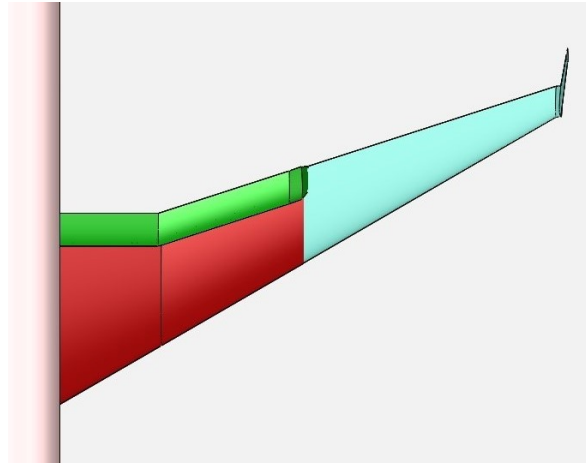


Figure 3.13: Blowing surface visualisation: here the region interested is indicated by the red colour.

$$C_{L_{\max}} = C_{l_{\max}} \frac{S_{\text{blow}}}{S_w} \cos \Lambda_{25_w} \quad (3.47)$$

where $C_{l_{\max}}$ is the maximum local lift coefficient with blowing, S_{blow} the portion of surface interested by blowing and S_w the wing surface, and the factor $\cos \Lambda_{25_w}$ accounts for three-dimensionality effect introduced by sweep [Av59]. Eq. (3.47) indicates that to maximize the blowing effect, the ratio of blown surface over total surface as to be as close as possible to 1, that is the reason why in the NASA X-57 distributed propellers cover all the wingspan [Bor+16].

The mass breakdown module substantially remains the same, except for the fact that section B is enriched of new elements, to include electric components mass, computed as explained in the previous section. The addendum with new elements is described in Table 3.4.

B	Propulsion
B4	Cables
B5	Batteries
B6	gas turbine and generators
B7	Inverters and converters
B8	Cooling system
B9	PMU

Table 3.4: Proposed addendum to mass breakdown standard [DGA84] to include electric components mass.

Finally, performance module is modified to include the presence of two power sources. At each iteration i the engine model gives in output the battery and gas turbine power P_{b_i} and P_{GT_i} (in non balanced flight) or the equivalent power rates δ_{b_i} and δ_{GT_i} (in balanced flight) together with the PSFC. The energy and the fuel consumption are updated:

$$E_{c_{i+1}} = E_{c_i} + P_{b_i} \Delta t \quad (3.48a)$$

$$m_{f_{i+1}} = m_{f_i} + P_{GT_i} (\text{PSFC}) \Delta t \quad (3.48b)$$

With the information of energy and fuel consumption during the time step Δt it is possible to update the values of aircraft mass and battery SoC:

$$SoC_{i+1} = 1 - \frac{\sum_{j=0}^i E_{c_j}}{E_b} = SoC_i - \frac{E_{c_i}}{E_b} \quad (3.49a)$$

$$m_{i+1} = m_{TO} - \sum_{j=0}^i m_{f_j} = m_i - m_{f_i} \quad (3.49b)$$

Note that Eq. (3.49a) is the discrete version of Eq. (3.8).

At takeoff, no rotation is considered anymore, thanks to the blowing that provides enough lift to takeoff in gliding, as *i.e.* the B-52 does. This assumption has been done because rotational qualities can be hardly met in a blowing configuration, but the drawback is that the takeoff field length may result increased compared to an aircraft with same properties that rotates to takeoff. As far as the total length is within the maximum limit given by operational requirements for the category of aircraft [ICA17; dW97] no issues arise for the purpose of this research, but next studies must include detailed aerodynamic studies in takeoff condition to assess the real impact of gliding takeoff. No effects due to a different wing setting at takeoff are foreseen, since it can be assumed that the blowing depends solely on the propulsive features and not the settings; as a consequence neither in cruise any impact is considered.

At this point, the MDA to size the proposed concept is ready, the following step is to integrate it within OpenMDAO to obtain the MDO formulation.

3.4.2 MDO formulation

In practice, the MDO formulation for the hybrid DEP aircraft is obtained by replacing the MDA of Fig. 2.11 with the MDA shown in Fig. 3.11. The architecture is still the MDF, with all the advantages and drawbacks already mentioned in Chapter 2. The resulting xDSM diagram is shown in Fig. 3.14, with the procedure details explained in Algorithm 7.

Algorithm 7 Integrated version of FAST algorithm description. Numbering refers to Fig. 3.14.

Require: Initial design parameters (TLAR), design variables initial vector $\underline{x}^{(0)}$

Ensure: Sized aircraft, drag polars, masses, performance, \underline{x}^*

0: Initialise the optimisation loop: initial values are read from the xml file.

repeat

1: Initialise DEP electric components.

2: Initialise the MDA, used to get a viable aircraft.

repeat

3: Compute the MTOW.

4: Compute the aircraft geometry and perform the mass breakdown, to estimate weight of all components.

5: Compute the static margin.

6: Aerodynamics calculation, based on the same equations of the original version.

7: Compute the aircraft performance.

8: Check the convergence. Criterion is the same of Eq. (2.3).

until 8 \rightarrow 3: MDA has converged

9: Evaluate the objective function. If a gradient based solver is used, this analysis computes also derivatives.

10: Evaluate the design constraints. If a gradient based solver is used, this analysis computes also the derivatives of each constraint.

11: Check if the optimisation has converged. If not, this analysis updates \underline{x} for the next iteration.

until 11 \rightarrow 1: MDO has converged

Similarly to what has been done with the traditional aircraft, some sizing conditions have become design constraints of the problem. In particular, the battery volume τ_b is a design variable, subject to the two constraints of Eq. (3.9a) and Eq. (3.9b). Similarly to the previous case on the wing area sizing, the two inequalities enlarge the design space exploration, and it is up to the optimiser to find the best value of battery volume that minimises the objective function.

Also Eq. (3.42) is rewritten in the following form:

$$\tan \gamma_{400} \simeq \gamma_{400} = \frac{T_{400}}{m_{400}g} \frac{N_{core}}{N_{core} - 1} N_{EM} - \frac{1}{\left(\frac{L}{D}\right)} \geq \frac{2.4}{100} \quad (3.50)$$

with $T_{400} = f(P_{400})$, and P_{400} is added to design variables vector. This equation replaces the

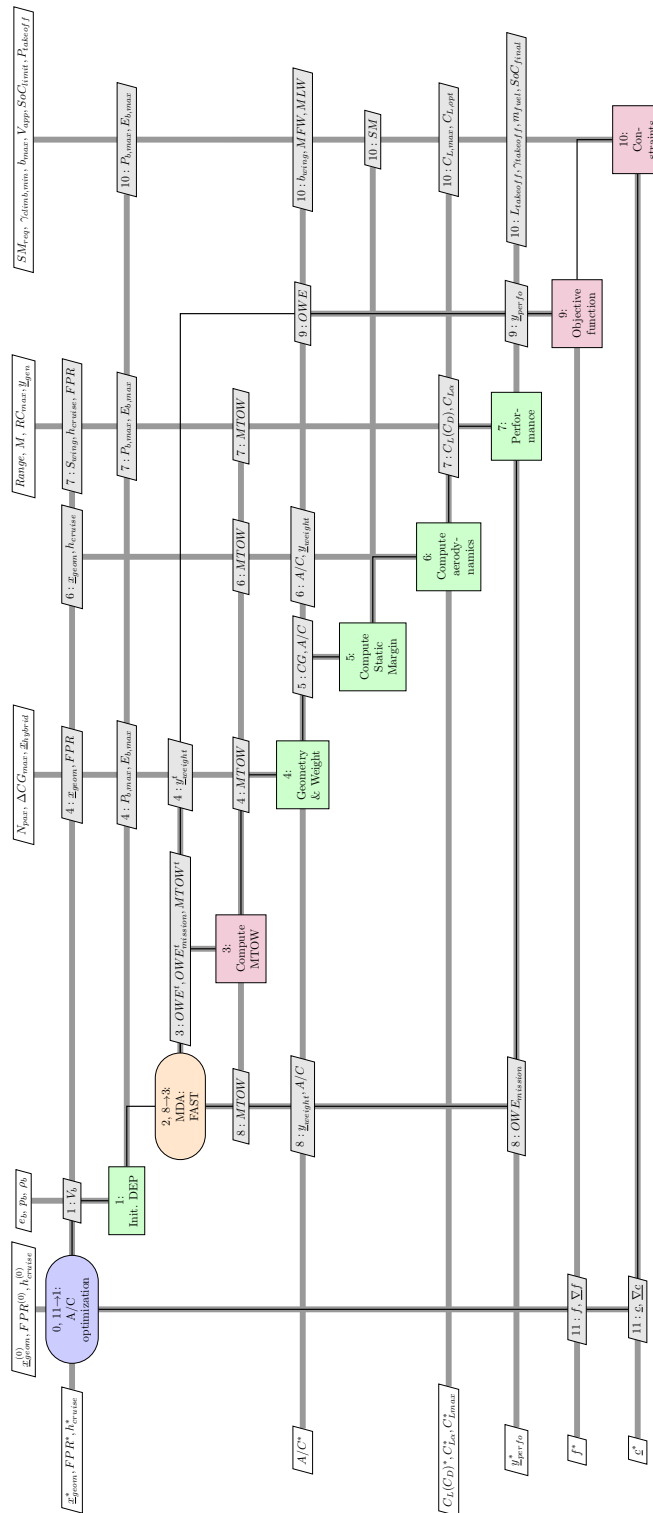


Figure 3.14: xDSM diagram for the integrated version of FAST, tailored to optimisation of hybrid aircraft with distributed electric propulsion.

old one in the CCM, regarding the CS-25.121(b) condition. Other certification specifications and operational requirements are treated in a similar manner.

Note that the variable P_{400} affects the battery design too, through Eq. (3.44).

3.5 Exploration of hybrid aircraft with distributed electric propulsion

3.5.1 2035 technology assessment

One of the main challenges in the design of a hybrid aircraft EIS2035 is to assess the technological characteristics of electric component at that horizon. Indeed, literature review reveals that the perspectives of available technologies in 2035 present large dispersion. As an example, for what concerns batteries, Hepperle [Hep12] proposes a value of e_b equals to 350 Wh kg^{-1} , whereas Bradley [BD12] recommends a value of 750 Wh kg^{-1} . Several authors deal with the problem of defining perspectives [Fra15; Ste+12b; BD15; Hep12; Dev+15; Bro11; Kuh+12; NAE16; Mad+16; Cin+17b; Por+14a] for the key technological parameters, notably the power density and the efficiency; Table 3.5 reports the design space exploration for technologies, according to data found in literature. For sake of clarity, for each parameter are defined also the mean value μ and the coefficient of variation σ^* , defined as the ratio of variance σ and the mean value μ :

$$\sigma^* = \frac{\sigma}{\mu} \quad (3.51)$$

		Min.	Max.	μ	σ^*
e_b	$[\text{Wh kg}^{-1}]$	350	750	550	0.21
ρ_b	$[\text{kg L}^{-1}]$	1.5	2	1.5	0.08
η_b		0.9	0.98	0.94	0.02
p_{GT}	$[\text{kW kg}^{-1}]$	5.5	8.5	7.0	0.12
p_g	$[\text{kW kg}^{-1}]$	12	15	13.5	0.06
η_g		0.85	0.98	0.915	0.04
p_{EM}	$[\text{kW kg}^{-1}]$	8	19	13.5	
η_{EM}		0.95	0.99	0.97	0.01
p_{IC}	$[\text{kW kg}^{-1}]$	15	20	17.5	0.08
η_{IC}		0.9	0.99	0.945	0.03
p_{cs}	$[\text{kW kg}^{-1}]$	1.5	2.5	2	0.14
p_{core}	$[\text{kW kg}^{-1}]$	15	25	20	

Table 3.5: Design space exploration for technological parameters, in 2035 perspectives, according to bibliographic review. In bold the value with biggest uncertainty.

It is evident that the major uncertainty is in the battery energy density e_b (almost 21%).

Note that the battery specific power density p_b is not included: indeed, it depends on

the battery energy density, according to the Ragone plot (see also Fig. 3.4) [Rag68]. Hereby, it is assumed that $p_b = 4e_b$, which seems to be a compromise between energy and power requirement. The gas turbine efficiency is not present too, because it is already included in the GSP model. Last remark on the assumptions concerns the cooling system and the electric core. For these devices, no information have been found in literature; a value with today technology has been estimated from Siemens work [Ant17], and an improvement of 40% is foreseen to define the maximum variation.

In Table 3.12 cables parameters are missing: indeed, they are the only components for which it is certain that no values below the threshold indicated of 2160 V are of interest. A milestone in this study is the CENTRELINE project (see Fig. 1.13), which demonstrates that 2160 V represents the minimum value to have feasible results for aeronautical applications [BSH18], and for this reason this value is adopted. No uncertainty is foreseen because reaching even higher values is challenging. Large scale experimentation has been done in the high-voltage transport, to address its main issues and make it available for civil transport aircraft [Xin+04; Arm+15] in the near future.

Due to the large uncertainty on the technological level, it has been decided to carry out a sensitivity analysis, to understand the impact of these characteristics on the overall design. The impact of technologies is assessed through a sensitivity analysis and results of this simulation are the Sobol indices. These are parameters, varying between 0 and 1, that describe the reduction in variance if a variable i is kept constant. In other word, they quantify the relative importance of each variable on the overall design, at first order. The analysis of these indices help to understand also if there are interaction between variables. If the sum of the first order is equal to one, all the variance is explained and then there are no low order interaction; if it is not the case, the total Sobol indices can be obtained to understand how variables interact each other. Two different cases have been considered:

1. Fixed battery, to estimate also which are the parameters that impact mostly the final battery state of charge SoC_f ;
2. Battery resizing, in order to have $SoC_f=0.20$; in this case batteries are totally discharged and all the possible energy is used.

To perform these analyses, the geometry parameters are the same of the A320 baseline, reported in Table 2.5; the range chosen is 1200 nmi. In particular, since we are interested in the impact of input variables on the overall design, a global sensitivity analysis is performed [SCS00]; indices are estimated considering some key parameters in aircraft design, as energy consumption of empty weight.

The method to obtain Sobol indices is the Polynomial Chaos Expansion PCE [BS10a]. In addition, bootstrap method is applied to assess the validity of results [Dub+14]. This consists in repeating the estimation several times and analysing the mean value and the coefficient of variation of all the estimations. For completeness, a mathematical description of the method is presented in Appendix C.

The design of experiments is created via a latin hypercube sampling technique [Sac+89] and consists of 800 points; among these, 50 are randomly chosen as training set to estimate the error. A linear law for each of parameters in Table 3.5 is considered. Finally, to apply the bootstrap method, a total of 100 repetitions is used.

3.5.1.1 Sensitivity analysis – fixed battery case

The first analysis presented consists in keeping the battery fixed; MDA only makes all the masses converge to a viable aircraft. At the end, the aircraft has not used all the allowable energy by batteries, which may result in a bad sizing due to a useless batteries' oversizing. However, this approach allows to evaluate the parameters that impact the final state of charge, which is an useful information for designers.

Table 3.6 reports the first order Sobol indices mean value, related to OWE m_e , energy consumption E_c and also SoC_f , meanwhile Table 3.7 reports the relative coefficient of variation. In case the mean value is zero, by convention σ^* is replaced by the standard deviation σ ; an asterix superscript identifies the cases in which the convention is applied (leading to $\sigma = 0$ in the present case).

The main contribution to m_e is due to the battery density ρ_b , since it affects the battery's weight (see Eq. (3.10)) and represents the biggest percentage on structure's weight. Other parameters have equivalent contribution, which are in any case much less important. Battery's density is also the main parameter on E_c , but also efficiencies play a role. Recalling Eq. (3.2), they define the power delivered through the energy chain, and energy is directly related to power by time step.

Note that efficiencies have also more importance than the power densities; in other words mass penalties are not important as the power loss due to efficiencies. State of charge is mainly affected by battery's parameters, with e_b showing a greater contribution, as expected since it defines the energy level. Another remarkable result is that coefficient of variation is very large when the effect is not relevant: when the Sobol index is very low, design of experiments strongly affects results. However, since the effect is negligible, this limitation does not create problems in the final analysis. Finally, indices' sum is close to one: no interactions between variables are present.

The validity of PCE approximation is then ensured studying the relative mean square error MSE_r on the validation set. MSE_r is defined as the average squared difference between the estimated values and what is predicted:

$$MSE_r = \frac{1}{m} \sum_{i=0}^m \left(\frac{y_i - \hat{y}_i}{y_i} \right)^2 \quad (3.52)$$

where y_i is the observed values of the variable being predicted, \hat{y}_i its prediction using the PCE and m the sampling dimension, that it is recalled is equal to 100. Mean value and coefficient of variation of these quantities are reported in Table 3.8. The mean value μ is very

	m_e	E_c	SoC_f
e_b	7.74×10^{-2}	6.81×10^{-2}	7.34×10^{-1}
ρ_b	5.42×10^{-1}	2.69×10^{-1}	2.38×10^{-1}
η_b	3.44×10^{-2}	1.49×10^{-2}	1.43×10^{-3}
p_{GT}	9.02×10^{-2}	3.91×10^{-2}	1.66×10^{-3}
p_g	6.21×10^{-3}	2.77×10^{-3}	0
η_g	9.92×10^{-2}	4.29×10^{-2}	3.94×10^{-3}
p_{EM}	5.94×10^{-2}	2.58×10^{-2}	1.37×10^{-3}
η_{EM}	1.32×10^{-2}	1.09×10^{-1}	1.57×10^{-3}
p_{IC}	2.36×10^{-2}	1.01×10^{-2}	4.91×10^{-4}
η_{IC}	1.39×10^{-4}	3.93×10^{-1}	4.05×10^{-4}
p_{cs}	4.82×10^{-2}	2.15×10^{-2}	1.10×10^{-4}
p_{core}	2.82×10^{-5}	9.81×10^{-5}	0
Sum	9.94×10^{-1}	9.96×10^{-1}	9.84×10^{-1}

Table 3.6: Mean first order indices related to key parameters m_e , E_c and SoC_f ; in bold are marked the most relevant parameters. Fixed battery case.

	m_e	E_c	SoC_f
e_b	4.96×10^{-2}	2.37×10^{-1}	5.79×10^{-2}
ρ_b	8.71×10^{-3}	8.59×10^{-2}	1.76×10^{-1}
η_b	2.67×10^{-3}	8.06×10^{-1}	8.73
p_{GT}	4.28×10^{-2}	3.60×10^{-1}	8.03
p_g	2.93×10^{-1}	2.71	0*
η_g	3.63×10^{-3}	3.47×10^{-1}	4.21
p_{EM}	4.93×10^{-2}	5.35×10^{-1}	9.18
η_{EM}	1.60×10^{-1}	1.73×10^{-1}	9.92
p_{IC}	1.06×10^{-1}	1.50	2.28×10
η_{IC}	5.33	5.97×10^{-2}	2.65×10
p_{cs}	6.21×10^{-1}	6.20×10^{-1}	1.27×10
p_{core}	4.57×10^2	1.51×10^2	0*

Table 3.7: Coefficient of variation σ^* of Sobol indices related to key parameters m_e , E_c and SoC_f . Fixed battery case.

small, meanwhile σ^* is several orders of magnitude bigger, as expected recalling its definition. However, the quantity $\mu(1 \pm \sigma^*)$, which represents the limits of variation of MSE, is still under the tolerance of 1%, so validity of results is ensured.

	μ	σ^*
OWE	3.4×10^{-9}	8.24×10^3
E_c	5.0×10^{-6}	1.72×10^2
SoC_f	3.4×10^{-4}	2.43×10

Table 3.8: Mean value and coefficient of variation of MSE on training set for key parameters considered. Fixed battery case.

The importance of each parameter can be also visually seen thanks to a scatter plot, as in Fig. 3.15, which shows the impact of battery parameters over the key output variables. Dominant effects tend to align along a line, as *i.e.* happens in the plot OWE- ρ_b ; also more important is the effect, less wide is the curve. This is indication that the variance is very small. All the scatter plots are reported in Appendix D for completeness.

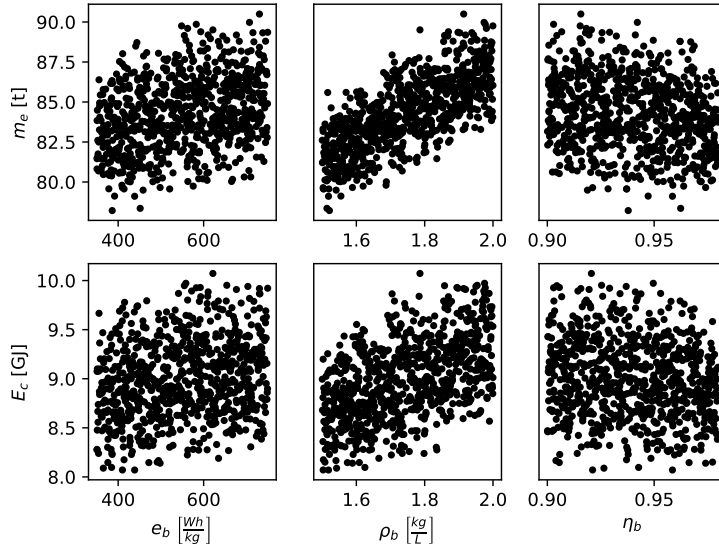


Figure 3.15: Effects on OWE m_e and energy consumption E_c of battery technology parameters. Fixed battery case.

It is also important to remark that battery's energy density e_b does not have any importance on structure and energy consumption. At first glance this is in opposition with what explained in Section 3.3.1, but the reason lies in the fact that geometry is fixed: battery's volume is not changing, and thus a variation in e_b simply affects the energy stored, and as a consequence the final SoC .

3.5.1.2 Sensitivity analysis – battery resizing

This section presents the second analysis, in which battery is included in the sizing loop to obtain $SoC_f = 0.20$. In this case there is no need to carry out an optimisation, since the problem involves only one design variable and it has an analytic solution. Indeed, combining Eq. (3.8) with Eq. (3.3) at final simulation time, the battery volume results to be

$$\tau_b = \frac{E_c}{(1 - SoC_f)\rho_b e_b} \quad (3.53)$$

Table 3.9 reports the Sobol indices, computed starting from the same DoE as before; as

complement, Table 3.10 reports the relative coefficient of variation. To be consistent with the approach used in this case, the variable SoC_f is replaced by the variable τ_b . Scatter plots of the analysis are reported in Appendix D.

	m_e	E_c	τ_b
e_b	9.24×10^{-1}	7.16×10^{-1}	8.01×10^{-1}
ρ_b	0	0	1.91×10^{-1}
η_b	1.19×10^{-2}	9.01×10^{-3}	8.83×10^{-4}
p_{GT}	1.41×10^{-2}	1.07×10^{-2}	2.74×10^{-4}
p_g	5.16×10^{-4}	4.07×10^{-4}	0
η_g	1.83×10^{-2}	1.45×10^{-2}	0
p_{EM}	8.90×10^{-3}	6.41×10^{-3}	3.06×10^{-4}
η_{EM}	1.47×10^{-3}	4.40×10^{-2}	0
p_{IC}	4.81×10^{-3}	4.14×10^{-3}	0
η_{IC}	0	1.82×10^{-1}	0
p_{cs}	1.25×10^{-2}	9.53×10^{-3}	0
p_{core}	4.82×10^{-2}	6.73×10^{-2}	0
Sum	9.94×10^{-1}	9.96×10^{-1}	9.83×10^{-1}

Table 3.9: Mean first order indices related to key parameters m_e , E_c and τ_b ; in bold are marked the most relevant parameters. Battery resizing case.

	m_e	E_c	τ_b
e_b	4.41×10^{-2}	4.98×10^{-2}	6.45×10^{-2}
ρ_b	0*	0*	2.44×10
η_b	2.56×10^{-2}	2.93	1.91×10
p_{GT}	1.95	1.99	3.64×10
p_g	2.03×10	2.95×10	0*
η_g	1.47	1.68	0*
p_{EM}	2.82	3.36	3.37×10
η_{EM}	1.05×10	8.12×10^{-1}	0*
p_{IC}	4.56	4.64	0*
η_{IC}	0*	2.39×10^{-1}	0*
p_{cs}	2.09	2.38	0*
p_{core}	6.74×10^{-2}	6.19×10^{-1}	0*

Table 3.10: Coefficient of variation σ^* of Sobol indices related to key parameters m_e , E_c and τ_b . Battery resizing case.

The first thing to note with respect to previous results of Table 3.6 is that, due to energy requirements, e_b becomes the most important parameter to impact masses and energy; there is still a contribution due to the efficiency of converters and inverters, but its importance is lower than in previous analysis. The most remarkable result is that the battery's density ρ_b , that in an off-design approach was the main player, now has no impact at all. At first glance, this result may be surprising, but it can be explained replacing the expression of τ_b

from Eq. (3.53) in Eq. (3.10), obtaining:

$$m_b = \frac{1}{e_b} \frac{E_c}{1 - SoC_f}. \quad (3.54)$$

Thus the battery mass does not depend on its density, which explains the index equal to zero.

For what concerns the other parameters, same remarks done in previous case on the coefficients of variation apply here too. Also, no interactions between variables are detected (first order index sum almost equal to one). In this case too, mean square error on training set has been computed, with the values reported in Table 3.11. As in previous case of Table 3.8 the total variation tolerance is under 1%, despite the several orders of magnitude between μ and σ^* , and results can be considered valid.

	μ	σ^*
m_e	5.7×10^{-5}	98.09
E_c	6.1×10^{-5}	91.53
τ_b	4.9×10^{-4}	31.62

Table 3.11: Mean value and coefficient of variation of MSE on training set for key parameters considered. Battery resizing case.

To conclude, the battery is identified as the most critical parameter in the hybrid aircraft design: every improvement done on other parameters is non sensitive as it. Also, e_b is the parameter with significant uncertainty, as shown in Table 3.5; reducing the exploration range for this quantity in the upcoming years will be a main issue to have more accurate design. This exercise also reveals that hybrid aircraft design is such a complex problem that it is not possible to evaluate technologies in off-design conditions, as happens *i.e.* for the mass reduction due to new materials. They need to be evaluated within the design process, since considering or not a single parameter in the design affects results in a significant way. Again, the MDO represents one of the best methods to get these interactions and avoid misleading in the design.

At this stage the impact of design technologies on the overall design has been quantified, and a choice of a technological scenario for the EIS 2035 must be done. The choice, reported in Table 3.12, represents a middle way between the most pessimistic and optimistic scenarios identified in Table 3.5. To note that the value of e_b chosen is, according to some authors, the limit of Li-Ion batteries [Fra15; Dev+15], being the value of 750 Wh kg^{-1} referred to other technologies. Nevertheless, $e_b = 500 \text{ Wh kg}^{-1}$ is the most common value used for design, *e.g.* the work of Brelje and Martins [BM18a] or the work of De Vries et al. [dHV19]. Centracchio et al. [CRI18] showed that $e_b = 500 \text{ Wh kg}^{-1}$ is also the minimum limit to obtain better performance than a reference aircraft, using conventional propulsion. For this reason this value has been used.

For what it concerns the cable's technology, the value of maximum current is in agreement with today's technologies, and the high voltage transport is under experimentation and ready

e_b	500	W h kg ⁻¹
p_b	2	kW kg ⁻¹
ρ_b	1.7	kg L ⁻¹
η_b	0.9	
p_{GT}	9	kW kg ⁻¹
p_g	13.5	kW kg ⁻¹
η_g	0.98	
p_{EM}	13.2	kW kg ⁻¹
η_{EM}	0.99	
p_{IC}	16.4	kW kg ⁻¹
η_{IC}	0.95	
p_{cs}	2	kW kg ⁻¹
p_{core}	20	kW kg ⁻¹
ΔV	2.16	kV
$i_{\max_{cab}}$	320	A
$\left(\frac{m}{L}\right)_{cab}$	1.0	kg m ⁻¹

Table 3.12: Technological parameters chosen for the design of hybrid aircraft, EIS 2035.

soon to enter into service. The other reason why they have not been included in the previous analysis is that the chosen values represent a threshold for non cryogenic technology, and there are no reasons to investigate worse values [Xin+04].

Next sections will present the results of the hybrid design, both without and with optimisation, using the EIS2035 scenario identified in Table 3.12.

3.5.2 Sizing of aircraft with distributed electric propulsion

This section provides results regarding the performance calculation of hybrid aircraft with distributed electric propulsion, using the MDA approach presented in Fig. 3.11. Results are mainly seen as a key to assess the overall procedure before going through the optimisation.

The top level requirements have already been set in Table 3.1, as well as the design parameters for the propulsive system are in Table 3.12. As said, the range is not fixed yet, but it is a parameter to vary, to study different design missions and get a tradeoff. For what it concerns the geometry, the same parameters as the A320 CERAS case of Table 2.5 are used.

At this point, only the number of electric motors, generators, batteries and FPR are missing. The most obvious choice for the turbines is to use two of them, due to the space allocation at the rear. The battery model presented in Sec. 3.3.1 is linear, and thus the number of batteries is relatively not important since everything is scaled. A total of 4 batteries are considered, for space allocation constraint in the cargo. Same considerations can be done for the electric cores. Considering the number of electric motors, it is set to 32 by the time, in arbitrary way; one of the next step coming into the optimisation is to evaluate different

configurations to find also the best value for this quantity. Finally, the FPR is arbitrarily set to 1.2; everything is reported in Table 3.13 for sake of clarity.

Number of electric motors	32
Number of generators	2
Number of batteries	4
Number of PMU	4
FPR	1.2

Table 3.13: Propulsive system top level parameters for the hybrid aircraft with distributed propulsion performance evaluations.

To consider the EIS2035, the assumptions done in Table 2.15 and Table 2.16 must be revised. For what has explained in Sec. 1.3.1.2 distributed propulsion impacts the wing mass positively from one hand because it reduces the bending moment, but negatively from the other hand because the torsion is more important. These two effects do not balance themselves, but the second one results to be dominant; then the wing mass is increased by 5%.

Concerning the aerodynamic improvement, all the hypotheses of Table 2.16 may be retained, with the exception of morphing wing. In fact, the distributed motors do not allow the wing to change its shape, and this benefit is removed. A value of $C_{l_{\max}}$ equals to 4.5 is foreseen because of the blowing on the wing [HRD16; Dee+17b].

The mission profile is defined by the power rates of Eq. (3.1) for each segment. One of the main requirements is that the aircraft have to fly fully electric up to 3000 ft; actually, preliminary results show that the power requirement expressed by Eq. (3.9b) is the sizing one for batteries. As a result, the energy content is so elevate that the entire climb can be carried out in electric mode. Table 3.14 reports the battery and gas turbine power rates for each segment. It is to highlight that they do not change, but they are the same for each configuration and mission analysed. Results for the hybrid configuration are compared with the A320 CERAS baseline test case, EIS2035, already studied in Chapter 2, with key design parameters collected in Table 2.17 and fuel consumption shown in Fig. 2.15.

Performances are evaluated considering three main parameters: the fuel consumption, the energy consumption and the PFEE, defined in Eq. (1.3). Kerosene density and energy content, needed for the energy evaluation, are reported in Table 3.15, according to data found in literature [Edw02].

The figures 3.16 to 3.18 report the comparison between the hybrid concept and the A320 CERAS baseline, on the chosen set of design ranges. Specifically, Fig. 3.16 shows the fuel consumption, Fig. 3.17 the energy consumption and Fig. 3.18 the PFEE. As a complement to these images, Table 3.16 reports the data for the concept, to compare with Table 2.17. The first thing to note is that the hybrid electric aircraft is more performant than the conventional for lower range. Both in Fig. 3.16, Fig. 3.17 and Fig. 3.18 is detected a point starting from which a conventional aircraft shows better performances than the hybrid concept proposed.

Segment	δ_b	δ_{GT}
Taxi	0.1	0
Takeoff	1	0
Climb to 3000 ft	0.9	0
Climb	0.7	0
Cruise	-	Computed
Descent	0	0.1
Alternate climb	0	0.8
Alternate cruise	-	Computed
Alternate descent	-	0.1
Hold	-	Computed
Landing	0.03	0

Table 3.14: Mission profile definition for the hybrid aircraft case, through the battery and gas turbine power rates defined in Eq. (3.1).

Density, ρ_{fuel}	0.785	kg L^{-1}
Energy content, J_{fuel}	34.6	MJ L^{-1}
Specific energy content, h_{fuel}	44.1	MJ kg^{-1}

Table 3.15: Kerosene properties [Edw02].

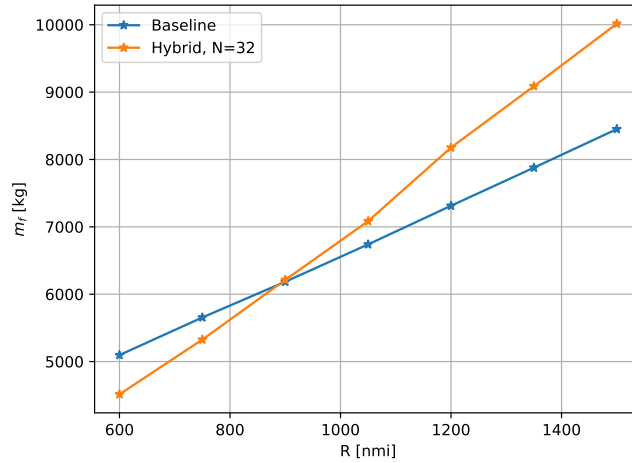


Figure 3.16: Fuel consumption as function of design range, comparison between the baseline and the hybrid aircraft with distributed propulsion.

This effect is due to the presence of batteries. In fact they introduce a relevant penalty in weight, as emerges also from the data in Table 3.16, and heavier aircraft need more thrust, and then fuel, to sustain the cruise.

On small range the cruise segment is shorter and hybrid aircraft can benefit of the reduction in fuel due to the zero emission in climb; to better clarify this point Table 3.17 shows the

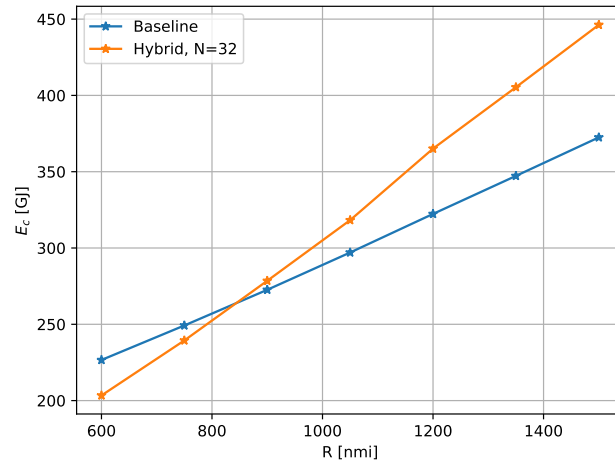


Figure 3.17: Energy consumption as function of design range, comparison between the baseline and the hybrid aircraft with distributed propulsion.

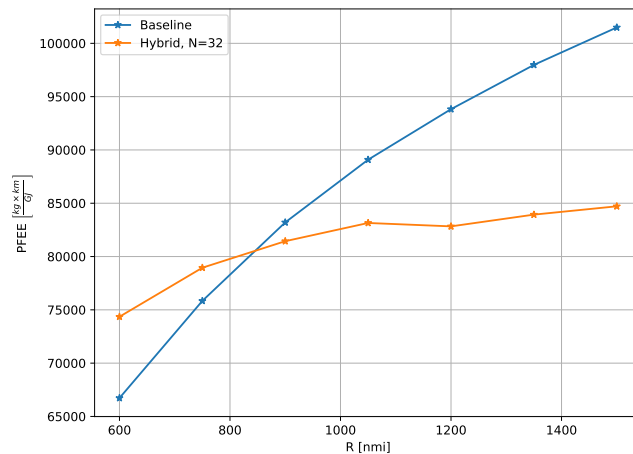


Figure 3.18: PFEE, defined in Eq. (1.3) as function of design range, comparison between the baseline and the hybrid aircraft with distributed propulsion.

fuel breakdown of the two concepts, for the case of $R = 900$ nmi. Due to the greater weight, only in cruise the hybrid aircraft consumes about 2 t more than the conventional aircraft, but this effect is partially mitigated by the save in other phases.

Also, having a look at Table 2.17 and Table 3.16, it comes out that the growth ratio of OWE is bigger in the hybrid aircraft than the conventional, because of the presence of batteries. Their sizing introduces a non linearity, because of “snowball” effect, which in this case is slightly detected between $R = 900$ nmi and $R=1200$ nmi. After 1500 nmi, batteries’ mass diverges so much that it is not possible anymore to get a viable aircraft: in fact, the

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	73.3	76.8	80.9	82.9
OWE	[t]	55.4	57.2	58.2	59.9
Wing area	[m ²]	112.29	115.03	118.0	120.26
Max. LoD		17.07	17.05	17.08	17.09
Battery volume	[m ³]	1.77	1.91	2.06	2.21
Fuel mission	[t]	4.51	6.21	8.18	10.01
Energy consumption	[GJ]	203.37	278.51	365.11	446.25
CAT.POL.A.410(a)-1	[ftmin ⁻¹]	2477.69	2563.84	2682.47	2564.74
CAT.POL.A.410(a)-2	[ftmin ⁻¹]	1934.02	1891.65	1836.72	1825.37
CS-25.119(a)	[%]	13.94	13.61	13.22	13.19
CS-25.121(a)	[%]	6.17	5.99	6.25	5.85
CS-25.121(b)	[%]	5.94	5.74	5.99	5.60
CS-25.121(c)	[%]	6.17	5.99	6.25	5.85
CS-25.121(d)	[%]	15.7	15.62	16.39	16.34

Table 3.16: Quantities of interest for the hybrid aircraft with distributed electric ducted fan, associated to TLAR of Table 3.1, $N_{EM}=32$.

Segment	Conventional	Hybrid
Taxi	294.87	0
Takeoff	51.89	0
Climb	1318.39	0
Cruise	1810.2	3974.84
Descent	157.16	88.2
Alternate mission	910.29	758.85
Holding	1101.44	1268.37

Table 3.17: Fuel breakdown for the R = 900 nmi mission, comparison between the conventional and the hybrid aircraft.

energy requirement grows with the mass, until is not possible to perform the given design mission (see Table 3.14) for lack of demanded power.

The point of intersection, that hereby will be named “breakdown range”, is shifted to the left in case of the energy. In fact, studying only the fuel consumption in hybrid aircraft is misleading, since it excludes the electrical source. Basically, in this case a second term appears in the energy equation, which shifts the energy vs. range curve on the top, and explains why the range breakdown is reduced. In our hypothesis (see Table 3.12), batteries have a specific energy of about 1.8 MJ kg^{-1} , and their weight is about 15 t. Therefore, the energy delivered by batteries is equivalent to about 1.8 t of fuel, which is around the amount of fuel saved in ground and climb.

The PFEE diagram of Fig 3.18 confirms what has been said from the other two figures; note that PFEE varies quadratically with the range. Recalling Eq. (1.3), at numerator the

product of energy and range appears, but the energy depends on the range, explaining the behaviour.

Another consideration can be drawn by Table 3.16 regarding the maximum LoD, which is slightly reduced compared to the conventional aircraft, because of the increased wetted area due to nacelle. However, it is to recall that the baseline mounts a high BPR ratio, which shows bigger wetted surface too, and this mitigates the effect. Note also that, in spite of the heavier aircraft, the wing is smaller than that of the baseline, thanks to the blowing effect which allows to reach a very high value of $C_{L_{max}}$. Aircraft satisfy the revised CS-25 certifications too, with some margin; from Table 3.16 emerges that the most stringent condition is the CS-25.121(b), which is in agreement with what has been said in Sec. 3.3.9.

Before proceeding, a latest analysis has been carried out, varying the number of electric cores from 2 to 16, to show the relevance of the distributed propulsion. In fact, at the lower bound a total of 50% of electric motors is inoperative in OCI condition, as at upper bound this percentage surges to 94%. This reflects in an overall desizing of the electric components; Fig. 3.19 shows this result in relation with the mass of the electric motors. At low N_{core} the desizing is more marked, and reaches an asymptotic value at higher N_{core} , corresponding to the ideal value of no failure.

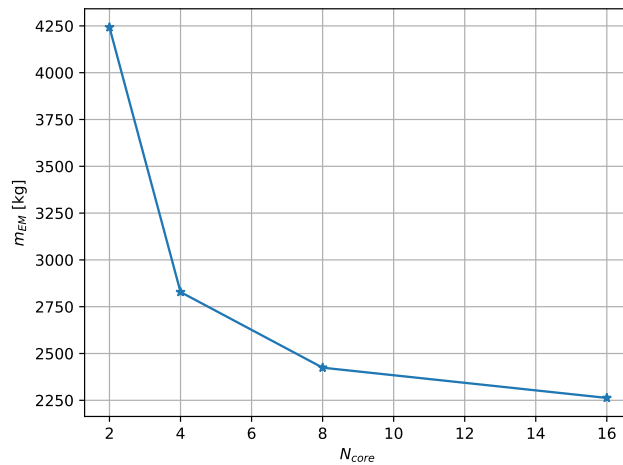


Figure 3.19: Electric motors' mass as function of number of electric cores for the hybrid aircraft concept, $N_{EM} = 32$, $R = 900$ nmi.

To conclude this section, the modified version of FAST that includes new features for hybrid aircraft with distributed propulsion has been assessed, the results being coherent with the expected trend. In literature there are other works that confirm the trend found here [Hep12; Por+14b; SIH13; Ste+12b]. Next section presents the results when this MDA is used in a MDO architecture, using the integrated version of FAST with OpenMDAO.

3.5.3 Optimisation of aircraft with distributed electric propulsion

3.5.3.1 Problem formulation

As done for the conventional aircraft, at first the problem formulation must be defined. Substantially, it does not differ from the optimisation problem of a conventional aircraft, reported in Table 2.9; nonetheless, some minor modifications are done, listed in the following.

- Beside the fuel consumption, it is of interest to consider also energy consumption or weighted function between m_e and E_c as objective;
- The bounds of wing position and vertical tails parameters have been changed, to account for the T-tail configuration.
- In a similar manner for the wing area design, the battery's volume τ_b is now contained in the design variables vector. Two new constraints on the final state of charge SoC_f and the battery power $\Delta P_b = N_b P_b - P_{400}$ have been added, in agreement with Eq. (3.9a) and Eq. (3.9b);
- Instead of computing the sizing power P_{400} from Eq. (3.50), this quantity is a design variable, and varies in order to comply with the CCM specifications, contained in the vector \underline{c}_{CCM} ;
- Scaling factor for gas turbine k_{GT} , defined in Eq. (3.12), as well as FPR are added to design variables vector;
- To have a feasible design, the electric motors must fit on the wing. At this purpose, the quantity $\Delta l_{nac} = L_{nac} - (b_w - w_f)$ is defined, where L_{nac} is the nacelle length, b_w the wing span and w_f the fuselage width. Note that $(b_w - w_f)$ is the usable space for electric motors, that may not be in the fuselage part. As it is defined, this quantity must be lower than 0 to ensure electric motors fit on the allowable space $\Delta l_{nac} \leq 0$.
- Latest, since the FPR is varying, it must be avoided the case of electric motors too big, which may lead to structural problem. It is not easy to define a proper maximum dimension for r_f , but having a look at the paper of Wick et al. [Wic+15] a rough estimation of the allowable fan radius to chord ratio $\bar{r}_f = \frac{r_f}{c}$ can be drawn. A reasonable threshold for this parameter is 0.15, that is the fan radius must not exceed the 15% of the mean aerodynamic chord. Thus the design constraint $\bar{r}_f \leq 0.15$ is added.

The problem formulation, with this addition just described, is reported in Table 3.18. It consists of a total of 21 design variables with associated bound constraints, 2 equality constraints and 15 inequality constraints.

Instead of directly run the optimisation problem, a sensitivity analysis is carried out first. This study helps to understand the impact of geometrical variables on the overall design, for this unconventional configuration, and eventually to reduce the problem size, in case some design variables result not relevant.

Category	Name	Size	Lower	Upper	Equals	Units	
Objective	$f(x)$	1	–	–	–	–	
Variables	S_w	1	100	150	–	m ²	
	x_w	1	18	24	–	m	
	AR_w	1	8	12	–	–	
	λ_w	1	0.2	0.6	–	–	
	Λ_{25_w}	1	20	45	–	deg	
	$(\frac{t}{c})_w$	1	0.1	0.15	–	–	
	S_{HT}	1	20	80	–	m ²	
	AR_{HT}	1	2	5	–	–	
	λ_{HT}	1	0.2	0.6	–	–	
	$\Lambda_{25_{HT}}$	1	20	45	–	deg	
	$(\frac{t}{c})_{HT}$	1	0.1	0.15	–	–	
	S_{VT}	1	15	50	–	m ²	
	AR_{VT}	1	1	2.5	–	–	
	λ_{VT}	1	0.85	1.0	–	–	
	$\Lambda_{25_{VT}}$	1	25	55	–	deg	
	$(\frac{t}{c})_{VT}$	1	0.13	0.18	–	–	
	k_{GT}	1	0.5	1.5	–	–	
	P_{400}	1	6	15	–	MW	
	τ_b	1	1.5	3	–	m ³	
	FPR	1	1.05	1.4	–	–	
	h_{toc}	1	30 000	40 000	–	ft	
	Total	21					
Constraints	Δm_f	1	0	–	–	kg	
	$\Delta C_{L_{app}}$	1	0	–	–	–	
	b_w	1	–	36	–	m	
	$\mathcal{M}_{takeoff}$	1	–	0	–	N m	
	$\Delta \mathcal{N}_{cruise}$	1	0	–	–	N m	
	ΔP_b	1	0	–	–	W	
	Δl_{nac}	1	–	0	–	m	
	\bar{r}_f	1	–	0.15	–	–	
	TOFL	1	–	2200	–	m	
	SM	1	0.05	0.10	–	–	
	$\tan \gamma_{400}$	1	0.024	–	–	–	
	\underline{c}_{CCM}	5	0	–	–	%	
	SoC_f	1	–	–	0.20	–	
	$\Delta C_{L_{toc}}$	1	–	–	0	–	
		Total	17				

Table 3.18: Optimisation problem definition for the hybrid aircraft with distributed propulsion case.

3.5.3.2 Sensitivity analysis

The sensitivity analysis is performed using the PCE method, already applied for the technological sensitivity analysis presented in Sec. 3.5.1. The main goal of this study is to understand how the parameters impact the design and eventually reduce the problem's size. For this reason not all the design variables of Table 3.18 are considered. Wing, tails surface and wing position are not taken into account, since in any case they cannot be removed from the problem. Instead, they are fixed to a constant value. Also, in order to have comparable results, τ_b is resized according to Eq. (3.53) to always have the same final state of charge, recalled to be equal to 0.20. Battery volume is then treated as a model output instead of input. For all the other variables, the same design space defined in Table 3.18 is considered. The configuration chosen for the sensitivity corresponds to $R = 900$ nmi and $N_{EM} = 32$.

The design of experiments consists of 800 points, whereas 750 belong to the training set, and the remaining to the validation set. Sobol indices are computed for the most relevant parameters in performance evaluation, and aircraft design in general: the energy consumption E_c , which replaces the fuel consumption to consider also the electric power generated, the OWE m_e , the maximum LoD value $\left(\frac{L}{D}\right)_{\max}$, the static margin SM and, for what just described, the battery volume τ_b .

Table 3.19 presents first order Sobol indices mean value μ , meanwhile Table 3.20 reports the relative coefficients of variation. Once more, an asterisk indicates the case in which σ^* is replaced by its variance, being the mean value μ equals to zero. Scatter plots of this analysis are reported in Appendix D.

	E_c	τ_b	m_e	$\left(\frac{L}{D}\right)_{\max}$	SM
AR_w	7.53×10^{-1}	3.41×10^{-2}	4.37×10^{-3}	6.02×10^{-1}	3.99×10^{-3}
λ_w	2.58×10^{-3}	6.28×10^{-4}	3.83×10^{-4}	7.47×10^{-4}	2.14×10^{-2}
$\left(\frac{t}{c}\right)_w$	0	7.49×10^{-3}	1.29×10^{-2}	4.98×10^{-3}	5.34×10^{-3}
Λ_{25_w}	1.02×10^{-1}	1.85×10^{-2}	7.33×10^{-3}	2.95×10^{-2}	2.43×10^{-1}
AR_{HT}	1.37×10^{-3}	2.73×10^{-4}	4.66×10^{-4}	5.03×10^{-4}	5.61×10^{-1}
λ_{HT}	0	0	0	1.06×10^{-4}	0
$\left(\frac{t}{c}\right)_{HT}$	8.77×10^{-4}	0	0	5.81×10^{-4}	1.21×10^{-4}
$\Lambda_{25_{HT}}$	2.50×10^{-3}	1.02×10^{-5}	2.37×10^{-5}	1.73×10^{-3}	1.19×10^{-1}
AR_{VT}	0	9.23×10^{-6}	4.94×10^{-5}	5.01×10^{-5}	3.22×10^{-4}
λ_{VT}	4.16×10^{-6}	5.13×10^{-6}	5.93×10^{-6}	0	0
$\left(\frac{t}{c}\right)_{VT}$	0	0	0	3.06×10^{-5}	0
$\Lambda_{25_{VT}}$	1.27×10^{-3}	0	5.43×10^{-4}	3.04×10^{-4}	6.41×10^{-3}
FPR	1.26×10^{-1}	9.31×10^{-1}	9.65×10^{-1}	3.57×10^{-1}	2.06×10^{-2}
Sum	9.88×10^{-1}	9.92×10^{-1}	9.92×10^{-1}	9.97×10^{-1}	9.82×10^{-1}

Table 3.19: First order Sobol indices mean value μ key output variables with respect to inputs, hybrid distributed propulsion case. Most relevant parameters for each output are written in bold.

	E_c	τ_b	m_e	$\left(\frac{L}{D}\right)_{\max}$	SM
AR_w	6.62×10^{-2}	8.65×10^{-1}	4.13	5.18×10^{-2}	1.67
λ_w	5.96	2.22×10	4.10×10	8.12	5.78×10^{-1}
$\left(\frac{t}{c}\right)_w$	0*	2.84	1.71	1.90	1.33
Λ_{25_w}	4.01×10^{-1}	1.71	3.37	5.47×10^{-1}	8.66×10^{-2}
AR_{HT}	1.02×10	5.96×10	2.19×10	1.18×10	4.01×10^{-2}
λ_{HT}	0*	0*	0*	0*	2.38×10
$\left(\frac{t}{c}\right)_{HT}$	1.33×10	0*	0*	1.04×10	0*
$\Lambda_{25_{HT}}$	6.05	7.48×10^2	3.51×10^2	3.97	1.31×10^{-1}
AR_{VT}	0*	7.30×10^2	1.99×10^2	6.19×10	1.19×10
λ_{VT}	1.34×10^3	1.17×10^3	1.08×10^3	0*	0*
$\left(\frac{t}{c}\right)_{VT}$	0*	0*	0*	9.09×10	0*
$\Lambda_{25_{VT}}$	1.01×10	0*	2.39×10	1.41×10	1.32
FPR	3.68×10^{-1}	6.72×10^{-2}	4.89×10^{-2}	8.80×10^{-2}	5.61×10^{-1}

Table 3.20: First order Sobol indices coefficient of variation σ^* for key output variables, with respect to inputs, hybrid distributed propulsion aircraft case. An asterisk identifies the case in which the mean value μ is zero and σ^* is replaced by convention with its variance σ .

The first thing to note is that the energy consumption is mainly affected by two parameters: wing aspect ratio and FPR. The effect is quite intuitive, since wing aspect ratio is the main parameter for the LoD through Eq. (2.12), as can be seen also from the Sobol index equals to 0.753, but the FPR contributed to the aerodynamics (index equals to 0.126) since it defines the fan size (see Fig. 3.9), and so the wetted surfaces due to nacelle. Secondly, the FPR defines also the propulsive efficiency, and then the thrust/power requirement. It is to note that also the wing sweep plays a role on the energy consumption. Unlikely from what expected, this is not due to an aerodynamic effect (its contribution to maximum LoD is not relevant), but in the first phases of flight it impacts the $C_{L_{\max}}$, because of the three-dimensionality [Av59], as expressed by Eq. (3.47). A reduction in Λ_{25_w} results in a reduced $C_{L_{\max}}$, and then more thrust is needed at takeoff configuration to start climbing. Viceversa, and increase of Λ_{25_w} leads to an higher $C_{L_{\max}}$, which reduces the thrust requirement, saving energy.

FPR accounts for more than 90% in the battery sizing. In fact, since it regulates the thrust/power through the propulsive efficiency, it sizes the energy requirement for the battery. The same contribution appears on OWE, since the batteries represent the biggest percentage of OWE, with a weight that overcomes 15 t.

The horizontal and vertical tails geometries seem to not have any relevant effect. It is strictly related to the models used in FAST, that are simplified. Aerodynamics and masses depend on very few set of parameters, sometimes linearly, and as a result parameters like taper ratio or thickness-to-chord ratio have small or no impact on overall design. More refined model may include other dependencies, with the results that parameters here neglected can have a non negligible impact.

Still HT parameters have a main role in the static margin definition, since they impact the neutral point and as consequence stability [And12] (see Eq. (2.7)). The same effect can be expected from the wing aspect ratio, which affects the wing lift slope and then the neutral point, but this is not the case since in the chosen range the variation of this quantity is small compared to variation of HT lift slope.

From the analysis of the coefficients of variation reported in Table 3.20 emerges that σ^* tends to diverge when the mean value is close to zero (see *i.e.* the values of μ and σ^* for the maximum lift-to-drag ratio with respect to VT taper ratio). Recalling the definition $\sigma^* = \sigma/\mu$, the result is coherent; its statistical interpretation is that when the mean value is small, it is difficult to properly estimate the variance, and thus the dispersion is high. However, it does not present any issue since the associated parameters are not relevant, and reducing the variance is not of interest in the present case. Robustness is assured by the quantity $\mu(1 \pm \sigma^*)$, that defines the range of variation with a confidence interval of 68%, which is small in all cases.

Finally, Table 3.21 contains the MSE mean values and coefficients of variation for output parameters. As noted for the previous case, σ^* tends to diverge when μ is very small, as it is natural. In any case, $\mu(1 \pm \sigma^*)$ is always below the 1% tolerance, and thus the PCE approximation is considered reliable and the results validated.

	μ	σ^*
E_c	5.03×10^{-5}	5.83×10^{-1}
τ_b	3.64×10^{-4}	2.38×10^{-1}
m_e	4.93×10^{-5}	6.74×10^{-1}
$\left(\frac{L}{D}\right)_{max}$	6.16×10^{-7}	6.25×10^{-1}
SM	1.91×10^{-4}	3.26×10^{-1}

Table 3.21: Mean value μ and coefficient of variation σ^* of the relative MSE on validation set for the sensitivity analysis of Table 3.19.

This exercise, beyond helping to understand the effect of each parameter on the overall design, allows to reduce the problem size. Wing taper ratio λ_w , HT taper ratio λ_{HT} , thickness to chord ratio $(t/c)_{HT}$ and the four vertical tail variables are not as relevant as other parameters and can be considered constant during the optimisation process. A reduction in the problem size is reflected on the computational cost, both in the cases in which the solver is using or not the gradients. In that way the size of \underline{x} is reduced from 20 to 13 (about 35%).

Next sections present the result of different optimisation problems, varying the objective function and the configuration (variation of number of electric motors).

3.5.3.3 Mono-objective optimisation

To solve the optimisation problem the same set up reported in Table 2.10 is used also here for the hybrid aircraft case, always considering 10 different initial points. It may be of interest to include the number of electric motors in the problem; unfortunately they are discrete and no suitable algorithms that deal with discrete variables is available in OpenMDAO [Bel+13]. Thus, three different configurations have been analysed, varying the number of electric motors from 16 to 48, to consider distributed propulsion impact. The set up is the same used for the optimisation of the A320 CERAS test case and reported in Table 2.10. It is recalled that the gradient-based algorithm is SNOPT [GMS05], with direct solver for the solution of derivatives system. The tolerance, both for the MDA and the MDO, is set to 10^{-6} .

Each of the configurations has been optimised considering as objective functions the fuel consumption and the energy consumption; they have been compared with the optimised A320 CERAS aircraft, EIS2035, the results of which are reported in Table 2.18. In mathematical notation, the two problems can be written as:

$$\begin{cases} \text{minimise} & m_f \\ \text{with respect to} & \underline{x} \in \mathbb{R}^{18} \\ \text{subject to} & \underline{c}(\underline{x}) \in \mathbb{R}^{17} \end{cases}$$

and

$$\begin{cases} \text{minimise} & E_c \\ \text{with respect to} & \underline{x} \in \mathbb{R}^{18} \\ \text{subject to} & \underline{c}(\underline{x}) \in \mathbb{R}^{17} \end{cases}$$

where the design variables vector \underline{x} and the constraint vector $\underline{c}(\underline{x})$ are defined in Table 3.25

Results are presented in the following: Fig. 3.20 shows the fuel consumption as a function of range, Fig. 3.21 the energy consumption as a function of range, meanwhile Fig. 3.22 the PFEE. All the plots are representative of the three configurations ($N_{EM} = 16, 32, 48$) and are compared with the reference aircraft. For completeness, the design's quantities of interest are also reported in Table 3.22 for the case of $N_{EM} = 16$, in Table 3.23 for the case of $N_{EM} = 32$ and in Table 3.24 for the case of $N_{EM} = 48$.

First to note is that the geometry that minimises the fuel consumption is the same that minimises the energy consumption, which can be intuitive as a results since they are correlated through a linear law. Then, the trends are not different from that of Fig. 3.16, Fig. 3.17 and Fig. 3.18: for each configuration, a range breakdown exists, that varies with the number of electric motors; also regarding the energy the point is shifted to right.

From these results, the most interesting thing that emerges is the optimal number of electric motors: $N_{EM} = 32$ seems to be the most performing configuration. Indeed, the case $N_{EM} = 16$ shows the best aerodynamic performance, with a maximum LoD around 18.05, because it has less wetted area. Despite that, the propulsion is poorly distributed, and to satisfy the constraint on fan dimension, the FPR needs to be augmented, around 1.3 from Table 3.22, worsening the propulsive efficiency.

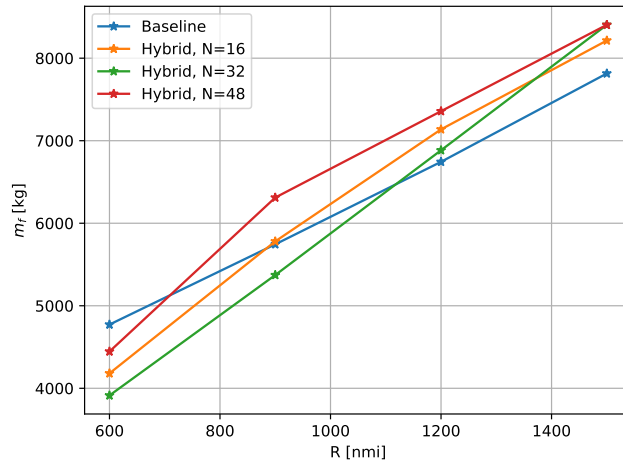


Figure 3.20: Fuel consumption as function of design range, comparison between the optimised baseline and hybrid aircraft with distributed electric propulsion.

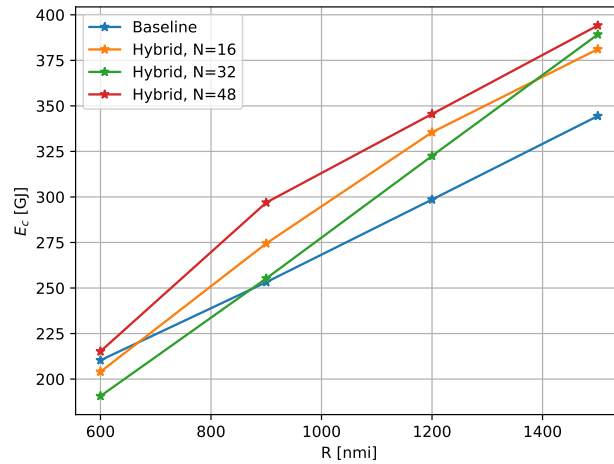


Figure 3.21: Energy consumption as function of design range, comparison between the optimised baseline and the hybrid aircraft with distributed electric propulsion.

The opposite case, $N_{EM} = 48$, instead does not show any issue regarding the fan size, but due to the large number of motors that need to be included over the wing, the FPR is increased in any case to reduce their size. Moreover, it has more wetted surfaces and the aerodynamics is significantly worsened. The combination of these two effects makes this configuration never performing over the others.

The case $N_{EM} = 32$ represents a balance between aerodynamics and propulsive efficiency. The maximum LoD is only 1.3% lower than the case with 16 electric motors, but the FPR is significantly lower (around 1.1 from Table 3.23), resulting in a good aerodynamics and

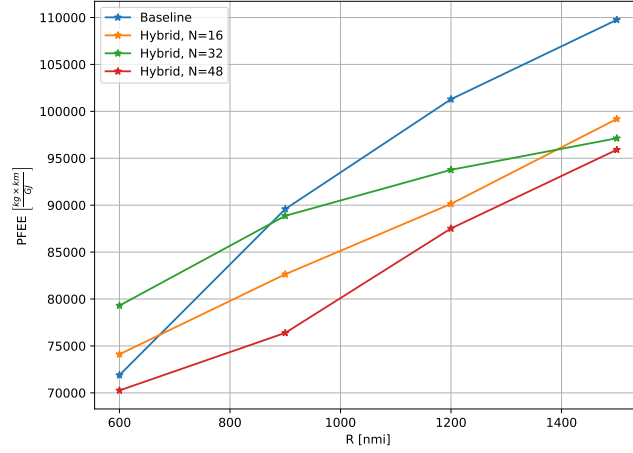


Figure 3.22: PFEE, defined in Eq. (1.3) as function of design range, comparison between the optimised baseline and the hybrid aircraft with distributed electric propulsion.

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	72.8	74.4	75.8	77.6
OWE	[t]	55.4	55.5	4504	56.6
Wing area	[m ²]	104.26	106.71	108.18	110.28
Max. LoD		18.05	18.03	18.04	18.03
Battery volume	[m ³]	1.56	1.67	1.86	1.94
FPR		1.26	1.28	1.28	1.29
Fuel mission	[t]	4.18	5.78	7.14	8.21
Energy consumption	[G.J]	204.03	274.47	335.50	381.13
CAT.POL.A.410(a)-1	[ftmin ⁻¹]	1438.64	1355.65	1324.17	1193.95
CAT.POL.A.410(a)-2	[ftmin ⁻¹]	1312.39	1310.58	1648.61	1307.07
CS-25.119(a)	[%]	12.27	12.25	12.09	12.21
CS-25.121(a)	[%]	24.02	24.76	24.57	24.2
CS-25.121(b)	[%]	2.41	2.46	2.51	2.76
CS-25.121(c)	[%]	24.10	23.73	23.23	23.14
CS-25.121(d)	[%]	10.80	10.80	10.65	10.76

Table 3.22: Quantities of interest for the optimised hybrid aircraft with distributed electric ducted fan, $N_{EM}=16$.

propulsion. Thus this case is the most performing among the three. This is also reflected in the battery volume, which is lower for this case than the others for all the range values, even if the masses are continuously increasing for the higher number of elements present.

Nonetheless, even for the most performing configuration the zone of interest is still limited to around 1150 nmi regarding the fuel and 900 nmi regarding the energy, because of the batteries' weight divergence. In any case, note that the range breakdown is larger with

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	77.7	78.4	70.1	80.4
OWE	[t]	59.9	60.3	60.9	61.3
Wing area	[m ²]	119.89	121.26	124.26	128.42
Max. LoD		17.81	17.82	17.81	17.81
Battery volume	[m ³]	1.55	1.67	1.72	1.92
FPR		1.12	1.12	1.12	1.13
Fuel mission	[t]	3.91	5.37	6.88	8.39
Energy consumption	[GJ]	190.67	255.24	322.52	389.20
CAT.POL.A.410(a)-1	[ftmin ⁻¹]	1125.10	1175.56	1142.56	1058.09
CAT.POL.A.410(a)-2	[ftmin ⁻¹]	1209.61	1267.16	12607	1135.13
CS-25.119(a)	[%]	11.25	11.62	11.61	11.60
CS-25.121(a)	[%]	24.59	24.29	24.29	22.74
CS-25.121(b)	[%]	2.40	2.41	2.51	2.52
CS-25.121(c)	[%]	23.46	23.18	23.18	21.81
CS-25.121(d)	[%]	9.79	10.14	10.14	10.15

Table 3.23: Quantities of interest for the optimised hybrid aircraft with distributed electric ducted fan, $N_{EM}=32$.

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	80.5	82.4	84.1	83.9
OWE	[t]	62.5	63.9	64.7	64.2
Wing area	[m ²]	118.26	124.12	129.1	124.08
Max. LoD		17.49	17.47	17.47	17.45
Battery volume	[m ³]	1.67	1.92	2.13	2.21
FPR		1.34	1.34	1.35	1.37
Fuel mission	[t]	4.45	6.31	7.36	8.40
Energy consumption	[GJ]	215.22	296.92	345.54	394.16
CAT.POL.A.410(a)-1	[ftmin ⁻¹]	950.35	1028.93	790.61	876.07
CAT.POL.A.410(a)-2	[ftmin ⁻¹]	1143.42	1233.99	1063.84	1228.31
CS-25.119(a)	[%]	10.78	11.01	10.78	10.97
CS-25.121(a)	[%]	22.75	22.75	22.27	22.68
CS-25.121(b)	[%]	2.61	2.52	2.84	2.58
CS-25.121(c)	[%]	21.80	21.86	21.13	21.20
CS-25.121(d)	[%]	9.36	9.52	9.38	9.48

Table 3.24: Quantities of interest for the optimised hybrid aircraft with distributed electric ducted fan, $N_{EM}=48$.

respect to the non optimised case of Fig. 3.16 and Fig. 3.17. In fact, thanks to blowing, the wing area of the non optimised aircraft is lower for hybrid case, and it has more margin for improvement before hit the span limit of 36 m.

Unlike the previous non optimised case, the non linearity is more evident, especially for

$N = 48$. In this case not only the batteries but also the FPR has an effect in removing the linearity. It is also to note that, regarding the PFEE, both $N_{EM} = 16$ and $N_{EM} = 48$ are in a zone of linearity for the curves, the quadratic term will be more relevant at still higher ranges.

On the certification side, all the configurations show to comply with the revised CS-25; also results from Table 3.22, Table 3.23 and Table 3.24 confirm the assumption regarding the most stringent condition to meet: it is the CS-25.121(b), related to the climb rate at 400 ft of altitude and in OCI case.

Another remark concerns the best cruise altitude, that for the conventional configuration was around 34 kft, as in Table 2.12. Due to the heavier mass, for the hybrid aircraft this value is sensibly lower, around 31 kft.

In Sec. 3.3.7 it has been given a formulation for estimating the cable efficiencies, which is Eq. (3.26). From Eq. (3.26) it can be deduced that losses decrease with the transport voltage, which is very high in the case studied (3 kV). The estimation of cable efficiency for the hybrid aircraft, in fact, is around 0.995, that is only 0.5% of losses are detected in the system. As a matter of fact, they can be considered negligible.

Finally, to note that no evidence of local minima is detected. For all the points studied, algorithm always converges towards the same solution, no matter the initial point, as happens for the previous case of the conventional aircraft reported in Table 2.13. For conciseness, tables containing the values are not shown here.

The last optimisation done concerns the mission profile. Indeed, it is evident from previous results that the proposed hybrid aircraft is strongly penalised by batteries, despite they are needed to satisfy the TLAR reported in Table 3.1. However, a further simulation is done, fixing the geometry to one of previous cases and including as a design variable the power rates, for battery and gas turbine, and the volume coefficient. The purpose is to understand if, from an optimal point of view, it is more beneficial to fly without batteries, or to reduce the electrification proposed. To do that, the previous requirement of flight fully electric at least up to 3000 ft is removed.

The optimisation problem formulation is reported in Table 3.25. Beside the power rates and the battery volume also the sizing power and the FPR are design variables, subject to only 5 constraints. Note that the value $\tau_b = 0$ may introduce a singularity, since the SoC is not defined in this point, in agreement with Eq. (3.8). By convention, it is assumed that in case $\tau_b = 0$, $SoC(t) = 1$ for every t . This is equivalent to a case in which there are batteries without energy, and they are not used.

The configuration chosen to run this simulation is the case with $N_{EM} = 32$ and $R = 900$ nmi. As said, geometry is frozen, except for τ_b and FPR. Table 3.26 sums up the results, comparing the previous analysis, referred as baseline, with the optimised one for the mission. As expected, this simulation shows that the optimal aircraft tends to remove batteries, because they introduce such a penalty in weight to result not well performing. The new configuration,

Category	Name	Size	Lower	Upper	Units
Objective	E_c	1	–	–	–
Variables	δ_{GT}	3	0	1	–
	δ_b	3	0	1	–
	P_{400}	1	6	15	MW
	FPR	1	1.05	1.4	–
	τ_b	1	0	2	m ³
	Total		9		
Constraints	SoC_f	1	0.20	–	–
	ΔP_b	1	0	–	W
	Δl_{nac}	1	–	0	m
	\bar{r}_f	1	–	0.15	–
	$\tan \gamma_{400}$	1	1	0.024	–
	Total		5		

Table 3.25: Optimisation problem definition for the mission profile, hybrid aircraft case, $N_{EM} = 32$, $R = 900$ nmi.

in fact, shows an OWE lower of more than 16 t, and this is reflected in a fuel consumption reduced of more than 20%. Also, since the aircraft is lighter, the thrust requirement in cruise is lower and the FPR goes more towards the lower bound, increasing the propulsive efficiency.

		Baseline	Optimised
MTOW	[t]	78.4	59.7
OWE	[t]	60.3	41.2
Battery volume	[m ³]	1.67	0
FPR		1.12	1.08
Fuel consumption	[kg]	5371.7	4512.6

Table 3.26: Comparison between the baseline and the optimised mission profile for the hybrid aircraft with distributed propulsion, $N_{EM} = 32$, $R = 900$ nmi.

The resulting aircraft is similar to DRAGON configuration [Sch+19], where the hybrid propulsion is generated by two gas turbines only. This exercise helps also to assess the effect of batteries, and exploit a different solution in case the battery technology will not be mature enough to match the 2035 perspectives done reported Table 3.12.

Next section will conclude the optimisation analysis carrying out a multi-objective problem, for which the difference between a gradient free and gradient based algorithm is exploited.

3.5.3.4 Pareto frontier with gradient information

This section tackles the problem of multiobjective optimisation: it is not rare, in fact, that a designer need to consider multiple conflicting objectives [Mie08]. Having two or more objec-

tives results in a set of optimal points, known as the Pareto frontier, or Pareto front [Par71]. The problem of the Pareto frontier has been first defined in 1907 in economic area, and it has been widely used in other disciplines. In engineering system its interest it mainly related to the possibility from the designer to choose between a range of optimal points for an optimisation problem, since often a choice *a priori* is not possible.

However, the generation of the entire Pareto front is costly. Many methods have been developed through the years to get efficiently the frontier, but the simulation is still very intensive, especially when the number of objectives grows up [MA04; CZM13; Dé12]. In the following, the number of objectives is limited to two, for the hybrid aircraft with distributed propulsion. The goal is to get the Pareto front with respect to the structural weight m_e and the energy consumption E_c . Indeed, this situation is of great interest since the two quantities are in contrast each other, and are directly related to cost analysis [Ros05h]. OWE is considered in place of MTOW, because the last one already includes fuel weight and it depends directly on the other objective, whereas the OWE depends only indirectly from the fuel [Sch18]. The chosen configuration for this analysis is the case with $N_{EM} = 32$ and $R = 900$ nmi; the problem is the same of Table 3.18, with the adding of m_e in the objective category.

Two different methods have been compared: a genetic algorithm, called NSGA-II [Deb+02], which is very costly, and SNOPT. NSGA-II does not use any gradient information, but it evaluates a prescribed number of points, and among them it identifies the feasible ones, and the ones belonging to the Pareto frontier. The optimisation problem can be written as

$$\begin{cases} \text{minimise} & \underline{f}(\underline{x}) = [m_e, E_c] \in \mathbb{R}^2 \\ \text{with respect to} & \underline{x} \in \mathbb{R}^{18} \\ \text{subject to} & \underline{c}(\underline{x}) \in \mathbb{R}^{17} \end{cases}$$

with \underline{x} and $\underline{c}(\underline{x})$ defined in Table 3.18. In the case here considered, 20000 points have been generated with NSGA-II.

SNOPT can not handle two objectives; to get the Pareto frontier a weighted scalar function is defined:

$$f(\underline{x}, \alpha) = \alpha \frac{E_c(\underline{x})}{E_{c_{ref}}} + (1 - \alpha) \frac{m_e(\underline{x})}{m_{e_{ref}}} \quad (3.55)$$

where $\alpha \in [0, 1]$, $m_{e_{ref}}$ and $E_{c_{ref}}$ are two reference quantities, used for normalization, referred to the A320 CERAS optimum case, for the chosen range. Varying α the Pareto frontier is exploited. For each value of $\alpha \in [0, 1]$, the problem takes the following form:

$$\begin{cases} \text{minimise} & f(\underline{x}, \alpha) \in \mathbb{R} \\ \text{with respect to} & \underline{x} \in \mathbb{R}^{18} \\ \text{subject to} & \underline{c}(\underline{x}) \in \mathbb{R}^{17} \end{cases}$$

The exploration space for NSGA-II is shown in Fig. 3.23, where all the 20000 points are identified. Among them, the feasible ones are marked in blue, and the points not dominated by another one, which then belong to Pareto front, are marked in red. The generation of

Pareto frontier with this algorithm required 41.9 h (about 1 day and 17 hours) on a single processor machine, confirming the statement done earlier on the intensive computational cost for these methods. It is to highlight that there is no clear method to choose the right number of exploration points, it is done empirically to ensure that the optimal set obtained is continuous and does not present large discontinuities.

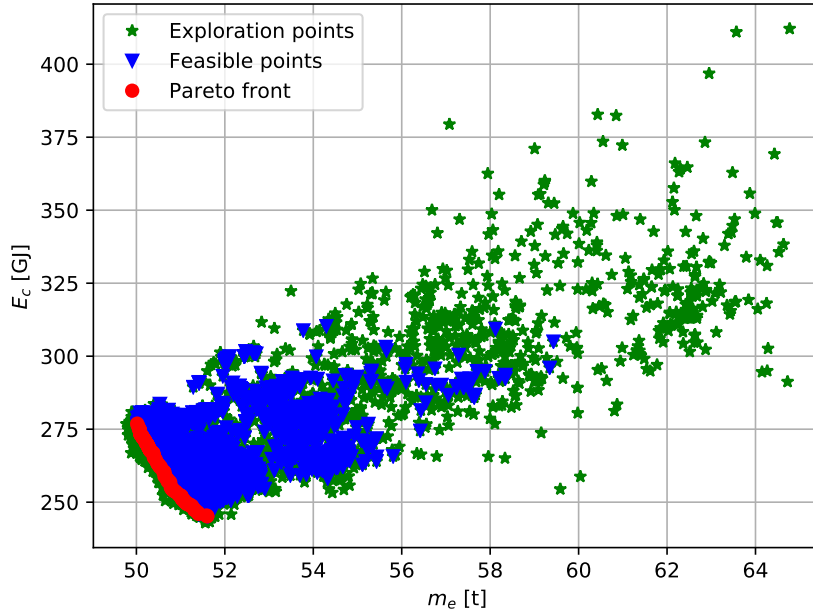


Figure 3.23: Exploration points using NSGA-II, for the multiobjective optimisation of hybrid aircraft, $N_{EM} = 32$ and $R = 900$ nmi. 20000 points considered.

The detailed Pareto frontier is shown in Fig. 3.24, where curves obtained from NSGA-II and SNOPT are compared. The parameter α is varying from 0 to 1 moving from left to right: the left side is a zone at which the parameters are set to reduce the weight, *i.e.* aspect ratio at lower bound, penalising the LoD ($\alpha = 0$); moving towards the left side the aerodynamics is improving (leftmost point corresponds to $\alpha = 1$). It is to note that the two methods are comparable each other and lead to the same curve, with the difference that using the gradient information in SNOPT, a single point is obtained in around 30 min, and the generation of all the 11 points from $\alpha = 0$ to $\alpha = 1$ requires about 5.8 h, speeding up the generation of about 6 times. However, the information of 5.8h is misleading, since it is the sum of all the simulations' times, but in practice they can be run in serial at the same, as far as the `xml` input file is different for each point. In that way, a reasonable Pareto frontier can be generated in about 1 h.

To better assess the differences between the two methods, the \mathcal{L}_2 -norm for the objective function vector $\underline{f} = [m_e, E_c]$ and the design variables vector is computed. This norm is mainly indicated for multiobjective optimisation problems [GF15]. Results are reported in

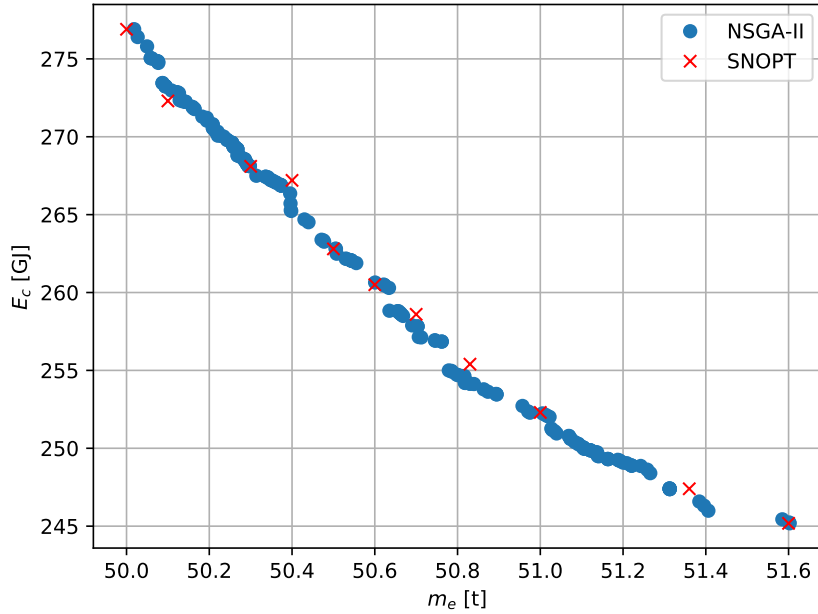


Figure 3.24: Comparison between the Pareto frontier obtained with NSGA-II and SNOPT, through the composite function in Eq. (3.55). Hybrid aircraft case, $N_{EM} = 32$ and $R = 900$ nmi.

Table 3.27: being the norm of the difference very small, it can be concluded that the final optimal set is the same for both methods.

$$\begin{array}{|l|l|} \hline \|\underline{f}_{SNOPT}^* - \underline{f}_{NSGAI}^*\|_2 & 3.67 \times 10^{-5} \\ \hline \|\underline{x}_{SNOPT}^* - \underline{x}_{NSGAI}^*\|_2 & 2.49 \times 10^{-4} \\ \hline \end{array}$$

Table 3.27: \mathcal{L}_2 -norm calculation between the final objective function and design variables vector. The subscript identifies the method.

For completeness, Fig. 3.25 presents the visualisation, obtained in VSP, of three different configurations chosen within the Pareto frontier, and corresponding to $\alpha = 0$, $\alpha = 0.5$ and $\alpha = 1$. Note that the main effect is on the wing, which is increasing its span from one limit to another.

From a designer point of view, the Pareto frontier exhibits a tradeoff between disciplines and gives a set of optimal configuration, it is up to the designer to choose one of the points according the needings. As example, if the main objective is to achieve a reduction of fuel (energy) consumption, it is whorthy to consider points on the right on the plot shown in Fig. 3.24; on the other side, points on the left corresponds to a minor mass which suggests that the initial investment may be reduced [PKG14]. It is to note that the slope of the frontier changes in proximity of the point $\alpha = 0.5$: indeed, the reduction of the mass is

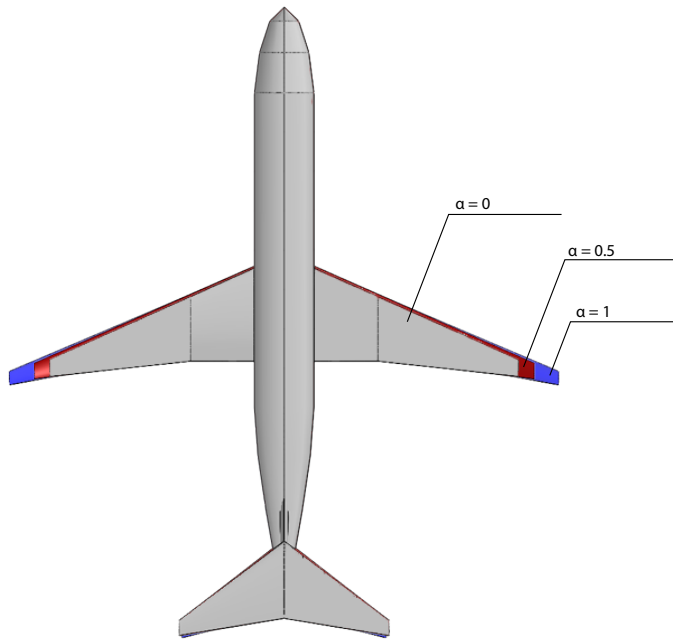


Figure 3.25: Comparison between three different configurations, chosen within the Pareto frontier for $\alpha = 0$, $\alpha = 0.5$ and $\alpha = 1$ in Eq. (3.55).

obtained reducing the aspect ratio, which means that also the aerodynamic is worsened. As a consequence, more thrust is required, especially in climb, which leads to an increase of the battery volume, but this parameters make the mass increase again, and so there is a snowball effects which finally make the battery mass diverge. The difference in slope is due to the divergence of battery mass in the zone of the right of Fig. 3.24; perhaps a suitable zone for the designer is the one before the change of the slope, where the energy is still reduced but the increase in mass is not important yet ($0.5 \leq \alpha \leq 1$).

3.6 Conclusion

This chapter is dedicated to the exploration and performance evaluation of the hybrid aircraft, with distributed electric propulsion, shown in Fig. 3.2. Modelisation of the propulsive chain, in all its components, is first described, followed by a revision of sizing procedure, to evaluate performances of the new proposed concept. Sensitivity analysis on the electric components' technology is presented, considering perspectives for 2035, to assess their impact on the overall design and define a baseline. Then, the hybrid aircraft is studied, for a given set of design ranges, and compared with the A320.

Results using the MDA show that, for a given set of TLAR and geometrical inputs, the hybrid aircraft is more performing than the baseline up to a certain range, called "range breakdown", which is around 1000 nmi. This behaviour is explained considering that batteries introduce a relevant penalty in weight, which is empty mass carried in cruise. At short ranges,

the impact of having a fully electric climb overcomes the effect of a heavier aircraft in cruise, but on longer ranges the batteries' weight diverges soon, making the aircraft so heavy that the baseline shows better fuel and energy consumptions; after 1600 nmi no feasible hybrid aircraft has been achieved.

Then, the MDO formulation, using the integrated version of FAST and OpenMDAO, is used to optimise the concept. Three different configurations, varying the number of electric motors from 16 to 48, are taken into account, to evaluate the impact of distributed propulsion. Trends regarding fuel and energy consumption are similar to the previous case without optimisation, but the "breakdown range" is extended up to 1200 nmi because there is more margin of improvement, before reaching the span limit, thanks to the blowing effect over the wing. Also, the case with 32 motors is the most performing among the three configurations, because it balances propulsive and aerodynamic efficiency. This result descends directly for the MDO peculiarity to consider interaction and coupling between different disciplines, and find the best balance among them. A final mission optimisation confirms also that mass penalties introduced by batteries are so relevant, that is more convenient to fly without any electric assisted phase.

Finally, a Pareto front is obtained, comparing a genetic algorithm and a gradient based algorithm, to assess the advantage of using derivatives in the optimisation process. The computational cost in the second case is reduced of more than 70%, confirming that, despite the great efforts spent in computing analytic derivatives, the computational time is sensitively reduced.

At this point, the MDO formulation is ready, and it has been demonstrated its capability to deal with the problem of unconventional configuration. In particular, it has been shown that it is capable to get all the interactions in an optimisation process, resulting in interesting tradeoff, that with the MDA approach may have been harder to capture. Then, the hybrid aircraft configuration is exploited, and thus the left side of the roadmap shown in Fig. 1.24 is fully covered. In particular, the main conclusion can be drawn is that the hybrid electric concept has a remarked zone of interest for its design, because of the penalties in mass introduced. To possibly extend the region of interest, is then of relevance to consider a Blended Wing-Body configuration, which naturally has a high value of LoD.

Next chapters set up the methodology for the Blended Wing-Body sizing and assess its performance in a similar way than was done in this chapter, in order to explore also the right branch of the PhD roadmap of Fig. 1.24.

Synthesis of the chapter

- The propulsive chain, based on distributed electric propulsion, is modelised and applied to a conventional tube-and-wing, to assess its advantages.
- The sizing loop is revised to consider new features of hybrid propulsion.
- From a technological point of view, there is a lot of uncertainty in the 2035 perspective: a sensitivity analysis identifies the battery as the most critical component for the sizing.
- The proposed tube-and-wing aircraft featuring distributed electric propulsion is explored in terms of performance.
 - The concept is evaluated against the reference A320 CERAS test case, resized at the same technological level.
 - The hybrid concept is advantageous up to a specific “breakdown range”. Due to the presence of batteries, below the range the electrified climb overcomes the penalties in weight; above the range the effect of having empty weight carried in cruise is more relevant.
 - Fuel consumption may be misleading for the evaluation. Energy is more sensitive since it includes the contribution of batteries and power required by subsystems.
 - Optimisation is carried out considering 16, 32 and 48 ducted fans distributed along the wing. Results show that the configuration with 32 electric motors represents a balance between aerodynamics and propulsion and it is the most performing.
 - Batteries are identified as the main source of penalties in mass. Mission optimisation shows that for the fuel reduction is more convenient to remove these elements and generate electric power only by the gas turbines.
- For the test case of a Pareto frontier, the computational performance of a gradient-based methods are assessed against a gradient-free method. Results show that the deployment of analytic derivatives reduces the computational cost of about 70%, which is a key feature for designers.

Research contribution

- **Conference paper.** A. Sgueglia, P. Schmollgruber, N. Bartoli, O. Atinault, E. Benard and J. Morlier, *Exploration and sizing of a large passenger aircraft with distributed electric ducted fan*, AIAA SciTech 2018 proceedings, Kissimmee, Florida (USA), 2018. DOI: [10.2514/6.2018-1745](https://doi.org/10.2514/6.2018-1745)
- **Journal paper.** A. Sgueglia, P. Schmollgruber, E. Benard, N. Bartoli, J. Morlier, J. Jasa, J. R. R. A. Martins, J. T. Hwang and J. S. Gray, *Development of a multidisciplinary design optimization framework with gradient calculation applied to hybrid aircraft*, Journal of Aircraft, 2020.
- **Book chapter.** A. Sgueglia, S. Dubreuil and N. Bartoli, *Technologies sensitivity analysis of an hybrid aircraft*, Chapter 10 of the book “Aerospace system analysis and optimization in uncertainty”, edited by L. Brevault, M. Balesdent and J. Morio. Springer Optimization and its Application. New York: Springer, 2020.

Chapter 4

Design methodology and exploration of the Blended Wing-Body concept

Résumé

Ce chapitre, qui conclut la thèse, a pour objectif de définir une méthodologie de dimensionnement pour l'aile volante (BWB) et de l'appliquer au cas test de cette recherche.

Le problème principal, lié à une telle configuration, est le manque de données publiques de référence, ce qui peut compliquer la validation des méthodes appropriées pour l'aile volante. Pour résoudre ce problème, une procédure multifidélité a été mise en place: pour toutes les disciplines clés (aérodynamique, contrôle, structure), la haute-fidélité a été utilisée afin de valider ou éventuellement corriger les méthodes mises en œuvre dans FAST. Pour ce faire, une géométrie de référence commune a été définie à l'ISAE-Supaero et à l'ONERA. Certaines analyses hors conception, liées à l'embarquement des passagers et à la disposition interne de la cabine, ont également été réalisées afin de comprendre la faisabilité du concept du point de vue de la certification. Il est à noter que cette partie du travail a été réalisée en collaboration avec une équipe d'étudiants en master à l'ISAE-Supaero travaillant dans différents domaines liés à la conception avion. Une fois ces modèles identifiés, une synthèse de la conception BWB est fournie.

Ensuite, la boucle de conception a été modifiée pour tenir compte des nouvelles méthodes adaptées au BWB. Enfin, en intégrant ce travail au groupe motopropulseur défini au Chapitre 3 et en incluant la boucle de dimensionnement résultante dans l'architecture MDO présentée au Chapitre 2, l'outil d'optimisation pour l'aile volante à propulsion électrique distribuée est obtenu.

Les résultats sont divisés en deux parties: l'aile volante est d'abord explorée en considérant les moteurs conventionnels, puis le concept de propulsion électrique distribuée est considéré. La première partie des résultats a été réalisée pour comprendre les avantages découlant de l'architecture BWB uniquement; les performances sont évaluées par rapport à l'avion A320 CERAS. Il est démontré que la BWB réduit la consommation de carburant d'environ 15% ; de plus, cela permet d'avoir plus de flexibilité dans les opérations grâce à un diagramme étendu de la charge utile. Enfin, l'aile volante proposée avec une propulsion électrique distribuée est prise en compte. Les résultats sont similaires à ceux obtenus pour les avions hybrides du Chapitre 3, mais grâce au haut rendement aérodynamique offert par cette architecture, la zone d'intérêt pour la conception est agrandie jusqu'à 1400 nmi. Le cas de 32 moteurs offre encore le meilleur compromis entre l'aérodynamique et la propulsion, et s'avère être le plus performant. Les résultats finaux du Chapitre 3 ont incités à étudier une configuration où l'énergie est générée uniquement par des turbines à gaz: sans batterie, l'aile volante est toujours plus performante que l'avion de référence, confirmant le fait déjà identifié que les batteries introduisent une pénalité non négligeable en poids.

Enfin, le chapitre se termine par quelques conclusions générales et des suggestions de développements futurs. En particulier, les prochains travaux devraient prendre en compte différentes géométries afin de consolider les résultats issus de la haute-fidélité et d'analyser l'impact des portes de la soute et d'embarquement sur la structure. L'aspect évacuation doit également être pris en compte. En effet, en raison de l'importance primordiale du contrôle pour cette configuration, cette discipline doit être directement incluse dans la boucle de conception (au moins pour le contrôle longitudinal) et ne pas être considérée dans une procédure off-design.

Contents

4.1	Introduction	157
4.2	Development of models tailored to Blended Wing-Body sizing	158
4.2.1	Research strategy	158
4.2.2	High fidelity aerodynamic studies for the Blended Wing-Body	159
4.2.3	Control surfaces sizing for the BWB longitudinal control	165
4.2.3.1	The control problem formulation	165
4.2.3.2	The longitudinal control for a BWB configuration	168
4.2.3.3	Sensitivity analysis on the BWB stability	171
4.2.4	Blended Wing-Body structural design	174
4.2.4.1	Modelling of the Blended Wing-Body internal structure	174
4.2.4.2	Static analysis	175
4.2.5	Nacelle integration in the Blended Wing-Body architecture	178
4.2.6	Blended Wing-Body design synthesis	182
4.2.6.1	Planform sizing	182
4.2.6.2	Cabin modelling	182
4.2.6.3	Transition zone and outer wing modelling	186
4.2.6.4	Subsystem positioning	187
4.3	Methodology for the Blended Wing-Body sizing	191
4.3.1	MDA sizing loop	191
4.3.2	MDO formulation	194
4.4	The Blended Wing-Body featuring conventional propulsion	195
4.4.1	Design mission analysis	195
4.4.2	Operational area assessment	198
4.5	The Blended Wing-Body with distributed electric propulsion	201
4.5.1	Problem formulation	201
4.5.2	Sensitivity analysis results	201
4.5.3	Mono-objective optimisation results	205
4.5.4	Pareto frontier for the proposed BWB concept	211
4.5.5	Results for an hybrid BWB concept without batteries	213
4.6	Conclusions	215

Outline

- To tackle the lack of reference data for the Blended Wing-Body, a research strategy is defined.
- The Multidisciplinary Design Analysis loop is revised, to take into account a Blended Wing-Body architecture.
- The integration of the MDA loop within the MDO formulation found in Chapter 2 and the propulsive model identified in Chapter 3 are explained.
- The Blended Wing-Body is explored:
 - First considering conventional propulsive system;
 - Then with the distributed electric propulsion integration. 16, 32 and 48 distributed electric motors are considered, to study the effect of this parameter on the overall design.

4.1 Introduction

This chapter exploits the BWB concept, which is the second key innovative aspect introduced. The first part of the chapter addresses one of the issue related to BWB mentioned in Chapter 1, that is the lack of reference data for a BWB and relative lack of models tailored for the conceptual design stage. To comply with the issue, a research strategy based on high-fidelity has been set up. Simulations are carried out for different disciplines, using CFD, FEM and other methods, and the result are then used as database for the validation, or eventually correction, of the methods implemented in FAST. A common reference geometry is defined for this benchmarking phase. The outcomes of this procedure are described in Sec. 4.2; following disciplines are detailed:

1. Aerodynamics, in order to find proper corrections to methods used in FAST, using CFD analysis.
2. Mass estimation, to replace the models used in FAST with equations tailored for the BWB concept, using FEM analysis.
3. Longitudinal control. Despite it is not included yet in the MDA sizing loop of FAST, it is of primary importance for a BWB architecture to design the control surfaces, in order to assess the feasibility of the concept concerning the trimming. If this analysis shows that the BWB cannot be trimmed easily, there is no reason to proceed with a full sizing. Study is limited to longitudinal control at low speed.
4. Integrated nacelle tradeoff, to evaluate the impact of a BLI on the overall architecture, and model it at basic level with a corrective factor.
5. Boarding simulation, to propose a reasonable boarding door positioning for further studies.

At each step, assumptions and limits are stated, to identify future steps in the BWB sizing development. The revised models are integrated in FAST, to obtain a methodology for the BWB sizing, as explained in Sec. 4.3. In agreement with the Ph.D. roadmap shown in Fig. 1.24, the MDA is defined considering conventional propulsion, and only at the end the final MDO formulation for the BWB with DEP is obtained merging models from Chapter 3 with that defined here. This phase of the work has been carried out with the help of several master students at ISAE-Supaero, working on different area. The teams have been coordinated in order to arrive at the final BWB methodology.

The second part of the Chapter is mainly related to the application of the procedure defined for the performance evaluation of the BWB. First, the analysis of a BWB with conventional propulsion is carried out in Sec. 4.4, fulfilling the right branch of Fig. 1.24. Afterwards, Sec. 4.5 reports the results for the final concept here proposed, that is the BWB featuring DEP. The same set of simulations done for the hybrid TAW in Chapter 3 are repeated here for the BWB. Finally, Sec. 4.6 sums up the main conclusions.

Research contribution is listed below.

- The revised version of FAST for the BWB with conventional propulsion is described in the 2018 EASN conference proceedings, held in Glasgow in September 2018 [Sgu+18b].
- The multifidelity methodology and the results for the BWB with distributed propulsion have been presented at 2019 EASN conference, held in Athens in September 2019, in two dedicated sessions.
- The methodology adopted is described in a journal paper submitted to Open Aerospace [Sgu+19].
- The results for the BWB with DEP will be presented at the AEC 2020, held in Bordeaux in February 2020 [Sgu+20a].

4.2 Development of models tailored to Blended Wing-Body sizing

4.2.1 Research strategy

The research strategy for the development of models tailored to BWB for conceptual design proceeds thanks to the help of high fidelity tools. CFD, FEM and similar methods are used to benchmark the models adopted in FAST, to assess their validity or to find proper corrections. At this scope, a reference geometry must be defined, that is shown in Fig. 4.1. The outer wing uses supercritical airfoil to reduce the wave drag [Sar+10]. These airfoils have a negative pitching moment, to counterbalance their contribution reflex airfoil are used in the centerbody [Hep18; Hep90], as they have positive pitching moment. The choice is made in order to achieve a near zero pitching moment, since a tailplane is not present [Ale14; SV02] and $C_M = 0$ helps to obtain stability.

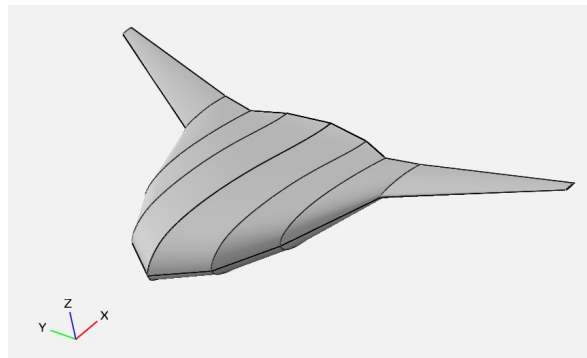


Figure 4.1: ISAE-Supaero and ONERA Blended Wing-Body reference geometry.

The TLAR of this reference geometry are the same of the Airbus A320, reported in Table 4.1, together with some main parameters. MTOW is estimated from the Breguet

Number of passenger	150	
Range	2750	nmi
Cruise Mach	0.78	
Aspect ratio	5.37	
MTOW	90.2	t
Surface	313	m ²
MAC	9.68	m
Cruise altitude	35000	ft

Table 4.1: TLAR and main parameters for the ISAE-Supaero and ONERA Blended Wing-Body reference geometry.

equation [Ros05a], and it is just a first estimate that needs to be redefined later on. The first estimate of wing surface is obtained through a constraint analysis, which indicates the requirement of vertical speed at top of climb as the sizing one for the surface. This point will be also addressed later in this chapter. The chord distribution is arbitrarily chosen, the only requirement to meet is the volume of the cabin. Mean aerodynamic chord is obtained through its definition:

$$\bar{c} = \frac{2}{S_w} \int_0^1 c^2(\eta) d\eta \quad (4.1)$$

where η is the non-dimensional y -section and $c(\eta)$ the chord distribution. With a first assumptions of materials and subsystem location, from OpenVSP is possible to estimate the center of gravity position, which results at 30% of MAC approximately; this is a key parameter for the studies on longitudinal stability and control presented later.

It is to highlight that this geometry has not been optimised, but it is only a first reasonable configuration, used for studies and validation purposes. Because of the lack of optimisation, it may be expected that the global efficiency will not be satisfying, but in this context these and other similar issues are not treated.

4.2.2 High fidelity aerodynamic studies for the Blended Wing-Body

As remarked in the previous section, methods to estimate the C_D , described by Eq. (2.14), Eq. (2.11) and Eq. (2.12) may lose of validity. The induced drag is derived by the lifting line theory, which is valid for small thickness-to-chord ratio and high aspect ratio. The first assumption may not be respected in the centerbody section, which has a relative thickness of about 15-18% [KS15], the second instead is to verify since the BWB has intrinsically lower AR than conventional aircraft. Wave drag is the hardest term to estimate, and the equation adopted is valid as far as the wing is not highly swept (below 25 deg), whereas the BWB generally is very swept, especially in the center section.

The CFD procedure is then adopted, to estimate each term and assess the error. The software used is SU² [Ara+14; Eco+16], an open-source CFD code developed at Stanford University. Unfortunately, it does not have its own mesher, requiring an external software

for meshing purposes. At today, there is no big choice in meshing code, and most of them are commercial: in this research it has been used ICEM, belonging to the ANSYS repository [ANS19]. The great advantage of ICEM is the O-Grid functionality, which allows to generate a good meshing around the body and decrease the cell size up to the far field, without losing the orthogonality of cells or the skewness [de 15b]. For more details it is possible to refer to ANSYS manual guide.

Thanks to the O-grid feature, the number of cells is reduced: the final mesh for the BWB in real scale is made up of 8373239 cells; a detail of the meshing around the body is shown in Fig. 4.2. Already at first sight, from Fig. 4.2 quality mesh can be appreciated. However, it is

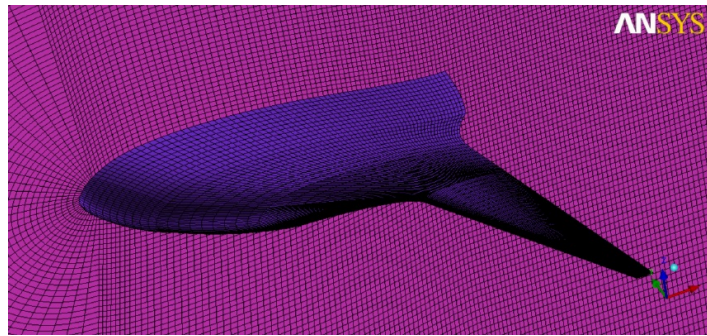


Figure 4.2: Detail of the Blended Wing-Body mesh around the body.

ensured checking that the skewness ratio tends to zero and the non-orthogonality is avoided. This last condition is critic particularly at the trailing edge, where sharp airfoil profiles make association with block a challenging task.

The mesh is then given as input at SU², which converts it in a compatible format. The simulation is defined through a configuration file, since SU² does not have a Graphical User Interface (GUI); within this file all the numerical and convective schemes must be defined. Of course, a unique choice does not exist, and a bad definition may strongly affect the convergence; the chosen simulation set-up is reported in Table 4.2. The model is a fully turbulent

Mach	0.78
Altitude	35000 ft
Model	RANS
Turbulence model	Spalart-Allmaras
Convective scheme	JST
Limiter	Van Albada
Spacial scheme	Grenn Gauss
CFL number	0.95
Linear solver	ILU

Table 4.2: Set up of CFD RANS simulations in SU2 for the BWB reference geometry aerodynamic study.

RANS, which means that it includes all the terms of Navier-Stokes equations [LL87]: both

the terms related to pressure and velocity field, mainly related to induced and compressibility term [MS98a], and the term related to the tensor stress which explains the viscous term [MS98b]. The simulation point is the one corresponding to cruise; CFD schemes and solvers are chosen following the indication of classical CFD handbooks to ease the convergence [FP02; And11]. The turbulent Spalart-Allmaras is chosen because it is the most indicated for transonic regime [Pop00], limiter is considered to schematise the shock wave, which represents a discontinuity in the flow field [LeV92], and the CFL number is chosen close to 1 to facilitate the convergence [LeV07]. The boundary conditions are of inlet/outlet at the far field and no-slip condition on the body: in that way, the velocity on the body is imposed to be zero, as comes out from the Prandtl theory for the boundary layer [MS98b]. Other planes are of symmetry.

Several points, at different angles of attack from -3 to 10 deg, are evaluated; results are compared with the polars obtained in FAST, and with VSPAero, a suite included in OpenVSP to compute aerodynamics using a Vortex-Lattice method (VLM). For the convergence, the residuals are studied: if the main force parameters C_L , C_D and C_M reach a constant value with a given tolerance, the simulation is considered over and converged. Among the three, the most critic coefficient is C_D , since to have an accurate estimation a tolerance of 10^{-6} is needed. An example of CFD history is given in Fig. 4.3.

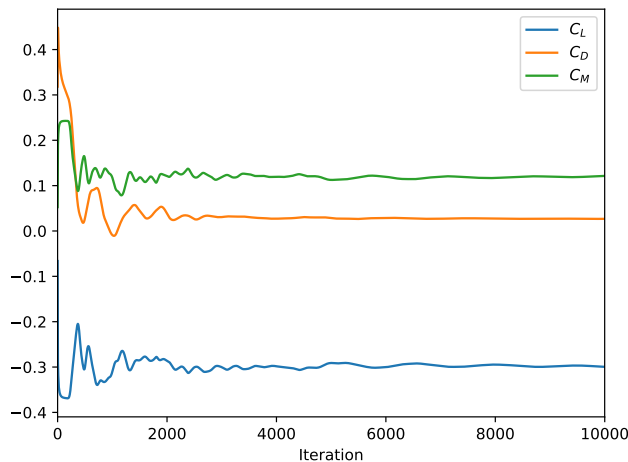


Figure 4.3: Convergence history example for CFD simulation, $\alpha=-3$ deg, $M=0.78$ and $h=35000$ ft.

First curve presented is the $C_L - \alpha$, shown in Fig. 4.4. Visually, it can be seen that FAST, VSP and SU^2 are in good agreement in the linear zone, then at high angle of attack both FAST and VSP still show a linear trend, whereas SU^2 captures the stall. This is expected since in FAST the curve is obtained simply as a straight line from the estimation of the slope $C_{L\alpha}$ using the result from lifting line, and VSP uses a VLM method which has in its limitation the non viscous flow hypothesis. However, for the cruise the most interesting zone is the linear one, and in this region no corrections are needed. This is also confirmed having a look at the

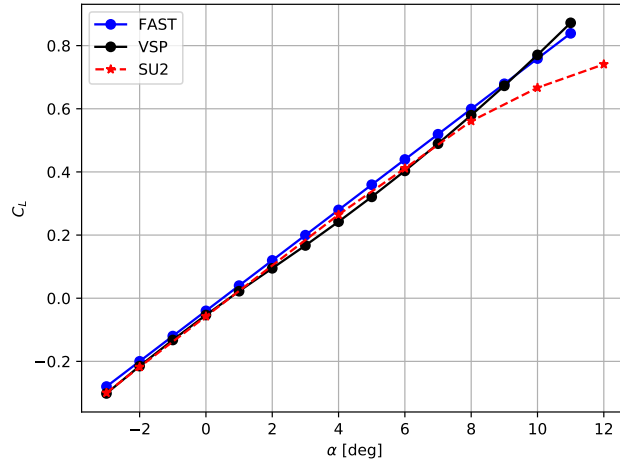


Figure 4.4: $C_L - \alpha$ curve, comparison between SU2, FAST and OpenVSP. RANS simulation case, $M=0.78$ and $h=35000$ ft.

values of the slope $C_{L\alpha}$ reported in Table 4.3: both of them slightly overestimate the value of SU2, but the difference is within the 1%, that is acceptable at this stage.

SU2	4.575 rad^{-1}
VSP	4.649 rad^{-1}
FAST	4.578 rad^{-1}

Table 4.3: Comparison of the slope $C_{L\alpha}$ estimated by SU2, VSP and FAST. RANS simulation case, $M=0.78$ and $h=35000$ ft.

The second curve shown is the polar $C_L - C_D$, depicted in Fig. 4.5. Contrarily to the previous case, here the three methods show differences. The first to note is that the VSP curve is shifted on the left, which means that the term C_{D_0} is underestimated. FAST and SU2 present instead a good agreement, still in the zone of low C_L ; at higher values SU2 estimates a drag coefficient much higher. Having assessed that C_{D_0} matches for both cases, the other two terms cause this divergence. Table 4.4 reports the values for the Oswald coefficient: for all the three methods there is a good match (maximum error is still below 2%). Since the parameter e is the same, the term C_{D_i} matches too. Indeed, from Eq. (2.12) the only parameter that may vary is e . As a conclusion, the drag divergence in SU2 is caused by the wave drag term:

SU2	0.986
OpenVSP	0.992
FAST	0.987

Table 4.4: Comparison of the Oswald coefficient e , estimated by SU2, FAST and OpenVSP. RANS simulation case. $M=0.78$ and $h=35000$ ft.

it seems that FAST and OpenVSP underestimate this term. This is expected in OpenVSP,

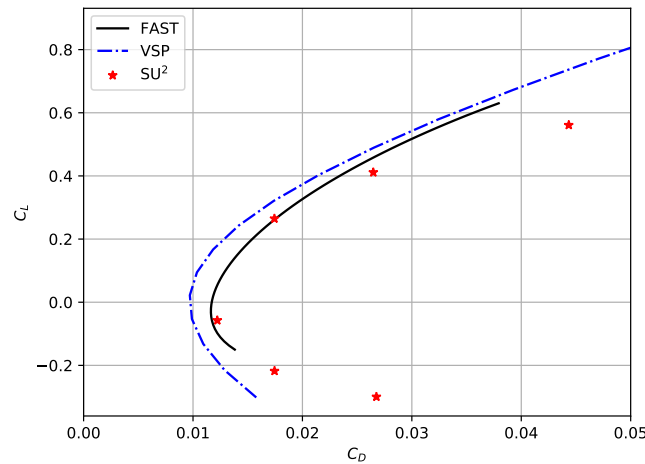


Figure 4.5: $C_D - C_L$ curve, comparison between SU2, FAST and OpenVSP. RANS simulation case $M=0.78$ and $h=35000$ ft.

since the VLM is valid only in subsonic flow; as far as FAST is concerned, it means that the method used can be applied to conventional aircraft but loses its validity for a BWB, mainly because of the highly swept configuration.

It is to mention that an Oswald coefficient near 1 confirms that the BWB is efficient from an aerodynamic point of view, since $e = 1$ corresponds to the optimal lift distribution. A BWB configuration is a low aspect ratio, and indeed the Jones theory for delta wing is more accurate than the Prandtl theory [de 15b]. This theory forecasts an elliptical distribution, which is confirmed by the Oswald coefficient; in fact $e = 1$ coincides with elliptical distribution [And11].

For completeness, the efficiency curve is shown in Fig. 4.6, where the LoD value drops off above $C_L = 0.5$ approximately. Note that the maximum LoD value is around 17-18: as stated at the beginning, the reference geometry is just a first estimate and has not been optimised to maximise the aerodynamics; however this issue is not addressed since for validation purposes only a comparison is of interest. Also, the optimum C_L is approximately 0.4, which is high for a BWB, perhaps this suggests that the initial estimate of 35000 ft as cruise altitude must be revised.

Finally, an analysis is done to estimate the Mach divergence, defined as the Mach number starting from which the following condition is satisfied:

$$\frac{dC_D}{dM} = 0.1 \quad (4.2)$$

The analysis is conducted varying the Mach number at a given angle of attack, $\alpha=1.5$ deg. Results are shown in Fig. 4.7: at low α the drag coefficient is almost constant, because the wave drag is near zero, but it start to diverge as soon as the transonic regime starts. The Mach divergence is marked in black and is equal to 0.803, so very close to the Mach design.

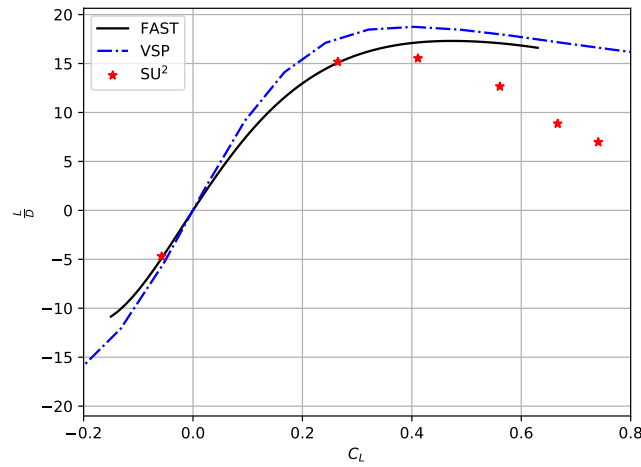


Figure 4.6: Lift-over-drag ratio curve, comparison between SU2, FAST and OpenVSP. RANS simulation case. $M=0.78$ and $h=35000$ ft.

This is not a favorable condition, and a further redesign may be done. The results from

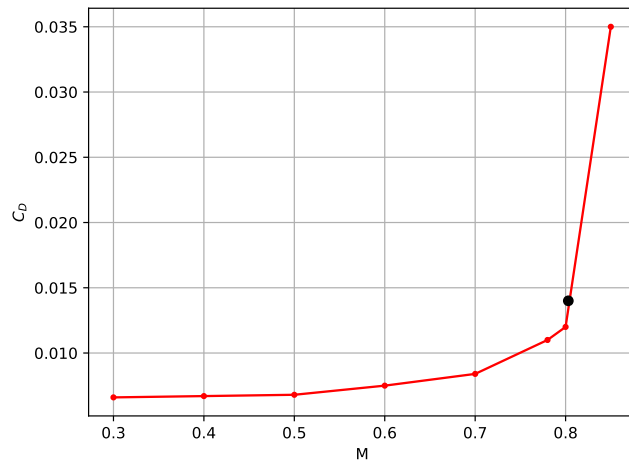


Figure 4.7: $C_D - M$ curve, $\alpha=1.5$ deg and $h=35000$ ft. Drag divergence point marked in black.

Fig. 4.7 state also that in low speed, when the wave drag is not relevant, a good agreement between low and high fidelity methods is expected, since it has already been shown that the induced drag estimation works well.

To conclude, this analysis shows that methods used in FAST still maintain their validity for the estimation of C_{D_0} and C_{D_i} terms, but the compressibility model fails. Thus the equation has been recalibrated, including a corrective term to match the results from high-fidelity. Also, from the CFD simulations the parameters C_{L_α} and C_{M_α} are estimated. From

their knowledge it is possible to compute the static margin as [And12]

$$SM = -\frac{C_{M_{cg\alpha}}}{C_{L_\alpha}} \quad (4.3)$$

The application of Eq. (4.3) yields to $SM = 0.46$, which is out of the allowable domain of 5 and 10% of the MAC. This may result in some difficulties to control the aircraft. This point will be addressed in next section, that reports the sizing of control surfaces for the longitudinal control.

4.2.3 Control surfaces sizing for the BWB longitudinal control

4.2.3.1 The control problem formulation

This section is devoted to the study of control surfaces sizing for a BWB, focusing on the problem of the longitudinal stability. The control discipline is not directly included in FAST, at this stage, but several work in literature marks the BWB stability and control as a priority for its design [NW96; KS15; PMP60; Wan12; AK89], and so it has been decided to carry out the design of control surfaces, for the longitudinal control, in order to understand if the concept can be trimmed in some way. In case of negative answer, there is no need to proceed with further sizing investigation.

At first order, considering small angles, longitudinal equations are decoupled from the lateral ones, and it is then possible to simplify the equations considering only the symmetry plane [Ros08]. The longitudinal flight dynamics equations are reported below, with the notation that follows the scheme of Fig. 4.8 [KC97; de 15a]; the moment is considered positive when it is pitching up.

$$\begin{cases} m\dot{V} = -\frac{1}{2}\rho V^2 S_w C_D + T - mg\gamma \\ mV\dot{\gamma} = \frac{1}{2}\rho V^2 S_w C_L - mg \\ I_{yy}\dot{q} = \frac{1}{2}\rho V^2 S_w \bar{c} C_{M_{cg}} \\ \dot{q} = \dot{\alpha} + \dot{\gamma} \end{cases} \quad (4.4)$$

In Eq. (4.4), m represents the mass, α the angle of attack, γ the flight path angle, V the velocity, I_{yy} the inertial moment along the y -axis, q the angular speed and the dot represents the derivative with respect to time.

To close the problem, an aerodynamic model for the computation of C_L , C_D and $C_{M_{cg}}$ needs to be defined. In the hypothesis of small angle of attack, it is possible to define some linear relations as follow:

$$\begin{cases} C_L = C_{L_0} + C_{L_\alpha} \alpha + C_{L_q} \frac{q}{\bar{c}V} + C_{L_{\delta_e}} \delta_e \\ C_D = C_{D_0} + kC_L^2 + C_{D_w} \\ C_M = C_{M_0} + C_{M_\alpha} \alpha + C_{M_q} \frac{q}{\bar{c}V} + C_{M_{\delta_e}} \delta_e \end{cases} \quad (4.5)$$

Beside the already known parameters, such as C_{L_α} and C_{M_α} , new quantities appear: δ_e is

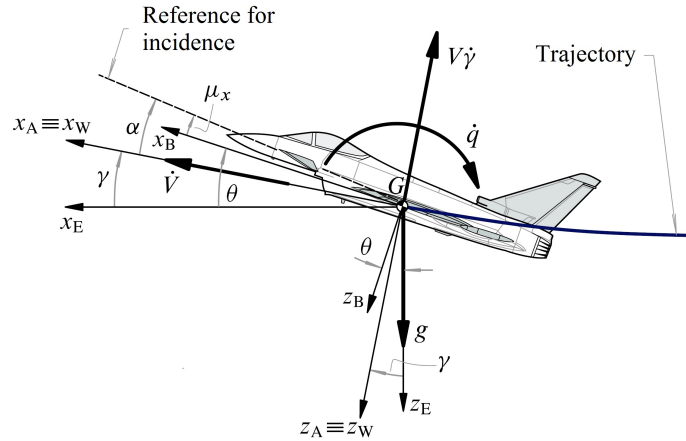


Figure 4.8: Aircraft diagram scheme, noting the angle of attack α , the flight path angle γ and the line for indices [de 15a].

the deflection of control surfaces, C_{L_q} and $C_{L_{\delta_e}}$ are the slope of C_L with respect to a variation of q and δ_e . C_{M_q} and $C_{M_{\delta_e}}$ have a similar meaning, referring to moment coefficient C_M . Note that C_M must be computed around the center of gravity, to have coherency with the set of Eq (4.4). Finally, k is computed from Eq. (2.12).

Combining Eq. (4.5) with Eq. (4.4), it is possible to linearize the flight dynamics equations. For brevity, this system of equations can be written in matrix form in the state space [KC97]:

$$\begin{cases} \dot{\underline{x}} = \mathbf{A}\underline{x} + \mathbf{B}\underline{u} \\ \underline{y} = \mathbf{C}\underline{x} \end{cases} \quad (4.6)$$

where \underline{x} is the state vector, that includes the entries the pitch rate q and the small variations of V , α and γ , \underline{y} is the output vector, including also the load factor n [Meg12], \underline{u} the control vector, which includes only the entry δ_e , and \mathbf{A} , \mathbf{B} and \mathbf{C} are three matrices. The formulation of Eq. (4.6) is easier to manipulate in a simulation system like Matlab/Simulink [Mat18], that will be used later.

At this point, for the BWB reference geometry only C_{L_0} , C_{M_0} , C_{L_α} and C_{M_α} are known from the CFD results of Sec. 4.2.2; the others must be estimated. C_{L_q} and C_{M_q} depend solely on the geometry meanwhile $C_{L_{\delta_e}}$ and $C_{M_{\delta_e}}$ depend also on the control surfaces definition, then an assumption on their placement must be done.

Table 4.5 reports the overall coefficients for the analysis to be conducted: the Mach is set to 0.3, and so the case is the low speed one; indeed the control surfaces must equilibrate the moment coefficient at low speed, Mach close to takeoff and sea level. In reality the aircraft must be trimmed at maximum C_L , but the objective is not achievable without a level of refinement that includes a full RANS model, and thus the flight domain is limited to the equilibrium point. The next improvement will be to enlarge this study at high lift, considering also the dutch-roll.

M	0.3	
I_{yy}	11165	kg m ²
C_{L_α}	4.47	rad ⁻¹
C_{M_α}	- 2.06	rad ⁻¹
C_{L_q}	0.79	rad ⁻¹
C_{M_q}	-0.88	rad ⁻¹

Table 4.5: Geometrical and aerodynamic coefficients for the BWB reference geometry, for longitudinal control surface purposes.

The slope C_{L_α} and C_{M_α} come from CFD simulations at $M = 0.3$; note that only 2 points in the linear zone are necessary for their estimation. The terms C_{L_q} and C_{M_q} , instead are computed using VLM method of AVL [MIT18a] and classical relations from Roskam [Ros08]. The inertial parameter I_{yy} is given by OpenVSP. It is to highlight that the procedure here is multifidelity, since it uses both CFD and VLM results.

Concerning the control surfaces placement, the work already done by Denieul has been used as reference [Den16]. The BWB is a tailless configuration, and then the idea of using a single control surfaces as ailerons and elevators arises; to stress their double capacity they are called generically “elevons”. Six different configurations have been considered, reported in Fig. 4.9, they are made up using just three basic elevon configurations:

- Type A, in the centerbody;
- Type B, in the inboard external wing;
- Type C, in the outboard external wing.

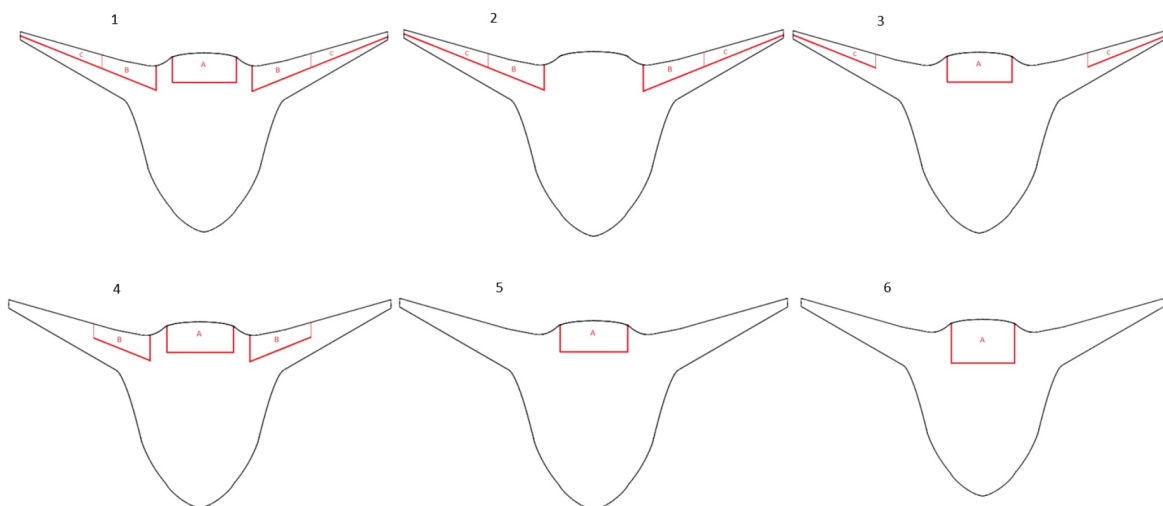


Figure 4.9: The 6 control surfaces configurations proposed for the BWB reference geometry for the purpose of this research activity.

The coefficients $C_{L_{\delta_e}}$ and $C_{M_{\delta_e}}$ are estimated considering VLM method and relations from Roskam book. Table 4.6 reports the value of these coefficients for each configuration. These coefficients can be also seen as efficiency; the bigger are (in absolute value), the less deflection is needed for a given manoeuvre.

		Configuration					
		1	2	3	4	5	6
$C_{L_{\delta_e}}$	[rad ⁻¹]	1.87	1.33	1.18	1.28	0.56	0.73
$C_{M_{\delta_e}}$	[rad ⁻¹]	-1.61	-1.18	-1.05	-0.98	-0.42	-0.49

Table 4.6: $C_{L_{\delta_e}}$ and $C_{M_{\delta_e}}$ coefficients for the 6 configurations shown in Fig. 4.9. They are computed using VLM technique [MIT18a].

Other important coefficient to evaluate is the hinge moment for control surfaces, defined as

$$\mathcal{M}_H = \frac{1}{2} \rho S_H c_H V^2 C_H \tag{4.7}$$

where H is the hinge moment and C_H the relative coefficient, S_H and c_H the reference area and length respectively for elevons. The hinge moment coefficient is modeled in a similar manner than the other aerodynamic coefficient:

$$C_H = C_{H_0} + C_{H_\alpha} \alpha + C_{H_{\delta_e}} \delta_e \tag{4.8}$$

The coefficients that appear in Eq. (4.8) are estimated directly in AVL; results for each configuration are reported in Table 4.7.

4.2.3.2 The longitudinal control for a BWB configuration

In order to draw conclusions, a closed loop control law is modeled in Matlab/Simulink [Mat18]; the problem is solved using the H_∞ technique [AN17]. The thrust effects are neglected in this analysis, thus relative terms in Eq. (4.4) are set to zero.

Four different criteria are considered to evaluate performances of the configurations: the hinge moment coefficient evaluation, the saturation limits (defined by the maximum load factor in the flight envelope, for the category chosen $n = 2.5$ [Meg12]), the surface deflection

		Configuration					
		1	2	3	4	5	6
C_{H_0}		0.002558	0.003074	0.001205	0.000801	-0.000516	-0.002178
C_{H_α}	[rad ⁻¹]	0.019881	0.017334	0.009186	0.012827	0.002598	0.011336
$C_{H_{\delta_e}}$	[rad ⁻¹]	0.032088	0.019938	0.015927	0.020709	0.008863	0.021461

Table 4.7: Hinge moment coefficients to define the model of Eq. (4.8) for the 6 different configurations shown in Fig. 4.9.

and the power demand for the elevons actuation, defined as [Fra+12]

$$P_{act}(t) = \dot{\delta}_e(t) \mathcal{M}_H(t) \quad (4.9)$$

These quantities are evaluated for each configuration shown in Fig. 4.9, on a given set of angles of attack. Results are shown in Fig. 4.10 for the elevon deflection, Fig. 4.11 for the maximum hinge moment and Fig. 4.12 for the actuator peak power. Results refer to a stationary condition, after the transitory period caused by an input law.

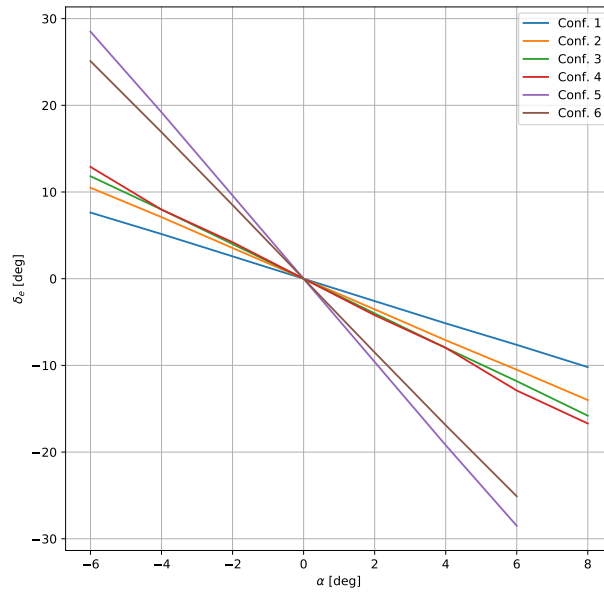


Figure 4.10: Elevon deflection δ_e for the 6 BWB configurations of Fig. 4.9, as function of demanded angle of attack.

In terms of elevons deflection (Fig. 4.10), the first configuration is indeed the one that gives the best results, especially for high variations of angle of attack (which are equivalent to high load factors). Configurations 2, 3 and 4 have similar properties, not so different from that of configuration 1 in any case, while the last two configurations are by far the less performing and reach saturation limit maneuver. Indeed the efficiency of the elevons type A is much lower than that of type B and C, and using them alone will require very high deflection to balance the aircraft. This is also seen from Table 4.6, which shows the efficiency for configurations 5 and 6 is worse than the others. It is to highlight that deflections are so high that before reaching the limit values, the flow may occur in stall phenomenon.

Coming to the hinge moment (Fig. 4.11), it is to note that configurations 1 and 2 represent again the most performing among the 6 configurations. Indeed, the hinge moment depends on the elevons deflection, and so the same conclusions as before can be drawn in this case.

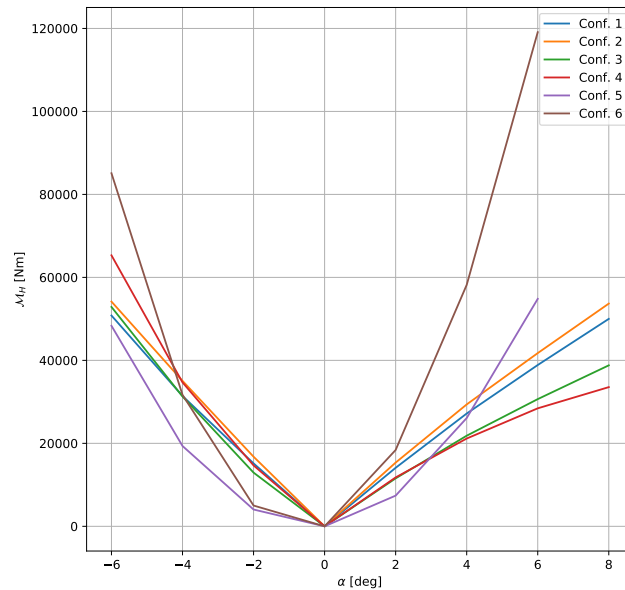


Figure 4.11: Maximum hinge moment for the 6 BWB configurations of Fig. 4.9, as function of demanded angle of attack.

Note that the higher the number of elevators, the smaller is the necessary total deflection and consequently the hinge moment. This reflects in a reduction of the actuator system, which needs to provide less power, saving mass and internal volume. The values, however, are quite high for all the configurations, but it is to remark that surfaces have big areas (between 10 and 12 m²), which is almost 10 times the size of a conventional A320 aileron. Nevertheless, a certain uncertainty is related intrinsically to the multifidelity adopted: despite the reliability in the CFD values, the VLM are based on limiting assumptions, which introduce an error, perhaps difficult to quantify at this stage. Also, it is recalled that the BWB reference aircraft is stable with a margin of 46%, and then more power is demanded to systems for the trimming.

Finally, the peak power is to be discussed (Fig. 4.12). Contrarily to other cases, configurations 3 and 4 represent the most performing for high variation of angle of attack. At low angle of attack, all the configurations show similar performances, even with some minor differences. This is due to the fact that, at small angle of attack, the power consumption demanded by smaller deflection compensates the smaller energy consumption of configurations 3 and 4. Also, configurations 5 and 6 seem to require less actuation power than the others for small variations, but their efficiency drops drastically for high changes, make them not worthy of further analyses.

To conclude, it seems that configurations 1 and 2 are the most interesting for BWB longitudinal control: despite they are not the most performing in terms of peak power, they are the best compromise among all the criteria. Configuration 1 features one elevon type A in

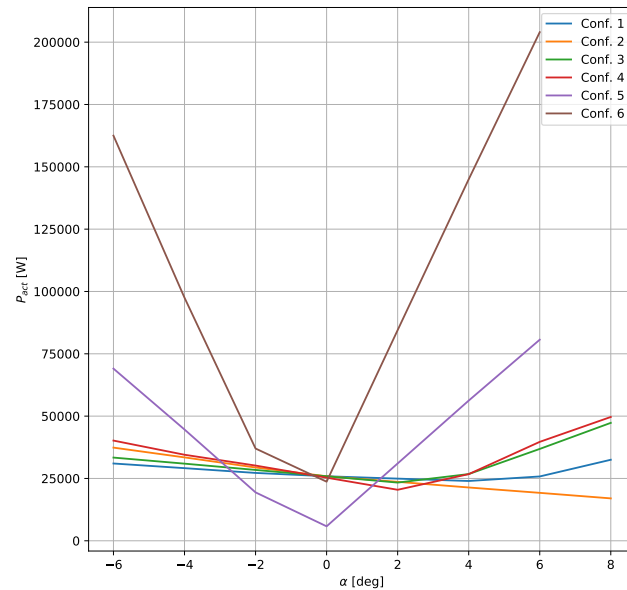


Figure 4.12: Peak power for the 6 BWB configurations of Fig. 4.9, as function of demanded angle of attack.

the centerbody, a location where it could be convenient to save space in order to accommodate propulsive or other aircraft systems. Moreover, one more elevon results in more weight and higher costs (design, operative and maintenance costs): despite the configuration is slightly more power efficient, results are so close that it seems the less power demanded does not compensate the greater weight and costs.

In conclusion, after the analysis here conducted, a configuration like the number 2 of Fig. 4.9 seems to be the best choice for the BWB longitudinal control. This configuration shows that the BWB concept can be trimmed with specific configuration of elevons. The choice done here leaves the centerbody trailing edge free, which can be used to locate distributed propulsion systems, a non trivial aspect.

However, it is to remark that this analysis has lots of limitations, related mainly to the numerical methods, but also to the thrust effects neglected, and in the future more detailed studies must be carried out, including also an assessment of the lateral control with the chosen configuration.

4.2.3.3 Sensitivity analysis on the BWB stability

Once that the configuration is selected, an analysis on the stability has been conducted. Indeed, it has been said that the BWB reference geometry is very stable, with a margin

of 46%, meanwhile for a BWB previous works suggest a reduced margin, near zero [NW96; AK89; Wan12]. In some cases it is also suggested to have an unstable aircraft, which is trimmed defining automatic control laws. Also, it is to underline that a margin of 5-10%, required for conventional aircraft in a BWB architecture is translated into a much greater distance between center of gravity and neutral point, because of the large chords; as example, for the BWB ISAE-Supaero and ONERA reference geometry 10% of the MAC corresponds to 1 m.

For this reason, the static margin is changed in order to understand how it impacts the trim condition, regarding the angle of attack α , the elevons deflection δ_e and the variation of LoD with respect to non trim condition. The analysis has been conducted using AVL, which automatically computes the trim condition. The neutral point is not known a priori, so a first estimate is given and then the position of the center of gravity is obtained reversing Eq. (2.5):

$$x_{cg} = x_n - SM\bar{c} \quad (4.10)$$

This procedure is iterated until the convergence is reached. It is recalled that in this research the assumption that SM is positive corresponds to a stable condition.

Results are shown in Fig. 4.13 regarding the three quantities of interested listed above. As expected, the SM strongly impacts the trim: for a margin of 10% the difference in LoD between trim and no trim condition is about 20%, as it decreases up to 2% for a margin near to zero. This is due to the elevons deflection which is lower, and then reduces phenomenon of separation at trailing edge. It is also to note that the angle of attack, for a margin of 10% is about 6 deg, which is unfeasible for modern aircraft, meanwhile it reduces to 4.5 deg for lower margin, that represents a more reasonable value.

It is to highlight that in this case the center of gravity is fixed in order to obtain the desired SM, and this procedure is set only for stability studying purposes, but in reality the SM represents an output and not an input of the system. As conclusion, for the BWB sizing reduced limits for the SM can be considered; to be conservative in the design and limit the risk, the case of unstable aircraft is not taken into account, and the modified condition states that the SM must be between 0 and 5%, in place of 5 and 10%:

$$0 \leq SM \leq 0.05 \quad (4.11)$$

At this point, the longitudinal control has been studied; the final configuration chosen defines which is the space needed for control surfaces and the usable space for distributed propulsion or other systems. Next section will present the structural design, in order to get a surrogate model for the mass estimation.

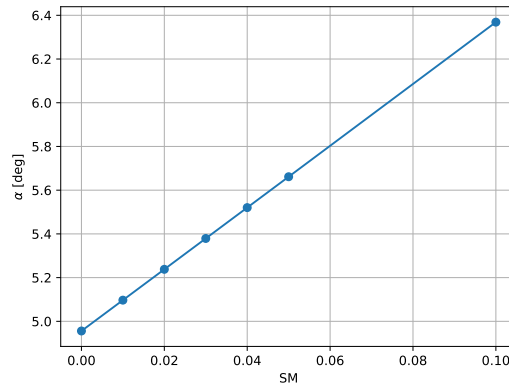
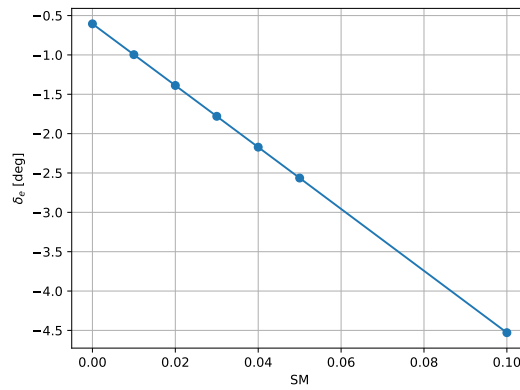
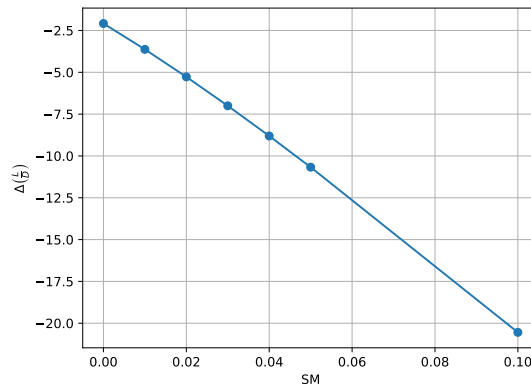
(a) Angle of attack α .(b) Elevon's deflection δ_e .(c) Variation of LoD value $\Delta\left(\frac{L}{D}\right)$.

Figure 4.13: Sensitivity analysis of trimmed condition with respect to the static margin. Quantities of interest considered are the angle of attack α , the elevon's deflection δ_e and the variation of LoD value between trimmed and non trimmed condition $\Delta\left(\frac{L}{D}\right)$.

4.2.4 Blended Wing-Body structural design

4.2.4.1 Modelling of the Blended Wing-Body internal structure

For structural design it is intended the definition of the cabin concept and the design of structural elements, such as ribs, stringers and spars. In Sec. 1.3.2.1 three different cabin concepts have been analysed, pointing out their advantages and issues regarding some criteria, as specified in Table 1.3. In this research, it has been decided to consider an integrated cabin, because it represents the best compromise between passenger comfort, aerodynamic and structural loads.

The structure is more complex than a conventional aircraft, since the cabin is not cylindrical anymore and elements pass through this part, so that the usable centerbody volume for payload is reduced. Following the work done by Bradley [Bra04], there are two spars, located at the leading edge (10% of the chord) and at 70% of the chord. In the integrated concept there is no separation between internal and external shell but just a single panels layer sustain both pressurization and aerodynamic load: these panels are modelled at thin plates with stringers to reinforce the structure, and they follow the thin plates theory [Meg12]. Regarding the stringers, some literature references use the equivalent thickness philosophy to allow a fast and changeable stringer properties and configuration [Bra04; Muk05]. This is a possibility to reduce computational cost; however, for the present study, however, beam theory is applied [Meg12] in order to have more accurate results. Finally, in the cabin there are some ribs to separate the centerbody from the transition zone, and eventually divide also the internal cabin. A drawing of the final concept is shown in Fig. 4.14; ribs have been omitted for visualisation purposes.

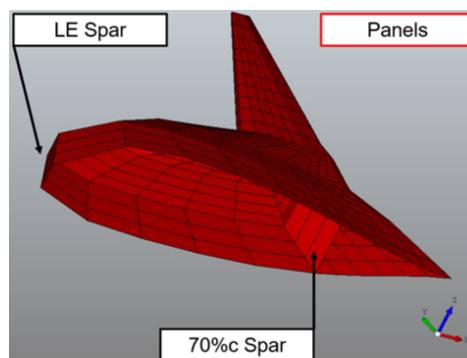


Figure 4.14: BWB geometry visualisation; ribs have been omitted for clarity purposes.

The analysis is carried out through the FEM technique; tools used are the software Patran for modelisation and meshing [MSC18] and Nastran for the structural analysis [Sie18]. Due to symmetry, only half of the BWB is considered, thus in the centerbody the symmetry boundary condition is applied.

Concerning the material, the classical Aluminium Alloy 7075 (AA7075) used in aeronautics

is considered by the time [ZZ12] and its properties are listed in Table 4.8. It is to note that

Young's modulus	71.7	GPa
Poisson ratio	0.33	
Max tensile stress	570	MPa
Density	2810	kg m ⁻³

Table 4.8: Aluminium alloy 7075 properties [Meg12].

this choice is mainly dictated by the fact that this material is widely used in aeronautics, but it is in contrast with what is suggested in literature. Van Dommelen and Vos [vV14], as well as Mukhopadhyay [Muk05] consider this material, but Liebeck argues that the high variation of pressure loads in the cabin favours the use of composite materials [LPR98], and different authors consider deep sandwich composite with honeycomb aluminium core [Muk07], isotropic and orthotropic composite materials [Muk96; Muk+04], and the advanced Carbon Fiber Reinforced Polymer (CFRP) material [Bra04]. In particular, this late one is used by Bradley to get the surrogate model described by Eq. (1.7).

4.2.4.2 Static analysis

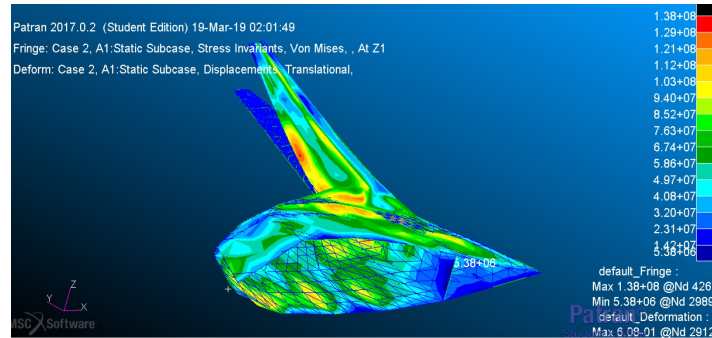
At the time, a static analysis is conducted to get the deformation and understand the feasibility of the concept to carry out the loads. Dynamic is not included, by this is not a limitation since such kind of analysis is more focused in studying the aeroelasticity effects, and this step can not be done if first it is ensured that in static condition the structure comply with sizing criteria. At the end, also an estimation of the mass can be done, which can be compared with the models adopted in FAST [DC12] and by Bradley [Bra04].

The pressurization loads come from the Bradley reference again [Bra04], which suggest a value of ultimate pressure differential of 18.6 psi. Aerodynamic loads come from the CFD analysis previously done in Sec. 4.2.2: they are concentrated into shear and bending applied to the outer rib of the centerbody. They are then multiplied by 2.5, which represents the ultimate design load for the sizing [Meg12]. Table 4.9 reports the load case for the static analysis.

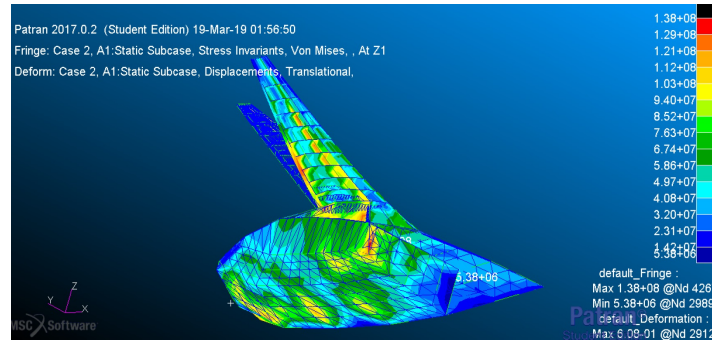
Pressurisation	18.6	psi
Vertical shear force	230	kN
Bending moment	1200	kN m
Load factor	2.5	
Aerodynamic load	From CFD	

Table 4.9: Loads applied on the BWB geometry for the FEM analysis considered.

Results of this static analysis are shown in Fig. 4.15 in terms of Von Mises stress; the optimisation of components to minimise the stress is carried out by the software. It can be observed that highest loads appear at the rear spar, in the pressurised area; in particular in



(a) Full model.



(b) Upper panels and Central ribs omitted for visualisation.

Figure 4.15: Static analysis results for the BWB reference geometry design.

the zone of connection between outer wing and centerbody. In this zone, the maximum Von Mises stress is of 136 MPa; due to the optimisation, this value is very close to the maximum allowable tensile stress. The wingtip is the most deflected zone, with a deflection of 61 cm. Also wing torsion is detected, in the effect of a twist down more pronounced at the wingtip.

The thicknesses of each component are reported in Table 4.10. Note that the ribs in the pressurised zone are three times thicker than that of the non-pressurised zone, because of the non-circular pressurization. However, dimensions are limited and in agreement with what is

Component	Thickness [m]
Panels	0.05
Ribs, non-pressurised	0.0073
Ribs, pressurised	0.033
Ribs, wing	0.001
Spars	0.0033

Table 4.10: Structural components thickness for the static analysis of BWB reference geometry, case of maximum load factor $n = 2.5$.

obtained in conventional aircraft.

From these data, it is possible to estimate also the total mass, which is of 31.4 t: the centerbody accounts for 22.6 t, meanwhile the outer wing accounts for 8.8 t. In this calcu-

lation, the mass coming from the FEM has been multiplied by a factor 2, to account joints, fasteners and other components not taken into account in the FEM model [Muk96; Muk+04]. The detailed mass breakdown for the components is illustrated in Fig. 4.16. The panels represent the majority of the mass, as it is responsible for sustaining both pressurization and aerodynamic load; also the stringers are slightly oversized since it incurs a bending due to the non-circularity of the centerbody.

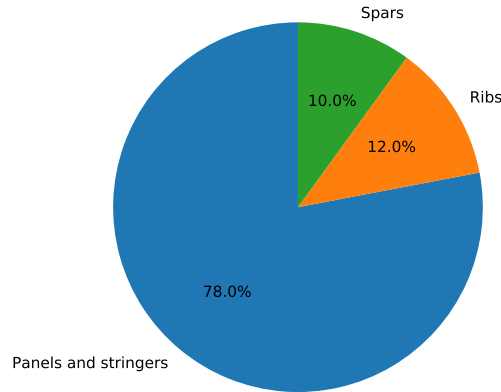


Figure 4.16: Structural components mass breakdown for the static analysis of BWB reference geometry.

A comparison between some available data in literature (see Table 1.4) shows that the value of 31.4 t is in the right order of magnitude for 250 or more passengers, but the value is doubled with respect to what has been estimated by Bradley for the 150 passengers BWB. A more detailed comparison between the FEM analysis and the low fidelity models, that are surrogate models described in Eq. (1.7) and the standard wing mass estimation used in FAST for the outer wing [DC12], is reported in Table 4.11. Table 4.11 identifies the major source of error in the centerbody: indeed, the model used in FAST for outer wing specifies the AA7075 as material, and thus is quite accurate, meanwhile Bradley to get its surrogate model for the centerbody mass considers the CFRP material.

	FEM	Surrogate model	Difference
Centerbody [t]	22.66	15.51	45.7%
Outer wing [t]	8.84	8.62	2.55%

Table 4.11: Comparison between the FEM analysis and the surrogate model for centerbody and outer wing, for the BWB reference geometry case. Aluminium alloy 7075 is used as material.

The CFRP material has significantly different properties. For the fiber configuration 0/90°C the density is 1550 kg m^{-3} , compared to 2810 kg m^{-3} for the AA7075, and the allow-

able tensile stress is 344 MPa, about 3 times higher than that of AA7075 (see Table 4.8).

For validation purposes, a new analysis is carried out considering the CFRM as material for the centerbody; results for mass estimation are reported in Table 4.12. In this new case, the difference is less than 2%, and then Eq. (1.7) is validated.

	FEM	Surrogate model	Difference
Centerbody [t]	15.67	15.51	1.6%

Table 4.12: Comparison between the FEM analysis and the surrogate model for centerbody and outer wing, for the BWB reference geometry case. CFRM material is used in the centerbody.

In conclusion, it has been shown that there is a good correlation between the FEM and the surrogate models, and thus the same model already adopted in FAST is retained for the outer wing, meanwhile for the centerbody Eq. (1.7) is used, eventually with a corrective factor to consider the aluminium alloy in place of the CFRM as material.

At this point, it is time to pass to the nacelle integration, in order to estimate the effect of an ingesting boundary layer. This will be the goal of the next section.

4.2.5 Nacelle integration in the Blended Wing-Body architecture

This section studies the integration of the nacelle in a BWB architecture, in order to estimate the effect of an ingesting device as the BLI. At this stage of the research, so much resources have been deployed in the CFD analysis that it has not been possible to carry out this analysis using the CFD, due to the high number of hours required by the modelisation, meshing and analysis.

For this reason, the study is carried out using the software MSES, developed at MIT by Mark Drela [Dre07]. The code is a medium fidelity software, that relies on hybrid methods between potential flow and CFD regression analysis, capable to analyse the flow field for multibody objects. Also, one of its greatest features is the possibility to optimise the body thanks to the LINDOP, a subroutine of MSES [Dre96]. LINDOP has been developed mainly for the optimisation of multi-element airfoils [Dre93], which is interesting to optimise a nacelle integrated in a BWB. The main limitation of MSES is that it is a 2D software, and all the three-dimensionality effects, which are not trivial in case of ingesting propulsors, are neglected.

The BWB reference geometry, shown in Fig. 4.1, is divided into different slices, and each one is studied separately using MSES. At the end, the global C_L and C_D values are obtained through numerical integration [RK99]. The electric motors are distributed only in the centerbody part, for what has been said in Sec. 4.2.3; the integrated geometry is shown in Fig. 4.17, in the symmetry plane (that of maximum length).

The flow condition for the analysis corresponds to the estimated design point and they

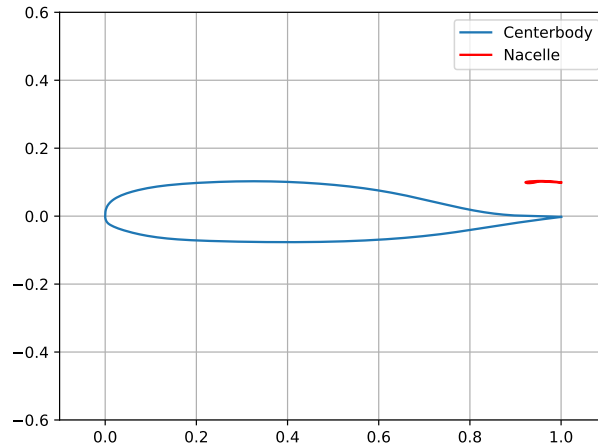


Figure 4.17: BWB reference geometry, together with integrated nacelle, at the symmetry section.

are reported in Table 4.13. The value of thrust coefficient is estimated by the knowledge of

Mach number	0.78
Angle of attack	1.5 deg
Reynolds	6.24×10^6
C_T	1.66×10^{-3}

Table 4.13: Condition for the study of nacelle effect in MSES.

the mass; in balanced flight it is possible to write

$$T = \frac{m_{cr}g}{\left(\frac{L}{D}\right)_{cr}} \quad (4.12)$$

The value of LoD comes from the CFD analysis. A total of 32 electric motors can be placed in the zone of interest, and thus this number is considered in the analysis. This value is estimated from the ducted fan sizing procedure described in Sec. 3.3.8.

The initial geometry for the nacelle is the NACA64A010; using the code LINDOP it is then optimised in order to reduce the drag coefficient, section by section. Drela suggests to use a multipoint optimisation [Dre93]: in fact, with the single point there are very good performance at the optimisation point, but in off design conditions they may not be satisfactory.

The objective function is

$$f = 0.75C_{D_{M=0.6}} + C_{D_{M=0.7}} + 1.25C_{D_{M=0.78}} \quad (4.13)$$

where the subscripts indicate the Mach number to which the C_D refers. In this way, all the transonic regime is covered, and the design point has more weight in the optimisation than

the others.

The final nacelle geometry, after the optimisation, is shown in Fig. 4.18, meanwhile the performance of the geometry with nacelle integrated is reported in Fig. 4.19, varying the Mach number. On the left there is the non optimised case, meanwhile on the right the optimised one.

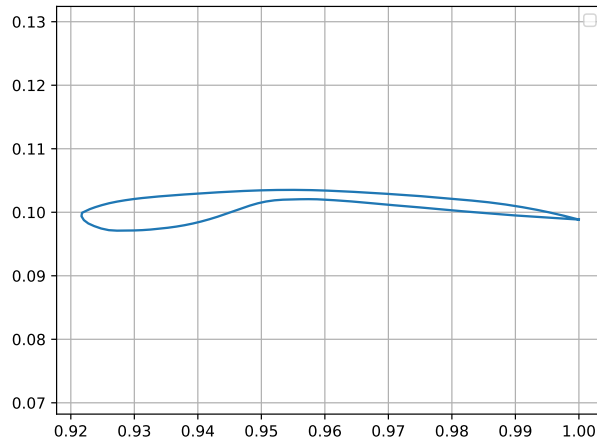


Figure 4.18: Detail of the optimised nacelle, mounted on the BWB.

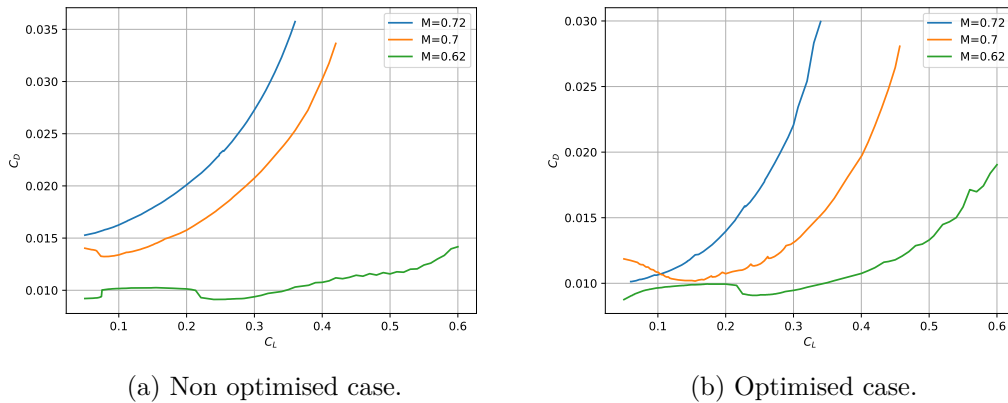


Figure 4.19: Performance comparison between the non optimised and optimised nacelle geometry using MSES.

From the comparison of Fig. 4.19 emerges that the baseline has not very good performances, despite the initial geometry of NACA 641010 is designed for transonic purposes [And11], but after the optimisation the wave drag is well reduced, and thanks to the multipoint adopted in Eq. (4.13) the reduction occurs for all the Mach numbers.

To estimate the effect of a BLI device, the procedure suggested by NASA is used [Gre+10b]. The drag coefficient can be decomposed in two terms, one related to the dissipation of energy C_ϕ and another one to the vortex dissipation C_{E_v} :

$$C_D = C_\phi + C_{E_v} \quad (4.14)$$

In case of ingestion, the term related to the energy dissipation is modified as

$$C'_\phi = C_{D_p} - f_{BLI} \frac{K_\infty - K_{TE}}{\rho_\infty V_\infty^3 S_w} \quad (4.15)$$

where C_{D_p} is the parasite drag of non ingesting case, f_{BLI} the fraction of the body's kinetic energy deflected ingested by the engine, K_∞ and K_{TE} the kinetic energy at inflow and trailing edge respectively.

From MSES it is possible to obtain all the boundary layer parameters, in particular the displacement and kinetic energy thickness: a comparison between the non ingesting and ingesting case is shown in Fig. 4.20.

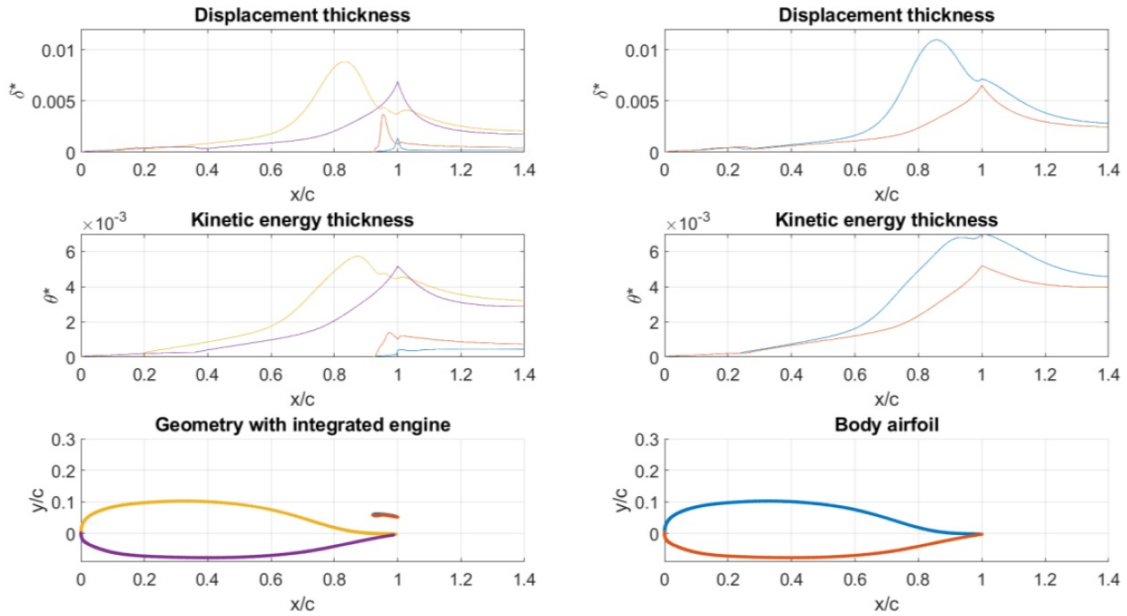


Figure 4.20: Displacement thickness and kinetic energy thickness comparison between the integrated geometry and the isolated body geometry.

Thanks to the knowledge of these parameters, through integration it is possible to estimate f_{BLI} and C_ϕ . For the condition of Table 4.13, the BLI effect is estimated in a reduction on the drag coefficient of 14%. The value is in agreement with estimations given by IATA reports [IAT13b], despite the limitations due to the 2D assumption.

In reality, for an ingesting device a flow distortion appears, as explained in Sec. 1.3.1.3,

which worsen the benefits; on the other hand, an ingesting architecture saves fuel because the nacelle wetted area is reduced, which is beneficial for aerodynamics and mass. So at the end the benefits coming from the BLI are a balance between these effects. A more accurate estimation can be obtained only using the CFD; for the purposes of this research these benefits are simply modelled with a corrective factor. To be conservative, a reduction in C_D of 10%, in place of 14% is considered for the evaluation of the concept. This value is in agreement with other studies on the BLI effects [IAT13b; Ste+12a; Ura+18].

The estimation of BLI is the last step that had to be carried out to finally correct the models; next section is deputed to define the parametrization for the BWB planform sizing and the internal arrangement.

4.2.6 Blended Wing-Body design synthesis

This section provides an exhaustive analysis of the decisions done in the BWB sizing: at first the parametrization adopted is presented, and then the final concept, including the subsystem positioning, is described. It is to highlight that most of the assumptions done in the second part are on a level of detail that can not be included in the conceptual sizing loop; however decisions on cargo, exit doors and so on must be done in order to give feasibility to concept, and limit the usable volume in the sizing process.

4.2.6.1 Planform sizing

Since the BWB relies on the idea of having a whole lifting surface, it is schematised as a wing with three or more sections, and the parametrization here adopted follows this concept. The planform is divided into three parts: centerbody, transition zone and outer wing, each one considered as a wing section. The entries for the sections are the same of a wing planform: sweep angle, taper ratio, span or aspect ratio, and thickness to chord ratio.

The parametrization is shown in Fig. 4.21, with the main parameters noted on the image. The hardest section to model is the central one, since it has to supply enough space for seats allocation; once that the cabin is fully sized, transition zone and outer wing can be easily obtained. The explanation of the sizing starts indeed from the cabin.

4.2.6.2 Cabin modelling

The cabin must allow enough space for the passengers allocation; following the work of Bradley [Bra04] the cabin is divided into bays, separated by ribs in an integrated design. Each bay is single aisle, with two lines of seats.

The starting point for the sizing procedure is the definition of an equivalent tube-and-wing configuration, with the same number of passengers per row of a bay, to know the length

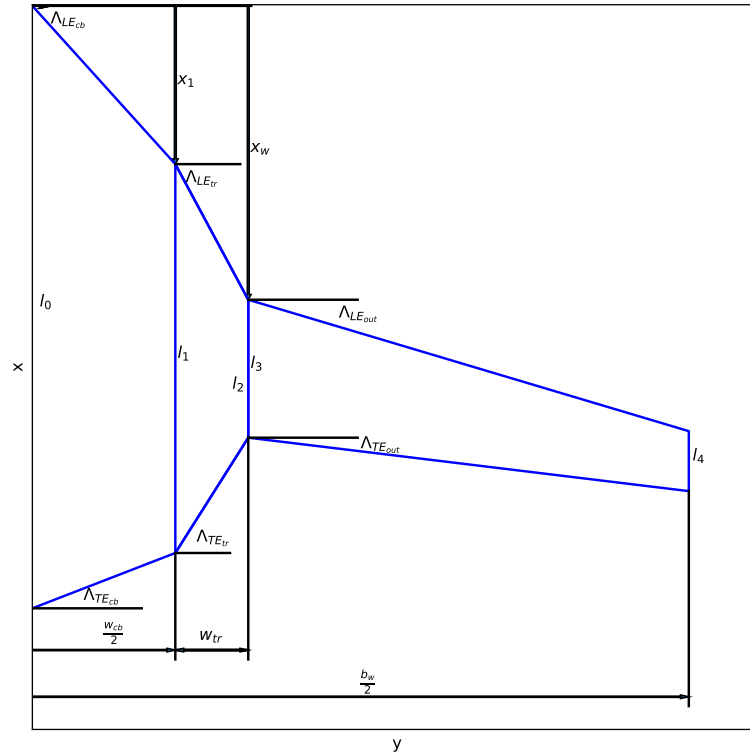


Figure 4.21: Planform scheme for the Blended Wing-Body sizing.

required for all the seats:

$$L_{req} = \sum_{i=1}^3 N_{r_i} L_i + N_{exit} W_{exit} \quad (4.16)$$

where N_{r_i} is the number of rows and L_i the length of the seats for the i class, N_{exit} and W_{exit} the number and the width of exit doors. In the case of a single class, which is the case of interest for the type of aircraft selected, $N_r = \frac{N}{6}$, where N is the number of passengers and 6 represents the seats per row in economic class.

The number of bays is then computed considering a rectangular cabin:

$$N_b = \left[\frac{L_{req}}{l_{out_{max}}} \right] + 1 \quad (4.17)$$

where $l_{out_{max}}$ is the maximum allowable outermost wall length, computed as it will be explained later, and the square brackets represent the integer function.

With some geometrical considerations, it is possible to write an equation to get the total

length available for seats in the BWB (see Fig. 4.22 for clarity):

$$L_{tot} = \sum_{i=1}^{N_b} \left[l_{out} + \frac{1}{2} (i-1) w_b \tan \Lambda_{cb} \right] = N_b l_{out} + \frac{1}{2} w_b \tan \Lambda_{cb} \sum_{i=1}^{N_b} (i-1) \quad (4.18)$$

with l_{out} outermost wall length, w_b the bay of a single width and Λ_{cb} the centerbody sweep angle, computed at leading edge.

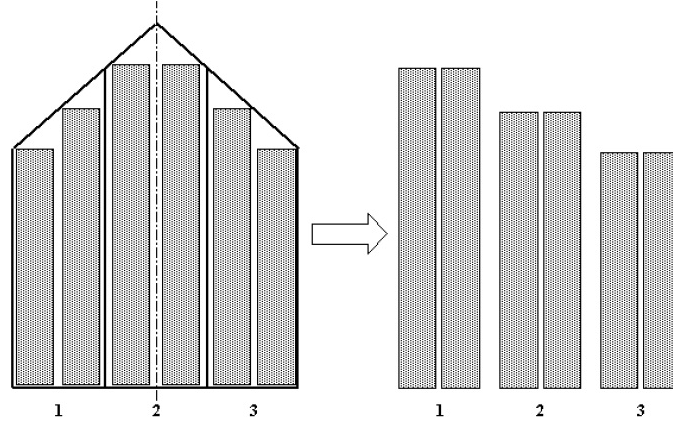


Figure 4.22: Seats arrangements for a three class BWB configurations.

Setting $L_{req} = L_{tot}$ yields to the following expression to compute the actual outermost wall length:

$$l_1 = \frac{L_{tot} - \frac{1}{2} w_b \tan \Lambda_{LE_{cb}} \sum_{i=1}^{N_b} (i-1)}{N_b} \quad (4.19)$$

and the cabin results fully defined, since the centerbody is then obtained as follows:

$$l_0 = l_1 + \frac{N_b}{2} w_b \tan \Lambda_{LE_{cb}} \quad (4.20)$$

A margin is then taken to allocate horizontal aisle and toilets, according to preliminary methods from Roskam [Ros05c]. These dimensions are only related to the pressurised cabin; recalling that this occupies the 70% of the centerbody, the total length is obtained dividing these values by 0.7.

This procedure allows to size a cabin, but it depends on the value of $l_{out_{max}}$, which is unknown at the beginning. Bradley suggests to use 15.6 m, with a centerbody sweep angle of 45 deg. In the reference paper, unfortunately, there are no information about the origin of this value [Bra04]; in this research it has been considered that the maximum length is deduced from the centerbody taper ratio. Since the value l_0 is unknown, an iterative procedure is needed.

The length must also supply the cabin vertical arrangement criterion. According to Airbus, the minimum cabin height has to be 1.95 m; considering a 12% structural margin [Ray18];

Ros05c] yields to a total height of 2.18 m. From the value of thickness-to-chord ratio it is then possible to estimate the total length needed in this section to provide such height:

$$l_1 = \frac{h_{min}}{\left(\frac{t}{c}\right)_{cb}} \quad (4.21)$$

An iterative procedure is set up to find the values of thickness-to-chord ratio and maximum outmost length of the final geometry.

In this way, the cabin planform is finally sized, but nothing has been said on the airfoil sizing yet. The only information known is that reflex airfoils are needed for stability purposes, as recalled several times [Ale14; NW96]. The most correct way is to include the airfoil sizing within the optimisation procedure, but this is unfeasible without the application of CFD, which is very costly.

The relation described by Eq. (4.21) can help to choose a value of thickness-to-chord ratio able to ensure enough space at the section with maximum thickness, but this is not sufficient to ensure that all the cabin fits in the profile. In fact, the minimum height criterion must be valid in all the sections, and the most stringent one is that corresponding to the last row of passengers (70% of the chord).

The relative thickness can be changed in post processing where the planform is obtained, but this is not coherent with the sizing process, and all the results will be misleading. Thus it is a key point to have the possibility to get as output a thickness-to-chord ratio that allows to choice an airfoil without the fitting problems. To do that, the analytic thickness distribution must be known, to be able to constraint the height value at 70% of the cabin.

The thickness distribution is know only for the NACA family [Av59], where

$$\pm y_t = \frac{t}{0.20} \left(0.2969\sqrt{x} - 0.1260x - 0.3516x^2 + 0.2843x^3 - 0.1015x^4 \right) \quad (4.22)$$

with y_t the thickness distribution, t the maximum thickness and x the abscissa; all of these parameters are in percentage of the chord.

Requiring that $y_t c = \frac{1.95 \times 1.12}{2}$ at $x = 0.7$ it is possible to correct the initial estimation of thickness-to-chord ratio, that suites the cabin height requirements. Once that this value is obtained within the sizing loop, it is possible to choose one of the NACA airfoil with the chosen relative thickness, avoiding the problem of fitting. In particular, the 5-digit series is worthy of attention because it is a family of reflex airfoil, that provides almost zero moment coefficient.

The condition described by Eq. (4.22) must be written for all the sections: in fact, the most stringent is the outmost section, where the length is smaller, but applying a constant thickness-to-chord ratio results in an oversizing of other sections, worsening the aerodynamics. For simplicity, in the sizing procedure only the symmetry and the outermost section are considered, and the mean value of thickness-to-chord ratio is taken for aerodynamic calculation.

However, it has to be remarked that the choice of NACA family has been done for simplicity and to close the problem, but it is just a first assumption that needs to be redefined in a more detailed design, with the help of high fidelity optimisation.

4.2.6.3 Transition zone and outer wing modelling

Once that the centerbody dimensions are got, the others come as consequence. For continuity, the root chord of the transition zone is equal to the tip chord of the centerbody; the tip chord of this zone is obtained by the definition of taper ratio as

$$l_2 = l_1 \lambda_{tr} \quad (4.23)$$

The surface of transition zone results to be:

$$S_{tr} = \frac{(l_2 + l_1) w_{tr}}{2} = \frac{(1 + \lambda_{tr}) l_1 w_{tr}}{2} \quad (4.24)$$

where w_{tr} is the width of transition zone, set to satisfy allocation criterion that will be later explained.

The sweep angle for this zone is not an input of the parametrization, but it is an output, according to the wing position:

$$\Lambda_{tr} = \arctan \frac{x_w - x_1}{w_{tr}} = \arctan \frac{x_w - w_{cb} \tan \Lambda_{LE_{cb}}}{w_{tr}} \quad (4.25)$$

The total planform surface is set by a top level criterion, as will be explained in next section. The knowledge of this surface plus the centerbody and the transition surface yields to the surface of outer wing solely:

$$S_{w_{out}} = S_w - S_{cb} - S_{tr} \quad (4.26)$$

and from Eq. (4.24) written for outer wing the root chord l_3 is obtained:

$$l_3 = \frac{2S_{w_{out}} b_{out}}{1 + \lambda_{w_{out}}} \quad (4.27)$$

with $b_{out} = b_w - w_{tr} - w_{cb}$. Of course, the total span is obtained by the aspect ratio definition as

$$b_w = \sqrt{AR_w S_w} \quad (4.28)$$

In this way, all the planform dimensions are fully defined. On the other plane, the thickness-to-chord ratio is sized considering space needing for the transition zone, and aerodynamic considerations, as for conventional aircraft, for the outer wing.

For sake of clarity, Table 4.14 reports all the geometrical entries needed for the adopted

parametrization.

Global	Centerbody	Transition zone	Outer wing
Aspect ratio	Sweep angle	Taper ratio	Sweep angle
Total area	Minimum cabin height		Relative thickness
	Taper ratio		Position
	Number of passengers		Taper ratio

Table 4.14: Sum up of geometrical entries for the BWB parametrization.

Finally, at this point the overall illustration, including some assumptions on the subsystems position, can be drawn, as in next section.

4.2.6.4 Subsystem positioning

The rendering of the Blended Wing-Body with distributed electric propulsion, final goal of this research, is shown in Fig. 4.23, as in OpenVSP. The electric motors are distributed at the trailing edge, in the centerbody, leaving free all the outer wing surface for control surfaces, as described in Sec. 4.2.3. At the wing tip there are two winglets, used also as vertical tails for lateral control.

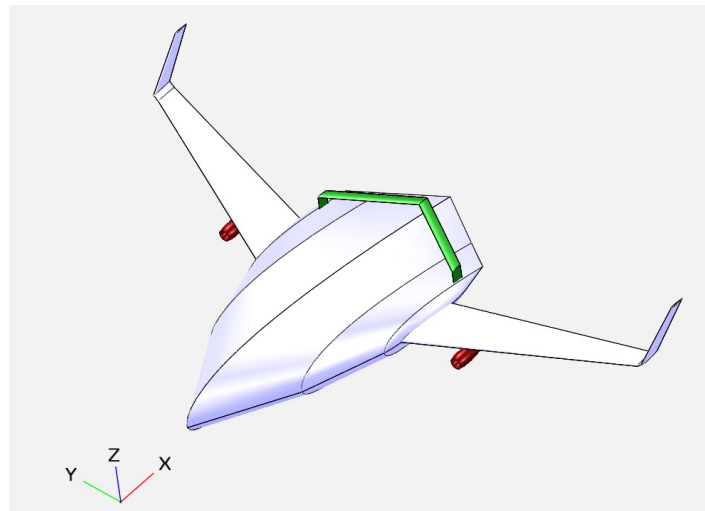


Figure 4.23: Final rendering of Blended Wing-Body with distributed propulsion.

It is to clarify that Fig. 4.23 just illustrates how the final concept looks like, but it is not yet a result of a proper sizing.

The first issue to deal with regards the boarding door, which is a point not well treated in literature. Some of the proposed concepts show boarding doors only at the leading edge (see *i.e.* [PSY18; Gre+10a]), but such a position may create problems since it does not account for the CS specification for large aeroplanes [EAS15]. The document states that each side of

the aircraft should be equipped with two doors of type I [Ros05c] for boarding, and two doors of type III for evacuation [Ros05c]. The first category is the most critical since they require fixed dimensions and a positioning at the front and the rear of the aircraft, meanwhile the second category does not have any constraint on the positioning, but only require to respect minimum dimensions and space between them [Ros05c; EAS15].

The requirement of boarding doors at the front and the rear of the aircraft has also been noted by Airbus, both for certification and acceptance purposes. A suitable arrangement for seats and boarding doors is shown in Fig. 4.24; the coloring helps to understand how each passenger is close to a door or not. In Fig. 4.24 emergency exits are not noted, but they

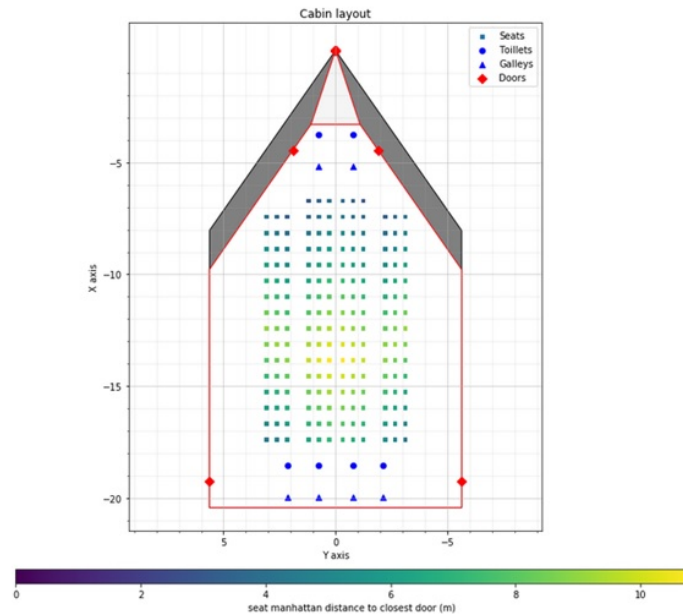


Figure 4.24: Seats arrangement and boarding doors position assumption for the BWB geometry.

are assumed to be in the central part of the cabin, coming out on the outer wing, as in a conventional aircraft. This configuration has been validated by Airbus experts, however it is to remark that it is just a proposition and not a detailed study. All related issues, such as the corridor that passes through the structure to allow passengers entrance, and the impact of the necessary cut-off on the structure must be detailed in future development. Note also that such configuration constraints the outer wing trailing edge, in order to leave enough space for the rear door.

One of the potential advantages is that the required boarding time may be reduced, thanks to the wider cabin that allows passengers to move in the cabin more freely. The colouring of Fig. 4.24 shows that there are just few places that are farer from an exit, but in mean all the others are close enough to reach its place in a reasonable time.

To confirm this theory, a boarding simulation is carried out, using a software called PAX-

elerate [Sch+16], which simulates the boarding using random dynamic algorithms for passengers' behavior [MN10]. Results are reported in Table 4.15 for the A320 cabin and the BWB

	A320	BWB
With handbags	11 min 47 s	8 min 12 s
Without handbag	9 min 54 s	7 min 4 s

Table 4.15: Boarding time for the BWB and the A320 reference aircraft with and without handbags, 150 passengers. Simulation carried out using PAXelerate [Sch+16].

cabin shown in Fig. 4.24. Both simulations with passengers carrying handbags and not show a reduced boarding time for the BWB. With these results, it has been decided to proceed with the proposed layout, and the choice has been validated by Airbus.

In a similar way, also the evacuation is expected to be facilitated in a BWB, despite by the time is still a point to be detailed. It is to not forget that in the middle of the cabin there is a rib, that works as structural element. This rib must be provided of some passages to go from a bay to another, that may weaken the structure: the effect is neglected at this stage.

The internal volume available is occupied by the cargo and the other subsystems, such as landing gears and propulsive element. The illustration of Fig. 4.25 clarifies the positioning, showing some details of internal arrangement.

The transition zone is used to place the cargo. For 150 passengers, the maximum payload to be placed in the freight is 6000 kg [Ray18; DC12]; in commerce different types of containers are available [Ros05c]. Among the possibilities, the LD3 are here considered: they have maximum dimensions of $153 \times 164 \times 200$ cm for a total capacity of 1588 kg, thus 4 of them are needed, as shown in Fig. 4.25a. The width of transition zone w_{tr} is fixed to 2 m to enable enough space to fit this type of containers.

Batteries and PMU are instead placed beneath the cabin. They do not need a lot of volume and can be stretched, so they can fit in the volume available in that zone. Also, this positioning allows to forward the center of gravity, resulting in an outer wing advanced toward the leading edge, leaving space at the rear for boarding doors. Note that to make batteries work properly, this zone must be pressurised too. In case the BWB uses conventional engines, the volume beneath the passengers cabin may be used for additional fuel tanks. The two gasturbines are placed beneath the wing: it is unusual to see engines in this position on a BWB, but among all the possibilities this one is the most reasonable. In any case, the gasturbines are considerably smaller than a turbofan engine, and they can be allocated there without any drawbacks regarding the height from the ground.

The landing gears are the remaining subsystems. Their dimensions are the same of the nose and main landing gear of the A320, increased of a percentage equals to the relative difference between the MTOW, to consider scaling effects. The nose landing gear, which is more compact, is beneath the cockpit, where the airfoil rounded shape leaves space. The main landing is instead placed after the main spar, at 70% of the chord. This position may not ensure enough rotational qualities at takeoff, but it is the only one possible. It is to

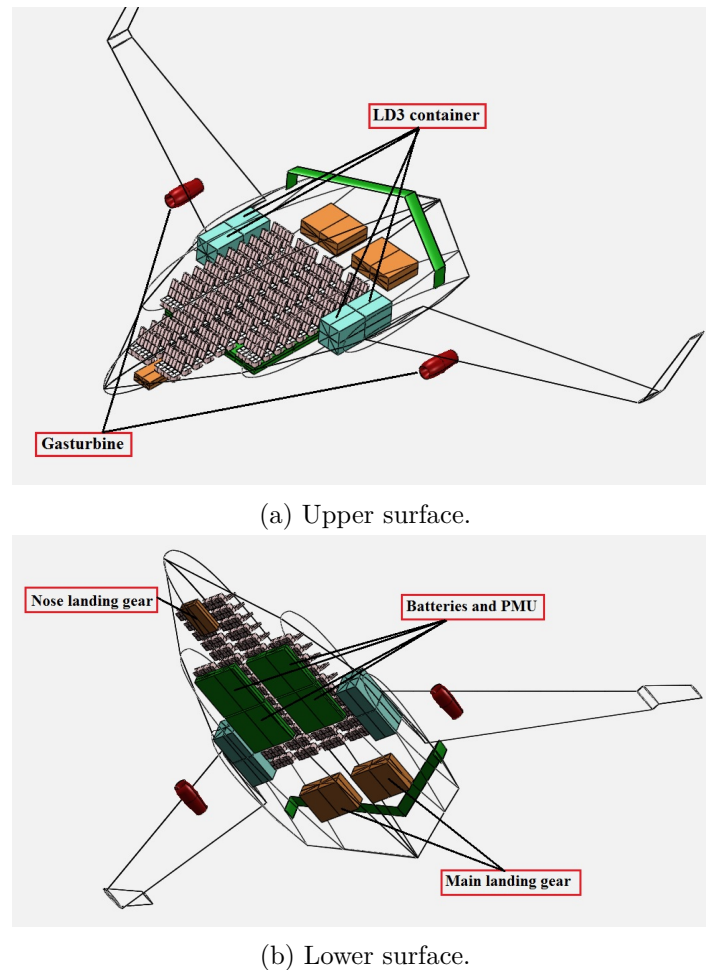


Figure 4.25: Blended Wing-Body with distributed propulsion rendering, detail of subsystems allocation.

not forget that the BWB is more compact and shows a considerably smaller total length, so the center of gravity variation is not as wide as for the conventional aircraft. To tackle this issue, it is assumed that the BWB can lift-off without rotation. To achieve that, the wing area must provide enough lift for a gliding takeoff in the required length: this condition is verified during the sizing loop, and later in the optimisation loop is added as a design constraint. The impact of no rotation is hard to estimate at this level: a priori, it can be assumed that the takeoff length is reduced, but in real such hypothesis opens the possibility to reduce the total height of landing gear. Thus the aircraft is closer to ground, which enhances the ground effect and improves the aerodynamic performances; detailed design to verify these considerations is marked in the suggested future development.

Page et al. [PSY18] developed a landing gear system that sets a virtual rotational point in order to ensure moment at takeoff in all the conditions. Unfortunately, they do not provide details since it is a patent; in this research the assumption of takeoff without rotation, as for the B-52, is done.

The description above has been done only considering the needing in volume for the main subsystems, but it does not present any detail on operations. For example, the cargo can be placed in the transition zone, but none has been said on the doors and systems to open and move containers. Same considerations are done for the batteries, that must be removed and inserted easily between one mission and another. These operations require cut-off, that must be properly sized, and weaken the structure. Future work on a more detailed design can not prescind by these aspects.

Next section will finally present the integration of all the methods developed in the sizing procedure, to design a BWB, and the further implementation of the MDA in an optimisation loop.

4.3 Methodology for the Blended Wing-Body sizing

4.3.1 MDA sizing loop

The revised sizing loop, tailored for the BWB, is shown in Fig. 4.26, with the detailed algorithm reported in Alg. 8. Note that, as intermediate step, the MDA presented here is intended to design a BWB with conventional propulsion; the hybrid architecture will be added later on.

Algorithm 8 FAST algorithm, tailored for the BWB sizing with conventional propulsion. Numbering is referred to Fig. 4.26.

Require: Initial design parameters (TLAR)

Ensure: Sized aircraft, drag polars, masses, design mission trajectory

0: Engine initialization.

1: First estimate of top level parameters, such as wing area, OWE and MTOW.

2: Initialise the sizing loop.

repeat

3: Wing area sizing. For the BWB the wing area is intended as total planform area.

4: Geometry is obtained and then resized to match stability constraint, according to the parametrization described in Sec. 4.2.6.

5: Aerodynamic calculation. Here corrective factors to adjust data with high fidelity are applied.

6: Mass breakdown analysis.

7: Performance calculation.

8: Update the value of MTOW, with the data coming from analyses 5 and 7, according to Eq. (2.4).

9: Check the convergence: if the tolerance is below the needed threshold, return the sized aircraft, otherwise proceed to next iteration.

until 9 → 3: MDA has converged

The xDSM scheme illustrated in Fig. 4.26 does not differ greatly from that one of Fig. 2.1. Indeed, the global procedure is always the same, at least regarding the call of analyses. The

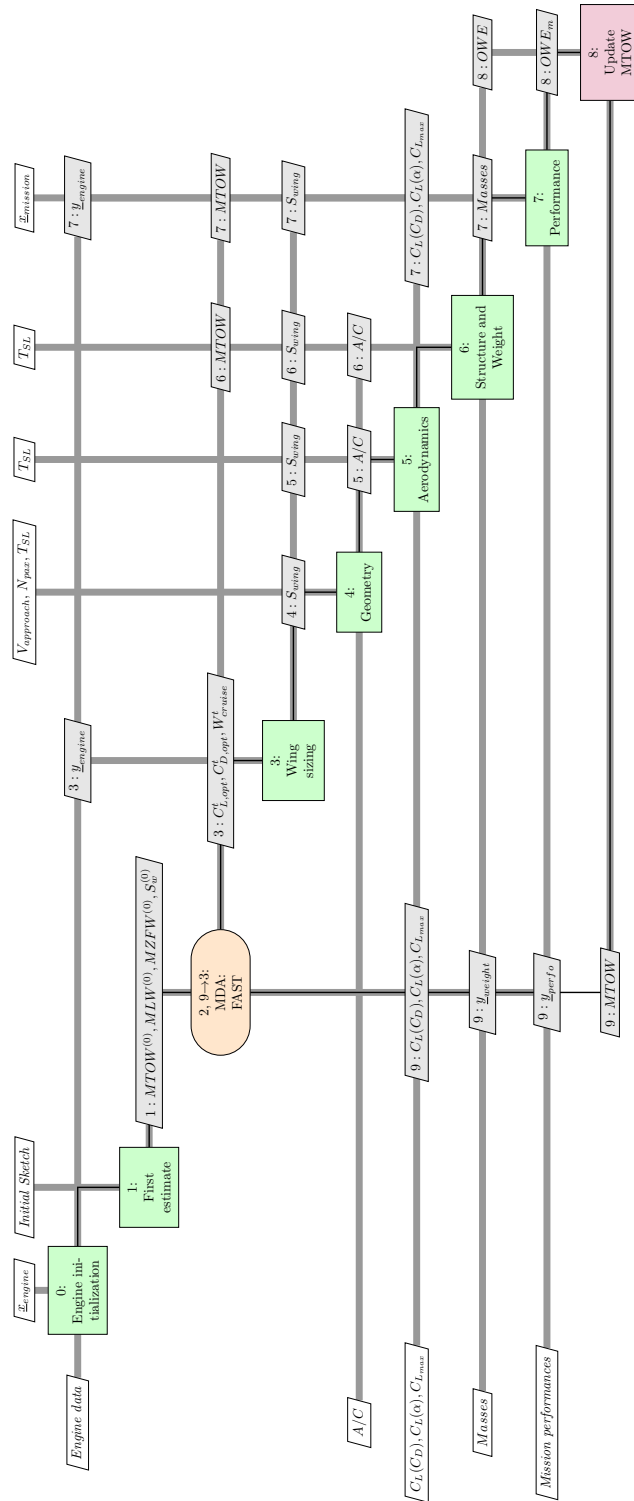


Figure 4.26: MDA loop tailored for the Blended Wing-Body sizing with conventional propulsion.

differences are in the modules adopted, that are tailored for the BWB, as described in previous sections.

The wing area, called at step 3, is also changed: it is to recall that a conventional aircraft must comply with approach condition and fuel stored, but these criteria may not be suitable for a BWB. Just as example, with the data of the BWB reference geometry reported in Table 4.1 the surface computed with the approach condition results to be around 150 m², as the planform reference area is 313 m².

To understand what is the proper condition, a constraint analysis is carried out [Ros05a]. This analysis gives as output the plot of thrust to weight as function of wing loading for different flight conditions. In particular, the criteria considered are:

- Approach constraint, to supply enough lift in this phase;
- Takeoff constraint, to ensure that the aircraft can depart in a prescribed runway length;
- Initial climb constraint, to ensure that at 400 ft and in OEI condition the climb rate is at least 2.4%;
- Top of climb constraint, to ensure that the aircraft has a reserve of vertical speed of 300 ftmin⁻¹;
- Geometrical constraint, in order to guarantee the total area is greater than the centerbody area only;
- Span constraint, which is limited to 36 m for this category of aircraft.

The constraint diagram for the BWB is shown in Fig. 4.27; reference mass is the MTOW, thrust is intended at sea level. On a conventional aircraft, for short and medium range the top of climb condition is not so relevant in the design; contrarily for the BWB it becomes the main limitation at the design space. It is also to note that the approach condition can not be the right one because the resulting area is lower than that of the centerbody. Another remarkable point regards the optimum point: the top of climb condition shows a minimum, which corresponds to the maximum LoD value at that point. Thus, at step 2 the top of climb condition replaces the approach condition for the BWB.

Geometry, aerodynamic and mass breakdown modules are modified to consider the models and correction developed in Sec. 4.2. Parametrization shown in Fig. 4.21 is used; for the vertical tail same methods as for the TAW concept are applied, with the only difference that for a BWB there are two surfaces in place of one, corresponding to the two winglets. Performance module and convergence criteria are not modified.

The next step is finally the definition of an MDO formulation for the Blended Wing-Body with distributed electric propulsion.

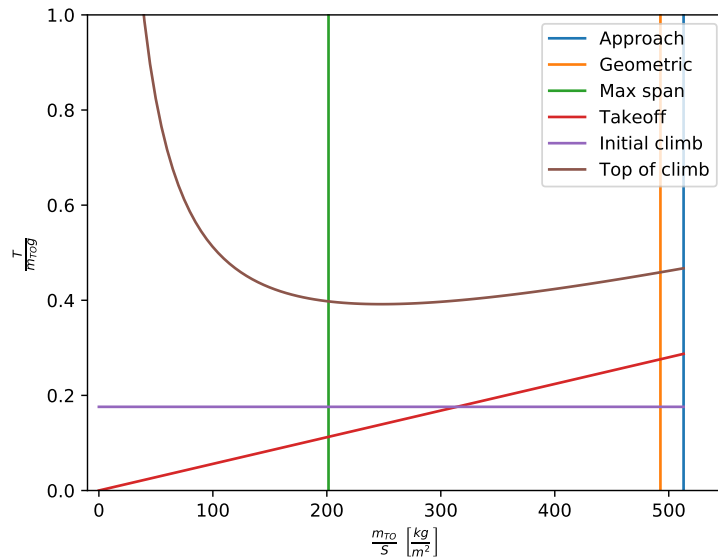


Figure 4.27: Constraint diagram for the BWB with conventional propulsion.

4.3.2 MDO formulation

The MDA represents an intermediate step to ensure the BWB sizing procedure works; it also allows to assess the advantage of the BWB solely, without the integration with distributed propulsion.

The final integration of the DEP into a BWB architecture can be easily obtained at this point of the research. In fact, all the individual modules for the BWB sizing and the DEP are ready, and thanks to the modular approach they can be directly inserted in the MDF architecture, replacing the old one.

The resulting procedure is identical to what has been shown in Fig. 3.14 and described in Alg. 7, with the modules regarding geometry, aerodynamics and structure tailored for the BWB replace the ones for conventional aircraft. The performance is not modified: in fact for this analysis aircraft is described as just a point with mass and aerodynamic properties, and it works fine for all the configurations as far mass and aerodynamics are valid.

This procedure will be applied in next section to optimise and evaluate performances of BWB featuring DEP.

4.4 The Blended Wing-Body featuring conventional propulsion

4.4.1 Design mission analysis

In this section performance for the BWB featuring conventional propulsion are evaluated, considering the same TLAR as the A320 reference aircraft, reported in Table 2.4.

The EIS2035 is considered, so the same assumptions done on structure and aerodynamics and reported in Table 2.15 and Table 2.16 respectively are retained. The only difference is that no reduction for the fuselage (equivalent to centerbody) is considered, since the use of new material is already contained in Eq. (1.7). Also regarding the propulsion, two LEAP type engines [CFM16] at the trailing edge are considered.

The geometrical inputs adopted are reported in Table 4.16: for the BWB, the subscript *out* indicates the outer wing only, meanwhile the subscript *w* refers to global parameters. The minimum centerbody height is 2.18 m as explained in Sec. 4.2.6; also to remark that thickness-to-chord ratio for outer wing is a mean value: in real, it is thicker at root and thinner at tip.

AR_w	3.2
$\Lambda_{LE_{cb}}$	45 deg
λ_{cb}	0.65
λ_{tr}	0.8
$\Lambda_{25_{out}}$	25 deg
$(\frac{t}{c})_{out}$	0.1
λ_{out}	0.3

Table 4.16: Geometrical inputs for the BWB with conventional propulsion sizing case.

The BWB aircraft is compared with A320 case study, resized to consider the same EIS2035. Results for the design mission are reported in Table 4.17. The BWB shows a heavier structure, which results in a greater MTOW, as expected because of the complexity of the structure. Nevertheless, the maximum LoD value is increased of 30%: the improved aerodynamics counterbalance the penalties in mass, and finally the fuel consumption is reduced of about 13%. The centerbody relative thickness is about 0.19: despite the value still makes the airfoil theory valid [Av59], it is higher than other BWB in literature, which suggest values around 0.15 [vV14; Gre+10a]. Indeed, the BWB examples found in literature are for very large passengers and long range (competitor of *i.e.* Boeing 777): for these geometries the chord are greater, and this lead to a reduced relative thickness. The size of the BWB here considered is smaller, and thus the centerbody is thicker. Higher relative thickness may be problematic in transonic, since it facilitates the formation of shock wave; a careful aerodynamic design is needed as further step. Regarding the certification, from Table 4.17 comes out also that, even if the BWB complies with all the CS-25, the performances are worse than the conventional

		Baseline	BWB
MTOW	[t]	68.3	73.9
OWE	[t]	40.9	48.4
Wing area	[m ²]	120.37	395.06
Max. LoD		17.02	22.92
Cruise altitude	[kft]	34.6	38.9
Fuel mission	[t]	13.6	11.8
CAT.POL.A.410(a)-1	[ftmin ⁻¹]	947.36	640.97
CAT.POL.A.410(a)-2	[ftmin ⁻¹]	736.79	633.95
CS-25.119(a)	[%]	21.52	12.27
CS-25.121(a)	[%]	3.66	0.79
CS-25.121(b)	[%]	5.53	4.28
CS-25.121(c)	[%]	6.96	7.46
CS-25.121(d)	[%]	8.41	2.12

Table 4.17: Comparison between the A320 resized to match EIS2035 and the BWB, with the TLAR reported in Table 2.4.

aircraft, except for the CS-25.121(c).

Another feature concerns the cruise altitude, which is higher than the conventional aircraft. In some way, this has already been detected in Sec. 4.2.2, where it is mentioned that the first estimate of cruise altitude is underestimating the real value. For a BWB, indeed, the wing loading is lower than for a reference aircraft:

$$\left(\frac{m}{S_w}\right)_{BWB} < \left(\frac{m}{S_w}\right)_{ref} \tag{4.29}$$

Let consider the C_L equation, described in Eq. (2.16). Replacing the velocity by its definition $V = Ma_\infty$ it is possible to manipulate the equation to put in evidence the wing loading:

$$C_L = \left(\frac{m}{S_w}\right) \frac{2g}{\rho M^2 a_\infty^2} \tag{4.30}$$

The combination of Eq. (4.30), written for the BWB and the reference aircraft, with the condition (4.29) yields to

$$\frac{C_{L_{BWB}}}{C_{L_{ref}}} < \frac{\rho_{ref} a_{\infty_{ref}}^2}{\rho_{BWB} a_{\infty_{BWB}}^2} \tag{4.31}$$

In case of the BWB, because of the greater area, the C_L in cruise (that is recalled, is equal to the optimal C_L) is smaller than the reference aircraft, as depicted in Fig. 4.28, that shows the comparison of the cruise polars for the BWB and the reference aircraft. This yields to conclude that, to satisfy the condition (4.31), the following relation holds:

$$\rho_{BWB} a_{\infty_{BWB}}^2 < \rho_{ref} a_{\infty_{ref}}^2 \tag{4.32}$$

The inequality expressed in (4.32) is verified only if the BWB flies at higher altitude, since both the density and the speed of sound decrease with this quantity. Therefore, it is explained

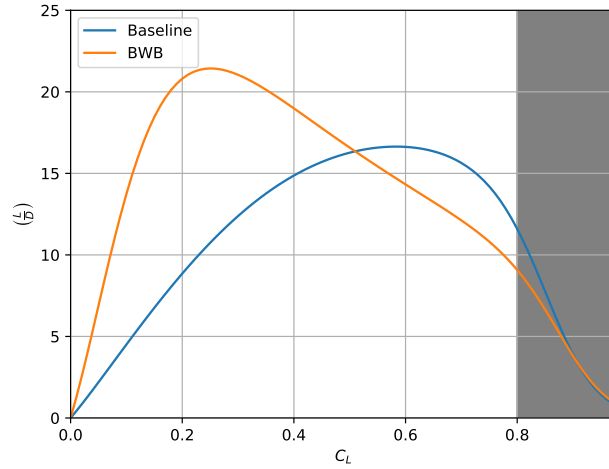


Figure 4.28: Comparison between the LoD curve for the reference aircraft and the BWB with conventional propulsion. Shading identifies the region where models are not accurate anymore, since the wave drag is not well predicted at high C_L .

the result noted in Table 4.17. The increased altitude may be an issue since for the BWB the actual rules for the routes and their management most likely need to be revised, to allow BWB flying at specified flight level. Also, the implication of the cruise altitude on the pollution level must be assessed. Finally, it is worth noting that the ratio between payload and MTOW is 0.18 for the BWB, compared with 0.20 for the reference aircraft, which may indicate that the BWB is commercially an inferior design compared to the baseline; this aspect must be detailed in further studies.

One of the point that has been remarked in the introduction is the necessity to design the airfoil in order to have a zero net C_M for stability. To this purpose, several authors consider reflex airfoil in the centerbody, to counterbalance the moment generated by transonic airfoils applied on the external wing [Ale14; SV02; NW96]. For the BWB considered here, the NACA 23021 [Av59] is used in the centerbody, the NACA0018 in the transition zone [Av59] and the NASA SC-410 in the external wing. All these airfoils are shown in Fig. 4.29, in real scale.

The aerodynamic analysis, carried out with the VLM method, allows to estimate the values of $C_{M_{cg}}$ around the cruise point. Results are shown in Fig. 4.30. From Fig. 4.30 is evident that the moment coefficient is near zero around the angle of attack of interest, which was the desired situation. Also, the slopes of $C_L - \alpha$ and $C_{M_{cg}} - \alpha$ curve are opposite in sign, which means that the aircraft is statically stable [And12]. It can be concluded then that the use of cambered airfoil helps indeed the design for a tailless configuration, since the aircraft is stable and generates a moment near zero.

Finally, the mass breakdown is illustrated in Fig. 4.31. It is the airframe, indeed, that accounts for the most of structural weight (about 60%); of this percentage, the centerbody represents more than half of the total weight, as expected. The outer wing accounts for a

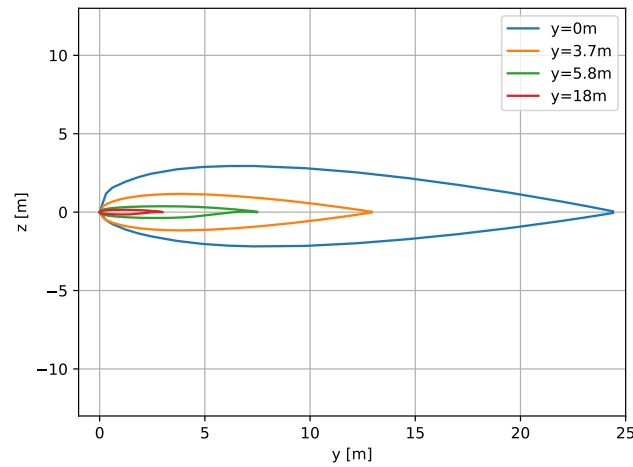


Figure 4.29: Visualization of the airfoils used in the BWB concept depicted in Fig. ?? at different sections, in real scale.

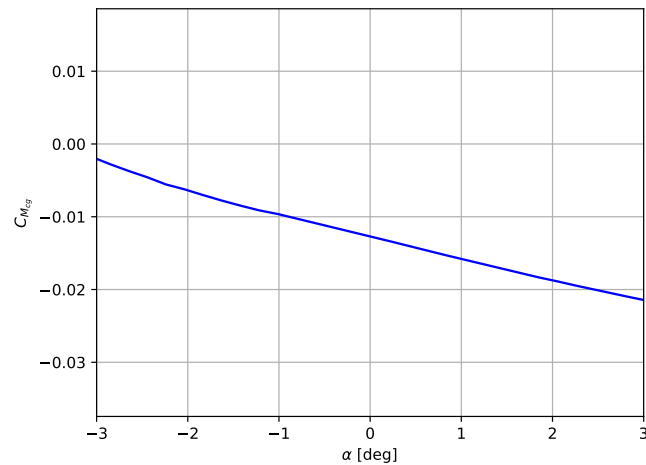


Figure 4.30: $C_{M_{cg}}$ vs. α curve around the cruise point for the BWB concept obtained.

30%, meanwhile the rest is equally divided by other components. Percentages are in line with values coming from internal work at ONERA, on the CICA V project [Def+18], and other examples in literature [vV14], despite the type is different.

4.4.2 Operational area assessment

The analysis of the BWB concept continues with an assessment of its performance in operational points. Indeed, for airlines, it is interesting to have aircraft efficient in different conditions, not only that of design. During the life cycle aircraft, in fact, very rarely it flies

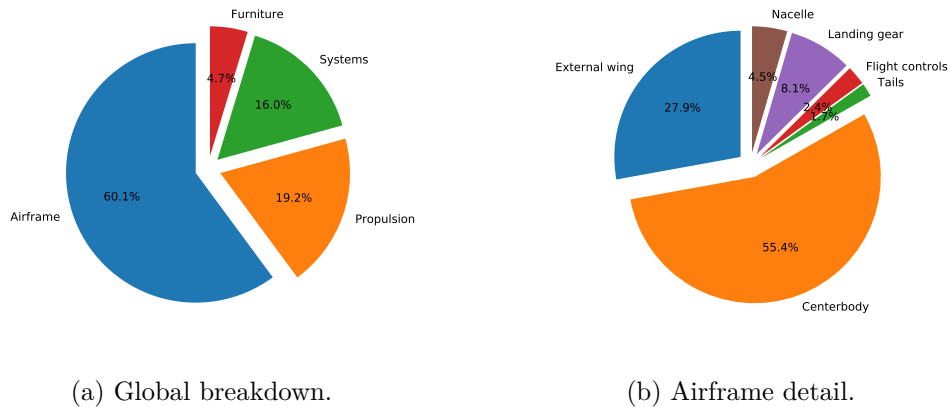


Figure 4.31: Mass breakdown for the BWB featuring conventional propulsion, with TLAR reported in Table 2.4. Mass norm is the reference French 2001/D, used in FAST [DGA84].

at its design range. For this reason, studies on the performance on other ranges than that of design have been carried out.

The ranges vary between 600 and 2200 nmi; results for the BWB and the baseline are shown in Fig. 4.32. From the diagram, it comes out that the BWB is more efficient for longer

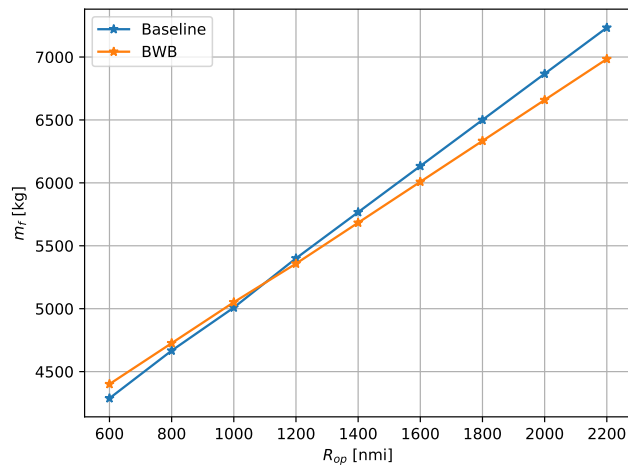


Figure 4.32: Comparison between the reference aircraft and the BWB with conventional propulsion for different operational ranges.

ranges, but at lower distances the baseline saves more fuel. This is linked to the comment done in previous section on the flight altitude for the BWB. Indeed, the disruptive concept needs to climb higher, which takes more time; specifically 31 min in place of 25 min. The engine model is the same for both aircraft, as well as the climb profile (in terms of CAS). Neglecting variations of thrust and SFC for the last phase of BWB climb (after it passes the cruise altitude of the reference aircraft) and recalling that $dm_f = T(\text{SFC})dt$, it can be

concluded that the ratio between the fuel consumption of the two aircraft is equal to the ratio between the time of climb. This means that, with numeric values given, the BWB consumes approximately 20% more fuel than the reference aircraft. On short distances, this quantity is not counterbalanced by the reduced FC in cruise, because of the shortness of this segment. This explains also why in literature most of the BWB concepts so far refer to long and very long range.

Finally, the Payload-Range curve is also obtained. Two different conditions have been taken into account for the BWB. The volume beneath the cabin is empty in this case, whereas no batteries are included (as in Fig. 4.25a), and it may be used for additional tanks. The amount of fuel stored is estimated by the knowledge of the volume and the density.

The Payload-Range, considering additional tanks and not, is shown in Fig. 4.33, compared with the baseline diagram. The maximum distance can be travelled at maximum payload is reduced for the BWB by about 200 nmi, because as said the concept is not competitive against the conventional TAW on short ranges. On the contrary, for longer distance the performances

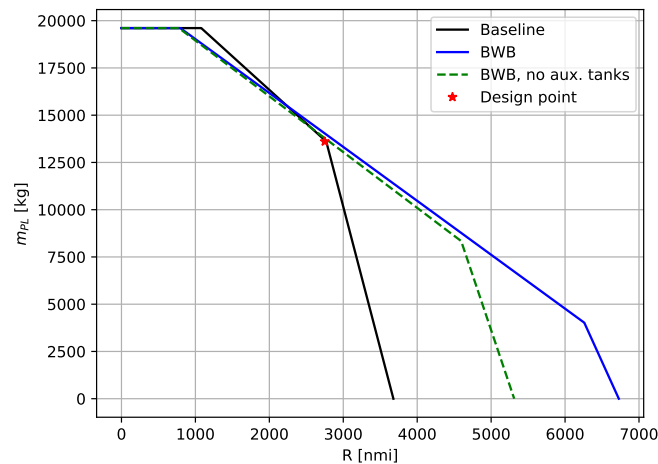


Figure 4.33: Payload-Range comparison between the reference aircraft and the BWB with conventional propulsion, considering the two cases with auxiliary tanks and not.

of BWB are so improved that ferry range is increased of about 1400 nmi in the case with no additional tanks, and almost 3000 nmi with additional tanks. The difference in MFW with and without tanks in the centerbody is of 6 t. This value alone can not explain a range increased of about 1600 nmi, but it is to not forget that mass is decreasing going on right, and so the mass is reduced not linearly but there is a combined effect.

Now that the BWB performances are well assessed, considering conventional engines, it is possible to pass to the exploration of the BWB with DEP, final objective of the research.

4.5 The Blended Wing-Body with distributed electric propulsion

4.5.1 Problem formulation

The problem statement for the optimisation of BWB with distributed electric propulsion is synthesized in Table 4.18. Besides the bounds of variables that are of course adapted to the BWB case, only minor differences are present, compared to previous case of the hybrid aircraft optimisation problem reported in Table 3.18.

- The parameters to define the centerbody are included in the design variables, according to the parametrization reported in Fig. 4.21. Note that the relative thickness has size 2, because the constraint on the height y_t is evaluated at symmetry and outmost plane;
- The horizontal tail parameters are removed, since the BWB is a tailless aircraft;
- The approach condition is replaced by the condition of minimum vertical speed at top of climb, as emerges from Fig. 4.27. The limits for the cruise altitude are augmented of 2000 ft in agreement with the peculiarity of the BWB that flies higher;
- The lower limit for fan over chord ratio \bar{r}_f is reduced to 0.05, because of the MAC which is more than doubled with respect to conventional aircraft;
- The static margin limits are reduced, in agreement with the discussion done in Sec. 4.2.3.3.

In total, the problem consists of 20 design variables subject to 17 design constraints (2 equalities and 15 inequalities).

As usual, before going through the optimisation of the BWB, a sensitivity analysis is presented, both to understand the impact of variables on overall design and to eventually reduce the size of the optimisation problem.

4.5.2 Sensitivity analysis results

As already done for the TAW with distributed propulsion, before going through the process of optimisation a sensitivity analysis is performed, using the PCE method (see Appendix C for more details).

In a similar way than the previous case, the wing and vertical tail surfaces, as well as the wing position and the cruise altitude are not considered, since it is not of interest to analyse their impact, being directly subject to design constraints and then not free to be modified by designer. Also, the battery volume is recomputed according to Eq. (3.53) to ensure for all points a final SoC equals to 0.20.

Category	Name	Size	Lower	Upper	Equals	Units	
Objective	$f(\underline{x})$	1	–	–	–	–	
Variables	S_w	1	250	450	–	m ²	
	x_{out}	1	12	16	–	m	
	AR_w	1	2.5	5	–	–	
	$\Lambda_{LE_{cb}}$	1	30	60	–	deg	
	λ_{cb}	1	0.5	0.8	–	–	
	$(\frac{t}{c})_{cb}$	2	0.15	0.24	–	–	
	λ_{tr}	1	0.6	0.8	–	–	
	λ_{out}	1	0.2	0.6	–	–	
	$\Lambda_{25_{out}}$	1	20	45	–	deg	
	$(\frac{t}{c})_{out}$	1	0.1	0.15	–	–	
	S_{VT}	1	15	50	–	m ²	
	AR_{VT}	1	1	2.5	–	–	
	λ_{VT}	1	0.85	1.0	–	–	
	$\Lambda_{25_{VT}}$	1	25	55	–	deg	
	$(\frac{t}{c})_{VT}$	1	0.1	0.15	–	–	
	k_{GT}	1	0.5	1.5	–	–	
	P_{400}	1	6	18	–	MW	
	τ_b	1	1	3	–	m ³	
	FPR	1	1.05	1.4	–	–	
	h_{toc}	1	32 000	42 000	–	ft	
		Total	21				
Constraints	Δm_f	1	0	–	–	kg	
	b_w	1	–	36	–	m	
	y_t	2	2.18	–	–	m	
	$\Delta \mathcal{N}_{cruise}$	1	0	–	–	N m	
	ΔP_b	1	0	–	–	W	
	Δl_{nac}	1	–	0	–	m	
	\bar{r}_f	1	–	0.05	–	–	
	TOFL	1	–	2200	–	m	
	SM	1	0	0.05	–	–	
	$\tan \gamma_{400}$	1	0.024	–	–	–	
	c_{CCM}	5	0	–	–	%	
	SoC_f	1	–	–	0.20	–	
	$\Delta C_{L_{toc}}$	1	–	–	0	–	
		Total	18				

Table 4.18: Optimisation problem definition for the BWB aircraft with distributed electric propulsion case.

Concerning the other variables, the design space is defined together with the problem in Table 4.18; the configuration chosen for sensitivity corresponds to $R = 900$ nmi and $N_{EM} = 32$.

The design of experiments consists of 800 points, whereas 750 belong to training set,

and the remaining to the validation set. As usual, Sobol indices are computed for energy consumption E_c , battery volume τ_b , OWE m_e , maximum LoD value $\left(\frac{L}{D}\right)_{\max}$ and static margin SM.

Table 4.19 presents first order Sobol indices mean value μ , meanwhile Table 4.20 reports the relative coefficients of variation; with the convention that in case the mean value μ is zero, coefficient of variation σ^* is replaced by its variance. An asterisk indicates the case where the convention is applied.

	E_c	τ_b	m_e	$\left(\frac{L}{D}\right)_{\max}$	SM
AR_w	6.82×10^{-1}	2.65×10^{-2}	5.21×10^{-1}	9.03×10^{-1}	2.33×10^{-2}
λ_{out}	3.31×10^{-3}	8.41×10^{-4}	1.99×10^{-2}	2.87×10^{-4}	3.26×10^{-2}
$\left(\frac{t}{c}\right)_{out}$	3.39×10^{-2}	1.72×10^{-2}	5.13×10^{-3}	9.98×10^{-5}	2.70×10^{-2}
$\Lambda_{25_{out}}$	3.14×10^{-2}	1.80×10^{-2}	3.39×10^{-2}	9.38×10^{-4}	1.34×10^{-1}
$\Lambda_{LE_{cb}}$	7.04×10^{-3}	5.88×10^{-4}	1.49×10^{-1}	1.06×10^{-2}	2.12×10^{-1}
$\left(\frac{t}{c}\right)_{cb}$	3.14×10^{-2}	1.54×10^{-3}	5.11×10^{-3}	1.42×10^{-2}	2.98×10^{-2}
λ_{cb}	1.35×10^{-2}	8.63×10^{-4}	1.25×10^{-2}	2.11×10^{-3}	1.56×10^{-1}
$\left(\frac{t}{c}\right)_{tr}$	5.01×10^{-3}	1.97×10^{-4}	3.21×10^{-3}	1.35×10^{-3}	3.78×10^{-2}
λ_{tr}	5.01×10^{-3}	2.64×10^{-2}	3.72×10^{-2}	1.84×10^{-4}	3.22×10^{-2}
AR_{VT}	3.69×10^{-3}	0	2.34×10^{-3}	6.15×10^{-4}	3.38×10^{-2}
λ_{VT}	2.96×10^{-3}	0	2.38×10^{-3}	2.91×10^{-4}	2.42×10^{-2}
$\left(\frac{t}{c}\right)_{VT}$	3.50×10^{-3}	6.94×10^{-5}	3.79×10^{-3}	4.39×10^{-4}	3.24×10^{-2}
$\Lambda_{25_{VT}}$	4.12×10^{-3}	0	3.05×10^{-3}	1.17×10^{-3}	2.31×10^{-2}
FPR	1.34×10^{-1}	9.07×10^{-1}	1.56×10^{-1}	6.16×10^{-2}	2.17×10^{-2}
Sum	9.66×10^{-1}	9.76×10^{-1}	9.56×10^{-1}	9.96×10^{-1}	7.89×10^{-1}

Table 4.19: First order Sobol indices mean value μ for key output variables with respect to inputs, BWB with distributed electric propulsion case. Most relevant parameters for each output are written in bold.

The first thing in evidence from Table 4.19 is that the FPR has a minor relevance than the previous case (see Table 3.19). In spite of the fact that the aspect ratio and the FPR still drive the energy consumption, and the FPR is still the only parameter to impact the battery volume, on the OWE the behavior is totally different.

In the case of a conventional TAW with distributed electric propulsion, this quantity was impacted mainly by the aspect ratio (with an index of about 0.7 in Table 3.19) with minor effects of FPR and Λ_{25_w} . In this case, instead, the aspect ratio is reduced, with an index of about 0.52, followed by the centerbody sweep and the FPR, with indices of about 0.15 and 0.16 respectively. The impact of FPR is explained regarding the battery sizing, as before, the others instead are not intuitive. The easier to explain is the sweep centerbody: in the parametrization adopted (see Fig. 4.21 and equations for cabin sizing), this quantity defines the centerbody surface, which impacts the OWE in agreement with Eq. (1.7). However, it has been said that most of the structural weight comes from the cabin, but results identify the aspect ratio as the most important parameter. In real, AR_w has double effect: from

	E_c	τ_b	m_e	$\left(\frac{L}{D}\right)_{\max}$	SM
AR_w	1.22×10^{-1}	1.41	2.21×10^{-1}	4.96×10^{-2}	5.47
λ_{out}	9.24	2.17×10	1.79	2.25×10	3.60
$\left(\frac{t}{c}\right)_{out}$	1.12	1.86	4.75×10^{-1}	7.76×10	4.89
$\Lambda_{25_{out}}$	1.18	1.84	4.56	9.98	2.28×10^{-1}
$\Lambda_{LE_{cb}}$	4.35	3.07×10	4.39×10^{-2}	3.10	1.08
$\left(\frac{t}{c}\right)_{cb}$	1.03	1.29×10	8.60	1.39	4.57
λ_{cb}	2.58	2.26×10	4.60	1.21×10	1.16
$\left(\frac{t}{c}\right)_{tr}$	5.14	7.62×10	1.28×10	8.28	3.36
λ_{tr}	2.53	8.42	1.00	4.79×10	3.59
AR_{VT}	6.76	0*	1.62×10	1.45×10	3.69
λ_{VT}	8.47	0*	1.66×10	3.34×10	5.36
$\left(\frac{t}{c}\right)_{VT}$	7.66	2.06×10^2	1.17×10	2.65×10	4.06
$\Lambda_{25_{VT}}$	6.21	0*	1.36×10	7.98	5.53
FPR	3.35×10^{-1}	7.38×10^{-2}	2.34×10^{-2}	4.76×10^{-1}	5.71

Table 4.20: First order Sobol indices coefficient of variation σ^* for key output variables, with respect to inputs, BWB with distributed electric propulsion case. An asterisk identifies the case in which the mean value μ is zero and σ^* is replaced by convention with its variance σ .

one side it affects indirectly the outer wing surface, and then its weight, and from the other side it affects the fuel consumption, and so the MTOW. As a conclusion, a change in aspect ratio makes the outer wing weight changing, but also the cabin weight, which depends on the MTOW through Eq. (1.7) again.

As already detected, the maximum LoD value is solely defined by the aspect ratio, even if among the other parameters the one that has bigger impact is the FPR, with an index of order 10^{-2} .

Finally, the SM is mainly affected by the sweep angles of outer wing and centerbody, and the centerbody taper ratio. Due to the absence of horizontal tail, in fact, the sweep angles are the only quantities that have impact on neutral point (through the effect on C_{L_α} , see Eq. (2.7)). The quantity λ_{cb} is also a player because it defines the planform for the cabin, and so its center of gravity. In particular, the procedure described in Sec. 4.2.6.1 states that indirectly the centerbody taper ratio makes the difference between a configuration with two or more bays, and which makes the center of gravity shift towards the leading edge.

Note that the sum of the first order indices is approximately 0.7 for the SM, this means that there are interaction between variables. To understand which are the variables coupled, total indices have been evaluated, using Eq. (C.4) reported in Appendix C. It results that the quantities that interact each other are the centerbody sweep $\Lambda_{LE_{cb}}$ and the centerbody taper ratio λ_{cb} , with total indices of 4.38×10^{-1} and 3.67×10^{-1} respectively. The coupling is quite intuitive since both of them impact the cabin planform, in agreement with equations presented in Sec. 4.2.6.1. The relationship is difficult to write since it is non-linear and even explicit, depending upon trigonometric functions.

Finally, a check on the results' validity is done. Robustness is assured looking at coefficients of variation reported in Table 4.20 and checking that the quantity $\mu(1 \pm \sigma^*)$ is below the required tolerance of 10^{-3} . Also, Table 4.21 contains the MSE mean values and coefficients of variation for output parameters: in this case too, the total variation $\mu(1 \pm \sigma^*)$ is below 1% and thus the PCE approximation is considered reliable and the results validated.

	μ	σ^*
E_c	3.89×10^{-4}	2.29×10^{-1}
τ_b	2.34×10^{-4}	7.86×10^{-1}
m_e	1.81×10^{-5}	3.82×10^{-1}
$\left(\frac{L}{D}\right)_{max}$	1.31×10^{-7}	3.90×10^{-1}
SM	4.91×10^{-4}	6.42×10^{-1}

Table 4.21: Mean value μ and coefficient of variation σ^* of the relative MSE on validation set for the sensitivity analysis of Table 4.19.

As a conclusion of this sensitivity analysis, it can be said that the BWB design is mainly affected by the parameters that define its aerodynamics, more than the propulsive parameters. This result is in line with the concept itself, which is naturally very aerodynamically efficient, as already noted in different points.

Also, a set of 8 variables results have minor impact on the design compared to others, being their Sobol index very small: λ_{out} , $\left(\frac{t}{c}\right)_{out}$, λ_{tr} , $\left(\frac{t}{c}\right)_{tr}$ and the 4 vertical tail variables. The problem size can be then reduced from 21 to 13 design variables, that is a total reduction of about 35%.

Next section will present the optimisation results based on the reduced problem, with 13 design variables.

4.5.3 Mono-objective optimisation results

This section reports the results for the optimisation of the BWB with distributed propulsion. The EIS is again 2035: assumptions on the technological components are the same as Table 3.12. Improvements for structure masses and aerodynamics are reported in Table 2.15 and Table 2.16, with two minor differences: no reduction is foreseen for the centerbody mass, since the effects of materials are already included in Eq. (1.7), whereas another 10% reduction for the friction coefficient is taken into account to model the BLI effect, in agreement with results of Sec. 4.2.5.

The simulations are the same already considered for the hybrid aircraft in Sec. 3.5.3 The BWB is optimised considering different design ranges, from 600 to 1500 nmi, with electric motors varying from 16 to 48. Since from the results in Sec. 3.5.3 it has been concluded that the configuration that optimises the fuel is the same that minimises the energy, only this last quantity is used as objective function. In mathematical notation, the problem can be written

as

$$\begin{cases} \text{minimise} & E_c \\ \text{with respect to} & \underline{x} \in \mathbb{R}^{18} \\ \text{subject to} & \underline{c}(\underline{x}) \in \mathbb{R}^{18} \end{cases}$$

Refer to Table 4.18 for the definition of \underline{x} and $\underline{c}(\underline{x})$.

Optimisation set up is the same applied in other problems during this research, reported in Table 2.10; the multistart approach is applied here too, with 10 different initial points randomly chosen using the LHS technique proposed by Sacks [Sac+89].

The first result to note for the BWB optimisation is that, contrary to previous cases, the multistart approach shows an evidence of local minima. As example, Table 4.22 reports the objective function and the norm constraint, as in Eq. (2.22), for the case with 32 electric motors and a range of 900 nmi, even if the same conclusion can be drawn for all the cases. From Table 4.22 it can be seen that all the points have reached convergence, but point 1, 5

	Run									
	1	2	3	4	5	6	7	8	9	10
f^*	213.5	206.8	206.9	206.8	213.7	214.0	206.6	206.8	206.8	206.7
$\ \underline{c}\ $	0	0	0	0	0	0	0	0	0	0

Table 4.22: Objective function and norm constraints, defined as in Eq. (2.22), for the 10 optimisation runs carried out for the BWB with distributed electric propulsion, $N_{EM} = 32$, $R = 900$ nmi.

and 6 are on a different value of objective. This minimum, which is local, corresponds to a solution where the max LoD value is maximised; in other word this point optimises the cruise segment. To give some values, for the local minimum LoD value is 24.6, whereas for the other points is 23.4.

As explained in previous section, when the value of maximum LoD is increased the curve is stretched, resulting in a less efficient aircraft in other points (see Fig. 4.28). So, despite the local minimum improves the cruise, it is not efficient in climb and descent phase. For this reason, the batteries are greater, resulting in heavier aircraft. To compensate the effect, the wing area for the local minimum is reduced in order to save some weight, but this does not counterbalance the effect of oversized batteries.

The existence of a local minimum is another example of the necessity of a MDO: the interaction between variables causes the two different configurations. Also, it is to note that the global minimum is not intuitive, since it is not the point of best aerodynamic efficiency.

In the following of the section, only global minima are shown. Next figures show the comparison between the three BWB configurations with conventional aircraft. Fuel consumption is depicted in Fig. 4.34, energy consumption is shown in Fig. 4.35 and finally PFEE is represented in Fig. 4.36. Complementary to the figures, Table 4.23, Table 4.24 and Table 4.25 report values for parameters of interest for the cases with 16, 32 and 48 electric motors respectively.

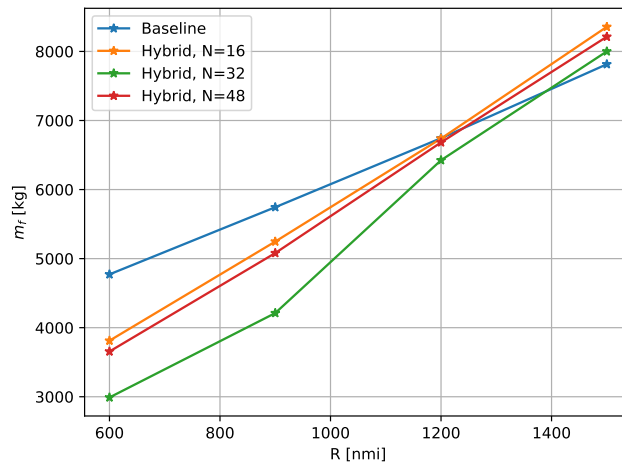


Figure 4.34: Fuel consumption as function of design range, comparison between the optimised baseline and the BWB with distributed electric propulsion. Three configurations have been analysed, corresponding to $N_{EM} = 16, 32, 48$.

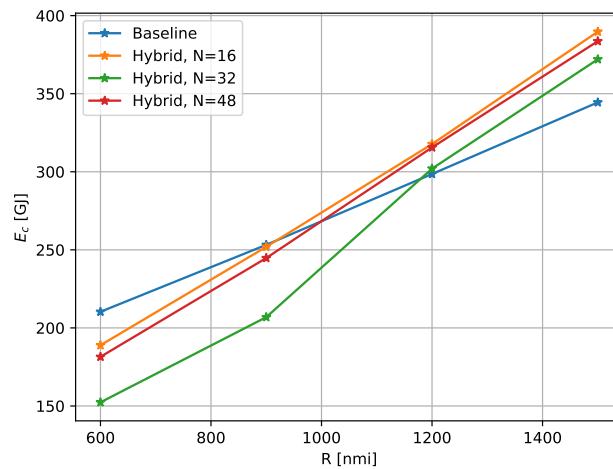


Figure 4.35: Energy consumption as function of design range, comparison between the optimised baseline and the BWB with distributed electric propulsion. Three configurations have been analysed, corresponding to $N_{EM} = 16, 32, 48$.

Results can be compared with that shown in Table 2.18. Both for the fuel and the energy consumption, the evidence of a “breakdown range” exists, and as in previous case, it is shifted to the left considering the energy. In all the cases, the zone of interest for the design is increased with respect to the hybrid BWB (see Fig. 3.20, Fig. 3.21 and Fig. 3.22). Curves are not linear, because of the effect of the FPR, which is more significant in the case with 32 electric motors.

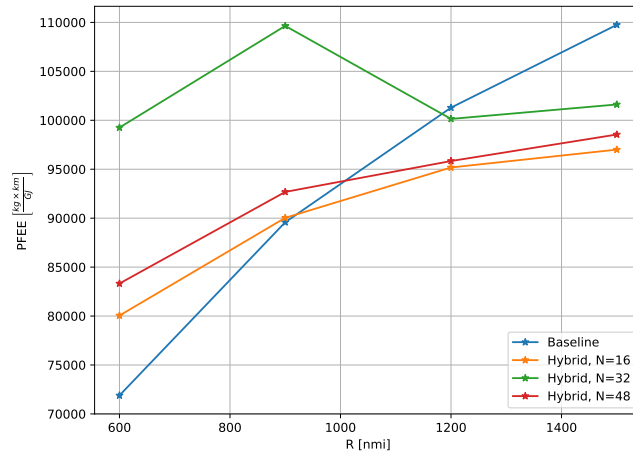


Figure 4.36: PFEE, defined in Eq. (1.3) as function of design range, comparison between the optimised baseline and the BWB with distributed electric propulsion. Three configurations have been analysed, corresponding to $N_{EM} = 16, 32, 48$.

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	83.8	85.9	87.6	91.3
OWE	[t]	65.6	67.1	68.3	69.3
Wing area	[m ²]	385.83	388.54	389.98	399.84
Max. LoD		24.02	23.89	23.88	23.83
Battery volume	[m ³]	1.3	1.83	2.02	2.26
FPR		1.38	1.40	1.37	1.40
Fuel mission	[t]	3.81	5.25	6.74	8.36
Energy consumption	[GJ]	188.90	251.92	317.74	389.71
CAT.POL.A.410(a)-1	[ftmin ⁻¹]	1534.40	1553.15	1490.01	1351.26
CAT.POL.A.410(a)-2	[ftmin ⁻¹]	2012.61	1971.61	1643.13	1524.97
CS-25.119(a)	[%]	9.13	10.03	10.01	9.61
CS-25.121(a)	[%]	10.91	14.92	14.56	13.45
CS-25.121(b)	[%]	2.42	2.64	2.42	2.68
CS-25.121(c)	[%]	10.91	9.82	14.55	13.42
CS-25.121(d)	[%]	8.01	8.98	8.96	8.43

Table 4.23: Quantities of interest for the optimised BWB with distributed electric ducted fan, $N_{EM} = 16$.

Also, the configuration with $N_{EM} = 32$ is the most performing one, since it represents a balance between aerodynamics and propulsive efficiency. Considering the PFEE, the range breakdown is about 1200 nmi, compared to 900 of hybrid TAW; $N_{EM} = 16$ and $N_{EM} = 48$ have similar performance, and the range breakdown is about 800 nmi. It is also interesting to note that the case with 32 electric motors shows a maximum for PFEE on a range of 900 nmi approximately.

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	90.7	91.3	91.9	93.4
OWE	[t]	74.1	75.3	76.9	78.3
Wing area	[m ²]	390.53	391.28	398.53	399.98
Max. LoD		23.43	23.39	23.02	23.01
Battery volume	[m ³]	1.27	1.48	1.69	1.77
FPR		1.15	1.16	1.19	1.21
Fuel mission	[t]	2.99	4.21	6.42	8.01
Energy consumption	[GJ]	152.35	206.87	302.00	372.02
CAT.POL.A.410(a)-1	[ftmin ⁻¹]	2012.61	1971.61	1643.13	1524.97
CAT.POL.A.410(a)-2	[ftmin ⁻¹]	1337.96	1334.37	1395.39	1393.73
CS-25.119(a)	[%]	10.84	10.82	12.25	12.05
CS-25.121(a)	[%]	22.62	22.29	17.54	18.28
CS-25.121(b)	[%]	2.46	2.59	2.51	2.83
CS-25.121(c)	[%]	22.51	22.19	17.54	18.27
CS-25.121(d)	[%]	9.65	9.63	11.05	10.84

Table 4.24: Quantities of interest for the optimised BWB with distributed electric ducted fan, $N_{EM} = 32$.

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	91.4	93.5	95.7	98.1
OWE	[t]	74.1	74.8	75.4	76.3
Wing area	[m ²]	340.42	340.38	341.81	341.76
Max. LoD		25.18	25.15	25.08	24.78
Battery volume	[m ³]	1.47	1.65	1.99	2.08
FPR		1.26	1.27	1.29	1.29
Fuel mission	[t]	3.65	5.08	6.68	8.21
Energy consumption	[GJ]	181.48	244.73	315.56	383.61
CAT.POL.A.410(a)-1	[ftmin ⁻¹]	1553.11	1478.16	1360.73	1279.13
CAT.POL.A.410(a)-2	[ftmin ⁻¹]	1684.02	1678.41	1586.46	1471.59
CS-25.119(a)	[%]	9.49	9.42	9.38	9.77
CS-25.121(a)	[%]	12.53	12.60	13.36	13.64
CS-25.121(b)	[%]	2.52	2.83	2.89	2.90
CS-25.121(c)	[%]	12.56	12.62	13.41	13.68
CS-25.121(d)	[%]	8.39	8.31	8.29	8.19

Table 4.25: Quantities of interest for the optimised BWB with distributed electric ducted fan, $N_{EM} = 48$.

However, the case with $N = 48$ shows an interesting behavior. The global minimum configuration is represented by the case with maximum LoD, and indeed Table 4.25 shows that its value is higher than other cases. This result is explained considering that, when the number of electric motors increases, the MTOW does the same; for this configuration,

penalties in weight are so relevant that the aircraft is not capable anymore to climb, and then it finds the path to reduce weight in order to reduce batteries and ease the climb.

The mass breakdown, for the case with 32 electric motors and a range of 900 nmi the mass breakdown, is provided in Fig. 4.37, with the global overlook on the left and details of airframe breakdown on the right. Compared to the case with conventional engines shown

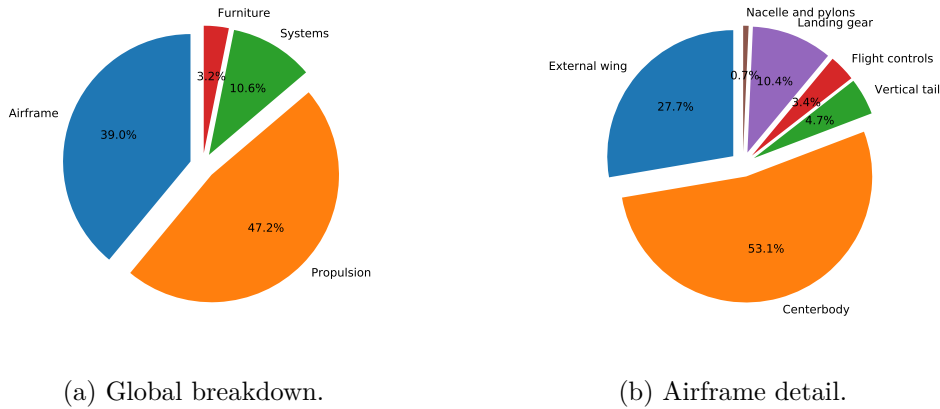


Figure 4.37: Mass breakdown for the BWB with distributed electric propulsion, $N_{EM} = 32$, $R=900$ nmi. Mass norm is the revised French 2001/D for hybrid architectures, used in FAST [DGA84].

in Fig. 4.31, the airframe contribution is almost halved whereas the propulsion contribution is more than doubled. This is mainly due to the presence of batteries, that again introduce the most relevant penalty in weight. Concerning the airframe division, because of the heavier MTOW the centerbody accounts for the 58% compared to 55% of previous case, but generally the order of magnitude does not change. It is useful to recall that cabin weight depends on the MTOW as described in Eq. (1.7), which explains the higher percentage.

Concerning the certification and the operational requirements, all the configurations comply with the proposed revised CS-25 for the hybrid propulsion. The top of climb and top of descent conditions are taken with a great margin; the most stringent one is the OCI condition at 400 ft. To assess the difference considering more margin on the minimum condition suggested by certification, a new optimisation is carried out, considering the case with 32 electric motors and range of 900 nmi. For this simulation, the lower limits of certification are taken as the A320 test case, reported in Table 2.8. The difference in fuel consumption is of 100 kg, because the power required is of course higher, and this increases the weight. However, the oversizing is in the order of 2.5 MW, since all the other conditions have already margin with respect to Table 2.8. Detailed comparison is reported in Table 4.26. This assessment is useful since a more refined design may take a safety limit than the minimum values of CS specifications, or gives an estimate of the impact in case rules will be different from the ones applied to a twin-engine aircraft, *e.g.* in case they will meet the ones for a four-engine, for which the CS-25.121(b) requires a slope of 3% in place of 2.4%.

Next section will present the Pareto frontier, comparing the results between a gradient

		CS-25 limit	A320 2005 limit
MTOW	[kg]	91277.08	91426.52
Power @ 400ft	[MW]	8.73	11.22
Battery volume	[m ³]	1.48	1.49
Fuel consumption	[kg]	4216	4330

Table 4.26: Comparison between the two BWB with DEP optimisation problems, considering the CCM lower limit as specified in the CS-25 [EAS17] and equals to the A320 2005 version, reported in Table 2.8. $N_{EM} = 32$, $R = 900$ nmi case.

free and a gradient based method.

4.5.4 Pareto frontier for the proposed BWB concept

The Pareto frontier is obtained in similar manner than has been done in Sec. 3.5.3.4. The two objective functions are the energy consumption E_c and the OWE m_e , which are related to costs. The genetic algorithm NSGA-II, which is an algorithm capable to tackle the multiobjective optimisation, is compared with SNOPT, that uses gradient. In mathematical notation, the problem assumes the following form:

$$\begin{cases} \text{minimise} & \underline{f}(\underline{x}) = [m_e, E_c] \in \mathbb{R}^2 \\ \text{with respect to} & \underline{x} \in \mathbb{R}^{18} \\ \text{subject to} & \underline{c}(\underline{x}) \in \mathbb{R}^{18} \end{cases}$$

with $\underline{f}(\underline{x}) = [m_e, E_c]$, \underline{x} and $\underline{c}(\underline{x})$ defined in Table 4.18. In the case of SNOPT the auxiliary function defined in Eq. (3.55) is used: varying the parameter α in the range $[0,1]$ all the points are exploited. In this case, the problem can be written as

$$\begin{cases} \text{minimise} & f(\underline{x}, \alpha) \in \mathbb{R} \\ \text{with respect to} & \underline{x} \in \mathbb{R}^{18} \\ \text{subject to} & \underline{c}(\underline{x}) \in \mathbb{R}^{18} \end{cases}$$

with $f(\underline{x})$ defined from Eq. (3.55) and $\alpha \in [0, 1]$.

The case considered for the Pareto frontier is the configuration with 32 electric motors, with a range of 900 nmi; problem is the same of Table 4.18 with two objectives in place of one. The exploration points used by NSGA-II are shown in Fig. 4.38, where feasible points are marked in blue, meanwhile points belonging to Pareto frontier in red. Compared to previous case of the hybrid TAW optimisation, 20000 points have not been sufficient to obtain a smooth Pareto, thus the number of points is increased until good results were obtained. At the end, 50000 points have been explored. The higher number of points results in a computational cost of about 85 h, confirming the high demand required by such algorithm.

The comparison between the Pareto frontier obtained with NSGA-II and SNOPT is shown in Fig. 4.39: visually the two curves are comparable each others, in fact differences are small,

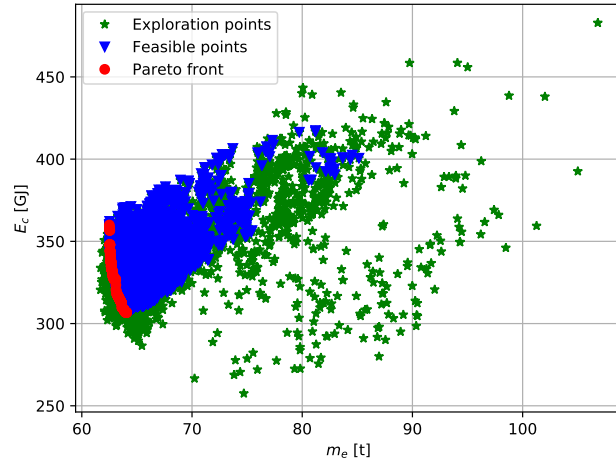


Figure 4.38: Exploration points using NSGA-II, for the multiobjective optimisation of BWB with distributed electric propulsion, $N_{EM} = 32$ and $R = 900$ nmi. 50000 points considered.

and are due to numerical approximation. To better assess the difference between the two

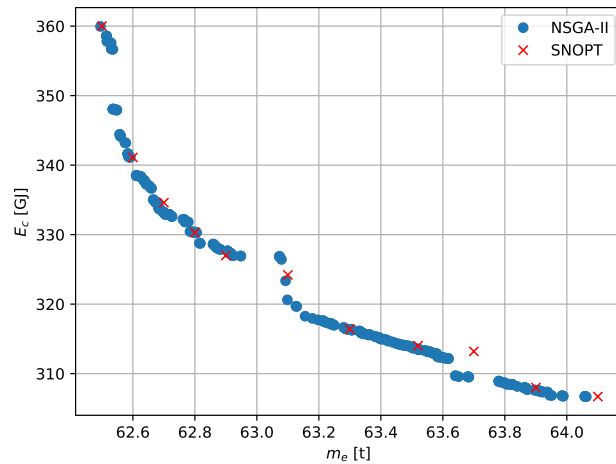


Figure 4.39: Comparison between the Pareto frontier obtained with NSGA-II and SNOPT, through the auxiliary function in Eq. (3.55). BWB with DEP case, $N_{EM} = 32$ and $R = 900$ nmi.

methods, the \mathcal{L}_2 -norm for the final objective function and design variable is computed and results are in Table 4.27.

Because of the existence of local minima, multipoint approach must be used for SNOPT simulations in this case too to ensure to get the global minimum, for each point. However, knowing where is the final solution, the initial point can be taken around the point, reducing the computational cost and eventually also the number of initial points. In total, for each α

$\ f_{SNOPT}^* - f_{NSGAI}^*\ _2$	6.84×10^{-6}
$\ x_{SNOPT}^* - x_{NSGAI}^*\ _2$	4.49×10^{-5}

Table 4.27: \mathcal{L}_2 -norm calculation between the final objective function and design variable vectors. The subscript identifies the method.

5 different $x^{(0)}$ are considered; in mean the time for a simulation is about 30 min, so finally the global computational time is about 25 h for the 11×10 simulation. In this case too the cost is higher than previous case, but the difference between the two approaches is still of about 60%; also it is to not forget that all the points can be run at same time, so a Pareto can be obtained in about 3 h. It is then confirmed that the gradient-based methods are more efficient than the gradient-free.

Concerning aircraft design aspects, the tradeoff shown in Fig. 4.39 is more difficult to explain than the previous case of hybrid aircraft. Points towards the right correspond to minimum energy, but they do not show the best aerodynamics. Indeed, as remarked earlier, these points show high wing surface to reduce the fuel/energy consumption in climb thanks to the lift generated; despite the LoD value is slightly decreased in cruise, on the overall mission the energy consumption is reduced. On the other side, to minimise the mass the optimiser goes towards a solution with a reduced wing area. In order to still have good performances in climb, points exhibit the same span (equals to the maximum, $b_w = 36$ m) in order to improve the aerodynamics and reduce the thrust requirement for climbing. Thus they are points of optimal aerodynamics. It is also worth noting that the trend is not linear, because of the battery weight divergence. The two regions identified represent then two different design philosophy, as for the global and local minimum described in the previous section. The switch between one and the other concept is marked by the discontinuity in the Pareto in proximity of $\alpha = 0.5$; for a designer the zone of major interest may be the one corresponding to $0.5 \leq \alpha \leq 1$, after the discontinuity, as the energy consumption is reduced but the mass aspects are not predominant yet.

Throughout all the exploration of hybrid and BWB concept, batteries have been identified as the most penalising component for weight; in the next section is finally explored a case where these elements are removed, in order to quantify their impact on the overall design.

4.5.5 Results for an hybrid BWB concept without batteries

This section exploits a particular case of BWB, where the electric power is supplied solely by the two turbogenerators. Indeed, since from the analysis of the hybrid TAW it has been noted that the penalties in weight introduced by batteries are so relevant to drastically impact the fuel and energy consumption. This has been confirmed also by the mission optimisation carried out in Sec. 3.5.3, where from the results is more convenient to remove batteries for fuel saving. These elements have been introduced by to satisfy the TLAR of zero emissions up to 3000 ft. However, fostered by previous results and other similar concepts in literature, like the DRAGON [Sch+19] or the N3-X [KBF08], it has been decided to analyse the BWB

aircraft where only the generators supply electric power. The analysis is also useful since the batteries' technology has the most uncertainty, and in case the values assumed here will not be available, another solution is studied.

To estimate the impact of absence of batteries, the same optimal configurations are considered; so at this stage no optimisation is done. Results in terms of fuel consumption are shown in Fig. 4.40. Since there is only one single source power, show the energy consumption and the PFEE curves is pointless, because they are simply scaled with respect to fuel consumption. Table 4.28, Table 4.29 and Table 4.30 report the quantities of interest for this

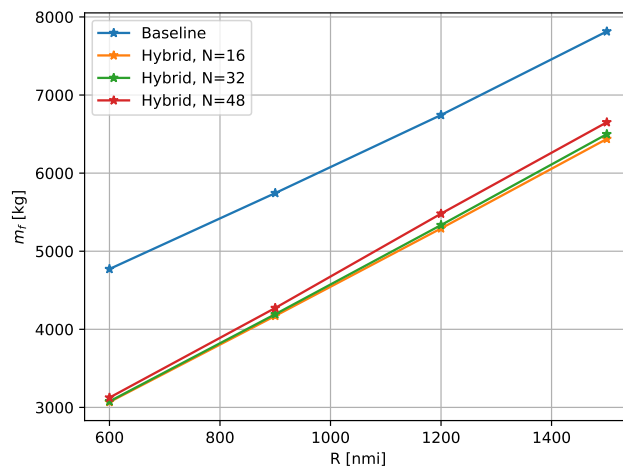


Figure 4.40: Fuel consumption as function of design range, comparison between the optimised baseline and the BWB with DEP, where the electric propulsion is obtained by turbogenerators solely.

case, with 16, 32 and 48 electric motors respectively.

Results show the absence of batteries reduces the MTOW of about 30 t, saving approximately 1.5 t of fuel. The concept is always more performing than the A320 baseline on the set of design ranges of interest; also the three configurations varying the number of electric motors are very similar among them. It is also to note that the maximum LoD is higher in this case too: thanks to the lighter aircraft, the thrust at top of climb, which is the sizing condition for the ducted fan, is smaller. As main effect, the ducted fans are smaller too, and the reduction in wetted surface makes the aerodynamics better.

On the certification side, all the conditions are respected with a great margin, both considering the limits from CS document and the A320 2005 version.

In conclusion, for hybrid propulsion it is more convenient to limit or even remove the batteries, unless it is strictly necessary, as in the case of this research where the goal was to have zero emission in the atmospheric boundary layer.

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	68.6	69.8	71.0	72.3
OWE	[t]	51.9	52.0	52.1	52.2
Max. LoD		25.59	25.56	25.54	25.51
Fuel mission	[t]	3.07	4.17	5.29	6.44
CAT.POL.A.410(a)-1	[ftmin ⁻¹]	2240.91	2168.93	2098.28	2028.51
CAT.POL.A.410(a)-2	[ftmin ⁻¹]	762.37	760.50	758.61	756.66
CS-25.119(a)	[%]	14.29	14.27	14.24	14.22
CS-25.121(a)	[%]	13.57	13.06	12.54	12.69
CS-25.121(b)	[%]	11.98	11.69	11.42	11.14
CS-25.121(c)	[%]	13.50	12.99	12.49	12.64
CS-25.121(d)	[%]	13.24	13.21	13.19	13.16

Table 4.28: Quantities of interest for the BWB with distributed electric ducted fan, power supplied by turbogenerators solely, $N_{EM} = 16$.

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	69.9	71.2	72.5	73.8
OWE	[t]	53.3	53.4	53.5	53.7
Max. LoD		25.61	25.62	25.59	25.56
Fuel mission	[t]	3.08	4.19	5.33	6.50
CAT.POL.A.410(a)-1	[ftmin ⁻¹]	2163.94	2093.61	2024.31	1955.93
CAT.POL.A.410(a)-2	[ftmin ⁻¹]	766.39	764.31	762.21	760.04
CS-25.119(a)	[%]	14.00	13.98	13.95	13.93
CS-25.121(a)	[%]	12.97	12.46	12.62	12.11
CS-25.121(b)	[%]	11.67	11.39	11.11	10.84
CS-25.121(c)	[%]	12.92	12.41	12.57	12.07
CS-25.121(d)	[%]	12.95	12.92	12.89	12.87

Table 4.29: Quantities of interest for the BWB with distributed electric ducted fan, power supplied by turbogenerators solely, $N_{EM} = 32$.

4.6 Conclusions

This chapter has the scope to define a procedure for the BWB sizing. The methodology adopted, that uses high fidelity on a common geometry to find methods suitable for conceptual design, allows to revise the sizing procedure with disciplines tailored for the BWB.

After these analyses aerodynamic, mass models have been adapted to the problem; and also the contribution coming from the nacelle integration and the BLI is estimated. Some details regarding boarding, evacuation, subsystems positioning and other aspects related to operations have also been discussed. Even if these aspects are not directly included in the conceptual sizing process, since they belong to another level of refinement, the discussion has been necessary to limit the risk of acceptance and feasibility (with respect to certification) of

		Range [nmi]			
		600	900	1200	1500
MTOW	[t]	72.1	73.4	74.8	76.1
OWE	[t]	55.4	55.5	55.7	55.8
Max. LoD		25.55	25.53	25.50	25.47
Fuel mission	[t]	3.12	4.27	5.48	6.65
CAT.POL.A.410(a)-1	[ftmin ⁻¹]	2046.94	1978.26	1908.70	1843.54
CAT.POL.A.410(a)-2	[ftmin ⁻¹]	765.51	763.92	762.23	760.60
CS-25.119(a)	[%]	13.58	13.56	13.53	13.51
CS-25.121(a)	[%]	12.76	12.26	11.73	11.87
CS-25.121(b)	[%]	11.19	10.91	10.63	10.37
CS-25.121(c)	[%]	12.70	12.20	11.68	11.81
CS-25.121(d)	[%]	12.53	12.50	12.47	12.45

Table 4.30: Quantities of interest for the BWB with distributed electric ducted fan, power supplied by turbogenerators solely, $N_{EM} = 48$.

the proposed concept.

The assumptions done are acceptable for the conceptual design, but of course they open new perspectives for a more detailed design. In particular, these issues are noted for further developments:

1. CFD optimisation for airfoil shape;
2. Lateral stability and control, for the elevons positioning and sizing;
3. Proper evacuation simulation, to ensure that aircraft is emptied in 180 s as requested by certification;
4. Estimation of the surface needed for cargo doors and cutoffs for batteries, PMU and electrical components;
5. Impact of operations on the design (*i.e.* the cutoffs weaken the structure, and they have an impact on mass);
6. Maintenance cost estimation.

Most of these aspects require large computational time to be included at conceptual design level [SH15], but they are key aspects that cannot be ignored in future development.

Once that the methodology has been defined, performances of a BWB architecture have been evaluated. At first, just a sizing has been carried out considering a BWB architecture mounting conventional high BPR engines. This analysis has been helpful in order to test the models adopted, separating the ones related to BWB from the ones specific for distributed electric propulsion. Results show that, due to the more complex architecture, BWB is heavier than a conventional aircraft, especially because of the cabin which is a relevant source of

weight. Nevertheless, the benefits coming from the better aerodynamics counterbalance this drawback and in the end the BWB saves about 20% of fuel, compared to conventional aircraft, on the same technology horizon. The tradeoff on operational missions shows instead that the BWB is very efficient in cruise, but the same is not true for other phases, and loses its advantage at very short range, where the cruise is not so long. Ferry range is of course increased because of the aerodynamics, and it may be ulteriorly augmented considering auxiliary tanks in the centerbody.

Then the study proceeds with the exploration of the BWB featuring DEP, in a similar way as done in Chapter 3 for the TAW concept mounting DEP. Starting from the sensitivity analysis it emerges that the most predominant parameters for performances are the ones that impact aerodynamics, confirming the assumption of very aerodynamically efficient concept. The optimisation results show that, in the limit of our model, the interaction between the disciplines leads to two different minima: a local one, corresponding to the most efficient cruise but worse performance in climb and descent, and a global one which is the best balance to reduce energy consumption in all phases.

Similarly to the case of TAW aircraft a range breakdown is detected, despite it is greater than the previous case. In terms of energy, it was approximately 900 nmi, against 1400 nmi for the BWB architecture. It is clear that the presence of batteries, that account for about 14 t, is penalising, in spite of the advantage of zero emission close to ground. For this reason, the same configurations have been studied considering the hybrid propulsion generated solely by the two turbogenerators. In this case performances are improved and the BWB is always more performing than the conventional aircraft in the range of interest (between 600 and 1500 nmi). The breakdown value is extrapolated and it results about 2200 nmi.

Finally, in this case too the Pareto frontier is obtained, showing the tradeoff between OWE and energy consumption. For this case, the genetic algorithm NSGA-II required 50000 points to have a smooth curve; however also SNOPT needed more time because the multistart approach must be used, to avoid the presence of local minima. In any case, the use of gradients speeds up the generation of Pareto of about 60%, in agreement with the other case of TAW aircraft featuring distributed propulsion.

In conclusion, the MDO formulation developed through the research has been applied on the BWB with distributed electric propulsion test case, with results that confirm the goodness of these techniques for unconventional configurations. Despite the relatively low number of design variables (contained to 21), the interaction between disciplines is so strong with respect to the design problem for conventional aircraft that MDO is necessary to get the best tradeoff. Otherwise, the intuition may be misleading, as *i.e.* in the case of the BWB, where surprisingly the configuration with best LoD value is not the optimal one.

Regarding the case study itself, the BWB with DEP is one of the most promising concepts since it is naturally very aerodynamically efficient, and opens new technologies, like the BLI, in conjunction with hybrid propulsion. However, in case of double source energy, the batteries limit the zone of interest for the design, at least in the limit of the technological assumptions done within this research. The concept does the best when the power is generated simply by

two turbogenerators.

Synthesis of the chapter

- Conceptual design methods implemented in FAST or available in literature have been validated using high-fidelity analyses.
- Off-design criteria are considered, such as the boarding and the subsystem displacements, in order to evaluate the acceptance of the concept. Suggestions for further development are given.
- The Blended Wing-Body concept with conventional engines is first explored:
 - On design mission it shows about 15% fuel reduction compared to conventional aircraft.
 - On operational missions the BWB is more performing on long range, whereas on short and very short range the reference aircraft is slightly better. The trend is explained because the BWB is not optimised for climb and descent segment, and it also flies at best altitude, thus when the cruise segment is reduced it loses its advantages.
 - Payload-Range is larger than the conventional aircraft, showing that the BWB concept has an extended operational domain, which makes this concept more flexible to operations.
- The Blended Wing-Body featuring distributed electric propulsion, objective of this research, is then evaluated:
 - The optimisation finds more than one region of interest for the design of the BWB. The most efficient aerodynamic configuration does not represent the global minimum, but the overall optimum BWB is represented by a balanced configuration between propulsion and aerodynamics.
 - In agreement with the results of Chapter 3, the concept shows a zone of interest for the design. However, it is enlarged compared to the previous case of hybrid tube-and-wing with distributed propulsion.
 - The case with 32 electric motors is again the most performing, because it represents the best compromise between aerodynamics and propulsive efficiency.
 - A simulation without batteries is carried out, since they represent the biggest penalty in mass. Results show that in case the electric power is produced solely by gasturbines the proposed concept is always more performing than the reference aircraft.
- The Pareto frontier simulation confirms the reduction in computational cost of about 70% with the utilisation of gradient's information.

Research contribution

- **Conference.** EASN 2019 in Athens: presentation of the multifidelity approach and the BWB with distributed propulsion, in separate sessions.
- **Conference paper.** A. Sgueglia, P. Schmollgruber, E. Benard, N. Bartoli and J. Morlier, *Preliminary sizing of a medium range Blended Wing-Body using a Multi-disciplinary Design Analysis approach*, MATEC Web of Conferences, Vol. 233, n. 14, 2018. DOI: [10.1051/mateconf/201823300014](https://doi.org/10.1051/mateconf/201823300014)
- **Conference PAPER.** A. Sgueglia, P. Schmollgruber, E. Benard, N. Bartoli and J. Morlier, *Exploration and optimization of a Blended Wing-Body Concept featuring distributed electric propulsion*, AEC 2020, Bordeaux (France), 2020.
- **Journal paper.** A. Sgueglia, L. Cerquetani, L. C. e Chuna Lima, D. A. Kharoub, P. Rodriguez Otero, H. Kaur, P. Traverso, S. S. C. Yella and E. Benard, *Multi-disciplinary and multifidelity exploration of a medium range Blended Wing-Body transport aircraft*, Aerospace, 2019. Under review.

Conclusions and perspectives

The reduction of the emissions in the upcoming years is one of the hardest challenges aviation has found. As a matter of fact, despite aviation accounts for 3% of total global emissions, the increasing number of aircraft flying everyday and the estimated trend for the next years will make this percentage grow up to unsustainable values, above 30-40%, very soon. Different organisations, like NASA in the United States and ACARE in Europe, published 2050 goals for the emissions reduction.

Unfortunately, the conventional tube-and-wing configuration has been developed for the past 60 years and it offers only small potential gains, that are not sufficient to match the goal required by the aforementioned organisation. Therefore, there is the need for disruptive changes in the design of the next generation of aircraft.

Among all the available new technologies, this research focuses on the integration of electric propulsion. It is indeed one of the most promising solution due to the fact that it is capable to achieve zero emissions. Also, it is already a reality on small scale airplanes: some manufacturers, such as Pipistrel in Slovenia, are building and selling two of roof passenger aircraft with a full electric propulsion chain. The perspective for the upcoming years related to the electric components performance, make this propulsion system and its application the large passenger aircraft segment interesting. Another important point is that hybrid/electric propulsion opens the design space thanks to new aeropropulsive effects, *i.e.* the wing blowing or the BLI.

Because of the expected large number of interactions between disciplines, greater than in the case of a conventional aircraft, the aircraft design problem itself must be revised. The revision includes an extension of the disciplines and the addition of multidisciplinary design optimisation MDO techniques. The later permits to deal with all the possible interactions between disciplines, and to finally optimise the design with respect to one or more objective functions.

The goal of this research is then to set up a MDO formulation, capable to solve the aircraft design problem of unconventional configurations at conceptual level. At this stage, performance evaluation is the main criteria to identify the most promising concept. The test case for this methodology is a Blended Wing-Body featuring distributed electric propulsion, tailored for the small and medium range segment. This concept has been chosen because the BWB has more internal volume than a classical TAW, and its large chord offers an opportunity

for an efficient BLI system, thanks to the application of distributed electric propulsion. Beside that, the BWB has naturally a very high aerodynamic efficiency, which plays a significant role in greening air transportation. Since the goal is to analyse a possible solution for the next generation aircraft, an EIS 2035 is considered. Technological assumptions, for aerodynamics, structures and electric components have been made considering this horizon.

The tool used during this research is FAST, the sizing tool developed jointly by ONERA and ISAE-Supaero. This tool has been integrated within OpenMDAO, an open source multidisciplinary optimisation framework by NASA Glenn Research Centre, in order to obtain an efficient MDO process. Within this sizing and optimisation code, different modules have been modified in order to consider both the characteristics of DEP and BWB architecture. The development has been made in three intermediate steps. A conventional TAW configuration featuring DEP has been studied first, then the BWB architecture mounting conventional engines has been sized; the BWB with DEP has been finally performed

At the end of this Ph.D. research, the following objectives concerning the design procedure have been achieved:

- The most suitable MDO architecture for this problem is the multidisciplinary feasible MDF. Indeed, it always returns a consistent aircraft even if the optimisation is stopped before the convergence. This is useful for designers to get tradeoff information. Also, as MDF requires a full MDA, and FAST already provides it, it was the most directly applicable architecture to be used.
- A new propulsive chain, considering dual energy sources (batteries and kerosene based engines) is modelled, first at global level and then component by component.
- A procedure for the performance evaluation in case of distributed electric propulsion has been developed and coded in FAST. The propulsive chain mentioned in previous point is considered. The resulting sizing loop has been tested on a conventional TAW architecture. At the end specific modules for hybrid architecture have been included in the MDF to carry out optimisations of the TAW featuring DEP concept.
- A procedure for the BWB sizing has been set up. In order to comply with the lack of reference data and model, a strategy that uses high fidelity calculations to validate or correct low fidelity methods for conceptual design has been set up. The MDA sizing loop in FAST has been then modified to consider the new unconventional architecture.
- Through the merging of the previous three points, a MDO formulation based on MDF, for the BWB with DEP has been finally defined and tested.

At each step, FAST has been used to evaluate the performance level of the unconventional configurations: the TAW featuring DEP, the BWB with conventional engines and the BWB with DEP. The performance of each concept is assessed against a conventional baseline aircraft, satisfying the same top level requirements and matching EIS2035 assumptions. Outcomes from these studies are listed below.

- The MDO formulation, based on MDF architecture, allows to obtain an optimal configuration in a short time, comparable to the simulation time of original FAST. The use of gradients speeds up the process greatly compared to gradient-free method, but the main drawback is that with the use of analytic derivatives the modules have been broken up, resulting in more than 200 different functions. This situation may be difficult to manage for a new user.
- A sensitivity analysis on the impact of electric components technology in 2035 perspectives shows that batteries are the component with the major impact. For this reason, the design is mainly driven by this parameter: any improvement in other technologies has negligible impact, as far as the uncertainty on batteries' technology is kept.
- On the case of a conventional TAW with hybrid propulsion, the DEP introduces a benefit in terms of fuel/energy consumption only at small distances. The mass due to batteries is the most penalising one, and the concept is better than the baseline only at short ranges, whereas the penalty in mass is counterbalanced by a fully electric segment. Range limit is about 900 nmi.
- Three different configurations, featuring each 16, 32, and 48 ducted fans have been analysed for the optimisation. The case with 32 electric motors results to be the most energy efficient in the region of interest. Indeed, it represents the best compromise between propulsive and aerodynamic efficiency.
- The BWB mouting conventional HBPR engines saves about 15% of fuel, compared to a baseline, and in general it shows better performance on operational missions, except for very short distances (600-800 nmi). In fact, it emerges that the BWB is very performing in cruise, but not in climb and descent, due to the higher mass and the different polar. On very short range, where the cruise distance is limited, the baseline is preferable.
- The BWB with DEP enlarges the design region of interest with respect to the previous case of TAW with DEP. However, a breakdown point is still detected, which is approximately 1400 nmi. The middle case with 32 electric motors represents again the best balance between aerodynamics and propulsion, and it is then the most performing configuration.
- Tradeoff between disciplines are obtained thanks to the study of the Pareto frontier. The region of major interest for designer is proposed in the set of optimal points belonging to the Pareto.
- Batteries have been identified as the most penalising component in terms of weight, as they introduce a mass of about 14 t. A sizing loop where the electric power is supplied by turbogenerators solely shows that removing the batteries on the BWB concept is the best solution for all the range of interest against the baseline. Despite this configuration does not match the zero-emission requirement close to ground, it may be of interest as it globally saves more fuel.
- For both the TAW and the BWB with DEP, the Pareto frontier is obtained through the genetic algorithm NSGA-II and the gradient based algorithm SNOPT. Results show

that with the gradient information is possible to obtain a reliable Pareto frontier with a reduction of CPU time of approximately 60%. This is a great asset for conceptual designers to initially explore the design space. It also confirms the initial idea of using gradients to achieve more efficient optimisation.

This research fulfilled its objectives and it provides a set of methods and tools for the sizing and performance evaluation of unconventional configurations to be used in the future by ISAE-Supaero and ONERA. However, the work is far from being over but represents an initial point, as there are still many points to be explored under the form of Ph.D. or Master's projects. All the main perspectives that came out from the work are listed below.

- Stability and control laws must be studied for the configurations with DEP, in order to properly size the control surfaces. For the BWB concept this aspect is even more important, due to the absence of an horizontal tail.
- Models to estimate cost, noise and emission of BWB and hybrid propulsion have to be defined.
- Impact of blowing phenomenon over the wing, due to the presence of ducted fans, must be assessed through CFD and eventually wind tunnel tests in order to assess lift, drag and momentum evaluation with respect to thrust load.
- More high fidelity analyses for the BWB must be carried out on aerodynamics, for more configurations in order to obtain a surrogate model that replaces the actual models based on k -factors in FAST and permits to refine the design.
- The impact of integrated ducted fans, and then the associated BLI, must be assessed on the BWB configuration using CFD. It is the only way to obtain more reliable results than that obtained with the quasi-3D simulation with MSES.
- Takeoff performance must be evaluated using more detailed tools, to better assess the impact of a takeoff without rotation.
- The off-design aspects mentioned for the BWB, related to operational aspects (*i.e.* cargo doors or the cut-offs necessary for maintenance) must be deeply investigated to ensure the validity of the concept. Also, the performances on operational missions of a given geometry have to be evaluated, considering different setting scenarios for the gas turbine and the batteries.
- Refined calculations that include different certification requirements, *e.g.* replacing the criteria from a twin to a three or four engine aircraft, or with new rules that may be released by interested bodies.
- The MDF has been used because it was the most intuitive and suitable architecture compatible with FAST, but more architectures should be considered. In fact, the MDF requires a MDA converging for each iteration, and this is costly in terms of global CPU time; other architectures like the IDF do not have this requirement and may help to reduce the total CPU time.

To conclude, the intention of this research was to provide a tool for the conceptual design of unconventional configurations, featuring hybrid distributed propulsion. The work so far represents a step forward with respect to studies found in literature, but there is still much to do ahead. The work performed during the 3 years of this Ph.D. provides the way for more refined and faster sizing and optimisation loops for unconventional configuration featuring hybrid/electric propulsion. The next projects and Ph.D. will rely on these developments and outcomes in order to revise and refine possible concepts for the next generation of aircraft. As in every life aspect... the best is yet to come!

Summary of research contribution

Subject	Chapter	Reference
Sizing procedure for hybrid aircraft	3	[Sgu+18a] SciTech 2018
Technological ensitivity analysis for hybrid aircraft	3	[SDB20]
Optimisation procedure for hybrid aircraft	2–3	[Sgu+20b]
Sizing procedure of a BWB concept	4	[Sgu+18b] EASN 2018
Multifidelity approach for BWB sizing	4	[Sgu+19] EASN 2019
Optimisation of a BWB featuring DEP	4	[Sgu+20a] EASN 2019 Conference AEC 2020

Bibliography

- [AA12] J. K. Ausserer and F. G. Armon. “Integration, validation, and testing of a hybrid-electric propulsion system for a small remotely piloted aircraft”. In: *10th International Energy Conversion Engineering Conference*. Atlanta, Georgia, USA, 2012.
- [AC12] J. J. Alonso and M. R. Colonno. “Multidisciplinary optimization with applications to sonic-boom minimization”. In: *Annual Review of Fluid Mechanics* 44.1 (2012), pp. 505–526.
- [AC17] K. R. Antcliff and F. M. Capristan. “Conceptual design of the parallel electric-gas architecture with synergistic utilization scheme (PEGASUS) concept”. In: *18th AIAA/ISSMO Multidisciplinary Analysis and Optimization Conference*. Denver, Colorado, USA, 2017.
- [ACA15] ACARE – Advisory Council for Aviation Research and Innovation in Europe. *ACARE project*. <http://www.acare4europe.com/sria>. 2015.
- [Aig+18] B. Aigner, I. van Gent, G. La Rocca, E. Stumpf, and L. L. M. Veldhuis. “Graph-based algorithms and data-driven documents for formulation and visualization of large MDO systems”. In: *CEAS Aeronautical Journal* 9 (2018), pp. 695–709.
- [Air18] Airbus. *A320 – Aircraft characteristics airport, airport and maintenance planning*. Airbus S.A.S. customer services, technical data support and services, 2018.
- [Air19] Airbus. *Airbus global market forecast 2019–2038*. <https://www.airbus.com/aircraft/market/global-market-forecast.html>. 2019.
- [AK05] N. E. Antoine and I. M. Kroo. “Framework for aircraft conceptual design and environmental performance studies”. In: *AIAA Journal* 43.10 (2005), pp. 2100–2109.
- [AK89] I. L. Ashkenas and D. H. Klyde. *Tailless aircraft performance improvements with relaxed static stability*. NASA Contractor report 181806. Hawthorne, California, USA, 1989.
- [Ale14] G. Alex. “Conceptual aerodynamic design of delta-type tailless unmanned aircraft”. In: *International Journal of Unmanned Systems Engineering* 2.2 (2014), pp. 1–15.
- [AN17] P. Apkarian and D. Noll. “The H_∞ problem is solved”. In: *Journal Aerospace Lab*. 1.13 (2017).

- [And10] J.D. Anderson Jr. *Aircraft performance and design*. 5th ed. McGraw-Hill, 2010.
- [And11] J. D. Anderson Jr. *Fundamentals of aerodynamics*. 5th ed. McGraw-Hill, 2011.
- [And12] J.D. Anderson, Jr. *Introduction to flight*. 7th ed. McGraw-Hill, 2012.
- [Ani+18] K. S. Anisimov, A. A. Savelyev, I. A. Kursakov, A. V. Lysenkov, A. A. Mirzoyan, and P. S. Prakasha. “Propulsion system – airframe integration and optimization of civil aircraft – AGILE EU project”. In: *31st Congress of the International Council of the Aeronautical Sciences*. Belo Horizonte, Brazil, 2018.
- [ANS19] ANSYS Inc. *ANSYS package, v2019R2*. <https://www.ansys.com/>. 2019.
- [Ant17] F. Anton. “High-output motor technology for hybrid-electric aircraft”. In: *eAircraft Electric & Hybrid Aerospace Technology Symposium*. Cologne, Germany, 2017.
- [AO06] B. Allan and L. Owens. “Numerical modeling of flow control in a boundary-layer-ingesting offset inlet diffuser at transonic Mach numbers”. In: *44th AIAA Aerospace Sciences Meeting*. Reno, Nevada, USA, 2006.
- [Ara+14] A. C. Aranake, S. R. Copeland, A. K. Lonkar, T. W. Lukaczyk, D. E. Manosalvas, K. R. Naik, A. S. Padrón, B. Tracey, A. Variyar, and J. J. Alonso. “Stanford university unstructured (SU²): open-source analysis and design technology for turbulent flows”. In: *52nd Aerospace Sciences Meeting*. National Harbor, Maryland, USA, 2014.
- [ARB12a] M. J. Armstrong, C. A. H. Ross, and M. J. Blackwelder. “Propulsion system component considerations for NASA N3-X turboelectric distributed propulsion system”. In: *SAE International Journal of Aerospace* 5.2 (2012), pp. 344–353.
- [ARB12b] M. J. Armstrong, C. A. H. Ross, and M. J. Blackwelder. “Trade studies for NASA N3-X turboelectric distributed propulsion system electrical power system architecture”. In: *SAE International Journal of Aerospace* 5.2 (2012), pp. 325–335.
- [Arm+15] M. J. Armstrong, M. Blackwelder, A. Bollman, C. Ross, A. Campbell, C. Jones, and P. Norman. *Architecture, voltage and components for a turboelectric distributed propulsion electric grid, NASA/CR-2015-218440*. 2015.
- [Arn+14] A. Arntz, O. Atinault, D. Destarac, and A. Merlen. “Exergy-based aircraft aeropropulsive performance assessment: CFD application to boundary layer ingestion”. In: *AIAA Aviation Forum*. Atlanta, Georgia, USA, 2014.
- [Ash82] H. Ashley. “On making things the best – aeronautical uses of optimization”. In: *Journal of Aircraft* 19.1 (1982), pp. 5–28.
- [ATA16] ATAG – Air Transport Action Group. <http://www.atag.org>. 2016.
- [Av59] I. H. Abbott and A. E. von Doenhoff. *Theory of wing sections, including a summary of airfoil data*. Dover publications Inc., 1959.
- [Bal+02] V. Balabanov, C. Charpentier, D. K. Ghosh, G. Quinn, G. Vanderplaats, and G. Venter. “Visualdoc: a software system for general purpose integration and design optimization”. In: *9th AIAA/ISSMO Symposium on Multidisciplinary Analysis and Optimization*. Atlanta, Georgia, USA, 2002.

- [Bar+16] A. K. Barlas, C. Tibaldi, F. Wahle, and H. A. Madsen. “Aeroelastic optimization of a 10MW wind turbine blade with active trailing edge flaps”. In: *34th Wing Energy Symposium*. San Diego, California, USA, 2016.
- [Bar+19] N. Bartoli, T. Lefebvre, S. Dubreuil, R. Olivant, R. Priem, N. Bons, J. R. R. A. Martins, and J. Morlier. “Adaptive modeling strategy for constrained global optimization with application to aerodynamic wing design”. In: *Aerospace Science and Technology* 90 (2019), pp. 85–102.
- [BB12] S. Burguburu and P.-M. Basset. “Turboshaft engine predesign and performance assessment”. In: *48th AIAA/ASME/SAE/ASEE Joint Propulsion Conference & Exhibit*. Atlanta, Georgia, 2012.
- [BCM17] G. C. Bucsan, K. B. Colline, and D. M. Mavris. “Generalized methodology for sizing unconventional propulsion and configuration aircraft”. In: *AIAA Aerospace Sciences Meeting*. Grapevine, Texas, USA, 2017, pp. 1–32.
- [BD11] M. K. Bradley and C. K. Droney. *Subsonic Ultra Green Aircraft Research: Phase I – Final report*. NASA/CR-2011-216847. 2011.
- [BD12] M. K. Bradley and C. K. Droney. *Subsonic Ultra Green Aircraft Research: Phase II. N+4 advanced concept development*. 2012.
- [BD15] M. K. Bradley and C. K. Droney. *Subsonic Ultra Green Aircraft Research: Phase II – Volume II – Hybrid Electric Design Exploration*. NASA/CR-2015-218704. 2015.
- [Bel+13] P. Belotti, C. Kirches, S. Leyffer, J. Linderoth, J. Luedtke, and A. Mahajan. “Mixed-integer nonlinear optimization”. In: *Acta Numerica* 22 (2013), pp. 1–131.
- [Ben62] J. F. Benders. “Partitioning procedures for solving mixed variables programming problems”. In: *Numerische Mathematik* 4 (1962), pp. 238–252.
- [BH14] J. J. Berton and W. J. Haller. “Noise and emissions assessment of the N3-X transport”. In: *52nd Aerospace Sciences Meeting*. National Harbor, Maryland, USA, 2014.
- [BHK13] J. Bedouet, N. Huynh, and R. Kervarc. “GAMME, a meta-model to unify data needs in simulation modeling (WIP)”. In: *Proceedings of the Symposium on Theory of Modeling & Simulations – DEVS Integrative M&S Symposium, article n. 14*. San Diego, California, USA, 2013.
- [Bis+18] M. Bishara, P. Horst, H. Madhusoodanan, M. Brod, B. Daum, and R. Rolfes. “A structural design concept for a multi-shell Blended Wing Body with laminar flow control”. In: *Energies* 11.383 (2018).
- [Blo95] C. L. Bloebaum. “Coupling strength-based system reduction for complex engineering design”. In: *Structural Optimization* 10.2 (1995), pp. 113–121.
- [BM+13] H. Budde-Meiwes, J. Drillkens, B. Lunz, J. Muennix, S. Rothgang, J. Kowal, and D. U. Sauer. “A review of current automotive battery technology and future prospects”. In: *Proceedings of the Institution of Mechanical Engineers, Part D: Journal of Automobile Engineering* 227.5 (2013), pp. 761–776.

- [BM18a] B. J. Brelje and J. R. R. A. Martins. “Development of a conceptual design model for aircraft electric propulsion with efficient gradients”. In: *Electric Aircraft Technologies Symposium* (2018).
- [BM18b] B. J. Brelje and J. R. R. A. Martins. “Electric, hybrid, and turboelectric fixed-wing aircraft: a review of concepts, models, and design approaches”. In: *Progress in Aerospace Sciences* 104 (2018), pp. 1–19.
- [BMK97] R. D. Braun, A. A. Moore, and I. M. Kroo. “Collaborative approach to launch vehicle design”. In: *Journal of Spacecraft and Rockets* 34.4 (1997), pp. 478–486.
- [Boe16] Boeing. *Current market outlook 2016-2035*. http://www.boeing.com/resources/boeingdotcom/commercial/about-our-market/assets/downloads/cmo_print_2016_final_updated.pdf. 2016.
- [Boh+18] B. Bohari, A. Borlon, P. B. Mendoza Santos, A. Sgueglia, E. Benard, M. Bronz, and S. Defoort. “Conceptual design of distributed propellers aircraft: non-linear aerodynamic model verification of propeller-wing interaction in high-lift configuration”. In: *AIAA SciTech Forum*. Kissimmee, Florida, USA, 2018, pp. 1–27.
- [Bon18] J. T. Bonet. “Blended wing body transport aircraft research & development”. In: *31st Congress of the International Council of the Aeronautical Sciences*. Belo Horizonte, Brasil, 2018.
- [Bor+16] N. K. Borer, M. D. Patterson, K. V. Viken, M. D. Moore, J. Bevirt, A. M. Stroll, and A. R. Gibson. “Design and performance of the NASA SCEPTOR distributed electric propulsion flight demonstrator”. In: *AIAA Aviation Technology, Integration, and Operations Conference*. Washington, DC, USA, 2016.
- [Bor+17] N. K. Borer, J. M. Derlaga, K. A. Deere, and M. B. Carter. “Comparison of aeropropulsive performance predictions for distributed propulsion configurations”. In: *AIAA Aerospace Sciences Meeting*. Grapevine, Texas, USA, 2017, pp. 1–16.
- [Bra04] M. K. Bradley. *A sizing methodology for the conceptual design of Blended Wing-Body transports*. NASA/CR-2004-213016. 2004.
- [Bra18] M. Bradley. “Design of electric and hybrid-electric aircraft”. In: *Presentation at Aviation Forum – Hybrid aircraft course*. Atlanta, Georgia, USA, 2018.
- [Bro11] G. V. Brown. “Weights and efficiencies of electric components of a turboelectric aircraft propulsion system”. In: *49th AIAA Aerospace Sciences Meeting*. Orlando, Florida, USA, 2011.
- [BS10a] G. Blatman and B. Sudret. “Adaptive sparse polynomial chaos expansion based on least angle regression”. In: *Journal of Computational Physics* 230.6 (2010), pp. 2345–2367.
- [BS10b] G. Blatman and B. Sudret. “Efficient computational of global sensitivity indices using sparse polynomial chaos expansions”. In: *Reliability Engineering & System Safety* 95.11 (2010), pp. 1216–1229.
- [BSH18] J. Bijewitz, A. Seitz, and M. Hornung. “Power plant pre-design exploration for a turbo-electric propulsive fuselage concept”. In: *AIAA Propulsion and Power Forum 2018*. Cincinnati, Ohio, USA, 2018.

- [BSS96] R. J. Balling and J. Sobieszczanski-Sobieski. “Optimization of coupled systems: a critical overview of approaches”. In: *AIAA Journal* 34.1 (1996), pp. 6–17.
- [BV18] M. Brown and R. Vos. “Conceptual design and evaluation of Blended Wing-Body aircraft”. In: *AIAA SciTech Forum*. Kissimmee, Florida, USA, 2018.
- [Cam03] D. J. Campbell. “Revolutionary propulsion and power for 21st century aviation”. In: *AIAA/ICAS International Air and Space Symposium and Exposition: The Next 100 Y*. Dayton, Ohio, USA, 2003.
- [Cam+05] R. Campbell, M. Carter, O. Pendergraft, D. Friedman, and L. Serrano. “Design and testing of a blended wing body with boundary layer ingestion nacelles at high Reynolds numbers (invited)”. In: *43rd AIAA Aerospace Sciences Meeting and Exhibit*. Reno, Nevada, USA, 2005.
- [Cam+11] C. Campbell, E. Dittman, J. MacRae, C. Ehringer, A. Stone, K. Lake, S. Haskins, and R. R. Mankbadi. “Design of a hybrid electrical propulsion system”. In: *52nd AIAA/ASME/ASCE/AHS/ASC Structure, Structural Dynamics and material Conference*. Denver, Colorado, USA, 2011.
- [Car04] M. Carlsson. “Reduced order model of a blended wing body aircraft configuration”. In: *Journal of Aircraft* 41.6 (2004), pp. 1523–1529.
- [Car09] G. M. Carlomagno. *Elementi di gasdinamica*. 1st ed. Liguori, 2009.
- [CER15] CERAS. *CERAS reference aircraft*. <https://ceras.ilr.rwth-aachen.de/>. 2015.
- [CFM16] CFM International. *LEAP engine specification*. <https://www.cfmaeroengines.com/engines/leap/>. 2016.
- [Che12] Y. Cheng. “Preliminary fuselage structural configuration of a flying-wing type airliner”. MA thesis. Cranfield, UK: Cranfield University, 2012.
- [Chu+16] H. Chung, J. T. Hwang, J. S. Gray, and H. A. Kim. “Allocation mission design optimization of next-generation aircraft using a parallel computational framework”. In: San Diego, California, USA: 57th AIAA/ASCE/AHS/ASC Structures, Structural Dynamics and Materials Conference, 2016.
- [Cin+17a] G. Cinar, D. N. Mavris, M. Emeneth, A. Schneegans, and Y. Fefermann. “Sizing, integration and performance evaluation of hybrid electric propulsion subsystem architectures”. In: *AIAA Aerospace Sciences Meeting*. Grapevine, Texas, USA, 2017, pp. 1–18.
- [Cin+17b] G. Cinar, D. N. Mavris, M. Emeneth, A. Schneegans, C. Riediger, Y. Fefermann, and A. Isikveren. “Development of a parametric power generation and distribution subsystem models at conceptual aircraft design stage”. In: *AIAA Aerospace Sciences Meeting*. Grapevine, Texas, USA, 2017, pp. 1–18.
- [Cla+17] S. Clarke, M. Redifer, K. V. Papathakis, A. Samuel, and T. Foster. “X-57 power and command system design”. In: *2017 IEEE Transportation and Electrification Conference and Explo ITEC*. Chicago, Illinois, USA, 2017, pp. 393–400.

- [CM47] R. H. Cameron and W. T. Martin. “The orthogonal development of non-linear functionals in series of Fourier-Hermite functionals”. In: *Annals of Mathematics* 48.2 (1947), pp. 385–392.
- [Cos11] L. A. Costello. “State of the art of pilotes electric airplanes, NASA’s centellian challenge data and fundamental design implications”. MA thesis. Daytona Beach, Florida, USA: Embry-Riddle Aeronautical University School, 2011.
- [Cra+94] E. J. Cramer, J. E. Dennis Jr., P. D. Frank, R. M. Lewis, and G. R. Shubin. “Probme formulation for multidisciplinary design”. In: *SIAM Journal on Optimization* 4.4 (1994), pp. 754–776.
- [CRI18] F. Centracchio, M. Rossetti, and U. Iemma. “Approach to the weight estimation in the conceptual design of hybrid-electric-powered unconventional regional aircraft”. In: *Journal of Advanced Transportation* 2018 (2018), pp. 1–15.
- [CSS75] R. I. Cukier, J. H. Schaibly, and K. E. Shuler. “Study of the sensitivity of coupled reaction systems to uncertainties in rate coefficients. III. Analysis of the approximations”. In: *The Journal of Chemical Physics* 63 (1975), pp. 1140–1149.
- [CSV09] A. R. Conn, K. Schienburg, and L. N. Vicente. *Introduction to derivative-free optimization*. 1st ed. Society for Industrial and Applied Mathematics SIAM, 2009.
- [CW16] F. Collier and R. Wahls. *ARMD Strategic Thrust 3: ultra-efficient commercial vehicles subsonic transport*. <https://www.nasa.gov/sites/default/files/atoms/files/armd-sip-thrust-3a-508.pdf>. Washington DC, Columbia, USA, 2016.
- [CZM13] K. Chircop and D. Zammit-Mangion. “On ϵ -constraint based methods for the generation of Pareto frontiers”. In: *Journal of Mechanics Engineering and Automation* 3 (2013), pp. 279–289.
- [Dé12] J.-A. Désidéri. “Multiple-gradient descent algorithm (MGDA) for multiobjective optimization”. In: *Comptes Rendus Mathématique* 350.5 (2012), pp. 313–318.
- [dBV18] R. de Vries, M. T. Brown, and R. Vos. “A Preliminary Sizing Method for Hybrid-Electric Aircraft Including Aero-Propulsive Interaction Effects”. In: *Aviation Technology, Integration, and Operations Conference*. Atlanta, Georgia, USA, 2018.
- [DC12] W. P. Dupont and C. Colongo. *Preliminary design of a commercial transport aircraft*. 2nd ed. Class notes, ISAE-Supaero, 2012.
- [de 15a] A. de Marco. *Quaderni di Dinamica e Simulazione di Volo*. Class notes, Università degli Studi di Napoli “Federico II”. <http://wpage.unina.it/agodemar/DSV-DQV/>, 2015.
- [de 15b] C. de Nicola. *Appunti per un corso di aerodinamica degli aeromobili*. 1st ed. Class notes, Università degli Studi di Napoli “Federico II”. http://wpage.unina.it/denicola/AdA/DOWNLOAD/Appunti_AdA_2014_2015.pdf, 2015.

- [Deb+02] K. Deb, A. Pratap, S. Agarwal, and T. Meyarivan. “A fast and elitist multiobjective genetic algorithm: NSGA-II”. In: *Evolutionary Computation, IEEE Transactions on* 6.2 (2002), pp. 182–197.
- [Dee+17a] K. A. Deere, J. K. Viken, S. A. Viken, M. B. Carter, M. R. Wiese, and N. Farr. “Computational analysis of a wing designed for the X-57 distributed electric propulsion aircraft”. In: *17th AIAA Aviation Technology, Integration, and Operations Conference*. Denver, Colorado, 2017.
- [Dee+17b] K. A. Deere, J. K. Viken, S. A. Viken, M. B. Carter, M. R. Wiese, and N. Farr. “Computational analysis of powered lift augmentation for the LEAPTech distributed electric propulsion wing”. In: *35th AIAA Applied Aerodynamics Conference*. Denver, Colorado, 2017.
- [Def+18] S. Defoort, M. Méheut, B. Paluch, R. Liaboeuf, R. Murray, D. Mincu, and J.-M. David. “Conceptual design of disruptive aircraft configurations based on high-fidelity OAD process”. In: *AIAA Aviation Forum*. Atlanta, Georgia, USA, 2018.
- [Den16] Y. Denieul. “Preliminary design of control surfaces and laws for unconventional aircraft configurations”. PhD thesis. ISAE-Supaero, 2016.
- [Dev+15] T.P. Dever, K. P. Duffy, a. J. Provenza, P. L. Loyselle, B. B. Choi, C. R. Morrison, and A. M. Lowe. *Assessment of technologies for noncryogenic hybrid electric propulsion, NASA/TP-2015-216588*. 2015.
- [DGA84] DGA – Direction Général de l’Armement. *Devis de masse des avions*. AIR 2001/D. 1984.
- [dHV19] R. de Vries, M. F. M. Hoogreef, and R. Vos. “Preliminary sizing of a hybrid-electric passenger aircraft featuring over-the-wing distributed-propulsion”. In: *AIAA SciTech Forum*. San Diego, California, USA, 2019.
- [Dil+18] E. Dillinger, C. Döll, R. Liaboeuf, C. Toussaint, J. Hermetz, C. Verbeke, and M. Ridel. “Handling qualities of ONERA’s small business concept plane with distributed electric propulsion”. In: *31st Congress of the International Council of the Aeronautical Sciences*. Belo Horizonte, Brasil, 2018.
- [Dre07] M. Drela. *A user’s guide to MSES 3.05*. MIT Dept. of Aeronautics and Astronautics, Cambridge, Massachusetts, USA. 2007.
- [Dre11] M. Drela. “Development of the D8 transport configuration”. In: *29th AIAA Applied Aerodynamics Conference*. Honolulu, Hawaii, USA, 2011.
- [Dre93] M. Drela. *Design and optimization method for multi-element airfoils*. MIT Dept. of Aeronautics and Astronautics, Cambridge, Massachusetts, USA. 1993.
- [Dre96] M. Drela. *A user’s guide to LINDOP 2.50*. MIT Dept. of Aeronautics and Astronautics, Cambridge, Massachusetts, USA. 1996.
- [Dub+14] S. Dubreuil, M. Berveillier, F. Petitjean, and M. Salaün. “Construction of bootstrap confidence intervals on sensitivity indices computed by polynomial chaos expansion”. In: *Reliability Engineering & System Safety* 121 (Supplement C) (2014), pp. 263–275.

- [DW60] G. B. Dantzig and P. Wolfe. “Decomposition principle for linear programs”. In: *Operations Research* 8.1 (1960), pp. 101–111.
- [dW97] A. G. de Barros and S. C. Wirasinghe. “New aircraft characteristics related to airport planning”. In: *First ATRG Conference*. Vancouver, Canada, 1997.
- [EAS12] EASA. *Commission Regulation (EU) n. 965/2012*. Official Journal of the European Commission, 2012. Chap. 4, p. 98.
- [EAS15] EASA. *Large aeroplane evacuation certification requirements, proposed CM-CS-008*. EASA–European Union Aviation Safety Agency, 2015.
- [EAS17] EASA. *Certification specifications for large aeroplanes CS-25, amd. 3*. EASA–European Union Aviation Safety Agency, 2017.
- [Eco+16] T. D. Economon, F. Palacios, S. R. Copeland, T. W. Lukaczyk, and J. J. Alonso. “SU2: An Open-Source Suite for Multiphysics Simulation and Design”. In: *AIAA Journal* 54.3 (2016), pp. 828–846.
- [EdC07] C. Hall E. de la Rosa Blanco and D. Crichton. “Challenges in the silent aircraft engine design”. In: *45th AIAA Aerospace Sciences Meeting and Exhibit*. Reno, Nevada, USA, 2007.
- [Edw02] T. Edwards. ““Kerosene” fuels for aerospace propulsion – composition and properties”. In: *38th AIAA/ASME/SAE/ASEE Joint Propulsion Conference & Exhibit*. Indianapolis, Indiana, USA, 2002.
- [Efr79] B. Efron. “Bootstrap methods: another look at the jackknife”. In: *The Annals of Statistics* 7.1 (1979), pp. 1–26.
- [Eic+06] D. J. Eichenberg, C. A. Gallo, P. A. Solano, W. K. Thompson, and D. R. Vrnak. *Development of a 32 inch diameter levitated ducted fan conceptual design, NASA/TM-2006-214481*. 2006.
- [Ert08] P. Erto. *Probabilità e statistica per le scienze e l’ingegneria*. 3rd ed. McGraw-Hill, 2008.
- [ESD82] ESDU. *Approximate methods for estimation of cruise range and endurance: aeroplanes with turbo-jet and turbo-fan engines*. ESDU – Engineering Sciences Data Unit, 1982.
- [Eur10] European Organisation for the Safety of Air Navigation. *EUROCONTROL specification for trajectory prediction*. Reference nr.: EUROCONTROL-SPEC-143, Edition 1.0. 2010.
- [Fel+11] J. L. Felder, G. V. Brown, H. D. Kim, and J. Chu. “Turboelectric distributed propulsion in a hybrid wing body aircraft”. In: *20th International Symposium on Air Breathing Engines (ISABE)*. Fotherburg, Sweden, 2011.
- [Fer38] E. Fermi. *Thermodynamics*. First paperback of lecture notes. Martson Gate, Great Britain: Amazon.co.uk, Ltd., 1938.
- [Fin60] R. Fink. *USAF stability and control DATCOM. AFWAL-TR-83-3048*. McDonnell Douglas Corporation, Douglas Aircraft Division, for the Flight Control division, Air Force Flight Dynamics Laboratory, Wright-Patterson AFB, Ohio. 1960, revised november 1965, revised april 1978.

- [FKB09] J. L. Felder, H. D. Kim, and G. V. Brown. “Turboelectric distributed propulsion engine cycle analysis for hybrid-wing-body aircraft”. In: *47th AIAA Aerospace Sciences Meeting*. Orlando, Florida, USA, 2009.
- [FM99] P. Fuglsang and H. Madsen. “Optimization method for wind turbine rotors”. In: *Journal of Wing Engineering and Industrial Aerodynamics* 80 (1999), pp. 191–206.
- [Fol+11] G. J. Follen, R. Del Rosario, R. A. Wahls, and N. K. Madavan. “NASA’s fundamental aeronautics subsonic fixed wing project: generation N+3 technology portfolio”. In: *SAE 2011 AeroTech Congress and Exhibition*. Toulouse, France, 2011.
- [FP02] J. H. Ferziger and M. Perić. *Computational methods for fluid dynamics*. 3rd ed. Springer-Verlag Berlin Heidelberg GmbH, 2002.
- [Fra+12] A. Fraj, M. Budinger, T. El Halabi, J. C. Maré, and G. C. Negoita. “Modelling approaches for the simulation-based preliminary design and optimization of electromechanical and hydraulic actuation systems”. In: *53th AIAA/ASME/ASCE/AHS/ASC Structures, Structural Dynamics and Material Conference*. Honolulu, Hawaii, USA, 2012.
- [Fra15] Fraunhofer Institute. *Technology roadmap energy storage for electric mobility 2030*. http://www.isi.fraunhofer.de/isi-wAssets/docs/t/en/TRM-ESEM-2030_en_web.pdf. 2015.
- [Fre+14] J. Freeman, P. Osterkamp, M. W. Green, A. R. Gibson, and B. T. Schiltgen. “Challenges and opportunities for electric aircraft thermal management”. In: *Aircraft engineering and aerospace technology* 86.6 (2014), pp. 519–524.
- [FS19] J. L. Freeman and B. T. Schiltgen. “ECO-150-300 design and performance: a tube-and-wing distributed electric propulsion airliner”. In: *AIAA SciTech Forum*. San Diego, California, USA, 2019.
- [FTC12] J. L. Felder, M. T. Tong, and J. Chu. “Sensitivity of mission energy consumption to turboelectric distributed propulsion design assumptions on the N3-X hybrid wing body aircraft”. In: *48th AIAA/ASME/SAE/ASEE Joint Propulsion Conference*. Atlanta, Georgia, USA, 2012.
- [Gan04] R. Ganguli. “Survey of recent developments in rotorcraft design optimization”. In: *Journal of Aircraft* 41.3 (2004), pp. 493–510.
- [GDS11] A. S. Gohardani, G. Doulgeris, and R. Singh. “Challenges of future aircraft propulsion: a review of distributed propulsion technology and its potential application for the all electric commercial aircraft”. In: *Progress in Aerospace Sciences* 47.5 (2011), pp. 369–391.
- [GF15] I. Giagkiozis and P. J. Fleming. “Method for multi-objective optimization: an analysis”. In: *Information Sciences* 293 (2015), pp. 338–350.
- [GMS05] P. E. Gill, W. Murray, and M. A. Saunders. “SNOPT: an SQP algorithm for large-scale constrained optimization”. In: *SIAM Review* 47.1 (2005), pp. 99–131.

- [Goh14] A. S. Gohardani. *Distributed propulsion technology*. 1st ed. NOVA publishers – Mechanical Engineering Theory and Applications series, 2014.
- [Gol+17] D. Goldberd, D. Nalianda, P. Pilidis, and R. Singh. “Economic viability assessment of NASA’s blended wing-body N3-X aircraft”. In: *53rd AIAA/SAE/ASEE Joint Propulsion Conference*. Atlanta, Georgia, USA, 2017.
- [Gor+18] Z. Goraj, B. Goliszek, M. Kowalski, A. Seitz, F. Peter, and F. Meller. “Strategy and implementation of a parametric CAD model for R2035 aircraft structure and external configuration”. In: *31st Integrational Congress of the Aeronautical Sciences ICAS*. Belo Horizonte, Brasil, 2018.
- [Gra+14] J. S. Gray, K. T. Moore, T. A. Hearn, J. T. Hwang, J. R. R. A. Martins, and A. Ning. “Automatic evaluation of multidisciplinary derivatives using a graph-based problem formulation in OpenMDAO”. In: *15th AIAA/ISSMO Multidisciplinary Design Analysis and Optimization Conference*. Atlanta, Georgia, USA, 2014.
- [Gra+18a] J. S. Gray, G. K. Kenway, C. A. Mader, and J. R. R. A. Martins. “Aero-propulsive design optimization of a turboelectric boundary layer ingestion propulsion system”. In: *2018 Aviation Technology, Integration, and Operations Conference, AIAA Aviation Forum*. Atlanta, Georgia, USA, 2018.
- [Gra+18b] J. S. Gray, C. A. Mader, G. K. W. Kenway, and J. R. R. A. Martins. “Modeling boundary layer ingestion using a coupled aeropropulsive analysis”. In: *Journal of Aircraft* 55.3 (2018), pp. 1191–1199.
- [Gra+19] J. S. Gray, J. T. Hwang, J. R. R. A. Martins, K. T. Moore, and B. A. Naylor. “OpenMDAO: An open-source framework for multidisciplinary design, analysis, and optimization”. In: *Structural and Multidisciplinary Optimization* 59.4 (2019), pp. 1075–1104.
- [Gre+10a] E. M. Greitzer, P. A. Bonnefoy, E. De la Rosa Blanco, C. S. Dorbian, M. Drela, D. K. Hall, R. J. Hansman, J. J. Hileman, R. H. Liebeck, J. Lovegren, P. Mody, J. A. Pertuze, S. Sato, Z. S. Spakovszky, C. S. Tan, J. S. Hollman, J. E. Duda, N. Fitzgerald, J. Houghton, J. L. Kerrebrock, G. F. Kiwada, D. Kordonowy, J. C. Parrish, J. Tylko, E. A. Wen, and W. K. Lord. *N+3 aircraft concept designs and trade studies, final report. Volume 1. NASA/CR-2010-216794/VOL1*. <https://ntrs.nasa.gov/archive/nasa/casi.ntrs.nasa.gov/20100042401.pdf>. 2010.
- [Gre+10b] E. M. Greitzer, P. A. Bonnefoy, E. De la Rosa Blanco, C. S. Dorbian, M. Drela, D. K. Hall, R. J. Hansman, J. J. Hileman, R. H. Liebeck, J. Lovegren, P. Mody, J. A. Pertuze, S. Sato, Z. S. Spakovszky, C. S. Tan, J. S. Hollman, J. E. Duda, N. Fitzgerald, J. Houghton, J. L. Kerrebrock, G. F. Kiwada, D. Kordonowy, J. C. Parrish, J. Tylko, E. A. Wen, and W. K. Lord. *N+3 aircraft concept designs and trade studies, final report. Volume 2: Appendices—design methodologies for aerodynamics, structures, weight, and thermodynamic cycles. NASA/CR-2010-216794/VOL2*. <https://ntrs.nasa.gov/archive/nasa/casi.ntrs.nasa.gov/20100042398.pdf>. 2010.

- [Gre87] J. A. Green. “Aeroelastic tailoring of aft-swept high-aspect-ratio composite wings”. In: *Journal of Aircraft* 24.11 (1987), pp. 812–819.
- [Gro+88] B. Grossman, Z. Gurdal, G. J. Strauch, W. M. Eppard, and R. T. Haftka. “Integrated aerodynamic/structural design of a sailplane wing”. In: *Journal of Aircraft* 25.9 (1988), pp. 855–860.
- [Gro+90] B. Grossman, R. T. Haftka, P.-J. Kao, D. M. Polen, and M. Rais-Rohani. “Integrated aerodynamic-structural design of a transport wing”. In: *Journal of Aircraft* 27.12 (1990), pp. 1050–1056.
- [Gur+10] O. Gur, M. Bhatia, J. A. Schetz, W. H. Mason, R. K. Kapania, and D. N. Mavris. “Design optimization of a truss-braced-wing transonic transport aircraft”. In: *Journal of Aircraft* 47 (2010), pp. 1907–1917.
- [Hab+18] A. L. Habermann, J. Bijewitz, A. Seitz, and L. Hornung. “Performance Bookkeeping for aircraft configurations with fuselage wake-filling propulsion integration”. In: *Deutscher Luft -und Raumfahrtkongress 2018. Paper-ID 2018-480230*. Friedrichshafen, Germany, 2018.
- [Haf73] R. T. Haftka. *Automated procedure for design of wing structures to satisfy strength and flutter requirements*. 1973.
- [Haf+75] R. T. Haftka, J. H. Starnes Jr., F. W. Barton, and S. C. Dixon. “Comparison of two types of optimization procedures for flutter requirements”. In: *AIAA Journal* 13.10 (1975), pp. 1333–1339.
- [Haf77] R. T. Haftka. “Optimization of flexible wing structures subject to strength and induced drag constraints”. In: *AIAA Journal* 14.8 (1977), pp. 1101–1106.
- [Haf79] R. T. Haftka. *Approximate methods for combined thermal/structural design*. Tech. Rep. TP-1428, NASA. 1979.
- [Haf85] R. T. Haftka. “Simultaneous analysis and design”. In: *AIAA Journal* 23.7 (1985), pp. 1099–1103.
- [Hep12] M. Hepperle. “Electric flight – potential and limitations”. In: *Tech. rep. STO-MP-AVT-209*. Braunschweig: NATO, 2012.
- [Hep18] M. Hepperle. *MH Airfoil aerotool*. <https://www.mh-aerotools.de/airfoils/index.htm>. 2018.
- [Hep90] R. Heppeler. *Airfoil design and data*. 1st ed. Springer-Verlag Berlin Heidelberg GmbH, 1990.
- [HG12] C. Heath and J. S. Gray. “OpenMDAO: framework for flexible multidisciplinary design, analysis and optimization methods”. In: *53rd AIAA Structures, Structural Dynamics and Material Conference*. Honolulu, Hawaii, USA, 2012.
- [HHH08] L. U. Hansen, W. Heinze, and P. Horst. “Blended wing body structures in multidisciplinary pre-design”. In: *Structural and Multidisciplinary Optimization* 36.1 (2008), pp. 93–106.

- [Hil+08] J. I. Hileman, J. B. Katz, J. G. Mantilla, and G. Fleming. “Payload fuel energy efficiency as a metric for aviation environmental performance”. In: *26th International Congress of the Aeronautical Sciences ICAS*. Anchorage, Alaska, USA, 2008.
- [Hil+10] J. I. Hileman, Z. S. Spakovswky, M. Drela, M. A. Sargeant, and A. Jones. “Airframe design for silent fuel-efficient aircraft”. In: *Journal of Aircraft* 47 (2010), pp. 956–969.
- [HM15] J. T. Hwang and J. R. R. A. Martins. “Parallel allocation-mission optimization of a 128-route network”. In: *15th AIAA/ISSMO Multidisciplinary Design Analysis and Optimization Conference*. Dallas, Texas, USA, 2015.
- [HM18] J. T. Hwang and J. R. R. A. Martins. “A computational architecture for coupling heterogeneous numerical models and computing coupled derivatives”. In: *ACM Transactions on Mathematical Software (TOMS)* 44.4 (2018).
- [HMP12] R. P; Henderson, J. R. R. A. Martins, and R. E. Perez. “Aircraft conceptual design for optimal environmental performance”. In: *The Aeronautical Journal* 116.1175 (2012), pp. 1–22.
- [HN18] J. T. Hwang and A. Ning. “Large-scale multidisciplinary optimization of an electric aircraft for on-demand mobility”. In: *AIAA/ASCE/AHS/ASC Structures, Structural Dynamics, and Materials Conference*. Kissimmee, Florida, USA, 2018, pp. 1–18.
- [Hoe65] S. F. Hoerner. *Fluid-Dynamic drag, theoretical, experimental and statistical information*. Published by the author, 1965.
- [Hoo+19] M. F. M. Hoogreef, R. Vos, R. de Vries, and L. L. M. Veldhuis. “Conceptual assessment of hybrid electric aircraft with distributed propulsion and boosted turbofans”. In: *AIAA SciTech Forum*. San Diego, California, USA, 2019.
- [Hor+13] M. Hornung, A. T. Isikveren, M. Cole, and A. Sizmann. “CE-Liner – Case study for eMobility in air transportation”. In: *AIAA Aviation Technology, Integration, and Operations Conference*. Los Angeles, California, USA, 2013.
- [HRD16] J. Hermetz, M. Ridel, and C. Döll. “Distributed electric propulsion for small business aircraft: a concept-plane for key-technologies investigations”. In: *30th Congress of the International Council of the Aeronautical Sciences*. Daejeon, South Korea, 2016.
- [Hug09] C. E. Hughes. “NASA collaborative research on the ultra high bypass engine cycle and potential benefits for the noise, performance, and emissions”. In: *19th ISABE International Symposium on Air Breathing Engines*. Montreal, Canada, 2009.
- [Hwa+14] J. T. Hwang, D. Y. Lee, J. W. Cutler, and J. R. R. A. Martins. “Large-scale multidisciplinary optimization of a small satellite’s design and operation”. In: *Journal of Spacecraft and Rockets* 51.5 (2014), pp. 1648–1663.
- [Hwa15] J. T. Hwang. “A modular approach to large-scale design optimization of aerospace systems”. PhD thesis. University of Michigan, 2015.

- [IAT13a] IATA – International Air Transport Association. *IATA Technology roadmap*. IATA, 4th edition. 2013.
- [IAT13b] IATA – International Air Transport Association. *IATA Technology roadmap – Technical annex*. IATA, 4th edition. 2013.
- [ICA16] ICAO – Committee on Aviation Environmental Protection. *2016 Environmental report*. <https://www.icao.int/environmental-protection/Pages/env2016.aspx>. 2016.
- [ICA17] ICAO. *The ICAO Aerodrome Reference Code*. ICAO–International Civil Aviation Organisation, 2017.
- [Ike06] T. Ikeda. “Aerodynamic analysis of a Blended-Wing-Body aircraft configuration”. MA thesis. Melbourne, Australia: RMIT University, 2006.
- [IS14] A. T. Isikveren and M. Schmidt. “Future transport aircraft ultra-low emissions technology options”. In: *GARS Workshop Air Transport and Climate Change*. Worms, Germany, 2014.
- [Isi+12] A. T. Isikveren, A. Seitz, P. C. Vranty, C. Pernet, K. O. Plötner, and M. Horning. “Conceptual studies of universally-electric systems architectures suitable for transport aircraft”. In: *Deutscher Luft-und Raumfahrt Kongress 2012*. Berlin, Germany, 2012.
- [Isi+14] A. T. Isikveren, S. Kaiser, C. Pernet, and P. C. Vranty. “Pre-design strategies and sizing techniques for dual-energy aircraft”. In: *Aircraft engineering and aerospace technology* 86.6 (2014), pp. 525–542.
- [Jan+17] R. Jansen, C. Bowman, A. Jankovsky, R. Dyson, and J. Felder. “Overview of NASA electrified aircraft propulsion (EAP) research for large subsonic transports”. In: *AIAA Propulsion and Energy Forum*. Atlanta, Georgia, USA, 2017.
- [JHM18a] J. P. Jasa, J. T. Hwang, and J. R. R. A. Martins. “Design and trajectory optimization of a morphing wing aircraft”. In: Kissimmee, Florida, USA: AIAA/ASCE/AH-S/ASC Structures, Structural Dynamics and Materials Conference, 2018.
- [JHM18b] J. P. Jasa, J. T. Hwang, and J. R. R. A. Martins. “Open-source coupled aerostructural optimization using Python”. In: *Structural and Multidisciplinary Optimization* 57 (2018), pp. 1815–1827.
- [JPM10] P. Jansen, R. E. Perez, and J. R. R. A. Martins. “Aerostructural optimization of nonplanar lifting surfaces”. In: *Journal of Aircraft* 47.5 (2010), pp. 1491–1503.
- [Kaw11] R. T. Kawai. *Acoustic prediction methodology and test validation for an efficient low-noise hybrid wing body subsonic transport*. Tech. Rep. NF1676L-14465, NASA. 2011.
- [KBF08] H. D. Kim, G. V. Brown, and J. L. Felder. “Distributed turboelectric propulsion for hybrid wing body aircraft”. In: *2008 International Powered Lift Conference*. London, UK, 2008.
- [KC97] A. M. Kuethe and C. Y. Chow. *Foundation of aerodynamics: base of aerodynamics design*. 5th ed. New York, USA: John Wiley & Sons, 1997.

- [Khe15] M. Khero. “Aero-propulsive coupling of an embedded distributed propulsion system”. In: *33rd AIAA Applied Aerodynamics Conference*. Dallas, Texas, USA, 2015.
- [Kim10] H. D. Kim. “Distributed propulsion vehicles”. In: *International congress of the aeronautical sciences*. Nice, France, 2010.
- [Kim+13] H. D. Kim, J. L. Felder, M. T. Tong, and M. J. Armstrong. “Revolutionary aeropropulsion concept for sustainable aviation: turboelectric distributed propulsion”. In: *21st International Symposium on Air Breathing Engines (ISABE)*. Busan, Korea, 2013.
- [Kim+14] H. D. Kim, J. L. Felder, M. T. Tong, J. J. Berton, and W. Haller. “Turboelectric distributed propulsion benefits on the N3-X vehicle”. In: *Aircraft Engineering and Aerospace Technology* 86.6 (2014), pp. 558–561.
- [Kir02] M. R. Kirby. *TIES for dummies (Technology identification, evaluation, and selection), basic how to’s to implement the TIES method*. 3rd ed. Aerospace System Design Laboratory, Georgia Institute of Technology, 2002.
- [Kir15] R. Kirner. “An investigation into the benefits of distributed propulsion on advanced aircraft configurations”. PhD thesis. Cranfield University, 2015.
- [KL13] H. Kim and M.-S. Liou. “Shape design optimization of embedded engine inlets for N2B hybrid wing-body configuration”. In: *Aerospace Science and Technology* 30 (2013), pp. 128–149.
- [KM10] G. J. Kennedy and J. R. R. A. Martins. “Parallel solution methods for aerostuctural analysis and design optimization”. In: *Proceedings of the 13th AIAA/ISSMO Multidisciplinary Analysis Optimization Conference*. Forth Worth, Texas, USA, 2010.
- [Ko+03] A. Ko, T. Leifsson, W. H. Mason, J. A. Schetz, B. Grossman, and R. T. Haftka. “MDO of a blended-wing-body transport aircraft with distributed propulsion”. In: *AIAA’s 3rd Annual Aviation Technology, Integration, and operations (ATIO) Forum*. Denver, Colorado, USA, 2003.
- [KPA18] H. D. Kim, A. T. Petty, and P. J. Ansell. “A review of distributed electric propulsion concepts for air vehicle technology”. In: *2018 AIAA/IEEE Electric Aircraft Technologies Symposium*. Cincinnati, Ohio, USA, 2018.
- [Kra+88] D. Kraft et al. *A software package for sequential quadratic programming*. DFVLR Obersfaffenhofen, Germany, 1988.
- [Kro01] I. Kroo. *Aircraft design: synthesis and analysis*. Desktop Aeronautics, Inc., 2001.
- [Kro+84] I. M. Kroo, S. Altus, R. Braun, P. Gage, and I. Sobieski. “Multidisciplinary optimization methods for aircraft preliminary design”. In: *5th AIAA/USAF/NASA/ISSM Symposium of Multidisciplinary Analysis and Optimization*. Panama City Beach, Florida, USA, 1984.
- [Kro97] I. M. Kroo. “MDO for large-scale design”. In: *Multidisciplinary design optimization: state-of-the-art, edited by N. Alexandrov and M. Y. Hussaini* (1997), pp. 22–44.

- [KS15] M. Kozek and A. Schirrer. *Modelling and control for a Blended Wing Body Aircraft. A case study*. 1st ed. Springer Internatinoal Publishing, 2015.
- [KSM03] A. Ko, J. A. Schetz, and W. H. Mason. “Assessment of the potential advantages of distributed propulsion for aircraft”. In: *International society for air breathing engines* (2003), pp. 1–9.
- [KST92] A. Kumar, D. J. Singh, and C. Trexler. “Numerical study of the effects of reverse sweep on scramjet inlet performance”. In: *Journal of Propulsion and Power* 8 (1992), pp. 714–719.
- [KT19] Jonathan L. Kratz and George L. Thomas. “Dynamic Analysis of the STARC-ABL Propulsion System”. In: *AIAA Propulsion and Energy 2019 Forum*. Indianapolis, Indiana, USA, 2019.
- [Kuh+12] H. Kuhn, A. Seitz, L. Lorenz, A. T. Isikveren, and A. Sizmann. “Progress and perspectives of electric air transport”. In: *28th International Congress of the Aeronautical Sciences, ICAS*. Brisbane, Australia, 2012.
- [KVv10] H. J. M. Kok, M/ Voskuji, and M. J. L. van Tooren. “Distributed propulsion featuring boundary layer ingestion engines for the blended wing body subsonic transport”. In: *51st AIAA/ASME/ASCE/AHS/ASC Structures, Structural Dynamics, and Materials Conference*. Orlando, Florida, USA, 2010.
- [Lam+16] P.-A. Lambert, D. Alejo, Y. Fefermann, C. Maury, B. Thoraval, J.-P. Salanne, and A. T. Isikveren. “Long-term hybrid-electric propulsion architecture options for transport aircraft”. In: *Greener Aviation 2016*. Brussels, Belgium, 2016.
- [Lan03] Lange aviation. *Antares 20E product*. <https://www.lange-aviation.com/en/produkte/antares-20e/>. 2003.
- [LeV07] R. J. LeVeque. *Finite difference methods for ordinary and partial differential equations. Steady-state and time-dependent problems*. 10th ed. SIAM Society for Industrial and Applied Mathematics, 2007.
- [LeV92] R. J. LeVeque. *Numerical methods for conservation laws*. 2nd ed. Springer Basel AG, 1992.
- [LHF17] Y. Liu, P. Horst, and J. Friedrichs. “Development of a methodology for assessing and exploiting innovative aircraft concepts and technologies”. In: *Aerospace Europe CEAS conference*. Bucharest, Romania, 2017.
- [Li+12] P. Li, B. Zhang, Y. Chen, C. Yuan, and Y. Lin. “Aerodynamic design methodology for blended wing body transport”. In: *Chinese Journal of Aeronautics* 25 (2012), pp. 508–516.
- [Li+14] Y. Li, J. Deng, C. Mu, Z. Xing, and K. Du. “Vertical distribution of CO₂ in the atmospheric boundary layer: characteristics and impact of meteorological variables”. In: *Atmospheric Environment* 91 (2014).
- [Lie04] R. H. Liebeck. “Design of the blended wing-body subsonic transport”. In: *Journal of Aircraft* 41.1 (2004), pp. 10–25.

- [Lio+17] M.-F. Liou, H. Kim, B. Lee, and M.-S. Liou. *Aerodynamic design of the hybrid wing body propulsion-airframe integration*. NASA Tech. Rep., <https://ntrs.nasa.gov/archive/nasa/casi.ntrs.nasa.gov/20170007963.pdf>. 2017.
- [Liu+18] Y. Liu, A. Elham, P. Horst, and M. Hepperle. “Exploring vehicle level benefits of revolutionary technology progress via aircraft design and optimization”. In: *Energies* 11 (2018), pp. 1–22.
- [Liv99] E. Livne. “Integrated aeroservoelastic optimization: status and direction”. In: *Journal of Aircraft* 36.1 (1999), pp. 122–145.
- [LKL16] M.-S. Liou, H. Kim, and M.-F. Liou. *Challenges and progress in aerodynamic design of hybrid wingbody aircraft with embedded engines*. NASA Tech. Rep. NASA/TM–2016-218309. 2016.
- [LL12] J. Lowry and J. Larminie. *Electric vehicle technology explained*. 2nd ed. John Wiley & Sons, 2012. Chap. 2, pp. 23–29, 45.
- [LL87] L. D. Landau and E. M. Lifshitz. *Course of Theoretical Physics: Volume 6 – Fluid Mechanics*. 2nd ed. Translated by J. B. Sikes and W. H. Reid. Oxford, United Kingdom: Elsevier BH, 1987.
- [LM12] A. B. Lambe and J. R. R. A. Martins. “Extensions to the design structure matrix for the description of multidisciplinary design analysis and optimization processes”. In: *Structural and Multidisciplinary Design Optimization* 46.2 (2012), pp. 273–284.
- [LM14] Z. Lyu and J. R. R. A. Martins. “Aerodynamic design optimization studies of a blended-wing-body aircraft”. In: *Journal of Aircraft* 51.5 (2014), pp. 1604–1617.
- [LPR98] R. H. Liebeck, M. A. Page, and B. K. Rawdon. “Blended wing-body subsonic commercial transport”. In: *AIAA Aerospace Sciences Meeting and Exhibit 98-0438*. 1998.
- [LSF90] E. Livne, L. A. Schmit, and O. Friedmann. “Towards integrated multidisciplinary synthesis of actively controlled fiber composite wings”. In: *Journal of Aircraft* 27.12 (1990), pp. 797–992.
- [MA01] K. J. Millman and M. Aivazis. “Python for scientists and engineers”. In: *Computing in Science & Engineering* 12.2 (201), pp. 9–12.
- [MA04] R. T. Marler and J. S. Arora. “Survey of multi-objective optimization methods for engineering”. In: *Structural and Multidisciplinary Design Optimization* 26 (2004), pp. 369–395.
- [Mad+16] N. Madavan, J. Heidmann, C. Bowman, P. Kascak, A. Janjowsky, and R. Jansen. “A NASA perspective on electric propulsion technologies for commercial aviation”. In: *Workshop on technology roadmap for large electric machines*. University of Illinois Urbana–Champaign, USA, 2016.
- [Mal74] F. S. Malvestuto Jr. *Aircraft transporter*. US Patent Office, 3,856,238. 1974.
- [Man24] C. W. Manzel. *Propelling mechanism for the airship and like, serial no. 321,008*. US Patent Office, 1,487,872. 1924.

- [Man99] V. M. Manning. “Large-scale design of supersonic aircraft via collaborative optimization”. PhD thesis. Stanford University, 1999.
- [MAR05] J. R. R. A. Martins, J. J. Alonso, and J. J. Reuther. “A coupled adjoint-sensitivity analysis method for high-fidelity aero-structural design”. In: *Optimization and Engineering* 6.1 (2005), pp. 33–62.
- [Mar14] J. R. R. A. Martins. “Large-scale multidisciplinary design optimization of aerospace systems”. In: *SIAM Conference on Optimization*. San Diego, California, USA, 2014.
- [Mar+17] M. Marwa, S. M. Martin, B. C. Martos, and R. P. Anderson. “Analytic and numeric forms for the performance of propeller-powered electric and hybrid aircraft”. In: *AIAA Aerospace Sciences Meeting*. Grapevine, Texas, USA, 2017, pp. 1–37.
- [Mat18] Mathworks. *Simulink – simulation and model-based design*. <https://www.mathworks.com/products/simulink.html>. 2018.
- [McD16] R. McDonald. *OpenVSP workshop*. https://nari.arc.nasa.gov/sites/default/files/attachments/Welcome%20%26%20overview_Mcdonald.pdf. 2016.
- [McK97] M. D. McKay. “Nonparametric variance-based methods of assessing uncertainty importance”. In: *Reliability Engineering & System Safety* 57.7 (1997), pp. 267–279.
- [Meg12] T. H. Megson. *Aircraft structures for engineering students*. 5th ed. Elsevier Aerospace Engineering, 2012.
- [MH13] J. R. R. A. Martins and J. T. Hwang. “Review and unification of methods for computing derivatives of multidisciplinary computational models”. In: *AIAA Journal* 51.11 (2013), pp. 2582–2599.
- [MHP02] J. D. Mattingly, W. H. Heiser, and D. T. Pratt. *Aircraft engine design*. 2nd ed. AIAA Education Series, 2002.
- [Mie08] K. Miettinen. “Introduction to Multiobjective Optimization: Noninteractive Approaches”. In: *Multiobjective Optimization: Interactive and Evolutionary Approaches*. Ed. by J. Branke, K. Deb K.and Miettinen, and R. Słowiński. Berlin, Heidelberg: Springer Berlin Heidelberg, 2008, pp. 1–26.
- [MIT18a] MIT. *AVL – Athena Vortex Lattice*. <http://web.mit.edu/drela/Public/web/avl/>. 2018.
- [MIT18b] MIT. *XFOIL – subsonic airfoil development system*. <https://web.mit.edu/drela/Public/web/xfoil/>. 2018.
- [ML13] J. R. R. A. Martins and A. B. Lambe. “Multidisciplinary design optimization: a survey of architectures”. In: *AIAA Journal* 51.9 (2013), pp. 2049–2075.
- [MM13] C. A. Mader and J. R. R. A. Martins. “Stability-constrained aerodynamic shape optimization of flying wings”. In: *Journal of Aircraft* 50.5 (2013), pp. 1431–1449.

- [MMT09] J. R. R. A. Martins, C. Marriage, and N. Tedford. “pyMDO: an object-oriented framework for multidisciplinary design optimization”. In: *ACM Transactions on Mathematical Software* 36.4 (2009), pp. 201–225.
- [MN10] C. M. Macal and M. J. North. “Toward teaching agent-based simulation”. In: *Proceedings of the 2010 Winter Simulation Conference*. Baltimore, Maryland, USA, 2010, pp. 268–277.
- [MN18] K. R. Moore and A. Ning. “Distributed electric propulsion effects on traditional aircraft through multidisciplinary optimization”. In: *AIAA Aerospace Sciences Meeting 2018*. Kissimmee, Florida, USA, 2018.
- [MOM18] V. Mukhopadhyay, T. A. Ozorosky, and M. L. McMillin. “Structural configuration analysis of advanced flight vehicle concepts with distributed hybrid-electric propulsion”. In: *AIAA Aerospace Sciences Meeting 2018*. Kissimmee, Florida, USA, 2018.
- [Mon53] R. J. Monaghan. *A review and assessment of various formulae for turbulent skin friction in compressible flow*. Aeronautical Research Council Tech. Rep., C.P. No. 142 (15.464). 1953.
- [MS98a] R. Monti and R. Savino. *Aerodinamica. Parte Prima: fondamenti e principi*. 1st ed. Napoli, Italy: Liguori editore, 1998.
- [MS98b] R. Monti and R. Savino. *Aerodinamica. Parte Seconda: regimi di moto*. 1st ed. Napoli, Italy: Liguori editore, 1998.
- [MSC18] MSC Software. *Patran User’s guide*. <https://simcompanion.mscsoftware.com/infocenter/index?page=content&id=DOC11694>. 2018.
- [Muk+04] V. Mukhopadhyay, J. Sobieszczansky-Sobieski, I. Kosaka, G. Quinn, and G. N. Vanderplaats. “Analysis, design, and optimization of noncylindrical fuselage for blended-wing-body vehicle”. In: *Journal of Aircraft* 41.4 (2004), pp. 925–930.
- [Muk05] V. Mukhopadhaya. “Blended wing body (BWB) fuselage structural design for weight reduction”. In: *16th AIAA/ASME/ASCE/AHS/ASC Structures, Structural Dynamics and Materials Conference*. Austin, Texas, USA, 2005.
- [Muk07] V. Mukhopadhyay. “A conceptual aerospace vehicle structural system modeling, analysis and design process”. In: *48th AIAA/ASME/ASCE/AHS/ASC Structures, Structural Dynamics, and Materials Conference*. Honolulu, Hawaii, USA, 2007.
- [Muk96] V. Mukhopadhyay. “Structural concepts study of non-circular fuselage configurations”. In: *SAE technical paper 965561, World Aviation Congress & Exposition*. Los Angeles, California, USA, 1996.
- [NAE16] NAEC. *Commercial aircraft propulsion and energy systems research: reducing global carbon emission*. National Academy of Engineering Committee on Propulsion and Energy Systems to Reduce Commercial Aviation Carbon Emissions, National Academies Press, 2016.

- [Nag+12] B. Nagel, D. Böhnke, V. Gollnick, P. Schmollgruber, A. Rizzi, G. La Rocca, and J. J. Alonso. “Communication in aircraft design: can we establish a common language?” In: *28th Congress of the International Council of the Aeronautical Sciences*. Brisbane, Australia, 2012.
- [NAS13] NASA. *NASA X-48 project*. <https://www.nasa.gov/centers/dryden/news/NewsReleases/2013/13-08.html>. 2013.
- [NH16] C. L. Nickol and W. J. Haller. “Assessment of the performance potential of advanced subsonic transport concepts for NASA’s environmentally responsible aviation project”. In: *AIAA SciTech Forum*. San Diego, California, USA, 2016.
- [Nic16] L. Nicolai. *Lessons learned, a guide to improved aircraft design*. 1st ed. Library of Flight, AIAA, 2016.
- [NK10] S. A. Ning and I. M. Kroo. “Multidisciplinary considerations in the design of wings and wing tip devices”. In: 47.2 (2010), pp. 553–543.
- [NLR00] NLR. *GSP–Gasturbine Simulation Program*. <https://www.gspteam.com/about.html>. 2000.
- [NS12] M. Niță and D. Scholz. “Estimating the Oswald factor from basic aircraft geometrical parameters”. In: *Deutscher Lift- und Raumfahrtkongress 2012, Document ID: 281424*. 2012.
- [NW96] K Nickel and M. Wohlfahrt. *Tailless aircraft in theory and practice*. 2nd ed. Translated by E. M. Brown RN. AIAA Education Series, 1996.
- [OAG08] L. Owens, B. Allan, and S. Gorton. “Boundary-layer-ingesting inlet flow control”. In: *Journal of Aircraft* 45.4 (2008), pp. 1431–1440.
- [OEC11] OECD – Organisation for Economic Co-operation and Development. *OECD environmental outlook to 2050 – climate change chapter*. OECD, pre-release version. 2011.
- [Oli07] T. E. Oliphant. “Python for scientific computing”. In: *Computing in Science & Engineering* 9.3 (2007), pp. 10–20.
- [OM14] E. Ordoukhanian and A. M. Madni. “Blended wing body architecting and design: current status and future prospects”. In: *Procedia Computer Science* 28 (2014), pp. 619–625.
- [Ope18a] OpenMDAO. *An open-source framework for efficient multidisciplinary optimization*. v2.4 website: <http://www.openmdao.org/>. 2018.
- [Ope18b] OpenVSP. *A NASA open-source parametric geometry*. <http://openvsp.org/>. 2018.
- [OS16] P. Okonkwo and H. Smith. “Review of evolving trends in blended wing body aircraft design”. In: *Progress in Aerospace Sciences* 82 (2016), pp. 1–23.
- [PAG96] S. L. Padula, N. Alexandrov, and L. L. Green. “MDO test suite at NASA Langley Research Center”. In: *Proceedings of the 6th AIAA/NASA/ISSMO Symposium on Multidisciplinary Analysis and Optimization*. Bellevue, Washington, USA, 1996.

- [Pap+17] K. V. Papathakis, P. A. Burkhardt, D. W. Ehmann, and A. M. Sessions. “Safety considerations for electric, hybrid-electric and turbo-electric distributed propulsion aircraft testbeds”. In: *53rd AIAA/SAE/ASEE Joint Propulsion Conference*. Atlanta, Georgia, USA, 2017.
- [Par+05] W.-G. Park, H. S. Yun, H. H. Chun, and M. C. Kim. “Numerical flow simulation of flush type intake duct of waterjet”. In: *Ocean Engineering* 32.17–18 (2005), pp. 2107–2120.
- [Par71] V. Pareto. *Manual of political economy (manuale di economia politica)*. Translated by A. S. Schwier and A. N. Page. New York: Kelley, 1971 (1906).
- [PDA17] PDAS. *Digital Datcom software*. <http://www.pdas.com/datcom.html>. 2017.
- [Pei+16] L.V. Peijian, A. G. Rao, D. Ragni, and L. Veldhuis. “Performance analysis of wake and boundary-layer ingestion for aircraft design”. In: *Journal of Aircraft* 53 (2016), pp. 1517–1526.
- [Phi10] W. F. Phillips. *Mechanics of flight*. 2nd ed. Hoboken, New Jersey: John Wiley & Sons, Inc., 2010.
- [PI15] C. Pernet and A. T. Isikveren. “Conceptual design of hybrid-electric transport aircraft”. In: *Progress in Aerospace Sciences* 79 (2015), pp. 114–135.
- [Pip11] Pipistrel. *Taurus Electro G2 technical data*. <http://www.pipistrel.si/plane/taurus-electric/technical-data>. 2011.
- [Pip16] Pipistrel. *Alpha Electro technical data*. <https://www.pipistrel.ad/training/alpha-electro>. 2016.
- [Pit+11] D. M. Pitera, M. DeHaan, D. Brown, R. T. Kawai, S. Hollowell, P. Camacho, D. Bruns, and B. K. Rawden. *Blended wing body concept development with open rotor engine integration*. Tech. Rep. NASA/CR-2011-217303, Boeing & NASA. 2011.
- [PJM12] R. E. Perez, P. W. Jansen, and J. R. R. A. Martins. “pyOpt: A Python-Based Object-Oriented Framework for Nonlinear Constrained Optimization”. In: *Structures and Multidisciplinary Optimization* 45.1 (2012), pp. 101–118.
- [PKG14] C. Pernet, S. Kaiser, and C. Gologan. “Cost-based flight technique optimization for hybrid energy aircraft”. In: *Aircraft Engineering and Aerospace Technology* 86.6 (2014), pp. 591–598.
- [Pl13] K. O. Plötner, P. C. Vranty, M. Schmidt, A. T. Isikveren, and M. Hornung. *Impact of electrically powered transport aircraft on energy and battery demand for Germany*. Deutscher Luft- und Raumfahrtkongress (DLR), Document –ID: 1344. 2013.
- [Pla+07] A. P. Plas, M. A. Sargeant, V. Madani, D. Crichton, E. M. Greitzer, T. P. Hynes, and C. A. Hall. “Performance of a boundary layer ingestion (BLI) propulsion system”. In: *45th AIAA Aerospace Sciences Meeting and Exhibit*. Reno, Nevada, 2007.

- [Plo+13] K. O. Ploetner, M. Schmidt, D. Baranowsky, A. T. Isikveren, and M. Hornung. “Operating cost estimation for electric-powered transport aircraft”. In: *Aviation Technology, Integration and Operations Conference*. Los Angeles, California, USA, 2013.
- [PMP60] D. H. Perry, J. C. Morrall, and W. G. A. Port. *Low speed flight tests on a tailless delta wing aircraft (AVRO707B). Part 3 – lateral stability and control*. Royal Aircraft Establishment, C.P. No. 1106. 1960.
- [Pop00] S. B. Pope. *Turbulent flows*. 1st ed. Cambridge, United Kingdom: Cambridge University Press, 2000.
- [Por+14a] C. Pernet, S. Kaiser, A. T. Isikveren, and M. Hornung. “Integrated fuel-battery hybrid for a narrow-body sized transport aircraft”. In: *Aircraft Engineering and Aerospace Technology* 86.6 (2014), pp. 568–574.
- [Por+14b] C. Pernet, A. Seitz, A. T. Isikveren, and M. Hornung. “Methodology for sizing and performance assessment of hybrid energy aircraft”. In: *Journal of Aircraft* 52.1 (2014), pp. 341–352.
- [Por15] C. Pernet. *Electric drives for propulsion system of transport aircraft, new applications of electric drives*. Miroslav Chomat, IntechOpen, 2015. Chap. 5.
- [Pra+18] P. S. Prakasha, P. D. Ciampa, P. Della Vecchia, D. Ciliberti, M. Voskuij, D. Charbonnier, A. Jungo, L. Zhang, M. Fiority, K. Anisimov, and A. Mirzoyan. “Model based collaborative design& optimization of Blended Wing Body aircraft configuration: AGILE EU project”. In: *2018 Aviation Technology, Integration, and Operations Conference*. Atlanta, Georgia, USA, 2018.
- [Pri+18] S. Prince, D. Di Pasquale, K. Garry, and C. Nuzzo. “A rapid aerodynamic prediction method for unconventional transonic aircraft configurations”. In: *31st congress of the international council of the aeronautical sciences*. Belo Horizonte, Brazil, 2018.
- [PSY18] M. A. Page, E. J. Smetak, and S. L. Yang. “Single-aisle airliner disruption with a single-deck blended wing-body”. In: *31st Congress of the International Council of the Aeronautical Sciences*. Belo Horizonte, Brazil, 2018.
- [QA18] J. Qian and J. J. Alonso. “High-fidelity structural design and optimization of blended-wing-body transports”. In: *AIAA Aviation Forum*. Atlanta, Georgia, USA, 2018.
- [Qin+04] N. Qin, A. Vavalle, A. Le Moigne, M. Laban, K. Hackett, and P. Weinerfelt. “Aerodynamic considerations of blended wing-body aircraft”. In: *Progress in Aerospace Sciences* 40 (2004), pp. 321–343.
- [Rag68] D. V. Ragone. “Review of Battery Systems for Electrically Powered Vehicles”. In: *SAE Technical Paper*. SAE International, 1968.
- [Ray11] D. P. Raymer. *Advanced technology subsonic transport study, N+3 technologies and design concepts, NASA/TM 2011-217130*. 2011.
- [Ray18] D. P. Raymer. *Aircraft design: a conceptual approach*. 6th ed. Virginia: American Institute of Aeronautics & Astronautics, 2018.

- [RK99] D. L. Rodríguez and I. M. Kroo. “A 2D multidisciplinary design method for boundary layer ingesting inlets”. In: *37th AIAA Aerospace Sciences Meeting and Exhibit*. Reno, Nevada, USA, 1999.
- [RL16] J. Rheume and C. Lents. “Energy storage for commercial hybrid electric aircraft”. In: *SAE Technical paper 2016-01-2014* (2016).
- [RL97] J. Roskam and C.-T. E. Lan. *Airplane aerodynamics and performance*. 1st ed. DAR Corporation, 1997.
- [Rob47] R. C. Robinson. *High-speed aerodynamic characteristics of a 1/7-scale model of the Northrop YB-49 airplane*. National Advisory Council for Aeronautics, NACA RM No. A7C13. 1947.
- [Rod09] D. L. Rodriguez. “Multidisciplinary optimization method for designing boundary-layer-ingesting inlets”. In: *Journal of Aircraft* 46 (2009), pp. 883–894.
- [Ros05a] J. Roskam. *Airplane design part I: preliminary sizing of airplanes*. 4th ed. DAR Corporation, 2005.
- [Ros05b] J. Roskam. *Airplane design part II: preliminary configuration design and integration of the propulsive system*. 4th ed. DAR Corporation, 2005.
- [Ros05c] J. Roskam. *Airplane design part III: layout design of cockpit, fuselage, wing and empennage: cutaways and inboard profiles*. 4th ed. DAR Corporation, 2005.
- [Ros05d] J. Roskam. *Airplane design part IV: layout of landing gear and systems*. 4th ed. DAR Corporation, 2005.
- [Ros05e] J. Roskam. *Airplane design part V: component weight estimation*. 4th ed. DAR Corporation, 2005.
- [Ros05f] J. Roskam. *Airplane design part VI: preliminary calculation of aerodynamic, thrust and power characteristics*. 4th ed. DAR Corporation, 2005.
- [Ros05g] J. Roskam. *Airplane design part VII: determination of stability, control and performance characteristics: FAR and military requirements*. 4th ed. DAR Corporation, 2005.
- [Ros05h] J. Roskam. *Airplane design part VIII: airplane cost estimation: design, development, manufacturing and operating*. 4th ed. DAR Corporation, 2005.
- [Ros08] J. Roskam. *Airplane flight dynamics & automatic flight controls*. 1st ed. DAR Corporation, 2008.
- [Ros+14] C. Ross, M. Armstrong, M. Blackwelder, C. Jones, P. Norman, and S. Fletcher. “Turboelectric distributed propulsion protection system design trades”. In: *SAE Technical Paper 2014-01-2141* (2014), pp. 1–13.
- [Rou05] E. Roux. “Pour un approche analytique de la dynamique du vol”. PhD thesis. ISAE-Supaero, 2005.
- [Rou07] E. Roux. *Turbofan and turbojet engines – Database handbook*. Éditions Élodie Roux, 2007.

- [RSG14] S. Rondinelli, R. Sabatini, and A. Gardi. “Challenges and benefits offered by liquid hydrogen fuels in commercial aviation”. In: *Practical Responses to Climate Change (PRCC) 2014. Engineers Australia Convention 2014*. Melbourne, Australia, 2014.
- [RW98] J. L. Roberts and G. J. Walker. “Boundary layer ingestion effects in flush waterjet intakes”. In: *International Conference on Waterjet Propulsion II, RINA*. Amsterdam, Netherlands, 1998.
- [Sac+89] J. Sacks, W. J. Welch, T. J. Mitchell, and H. P. Wynn. “Design and analysis of computer experiments”. In: *Statistical science* (1989), pp. 409–423.
- [Sal+04] A. Saltelli, S. Tarantola, F. Campolongo, and M. Ratto. *Sensitivity analysis in practice. A guide to assessing scientific models*. 1st ed. John Wiley & Sons, 2004.
- [Sal+08] A. Saltelli, M. Ratto, T. Andres, F. Campolongo, J. Cariboni, D. Gatelli, Saisana L., and S. Tarantola. *Global sensitivity analysis. The primer*. 1st ed. John Wiley & Sons, 2008.
- [Sar+10] M. A. Sargeant, T. P. Hynes, W. R. Graham, J. I. Hileman, M. Drela, and Z. S. Spakovszky. “Stability of hybrid-wing-body-type aircraft with centerbody leading-edge carving”. In: *Journal of Aircraft* 47 (2010), pp. 970–974.
- [Sau13] M. Saucez. “Résolution des qualités de vol de l’aile volante Airbus”. PhD thesis. ISAE-Supaero, 2013.
- [Sch06] D. Scholz. *The Blended Wing Body (BWB) aircraft configuration*. Lecture for DGLR/VDI/RAeS/HAW. https://www.fzt.haw-hamburg.de/pers/Scholz/dglr/hh/text_2006_09_28_BWB.pdf, 2006.
- [Sch+16] M. Schmidt, M. Engelmann, T. Brügge-Zobel, M. Hornung, and M. Glas. “PAX-elerate – an open source passenger flow simulation framework for advanced aircraft cabin layouts”. In: *54th AIAA Aerospace Sciences Meeting*. San Diego, California, USA, 2016.
- [Sch+17a] P. Schmollgruber, J. Bedouet, A. Sgueglia, S. Defoort, R. Lafage, N. Bartoli, Y. Gourinat, and E. Benard. “Use of a certification constraints module for aircraft design activities”. In: *AIAA Aviation Forum*. Denver, Colorado, USA, 2017, pp. 1–19.
- [Sch+17b] S. L. Schnulo, J. Chin, A. D. Smith, and A. Dubois. “Steady state thermal analyses of SCEPTOR X-57 wingtip propulsion”. In: *17th AIAA Aviation Technology, Integration and Operations Conference*. Denver, Colorado, USA, 2017.
- [Sch18] P. Schmollgruber. “Enhancement of the aircraft design process through certification constraints management and full mission simulations”. PhD thesis. ISAE-Supaero, 2018.
- [Sch+18] P. Schmollgruber, N. Bartoli, J. Bedouet, E. Benard, and Y. Gourinat. “Improvement of the aircraft design process for air traffic management evaluations”. In: *AIAA SciTech Forum*. Kissimmee, Florida, USA, 2018.

- [Sch+19] P. Schmollgruber, C. Döll, J. Hermetz, R. Liaboeuf, M. Ridel, I. Cafarelli, O. Atinault, C. Fraçois, and B. Paluch. “Multidisciplinary exploration of DRAGON: an ONERA hybrid electric distributed propulsion concept”. In: *AIAA SciTech Forum*. San Diego, California, USA, 2019.
- [Sch65] L. A. Schmit. “Structural design by systematic synthesis”. In: *2nd Conference on Electronic Computation*. New York, NY, USA, 1965.
- [Sch81] L. A. Schmit. “Structural synthesis – its genesis and development”. In: *AIAA Journal* 19.10 (1981), pp. 1249–1263.
- [Sch84] L. A. Schmit. *Structural synthesis – Precursor and catalyst. Recent experiences in multidisciplinary analysis and optimization*. Tech. Rep. CP-2337, NASA. 1984.
- [SCS00] A. Saltelli, K. Chan, and E. M. Scott. *Sensitivity analysis*. 1st ed. John Wiley & Sons, 2000.
- [SDB20] A. Sgueglia, S. Dubreuil, and N. Bartoli. “Technologies sensitivity analysis of a hybrid aircraft”. In: *Aerospace system analysis and optimization in uncertainty*. Ed. by L. Brevault, M. Balesdent, and J. Morio. Springer Optimization and its Application. New York: Springer, 2020. Chap. 10.
- [Sei+12] A. Seitz, O. Schmitz, A. T. Isikveren, and L. Hornung. “Electrically powered propulsion: comparison and contrast to gas turbines”. In: *Deutscher Luft- und Raumfahrt Kongress 2012*. Berlin, Germany, 2012.
- [Sei+18] A. Seitz, F. Peter, J. Bijewitz, A. L. Habermann, Z. Goraj, M. Kowalsky, A. Castillo Pardo, C. Hall, F. Metter, R. Merkler, O. Petit, S. Samuelsson, B. Della Corte, and M. van Sluis, and G. Wortmann and M. Dietz. “Concept validation study for fuselage wake-filling propulsion integration”. In: *31st Integrational Congress of the Aeronautical Sciences ICAS*. Belo Horizonte, Brasil, 2018.
- [SF16] B. T. Schiltgen and J. Freeman. “Aeropropulsive interaction and thermal system integration within the ECO-150: a turboelectric distributed propulsion airliner with conventional electric machines”. In: *AIAA Aviation Technology, Integration and Operation Conference*. Washington, DC, USA, 2016.
- [Sfo14] P. Sforza. *Commercial airplane design principles*. 1st ed. Elsevier Aerospace Engineering Series, 2014.
- [SG08] P. Simon and Y. Gogotsi. “Materials for electrochemical capacitors”. In: *Nature Materials* 7 (2008), pp. 845–854.
- [Sgu+18a] A. Sgueglia, P. Schmollgruber, N. Bartoli, O. Atinault, N. Benard, and J. Morlier. “Exploration and sizing of a large passenger aircraft with distributed electric ducted fans”. In: *AIAA SciTech Forum*. Kissimmee, Florida, USA, 2018.
- [Sgu+18b] A. Sgueglia, P. Schmollgruber, E. Benard, N. Bartoli, and J. Morlier. “Preliminary sizing of a medium range blended wing-body using a multidisciplinary design analysis approach”. In: *MATEC Web of Conferences* 233.00014 (2018), pp. 1–8.

- [Sgu+19] A. Sgueglia, L. Cerquetani, L. C. e Chuna Lima, D. A. Kharoub, P. Rodriguez Otero, H. Kaur, P. Traverso, S. S. C. Yella, and E. Benard. “Multidisciplinary and multifidelity exploration of a medium range Blended Wing-Body transport aircraft”. In: *Aerospace* (2019). Submitted.
- [Sgu+20a] A. Sgueglia, P. Schmollgruber, E. Benard, N. Bartoli, and J. Morlier. “Exploration and optimization of a Blended Wing-Body concept featuring distributed electric propulsion”. In: *1st Aerospace European Conference AEC*. Bordeaux, France, 2020.
- [Sgu+20b] A. Sgueglia, P. Schmollgruber, E. Benard, N. Bartoli, J. Morlier, J. Jasa, J. R. R. A. Martins, J. T. Hwang, and J. S. Gray. “Development of a multidisciplinary design optimization framework with gradient calculation applied to hybrid aircraft”. In: *Journal of Aircraft* (2020).
- [SH13] O. Schmitz and M. Hornung. “Unified applicable propulsion system performance metrics”. In: *Proceedings of ASME Turbo Expo 2013: Turbine Technical Conference and Exposition*. San Antonio, Texas, USA, 2013.
- [SH15] R. Sturm and M. Hepperle. “Crashworthiness and ditching behaviour of blended-wing-body (BWB) aircraft design”. In: *International Journal of Crashworthiness* 20.6 (2015), pp. 592–601. eprint: <https://doi.org/10.1080/13588265.2015.1068997>. URL: <https://doi.org/10.1080/13588265.2015.1068997>.
- [Sha+14] J. C. Shaw, P. Norman, S. Galloway, and G. Burt. “A method for the evaluation of the effectiveness of turboelectric distributed propulsion power system architectures”. In: *SAE International Journal of Aerospace* 7.1 (2014), pp. 35–43.
- [Sha+15] J. C. Shaw, S. Fletcher, P. Norman, S. Galloway, and G. Burt. “Failure analysis of a turboelectric distributed propulsion aircraft electrical network: a case study”. In: *SAE Technical Paper 2015-01-2403* (2015), pp. 1–7.
- [Sie18] Siemens. *NX Nastran User’s guide*. https://docs.plm.automation.siemens.com/data_services/resources/nxnastran/10/help/en_US/tdocExt/pdf/User.pdf. 2018.
- [SIH13] A. Seitz, A. T. Isikveren, and M. Hornung. “Pre-concept performance investigation of electrically powered aero-propulsion systems”. In: *49th AIAA/ASME/SAE/ASEE Joint Propulsion Conference*. San Jose, California, USA, 2013.
- [Smi93] L. H. Smith Jr. “Wake ingestion propulsion benefit”. In: *Journal of Propulsion and Power* 9.1 (1993).
- [Sob93] I. M. Sobol. “Sensitivity estimated for non linear mathematical models”. In: *Math. Mod. Comp. Exp.* 1.4 (1993), pp. 407–414.
- [SR47] A. M. O. Smith and H. E. Roberts. “The jet airplane utilizing boundary layer air for propulsion”. In: *Journal of the Aeronautical Sciences* 14 (1947).
- [SR78] L. A. Schmit Jr. and R. K. Ramanathan. “Multilevel approach to minimum weight design including buckling constraints”. In: *AIAA Journal* 16.2 (1978), pp. 97–104.

- [SSP13] F. Stroscher, Z. Sika, and O. Petersson. “Reduced order model of a blended wing body aircraft configuration”. In: *Progress in Flight Dynamics, Guidance, Navigation, Control, Fault Detection and Avionics 6* (2013), pp. 635–650.
- [ST65] L. A. Schmit and W. A. Thornton. *Synthesis of an airfoil at supersonic Mach number*. Tech. Rep. CR 144, NASA. 1965.
- [Ste+12a] H. J. Steiner, A. Seitz, K. Wieczorek, K. Pl’otner, A. T. Isikveren, and M. Hornung. “Multi-disciplinary design and feasibility study of distributed propulsion systems”. In: *28th International Congress of the Aeronautical Sciences*. Brisbane, Australia, 2012.
- [Ste+12b] H. J. Steiner, P. C. Vranty, C. Gologan, K. Wieczorek, A. T. Isikveren, and M. Hornung. “Performance and sizing of transport aircraft employing electrically-powered distributed propulsion”. In: *Deutscher Luft- und Raumfahrtkongress*. Berlin, Germany, 2012.
- [Sud08] B. Sudret. “Global sensitivity analysis using polynomial chaos expansions”. In: *Reliability Engineering & System Safety* 93.7 (2008), pp. 964–979.
- [SV02] M. Stettner and R. Voss. “Aeroelastic, flight mechanic, and handling qualities of the MOB BWB configuration”. In: *9th AIAA/ISSMO Symposium on Multidisciplinary Analysis and Optimization*. Atlanta, Georgia, USA, 2002.
- [Tay79] J. Taylor. *Jane’s All the World Aircraft*. London: Jane’s, 1979.
- [TD09] O. Tremblay and L. A. Dessaint. “Experimental validation of a battery dynamic model for EV applications”. In: *World Electric Vehicle Journal* 3 (2009), pp. 289–298.
- [Tho13] J. Thorbeck. “DOC–Assessment method”. In: *3rd Symposium on Collaboration in Aircraft Design*. Linköping, Sweden, 2013.
- [TM08] P. A. Tipler and G. Mosca. *Physics for scientists and engineers*. 6th ed. W. H. Freeman and Company – New York, 2008.
- [TM10] N. P. Tedford and J. R. R. A. Martins. “Benchmarking multidisciplinary design optimization algorithms”. In: *Optimization and engineering* 11.1 (2010), pp. 159–183.
- [Tor86] E. Torenbeek. *Synthesis of subsonic airplane design*. Delft University Press, Martinus Nijhoff Publishers, 1986.
- [Tor91] E. Torenbeek. “Aerodynamic Performance of Wing-Body Configurations and the Flying Wing”. In: *SAE Transactions* 100 (1991), pp. 158–163. URL: <http://www.jstor.org/stable/44547589>.
- [TPP05] S. Tournier, J. Paduano, and D. Pagan. “Flow analysis and control in a transonic inlet”. In: *23rd AIAA Applied Aerodynamics Conference*. Toronto, Canada, 2005.
- [Ura+18] A. Uranga, M. Drela, D. K. Hall, and E. M. Greitzer. “Analysis of the aerodynamic benefit from boundary layer ingestion for transport aircraft”. In: *AIAA Journal* 56.11 (2018), pp. 4271–4281.

- [Van15] J. Van Boegart. “Assessment of potential fuel saving benefits of hybrid-electric regional aircraft”. MA thesis. TU Delft, 2015.
- [Van84] G. N. Vanderplaats. “Parallel solution methods for aerostructural analysis and design optimization”. In: *AIAA Journal* 22.11 (1984), pp. 1633–1640.
- [VB00] W. P. J. Visse and M. J. Broomhead. “GSP: a generic object-oriented gas turbine simulation environment”. In: *ASME. Turbo Expo: Power for Land, Sea and Air, Volume 1: Aircraft Engine; Marine; Microturbines and Small Turbomachinery*. V001T01A002. 2000.
- [VGH12] R. Vos, F. J. J. M. Geuskens, and M. F. M. Hoogreef. “A new structural design concept for blended wing body cabins”. In: *53rd AIAA/ASME/ASCE/AHS/ASC Structures, Structural Dynamics and Materials Conference*. Honolulu, Hawaii, USA, 2012.
- [vV14] J. van Dommelen and R. Vos. “Conceptual design and analysis of blended-wing-body aircraft”. In: *Journal of Aerospace Engineering* 228 (2014), pp. 2452–2474.
- [Wan12] F. Wang. “The comparison of aerodynamic and stability characteristics between conventional and blended wing body aircraft”. MA thesis. Cranfield, UK: Cranfield University, 2012.
- [WC10] S. Weihua and C. E. S. Cesnik. “Non linear aeroelasticity of a very flexible blended-wing-body aircraft”. In: *Journal of Aircraft* 47.5 (2010), pp. 1539–1553.
- [Wel+17] J. Welstead, J. L. Felder, M. D. Guynn, W. Haller, M. T. Tong, S. Jones, I. Ordaz, J. Quinlan, and B. Mason. *Overview of the NASA STARC-ABL (rev. B) advanced concept*. <https://ntrs.nasa.gov/search.jsp?R=20170005612>. 2017.
- [WF16] J. Welstead and J. L. Felder. “Conceptual design of a single-aisle turboelectric commercial transport with fuselage boundary layer ingestion”. In: *54th AIAA Aerospace Sciences Meeting*. San Diego, California, USA, 2016.
- [Wic+15] A. T. Wick, J. R. Hooker, C. J. Hardin, and C. H. Zeune. “Integrated aerodynamic benefits of distributed propulsion”. In: *AIAA SciTech Forum*. Kissimmee, Florida, USA, 2015.
- [WN18] L. Wiart and C. Negulescu. “Exploration of the Airbus "Nautilus" engine integration concept”. In: *31st Congress of the International Council of the Aeronautical Sciences*. Belo Horizonte, Brazil, 2018.
- [Xin+04] Y. Xin, B. Hou, Y. Bi, K. Cao, Y. Zhang, S. Wy, H. Ding, G. Wang, Q. Lui, and Z. Han. “China’s 30m, 35kV/2kA ac HTS power cable project”. In: *Superconduction Science and Technology* 17.5 (2004), pp. 332–335.
- [Xue+15] N. Xue, W. Du, J. R. R. A. Martins, and W. Shyy. “Lithium-Ion Batteries: Thermo-Mechanics, Performance, and Design Optimization”. In: *5 : Energy Storage* (2015), pp. 2849–2864.
- [Yoo+19] A. K. Yoon, D. Lohan, F. Arastu, J. Xiao, and K. Haran. “Direct drive electric motor for STARC-ABL tail-cone propulsor”. In: *AIAA Propulsion and Energy 2019 Forum*. Indianapolis, Indiana, USA, 2019.

-
- [Yu+18] Yin Yu, Zhoujie Lyu, Zelu Xu, and Joaquim R. R. A. Martins. “On the Influence of Optimization Algorithm and Starting Design on Wing Aerodynamic Shape Optimization”. In: *Aerospace Science and Technology* 75 (2018), pp. 183–199.
- [YWS15] G. Yingsong, Y. Whichun, and H. Shun. “Body freedom flutter of a blended wing body model coupled with flight control system”. In: *Procedia Engineering* 99 (2015), pp. 46–50.
- [ZNP08] D. W. Zingg, M. Nemec, and T. H. Pulliam. “A comparative evaluation of genetic and gradient-based algorithms applied to aerodynamic optimization”. In: *European Journal of Computational Mechanics* 17.1-2 (2008), pp. 103–126.
- [ZTW09] P. M. Zadeh, V. V. Toropov, and A. S. Wood. “Metamodel-based collaborative optimization framework”. In: *Structural and Multidisciplinary Optimization* 38.2 (2009), pp. 103–115.
- [ZZ12] S. Zhang and D. Zhao. *Aerospace materials handbook*. 1st ed. CRC Press, 2012.

Appendix A

FAST I/O file structure

```
<xml version="1.0" encoding="utf-8">
<fastDataModel xmlns:xsi="http://www.w3.org/2001/XMLSchema-instance"
xsi:noNamespaceSchemaLocation="fastDataModel.xsd">
<Aircraft id="143">
  <TLAR id="147">
    <!--Top level requirements-->
  </TLAR>
  <configuration id="146">
    <!--Configuration definition-->
  </configuration>
  <mission id="154">
    <sizing id="164" xsi:type="Sizing">
      <!--Design mission definition-->
    </sizing>
    <operational id="172" xsi:type="Oper">
      <!--Oper. mission definition-->
    </operational>
  </mission>
  <cabin id="155">
    <!--Seats, aisles and service dimensions-->
  </cabin>
  <geometry id="153">
    <wing id="185">
      <!--Wing geometry-->
    </wing>
    <high_lift id="160">
      <!--High lift geometry-->
    </high_lift>
    <fuselage id="162">
      <!--Fuselage geometry-->
    </fuselage>
    <ht id="166">
      <!--Horizontal tail geometry-->
    </ht>
    <vt id="157">
      <!--Vertical tail geometry-->
    </vt>
  </geometry>
</Aircraft>
</fastDataModel>
</xml>
```

```

        </vt>
        <propulsion id="161">
            <!--Engine geometry-->
        </propulsion>
        <LG id="176">
            <!--Landing gear geometry-->
        </LG>
    </geometry>
    <propulsion id="148">
        <!--Engine data definition-->
    </propulsion>
    <aerodynamics id="145">
        <!--Aerodynamics parameters-->
    </aerodynamics>
    <weight id="151">
        <airframe id="182">
            <!--Airframe masses-->
        </airframe>
        <propulsion id="184">
            <!--Propulsive masses-->
        </propulsion>
        <systems id="163">
            <!--Auxiliary system masses-->
        </systems>
        <furniture id="169">
            <!--Furniture masses-->
        </furniture>
        <crew id="183">
            <!--Crew mass-->
        </crew>
    </weight>
    <balance id="152">
        <airframe id="159">
            <!--Airframe CGs-->
        </airframe>
        <propulsion id="171">
            <!--Propulsive CGs-->
        </propulsion>
        <systems id="168">
            <!--Auxiliary system CGs-->
        </systems>
        <furniture id="170">
            <!--Furniture CGs-->
        </furniture>
        <crew id="180">
            <!--Crew CG-->
        </crew>
        <Payload id="177">
            <!--Payload CG-->
        </Payload>
    </balance>
</Aircraft>
</fastDataModel>

```

Appendix B

Review of MDO architecture

B.1 An introduction to the MDO

The multidisciplinary design optimization (MDO), as defined by Martins and Lambe [ML13], is a “field of engineering that focuses on the use of numerical optimization for the design of systems that involve a number of disciplines and subsystems”. The main motivation behind MDO is the multidisciplinary: generally, a system is driven by different disciplines at same time, and thus the interaction between them becomes even more important than the performance of an individual discipline. To take into account these interactions, MDO requires a well posed mathematical formulation. Solving the MDO problem early in the design process helps designers to improve the design, reducing at same time computational cost: it is then a powerful tool, that has become more and more important for engineers.

MDO origins can be traced back to '60 years, when Haftka [Haf73; Haf+75; Haf77; Haf79] and Schmit [Sch65; ST65; Sch81; Sch84] started to extend their experience in the structural optimization to other disciplines. Throughout decades, it has been successfully applied to a large variety of engineering problems: in the aerospace field, it has been used to solve the aeroelastic optimization, where structure, aerodynamics and control are strongly coupled [Ash82; Gre87; Gro+88; Gro+90; LSF90; Liv99; JPM10; NK10], rotorcraft design [Gan04], wind turbines design [FM99], spacecraft and satellite design [BMK97; Hwa+14], and even full aircraft design [Kro+84; Man99; AK05; HMP12; AC12]. It is to underline that the examples given vary from low fidelity problems, with limited number of design variables, to problems based on high fidelity, with thousands of variables involved. In general, low fidelity problems involve large number of disciplines, meanwhile high fidelity problems are limited to one/two disciplines, due to the computational time required. In recent years, thanks to the improvements in computational science and the new resources available, the major interest of MDO application is found within the high fidelity optimization: an example has already been given in Chapter 1, with respect to the BWB optimization carried out by Lyu and Martins [LM14].

The MDO process is mainly defined by its architecture, which is the ensemble of problem formulation and organization strategy (order of disciplines, model used, \dots). The MDO architecture, then, not only contains the algorithm used to find an optimal solution, but also the models that characterize the problem: replacing a low fidelity method with an higher one for an individual discipline will change the architecture, since it will lead to a different optimal solution, even with the same algorithm used.

Conceptually, many different architectures can be used to solve a given design problem, but not all of them will do the optimization with the same efficiency [TM10; MMT09; PAG96]: Fig. B.1 reports the results of a benchmarking of different MDO architectures, carried out by Tedford and Martins, clearly showing that there are some architectures that work well than others on a given design problem.

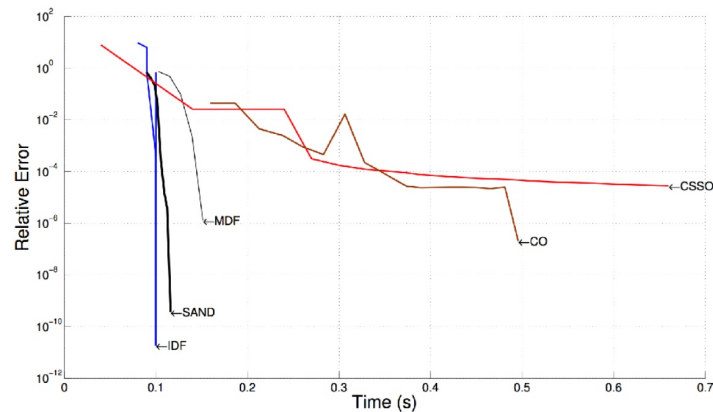


Figure B.1: Comparison between the relative error using different MDO architectures on a given design problem [TM10].

There are two family of MDO architectures: monolithic [Cra+94] and distributed [DW60; Ben62]. The first ones are tailored to solve a single problem optimization, meanwhile the second ones customize the problem and multiple optimization subproblems are solved with subsets of variables and constraints. Generally, the aircraft design problem is a fully coupled problem, where disciplines exchange information each others. As example, the aerodynamics and the structure sizing are strongly correlated: the aerodynamic loads are the main one to consider in the structural design. Thus there is no particular interest in optimizing each discipline separately, in a collaborative manner, but it is more relevant to have a top level optimizer that involves each discipline, as in monolithic architecture. For this reason, further details are provided only for this class of architectures. Nevertheless, it may be possible, for any reason, to have an aircraft design problem in which it is of interest to optimize disciplines separately, with a distributed architecture; then small notes on this class are provided by the end, following the division done by Martins and Lambe [ML13].

Further classification can be done based on the algorithm used. In particular, there are two main categories of algorithm: global or gradient-free [CSV09; ZTW09] and gradient based [MH13]. The first solves the problem in a "global" sense, that is they explore a certain

number of points contained in a prescribed design of experiment to finally get the optimum one. So the result is always the global minimum point; the main drawback is that they require a large number of points, and thus the computational cost may be high. On the other side, gradient based algorithms use the derivatives information to find the direction towards the minimum point. The gradient-based algorithms are more complicated to code than the gradient-free, since they require derivatives computation; also, they may lead to a different result because they may find a local minimum early in the process. However, if the gradients can be efficiently computed, the computational cost may be drastically reduced because of the limited number of iterations required [ZNP08]. In his Ph.D. thesis, Hwang set up a framework to compute analytic derivatives, using direct or adjoint method, for large-scale problems, called MAUD (Modular Analysis and Unified Derivatives) [Hwa15]. This procedure has been later used on a satellite optimization test case [Hwa+14], with promising results, and finally coded in OpenMDAO, an open-source optimization framework [Gra+19].

The notation for the MDO problem has been defined by Lambe and Martins [ML13] and it is reported in Table B.1. The first parameter to define is the objective function f , which is

Symbol	Definition
\underline{x}	Vector of design variables
\underline{y}	Vector of coupling variables (outputs from a discipline analysis)
\bar{y}	Vector of state variables (variables used inside only one discipline analysis)
f	Objective function
\underline{c}	Vector of design constraints
\underline{c}^c	Vector of consistency constraints
\mathcal{R}	Governing equations of a discipline analysis in residual form
N	Number of disciplines
$()^{(0)}$	Initial values of design variables
$()_0$	Functions of variables that are shared by more than one discipline
$()_i$	Functions of variables that apply only to discipline i
$()^*$	Functions of variables at their optimal value
$\bar{()}$	Approximations of a given function or vector of functions
$()^t$	Independent copies of variables distributed to other disciplines

Table B.1: Mathematical notation for MDO problem formulations, given by Martins and Lambe [ML13].

the parameter to be minimized at the end of the optimization problem. A design variable is a parameter that is always under the control of the optimizer, that is the parameter the objective function depends on. To differentiate local design variables, that concern a single discipline, to the shared one, the subscript $()_i$ and $()_0$ are used. The same convention applies to state variables and constraints. \bar{y} denotes generally a state variable, that is the output of a single discipline. Sometimes it is called response variable. The associated set of disciplinary equations in residual form is denoted by the symbol \mathcal{R} , so that the solution of the equations of discipline i is represented by the expression $\mathcal{R}_i = 0$. In a multidisciplinary approach some state variables are coupled: to note them, the notation y , without the bar, is

used. Another differentiation is done with the target variable, which is a copy of a coupled variable accessible to all the disciplines, and it is denoted by the superscript t . It has to be noted that, according to the problem, objective function may depend by state variables too.

Finally, an optimization problem may present design constraints, that are conditions to be respected to obtain a feasible solution. In the constraints are also added the consistency constraints c^c , which are a set of conditions to preserve consistency between coupling variable inputs and outputs at the optimal solution, *i.e.* for a discipline i it is possible to write $c_i^c = y_i^t - y_i = 0$.

To properly present an architecture, graphs are generally used [Aig+18]. Among the possible choices, in this work the already mentioned xDSM scheme is considered [LM12], with the definition given in Chapter 1. Thanks to this diagram, the sequence of operations implemented, together with the loop to solve, is presented in a clear and synthetic way.

B.2 A survey of monolithic architectures

The MDO problem in its most general form can be expressed as

$$\begin{aligned}
 &\text{minimize} && f_0(\underline{x}, \underline{y}) + \sum_{i=1}^N f_i(\underline{x}_0, \underline{x}_i, \underline{y}_i) \\
 &\text{with respect to} && \underline{x}, \underline{y}^t, \underline{y}, \bar{\underline{y}} \\
 &\text{subject to} && \underline{c}_0(\underline{x}, \underline{y}) \geq 0 \\
 &&& \underline{c}_i(\underline{x}_0, \underline{x}_i, \underline{y}_i) \geq 0 && \text{for } i = 1, \dots, N \\
 &&& \underline{c}_i^c = \underline{y}_i^t - \underline{y}_i = 0 && \text{for } i = 1, \dots, N \\
 &&& \mathcal{R}_i(\underline{x}_0, \underline{x}_i, \underline{y}_{j \neq i}^t, \bar{\underline{y}}_i, \underline{y}_i) = 0 && \text{for } i = 1, \dots, N
 \end{aligned} \tag{B.1}$$

which is known as the "all-at-once" (AAO) problem, where N represents the number of disciplines involved. This formulation contains all the elements described in previous section (coupling variables, state variables, residual, constraints and consistency constraints) directly in the problem statement. For sake of clarity, the notation $c_i \geq 0$ is used without loss of generality, since equality can be defined as pairs of inequalities with opposite sign.

The xDSM diagram for this problem is shown in Fig. B.2, where, to keep the diagram compact, the convention that any block referring to discipline i represents a repeated pattern for every discipline.

In practice, the AAO problem is never solved in this form because the consistency constraints can be easily eliminated without compromising the algorithm. More in general, different architectures can be deduced from Problem (B.1), depending on which equality constraint groups are eliminated. They are three: the simultaneous analysis and design SAND, the individual discipline feasible IDF and the multidisciplinary feasible MDF architecture, that have been well known in literature for a long time [Kro97; BSS96; Haf85; SR78].

The SAND architecture is obtained removing the consistency constraints by introducing a

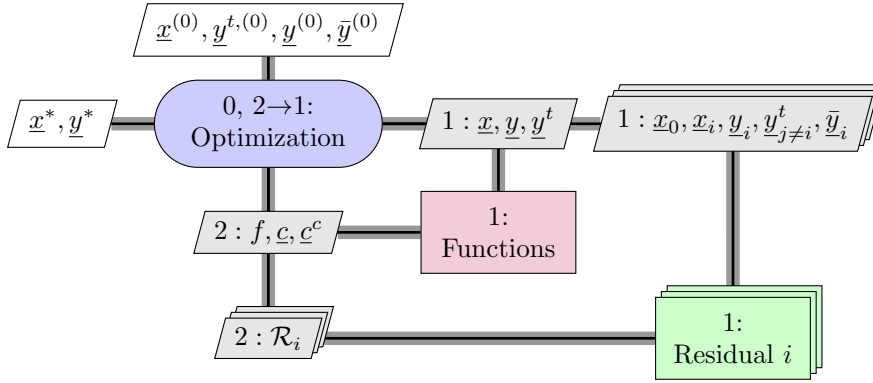


Figure B.2: xDSM diagram for the AAO problem.

single group of coupling variables to replace the separate target and response groups. This change yields to the following formulation:

$$\begin{aligned}
 &\text{minimize} && f_0(\underline{x}, \underline{y}) \\
 &\text{with respect to} && \underline{x}, \underline{y}, \bar{\underline{y}} \\
 &\text{subject to} && \underline{c}_0(\underline{x}, \underline{y}) \geq 0 \\
 &&& c_i(x_0, x_i, y_i) \geq 0 \quad \text{for } i = 1, \dots, N \\
 &&& \mathcal{R}_i(x_0, x_i, y_{j \neq i}^t, \bar{y}_i, y_i) = 0 \quad \text{for } i = 1, \dots, N
 \end{aligned} \tag{B.2}$$

The corresponding xDSM diagram is shown in Fig. B.3. The main feature of the SAND

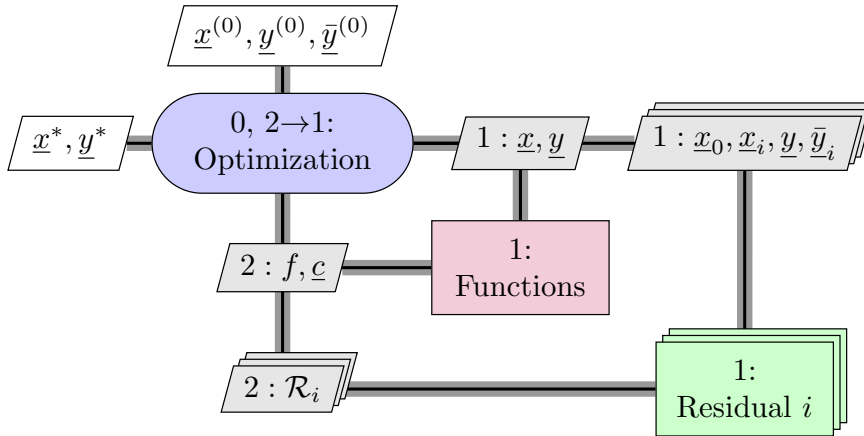


Figure B.3: xDSM diagram for the SAND architecture.

architecture is that, since there is no need to solve any discipline analysis at each iteration, the problem can be solved quickly by letting the optimizer explore regions infeasible with respect to the analysis constraints \mathcal{R}_i . However, it presents two main issues. First, despite there are no more consistency constraint, the formulation still requires all state variables

and discipline analysis equations, and then problem size at quick convergence can be issued in practice. Second, discipline analysis equations are treated explicitly and then residual values, and their derivatives in case of a gradient-based formulation, need to be available at the optimizer level. This means that, rather than computing y_i and \bar{y}_i , each discipline takes predetermined values of these parameters and returns the residuals \mathcal{R}_i . Often, in engineering, softwares for disciplines are “black box” that hide residuals and state variables and return directly coupling variables; also they are not accessible to users for editing. This limits the field application of SAND architecture.

To solve the issue, the discipline analysis constraints can be eliminated from Problem (B.1), yielding to the IDF architecture. The new statement is:

$$\begin{aligned}
 &\text{minimize} && f_0(\underline{x}, \underline{y}(\underline{x}, \underline{y}^t)) \\
 &\text{with respect to} && \underline{x}, \underline{y}^t \\
 &\text{subject to} && c_0(\underline{x}, \underline{y}(\underline{x}, \underline{y}^t)) \geq 0 \\
 & && c_i(x_0, x_i, y_i(x_0, x_i, \underline{y}_{i \neq j}^t)) \geq 0 \quad \text{for } i = 1, \dots, N \\
 & && c_i^c = y_i^t - y_i(x_0, x_i, \underline{y}_{i \neq j}^t) = 0 \quad \text{for } i = 1, \dots, N
 \end{aligned} \tag{B.3}$$

Diagram for IDF architecture is depicted in Fig. B.4.

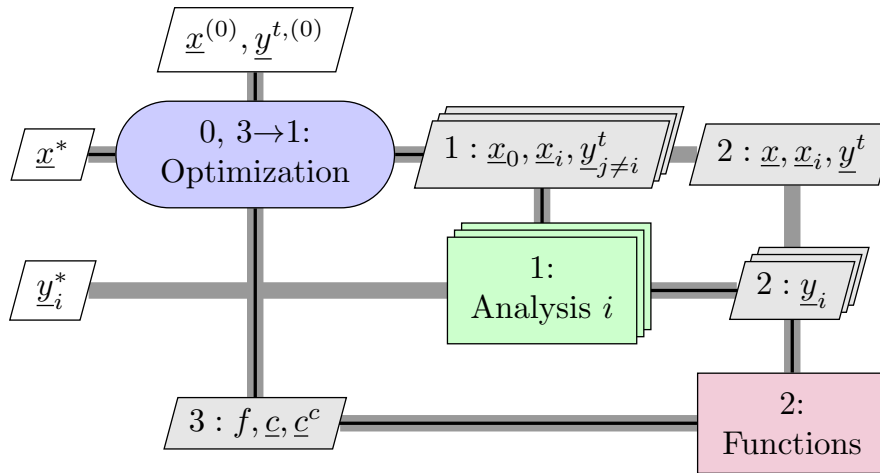


Figure B.4: xDSM diagram for the IDF architecture.

The main consequence of this reformulation is the removal of all the state variables and discipline analysis. IDF architecture finally allows the possibility to use "black box" analyses for the disciplines, enlarging the field of application of SAND, and it also enables parallel computation. Despite the IDF problem is smaller than the SAND, it needs in any case the consistency constraint and thus does not solve the first SAND issue, that is the large size. This can be a relevant point in the procedure when the problem is really large, *i.e.* as in the high fidelity optimization. Also, when the gradient-based are used, an accurate gradients calculation, needed for the optimal solution, can be very expensive in term of computational

cost [Hwa15], making the application of this architecture sometime unfeasible without a large amount of computational resources available.

To still reduce the problem size, the last modification that can be done is to remove from Problem (B.3) also the consistency constraints, or both the consistency constraints and the residual constraints from Problem (B.1), obtaining the MDF architecture:

$$\begin{aligned}
 &\text{minimize} && f_0(\underline{x}, \underline{y}(\underline{x}, \underline{y})) \\
 &\text{with respect to} && \underline{x} \\
 &\text{subject to} && c_0(\underline{x}, \underline{y}(\underline{x}, \underline{y})) \geq 0 \\
 &&& c_i(x_0, x_i, y_i(\underline{x}_0, x_i, \underline{y}_{i \neq j}^t)) \geq 0 \quad \text{for } i = 1, \dots, N
 \end{aligned} \tag{B.4}$$

The main consequence of the reformulation is that MDF requires a consistent set of coupling variables to be returned to the optimizer every time the objective and constraint functions are re-evaluated. In practice, it has to perform a fully MDA at each iteration. The xDSM diagram for the MDF architecture is shown in Fig. B.5, considering three disciplines.

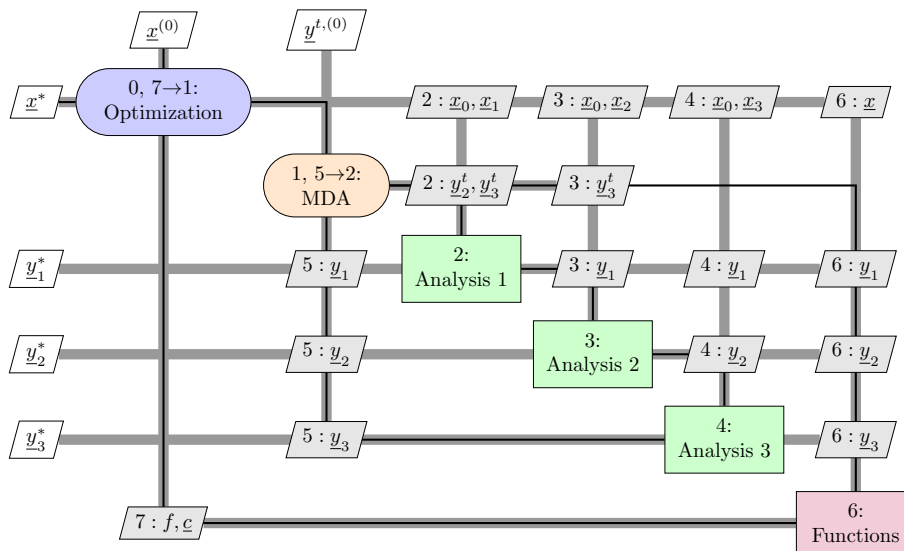


Figure B.5: xDSM diagram for the MDF architecture.

Because of the MDA to be solved at each iteration, MDF shows a slower convergence rate (see also Fig. B.1). It can be accelerated using proper algorithm for the MDA, like the Gauss-Seidel [Blo95] or the Newton [KM10] methods, or adding preconditioners to the linear system [LeV07]. Parallel computation also depends on the algorithm for the MDA, since some of them are sequential and do not allow parallelization.

The main advantage of the MDF is the reduced size of the problem, since only objective function, design variables and constraints are under the control of the optimizer. Also, it always returns a point that satisfies the consistency constraints, even if the optimization terminates earlier, because of the MDA. This feature is of main interest in aircraft design,

since it is still possible to get a tradeoff between final design and design variables, even if the optimization is not reached. However, it is to remark that only the consistency is assured, but not the feasibility: nothing ensures, indeed, that also design constraints are satisfied.

This last condition can be ensured choosing methods that maintain feasible design point during the iterations: methods to keep the feasible direction have been developed at that scope [Van84]. It is to note that the robust sequential quadratic programming methods, which represent a large category for gradient-based optimization, do not ensure the feasibility [GMS05; Kra+88].

The main drawback is the requirement of a converged MDA for each iteration. In case derivatives are needed, their calculation is more complicated than the IDF, because they need to be feasible with respect to all disciplines, and not only discipline feasible as in the IDF. The work of Martins and Hwang contains a set of methods to compute efficiently derivatives, to address the problem both in IDF and MDF architectures [MH13]. At this point, it has to emphasize that, despite the architectures are changing because of the elements added or removed, the MDO problem is always the same. Furthermore, it has the same set of optimal solution.

From the monolithic architecture is possible to derive the distributed architectures. In this category, problem is decomposed into multiple optimisation problems, solved sequentially. For completeness a classification of them is reported in Fig. B.6; more information can be found in the work of Martins and Lambe [ML13].

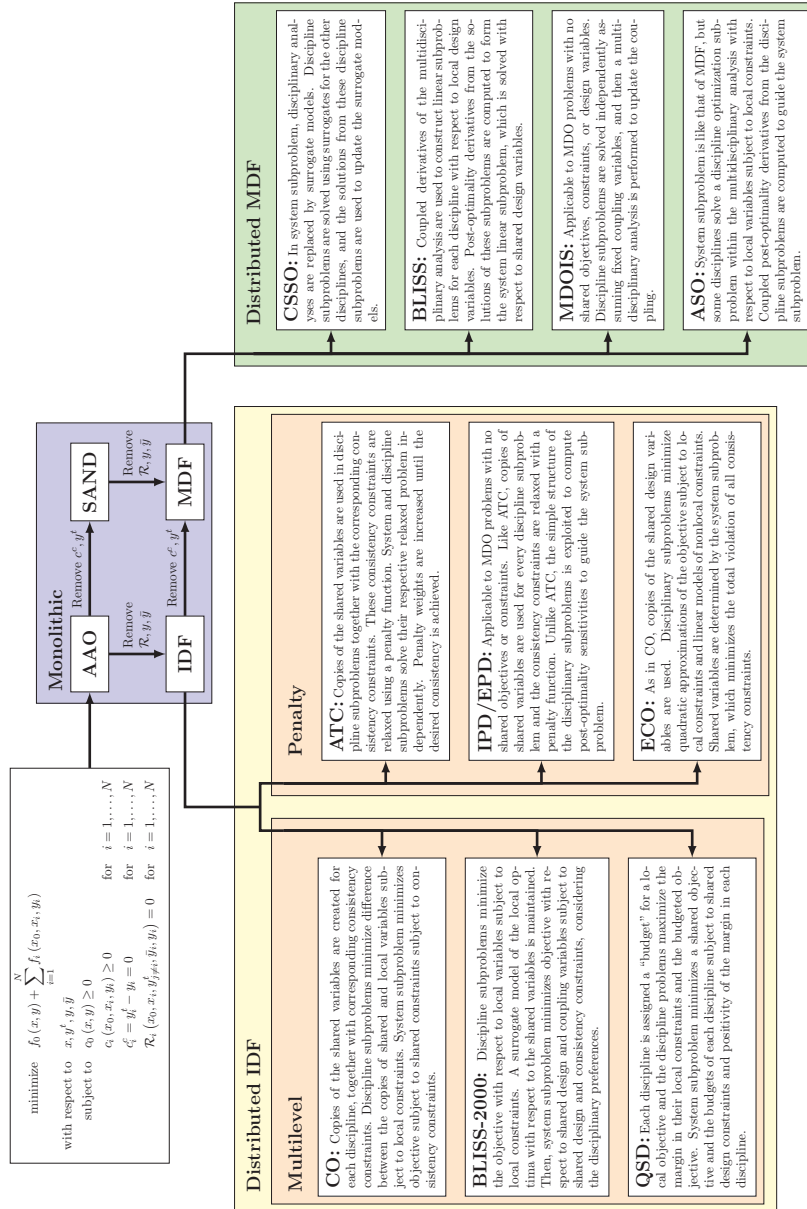


Figure B.6: Summary of MDO architectures [ML13].

Appendix C

Polynomial Chaos Expansion method for global sensitivity analysis

Polynomial chaos expansion (PCE) is a method developed belonging to the class of global sensitivity analysis methods [Sal+08].

For the purpose of explanation the notation x_i indicates the i -th element of a random vector \underline{x} , meanwhile the short notation $x_{\sim i}$ is used to indicate all the input variables but x_i . The number of input variables, that is the size of \underline{x} , is indicated by n ; finally $y = \mathcal{M}(\underline{x})$ represents a scalar output, computed with a generic method indicated as \mathcal{M} . It can be proven that [Ert08]

$$\sigma(y) = \sigma_{x_i} [E_{x_{\sim i}}(y|x_i)] + E_{x_i} [\sigma_{x_{\sim i}}(y|x_i)] \quad (\text{C.1})$$

In Eq. (C.1), E represents the expected mean value and $\sigma_{x_{\sim i}}(y|x_i)$ the variance when the factor x_i is fixed; then $E_{x_i} [\sigma_{x_{\sim i}}(y|x_i)]$ is the average variance left if x_i is fixed, and thus the term $\sigma_{x_i} [E_{x_{\sim i}}(y|x_i)]$ is the estimated reduction in variance when the parameter x_i is fixed. So, this method quantifies which is the reduction in variance if one input variable is fixed; in other word, it gives an indication about the relative importance of inputs on a given output.

In general, the variance can be divided into more terms, as in the analysis of variance (ANOVA):

$$\sigma(y) = \sum_{i=1}^n \sigma_{x_i} + \sum_{i,j>i}^n \sigma_{x_i,j} + \dots + \sigma_{123\dots k} \quad (\text{C.2})$$

where the first term represents the first order effects, and the other the coupled effects of second, third, ... order.

For additive models, $\sigma(y) = \sum_{i=1}^n \sigma_{x_i}$, that is the variance is explained by first order effects,

and there are no interaction between variables. In case of non additive models, part of the variance is explained by minor order terms.

Finally, first sensitivity indices are defined: they are the ratio between the reduction in variance when a variable x_i is fixed and the total variance.

$$s_i = \frac{\sigma_{x_i} [E_{x_{\sim i}}(y|x_i)]}{\sigma(y)} \quad (\text{C.3})$$

They quantify the reduction in variance if the variable x_i is fixed, and vary between 0 and 1. The considerations above can be rephrased saying that if the sum of the first order indices is equal to 1, the model is additive and minor order interactions between variables are meaningless. On the contrary, if the sum is smaller than one, then the weight of interactions between input variables is not negligible in the total variance of the response and these interactions need to be investigated more precisely. Since in practice it is not possible to consider all the orders, the notion of total indices is used. They are defined as

$$s_{T_i} = \frac{E_{x_{\sim i}} [\sigma_{x_i}(y|x_{\sim i})]}{\sigma(y)} \quad (\text{C.4})$$

and represent the expected variance that would be left if all inputs but x_i could be fixed. With the help of the total sensitivity indices, it is possible to get the interaction between the input parameters.

Among all the available methods to estimate this indices [McK97; Sob93; CSS75], the Sobol sensitivity test [Sob93] conjugates efficiency in computation and reliability in considering high number of interactions [Sal+04]. This method has been initially proposed by Sudret [Sud08] and it based on a polynomial chaos expansion approximation, that is very efficient in terms of numerical cost in the context of our study (low number of input variables and smooth mapping between inputs and outputs) than a Monte Carlo sampling [Sob93]. This approach has been further improved in [BS10b] using sparse PCE and will be used in the following.

In the hypothesis in which y is a second order random variable, it can be shown that [CM47]

$$y = \sum_{i=0}^{\infty} c_i \phi_i(\underline{x}) \quad (\text{C.5})$$

where $\{\phi_i\}_{i \in \mathbb{N}}$ is a polynomial basis orthogonal with respect to the probability density function (pdf) of \underline{x} (Legendre polynomials in case of uniform pdf) and c_i are unknown coefficients. Sparse PCE by Least Angle Regression (LAR) proposed by [BS10a] consists of the construction of a sparse polynomial basis $\{\phi_i\}_{\alpha \in \mathcal{A}}$, where $\alpha = (\alpha_1, \dots, \alpha_n)$ is a multi-index used to identify the polynomial acting with the power α_i on the variable x_i and \mathcal{A} is a set of index α . In practice \mathcal{A} is a subset of the set \mathcal{B} which contains all the index α up to a degree d *i.e.* $card(\mathcal{B}) = \frac{(d+n)!}{d!n!}$. Objective of sparse approach is to find an accurate polynomial basis $\{\phi_i\}_{\alpha \in \mathcal{A}}$ such as $card(\mathcal{A}) \ll card(\mathcal{B})$. This is achieved by Least Angle Regression *i.e.* unknown coefficients c_i are computed by iteratively solving a mean square

problem and selecting, at each iteration, the polynomial the most correlated with the residual [BS10a]. Finally, the following approximation is deduced:

$$y \approx \hat{y} = \sum_{\alpha \in \mathcal{A}} c_{\alpha} \phi_{\alpha}(\underline{x}) \quad (\text{C.6})$$

It should be noted that, in practice, identification of the unknown coefficients by LAR necessitates the evaluation of the model \mathcal{M} on a given design of experiments (DOE) sampled from the input space. Due to the orthogonality of the polynomial basis $\{\phi_i\}_{\alpha \in \mathcal{A}}$ it is possible to write:

$$\begin{cases} E[\hat{y}] = c_0 \\ \sigma[\hat{y}] = \sum_{\alpha \in \mathcal{A}} c_{\alpha}^2 E[\phi_{\alpha}^2(\underline{x})] \end{cases} \quad (\text{C.7})$$

where $E[\hat{y}]$ is the mean value and $\sigma[\hat{y}]$ is the variance of the output variable \hat{y} . It is shown in [Sud08] that the polynomial chaos expansion can be identified to the ANOVA decomposition, from which it is possible to show that the first order sensitivity index is

$$\hat{s}_i = \frac{\sum_{\alpha \in L_i} c_{\alpha}^2 E[\phi_{\alpha}^2(\underline{x})]}{\sigma[\hat{y}]} \quad (\text{C.8})$$

where $L_i = \{\alpha \in \mathcal{A} / \forall j \neq i \alpha_j = 0\}$; that is only the polynomials acting exclusively on variable x_i have been considered. The total sensitivity index can also be computed:

$$\hat{s}_{T_i} = \frac{\sum_{\alpha \in L_i^+} c_{\alpha}^2 E[\phi_{\alpha}^2(\underline{x})]}{\sigma[\hat{y}]} \quad (\text{C.9})$$

where $L_i^+ = \{\alpha \in \mathcal{A} / \alpha_i \neq 0\}$; that is all the polynomials acting on the variable x_i have been considered. In other words, all variance caused by its interactions, of any order, with any other input variables are included.

The accuracy of the sensitivity indices estimated thanks to PCE depends on the maximum degree d of the polynomials contained in the candidate basis \mathcal{B} and on the DOE used to compute the unknown coefficients c_{α} in Eq. (C.6). The degree d of the polynome is set to $d = 3$ for all the cases explored. Dubreuil et al. [Dub+14] suggested the bootstrap approach [Efr79] to assess the robustness of method. Training set and validation set are randomly chosen, the unknown coefficients of the PCE are computed and the corresponding sensitivity indices are estimated. These computations are repeated B times leading to an estimation of the mean values and the coefficients of variation for each sensitivity index.

Appendix D

Plot of sensitivity analysis results

D.1 2035 assessment – fixed battery case

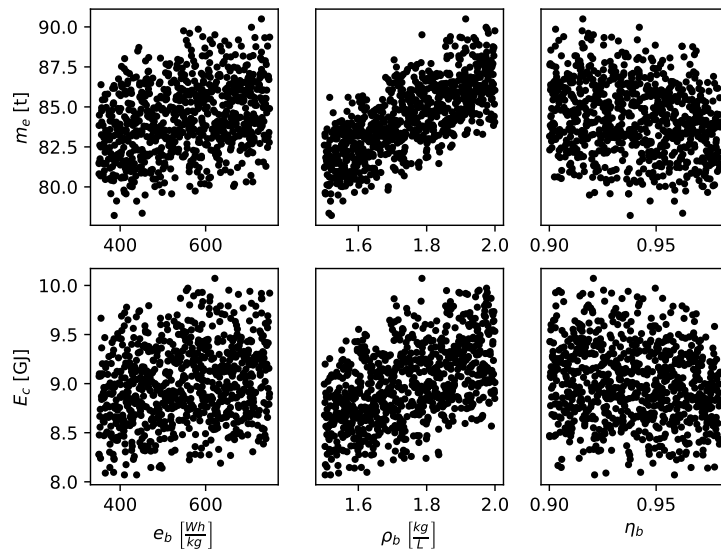


Figure D.1: Effects on OWE m_e and energy consumption E_c of battery technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Fixed battery case.

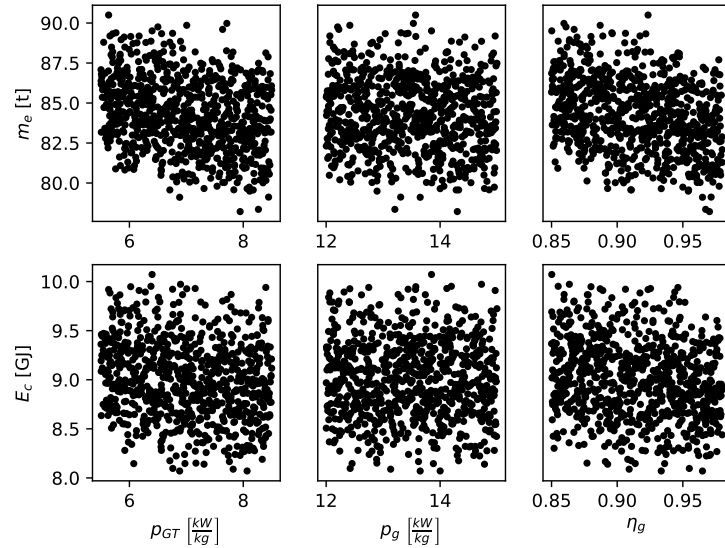


Figure D.2: Effects on OWE m_e and energy consumption E_c of gas turbine and generator technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Fixed battery case.

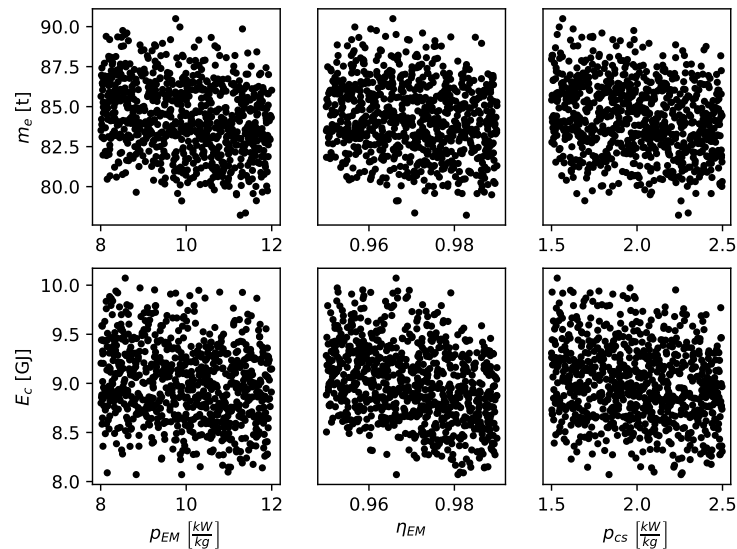


Figure D.3: Effects on OWE m_e and energy consumption E_c of electric motor and cooling system technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Fixed battery case.

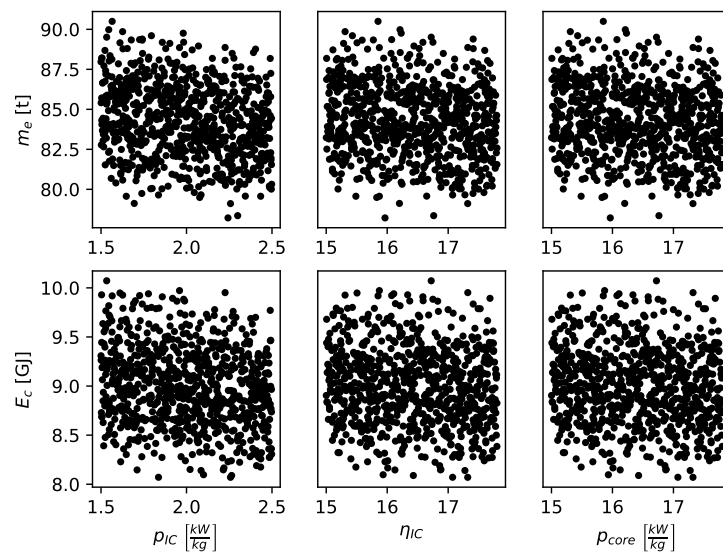


Figure D.4: Effects on OWE m_e and energy consumption E_c of inverter/converter and electric core technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Fixed battery case.

D.2 2035 assessment – battery resizing

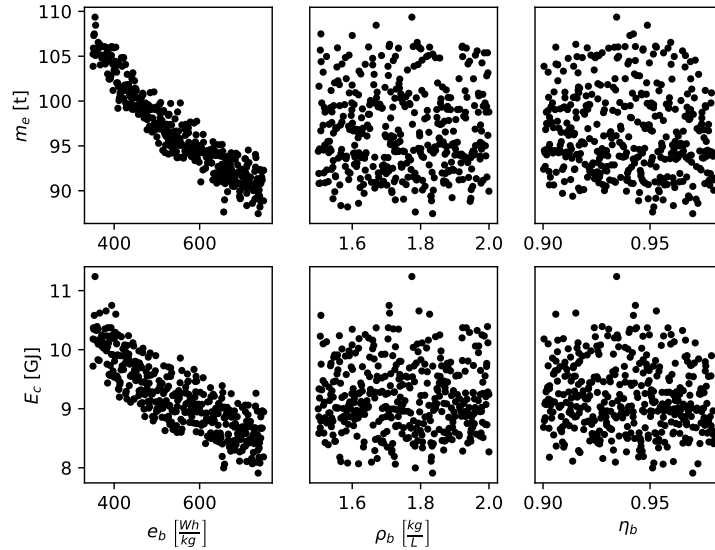


Figure D.5: Effects on OWE m_e and energy consumption E_c of battery technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Battery's resizing case.

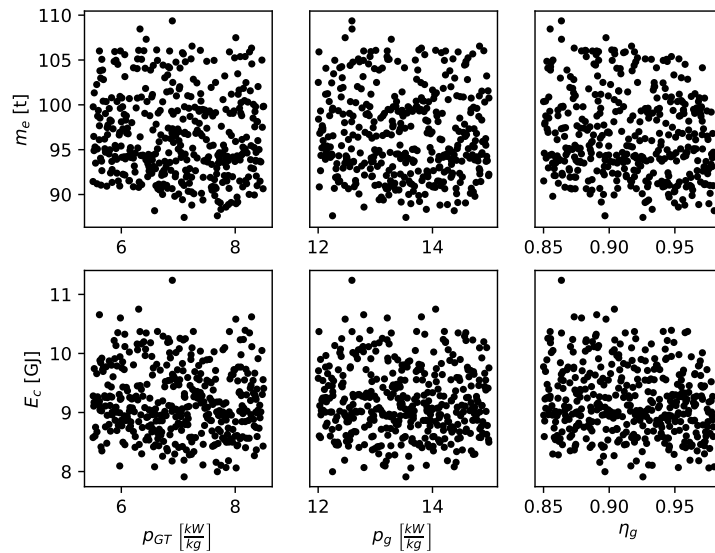


Figure D.6: Effects on OWE m_e and energy consumption E_c of gas turbine and generator technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Battery's resizing case.

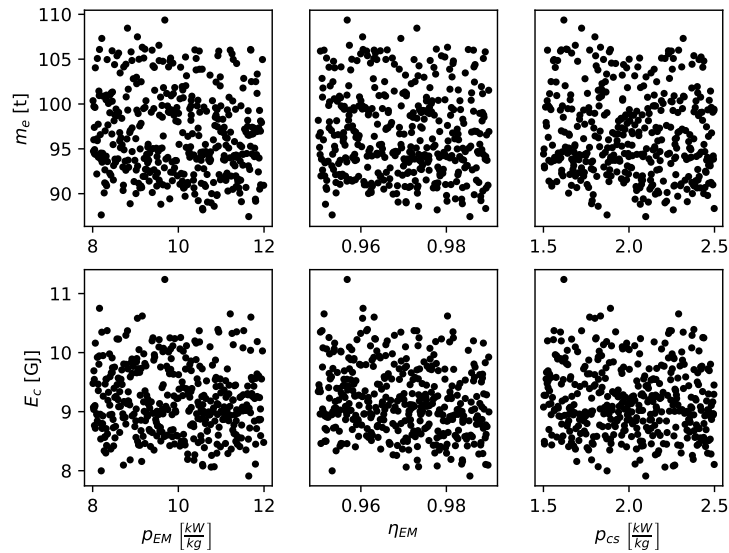


Figure D.7: Effects on OWE m_e and energy consumption E_c of electric motor and cooling system technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Battery's resizing case.

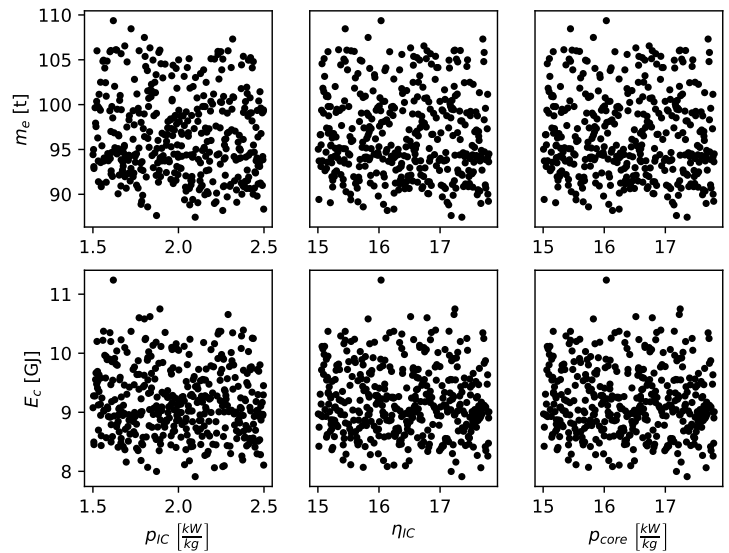


Figure D.8: Effects on OWE m_e and energy consumption E_c of inverter/converter and electric core technology parameters for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$. Battery's resizing case.

D.3 Tube-and-wing with distributed electric propulsion case

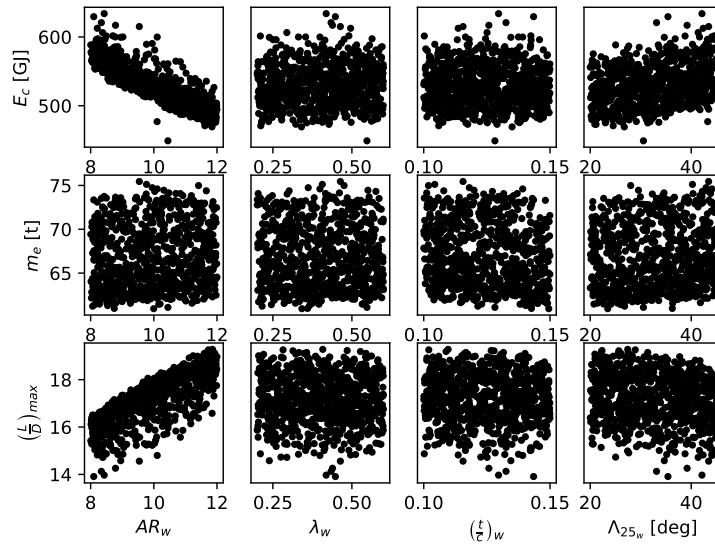


Figure D.9: Effect of wing parameters over energy consumption E_c , OWE m_e and maximum LoD for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$.

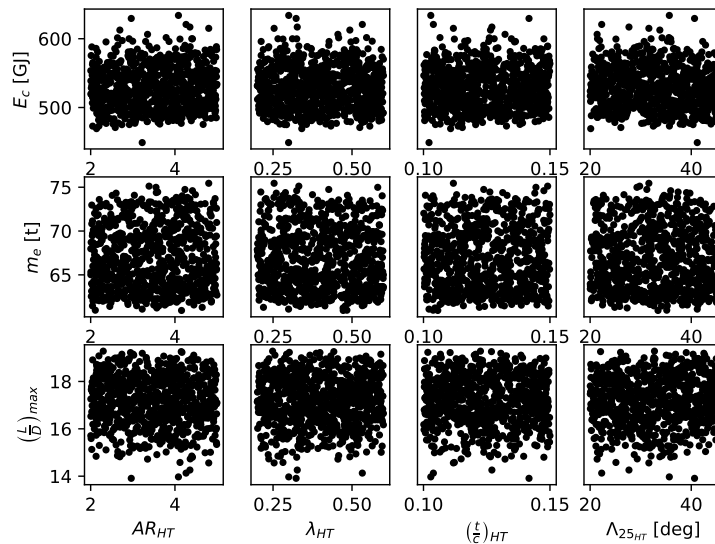


Figure D.10: Effect of HT parameters over energy consumption E_c , OWE m_e and maximum LoD for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$.

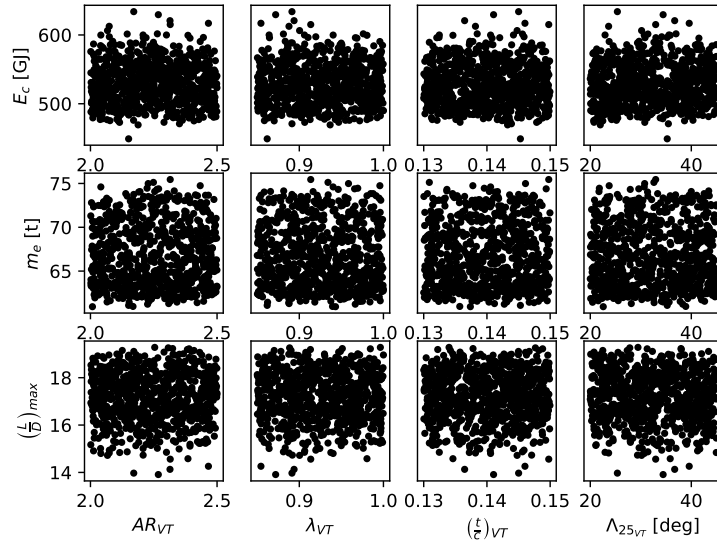


Figure D.11: Effect of VT parameters over energy consumption E_c , OWE m_e and maximum LoD for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$.

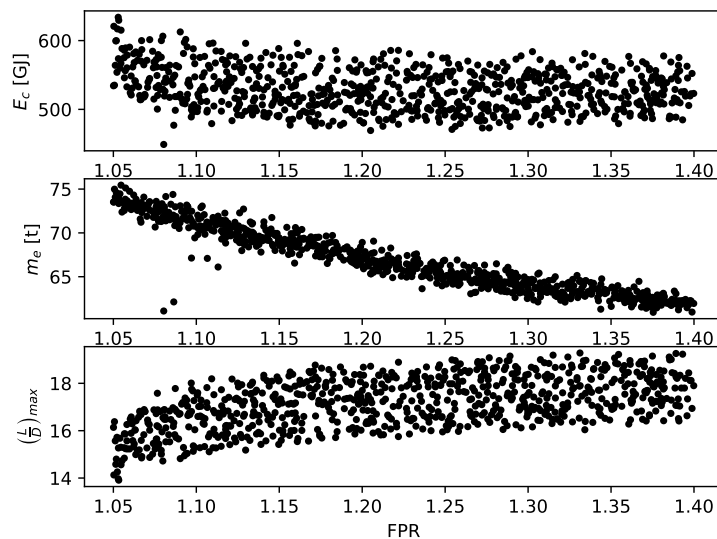


Figure D.12: Effect of FPR over energy consumption E_c , OWE m_e and maximum LoD for the hybrid aircraft case, $R = 900$ nmi, $N_{EM} = 32$.