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Metallurgy at the nanoscale: domain walls in nanoalloys

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In binary alloys, domain walls play a central role not only on the phase transitions but also on their physical properties and were at the heart of the 70's metallurgy research. Whereas it can be predicted, with simple physics arguments, that such domain walls cannot exist at the nanometer scale due to the typical lengths of the statistical fluctuations of the order parameter, here we show, with both experimental and numerical approaches how orientational domain walls are formed in CuAu nanoparticles binary model systems. We demonstrate that the formation of domains in larger NPs is driven by elastic strain relaxation which is not needed in smaller NPs where surface effects dominate. Finally, we show how the multivariants NPs tend to form an isotropic material through a continuous model of elasticity.

Fundamental understanding of phase transformation in metallurgy is crucial for many industrial applications. In this context of materials science, this refers to a broad spectrum of physical phenomena strongly influenced by the presence of imperfections that all crystals contain (point, line, surface or volume defects). In the specific case of A_xB_{1-x} bimetallic alloys research experienced an unprecedented boom in the 1960's, particularly with the study of first- and second-order phase transformations in relation to a singular type of defects present in solids, known as antiphase boundaries. These domain walls appear during the ordering process and are due to the presence of different sublattices which can be occupied either by A or B atom species during the nucleation stage, i.e. the translational symmetry is broken when going from one domain to another through this interface [1–3]. In first order phase transitions, by increasing temperature close to the transition one, the domain walls are progressively transformed into two order/disorder interfaces separate by the disordered phase, so-called wetting phenomena. These new interfaces are associated with two characteristic lengths. The first one is the length ℓ of the disorder layer and the second one is the correlation length (ξ) defining the characteristic distance of order parameter fluctuations and their ratio diverges at the transition temperature [4–6]. Except in the vicinity of the transition, these distances in bulk alloys remain very small (only a few interatomic spacings) compared to the size of domain walls explaining the stabilization of such ordered defects in materials. At the nanometer scale, statistical fluctuations of the order parameter can be of the same order of magnitude as the small size of the considered nano-objects meaning that for nanoparticles (NPs) withstanding chemically-ordered structures, domain walls should therefore not exist. However, in the specific case of bulk anisotropic phases ($L1_0$, DO_{22} , DO_{23} , \dots), the order-disorder phase transition is assisted by the formation of a multiple orientational domain wall

microstructures with well-defined orientational relationships. It has been demonstrated that this organization of the ordered domains relaxes the bulk elastic strain energy, since the multidomain morphology approximates an invariant plane strain [7]. Regarding NPs adopting similar anisotropic structure, the situation is not so obvious since the vicinity of free surfaces allows the fast relaxation of the elastic misfit, but it is not always the case. Indeed, it is known that non-crystalline structures such as icosahedral or multi-twinned NPs are stabilized by the presence of defects [8, 9]. This raises the question of whether order defects exist in finite-sized alloys such as bimetallic NPs. Interestingly, despite extensive studies in the 1980's on those types of defects, particularly driven by the advancement of electron microscopy (in case of Co-Pt [5], Cu-Au [10, 11], Cu-Pd [6], Fe-Al [12, 13], \dots), this fundamental metallurgy question has never been addressed at the nanoscale.

Given the importance of orientational domain walls in wide range of phenomena such as phase transition or growth mechanisms at the nanoscale as well as the physical properties of NPs, we investigate such defects by combining high-resolution transmission electron microscopy (HRTEM) experiments and atomic-scale simulations. We thus demonstrate the existence of orientation antiphase boundaries in case of large NPs (beyond 5 nm diameter) whose driving force is exactly the same as in bulk alloys, namely the minimization of elastic energy. Among all binary systems, CuAu is chosen as a model alloy since it is one of the most anisotropic material with a large tetragonalisation in the $L1_0$ ordered phase (low value of the c/a factor) and where three types of ordered rotational domains can coexist corresponding to different tetragonal axis in various directions. To determine if there is a size effect, NPs ranging from 2 to 8 nm were studied. This range was chosen based in the known deviations from bulk properties such as the melting temperature [14], the surface energy [15], or the order/disorder transition tem-

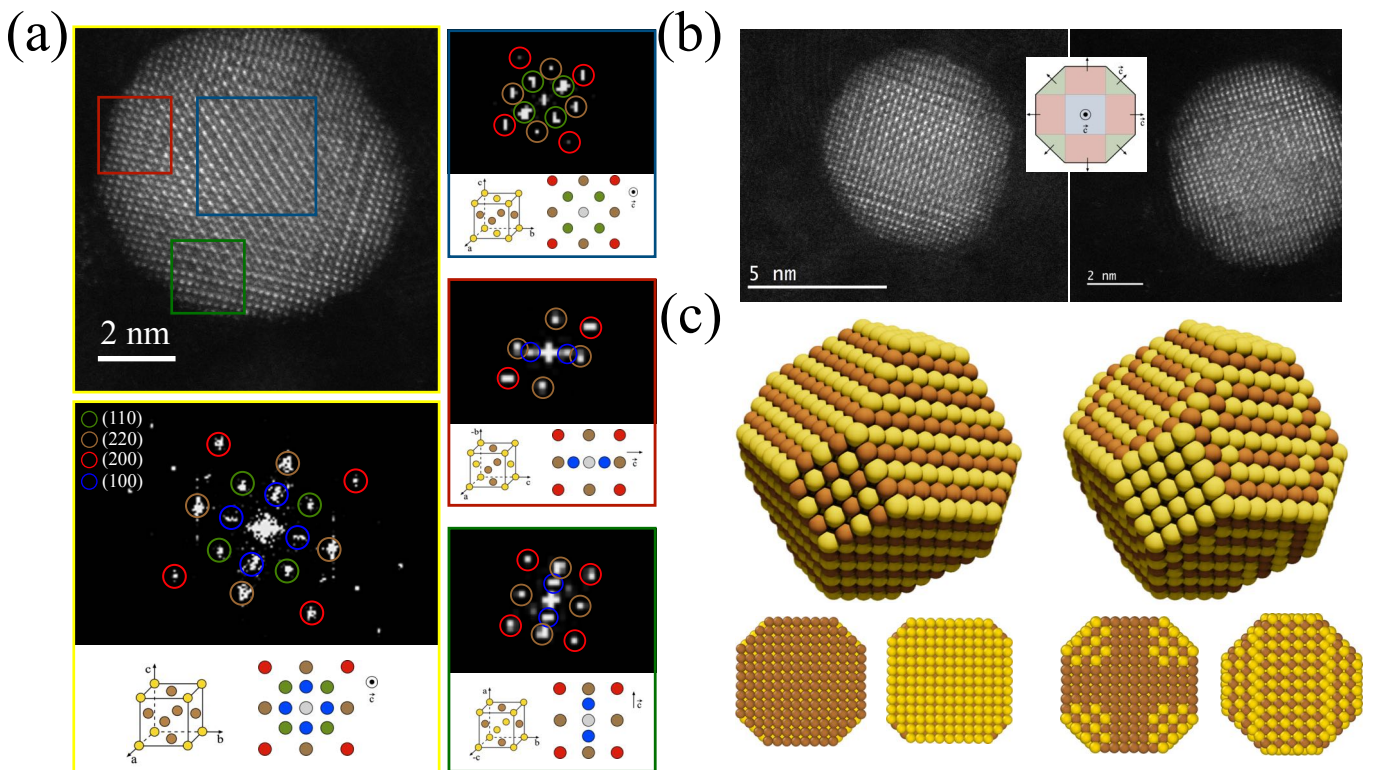


FIG. 1. (a) HR-STEM image of a $\text{Cu}_{50}\text{Au}_{50}$ NP (mean size of 8 nm) oriented along the $[001]$ axis (top) and its global diffraction pattern (bottom) corresponding to a L_{12} phase. The numerical diffraction pattern of the areas corresponding to the NP core (blue) and sides (red and green) are presented in the right panel. Note that in the diffraction scheme, the rectangles have been slightly oversized to illustrate the tetragonality. (b) Examples of $\text{Cu}_{50}\text{Au}_{50}$ NPs presenting multi-domain walls. (c) Schematic representations of the with mono-(left) and multi-variants (right) L_{10} NPs where some slice views are presented. Au atoms are in yellow and Cu atoms are in brown.

perature [16].

Fig. 1a shows a High Angle Annular Dark Field (HAADF) image of a $\text{Cu}_{50}\text{Au}_{50}$ NP oriented along the $[001]$ zone axis with a mean size of 8 nm acquired in scanning TEM (STEM) mode and its electron diffraction pattern obtained from numerical Fast Fourier Transform (FFT) analysis. Synthesis and TEM characterizations are given in Sec. I of the Supplementary Material. According to the extinction rules of the L_{10} phase, forbidden hkl reflections occur whenever h and k have different parity for a given l . Thus, the only possible superstructure reflection along this zone axis, is the 110 ones. However, 100 and 010 reflections (and equivalents) are observed on the FFT of the whole NP. This exhibits a characteristic $[001]$ zone axis diffraction of the L_{12} phase where all the superstructure reflections are present (Fig. 1a). This result is very surprising since the measured composition of the NP by Energy Dispersive X-ray Spectroscopy (EDX) gives a $\text{Cu}_{40}\text{Au}_{60}$ composition and not $\text{Cu}_{25}\text{Au}_{75}$ as expected in case of the L_{12} phase (see Sec. II of the Supplementary Material). To elucidate the physical origin of such observation, we conduct local structure analysis. The FFTs of the areas corresponding to the NP core and sides are shown in Fig. 1a. Due to the tetragonality of

the L_{10} phase, three orientational domains can appear, one with the c axis perpendicular to the substrate and two others with the c axis in the substrate plane and perpendicular to each other. The diffraction of the core of the NP shows 110 superstructures reflections characteristic of the L_{10} phase oriented along the $[001]$ axis (Fig. 1a). The sides of the NP exhibit diffraction pattern of the L_{10} structure viewed along the $[100]$ and $[010]$ directions with 001 superstructure reflections. These two domains have their c axis perpendicular to each other. This NP is then formed by ordered L_{10} orientational variants in coexistence, which is observed for the first time at the nanometer scale. This analysis explains the apparent conflicting results discussed beforehand. The L_{12} -like diffraction from the whole NP corresponds in fact to the superposition of the diffraction of the three orientational domains of the L_{10} phase that coexist within the NP (see Sec. III of the Supplementary Material). As shown in Fig. 1b, the presence of multivariants is characterized by clearly identifiable planes with alternating contrasts oriented according to the three possible variants. Consequently, the very in-depth HRTEM analysis revealed a unique structure, which remains stable during annealing, that differs significantly from the "classical" L_{10} struc-

ture, shown in Fig. 1c, where schematic representations of the NP are presented. Besides, the slice views highlight strong differences within the NP, where the multivariant structure differs from the alternating Cu and Au planes typical of the monovariant one.

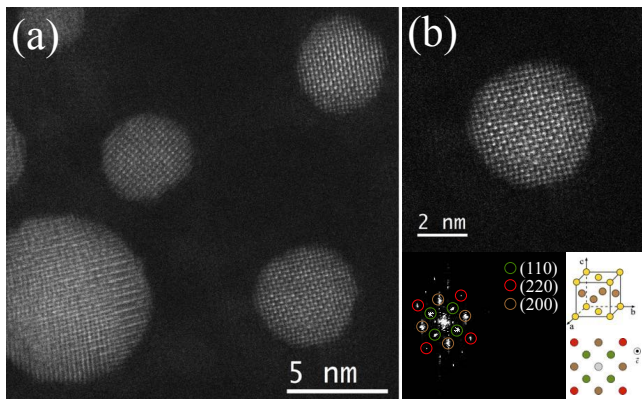


FIG. 2. (a) HR-STEM image revealing the presence of a large NP with wall domains and smaller NPs of the monodomain type. (b) HR-STEM image of a $\text{Cu}_{50}\text{Au}_{50}$ NP (mean size of 3 nm) oriented along the $[001]$ axis (top) and its FFT (bottom) corresponding to a L1_0 phase.

Strikingly, this coexistence is size dependent and only present in particles with mean diameter above about 4 nm. In contrast, smaller NPs appear as monodomain (Fig. 2). Furthermore, it is worth pointing out that this multidomain feature has never been observed in the case of NPs adopting an isotropic L1_2 phase. A typical example is presented in case of CuAu_3 composition where no contrast specific to multivariants is identified (see Sec. IV of the Supplementary Material). Accordingly, the size effects and the monovariant structure of the L1_2 phase highlighted experimentally strongly suggest that elasticity can be the driving force to stabilize multivariant domains.

In order to further understand the atomic mechanisms at the origin of the coexistence of multiple variants at the nanoscale, we perform Monte Carlo (MC) simulations in the canonical ensemble using a N -body potential derived from the second moment approximation (SMA) of the tight-binding (TB) scheme [17, 18]. Note that the simulations are performed at low enough temperatures to ensure that the NPs are in a L1_0 ordered state as in experiments. Further details regarding the TB-SMA potential and the MC calculations are given in Sec. V of the Supplementary Material. We considered truncated

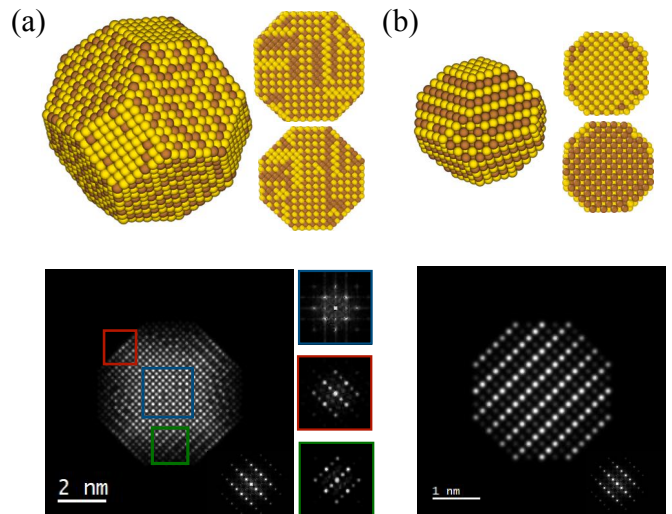


FIG. 3. Top: Equilibrium configurations of Cu-Au NPs after performing MC simulations and their local diffraction patterns. Global and cross-section views of a characteristic equilibrium configuration are presented for a NP containing (a) 6266 atoms where multivariant domains are identified and (b) 1289 atoms where monovariant domain is observed. Au atoms are in yellow and Cu atoms are in brown. Bottom: HRSTEM simulations images of the corresponding configurations imaged along the $[001]$ zone axis for the 6266 atoms NP and $[100]$ zone axis for the 1289 atoms NP. Diffraction patterns are given in inset.

octahedron $\text{Cu}_x\text{Au}_{1-x}$ NPs containing 1289 and 6266 atoms. This corresponds to NP sizes around 3 and 6 nm respectively, close to the size range explored experimentally. We first focus on the largest NP with a composition similar to that studied experimentally, i.e. $\text{Cu}_{40}\text{Au}_{60}$. After a complete MC relaxation of the system, the final structure is strongly perturbed, especially the monovariant configuration is no longer present (see Fig. 3a). However, it is difficult to identify whether multi-variant domains coexist within the NP. The cross-section views seem to display an organization close to a multi-variant structure, but do not allow one to be entirely conclusive. To take the structural analysis a step further, HRSTEM images are simulated and quantitatively analysed by FFT, as done experimentally. Fig. 3a (bottom) shows the simulated HAADF high resolution STEM image of the same NP using the Dr Probe Software provided by Barthel [42] (see technical details in Sec. VI of the Supplementary Materials). Structural features observed on this simulated nanoparticle are the same as the experimental ones. The whole NP exhibit a L1_2 -like diffraction pattern. At the center of the NP, there is one L1_0 variant oriented with the \mathbf{c} axis perpendicular to the plane of the figure while on the sides two variants with the \mathbf{c} axis in the fictitious substrate plane and perpendicular to each other are present. Furthermore, a smaller particle of 3

nm diameter is considered. In this particular case, the $L1_0$ -type structure remains stable after MC relaxation, again carried out after heating then cooling, above and below, the order-disorder phase transition (see Fig. 3b). The slice views clearly show the alternate Cu and Au planes along the c -axis typical of a $L1_0$ structure. Thus, the simulated image corresponding to the NP of 3 nm diameter is clearly the one of a monodomain $L1_0$ NP.

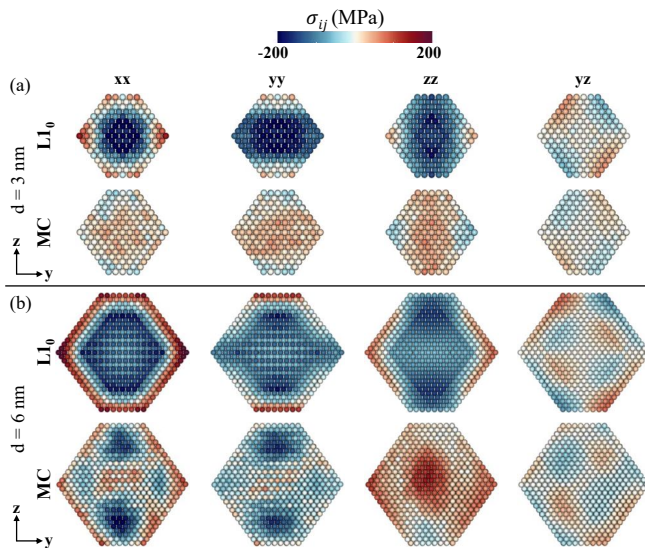


FIG. 4. Internal stress distribution in Cu-Au NPs of different sizes. σ_{xx} , σ_{yy} , σ_{zz} and σ_{yz} components are plotted for 3 nm diameter NPs in panel (a) and for 6 nm diameter NPs in panel (b) for $L1_0$ structure and after MC relaxation.

To capture the impact of elastic relaxation on the development of multivariant domains, we analyse the local stress (σ_{ij}) of each atom using the open source large-scale atomic/molecular massively parallel simulators (LAMMPS) package [20] by means of the stress maps. Only four stress components are discussed (σ_{xx} , σ_{yy} , σ_{zz} and σ_{yz}) since σ_{xy} and σ_{xz} are small. To evaluate size effect, the stress distributions have been calculated in case of small (3 nm) and large (6 nm) NPs and are displayed in Fig. 4 where negative and positive values correspond to compressive and tensile stress, respectively. The internal stress maps shows large stress values in the $L1_0$ structures due to the mismatch between Au and Cu layers. The analysis of the NPs after MC relaxation reveals that for both sizes a decrease of internal stress values due to the reorganisation of Au and Cu distribution inside the NPs as show in Fig. 4 (a) and (b). In particular, it is clear that the organization of ordered domains revealed in the largest NP stems from the redistribution of the internal stress and the relaxation of the elastic strain energy. Indeed, the maps corresponding to the diagonal terms are more homogeneously distributed within the NP compared

to the case of the monovariant one. Regarding, the non-diagonal terms, we can clearly see that the presence of multi-domains significantly reduces their contribution displaying values close to zero. To conclude, detailed analysis of the elastic distribution within the NP in form of stress map as well as histogram (see Sec. VII. of the Supplementary Materials) shows that the presence of the variants isotropises the stress contribution by adopting a homogeneous distribution coupled with specific components being null.

Interestingly, the formation of multivariant domains is not limited to the CuAu system. CoPt, that also shows a $L1_0$ order/disorder phase transition, exhibits the same behavior (see Sec. VIII of the Supplementary Materials). Since this mechanism is generalized, we here proposed a model based on elastic theory to explain the driving forces to stabilize the multidomain NPs. Hence, we first

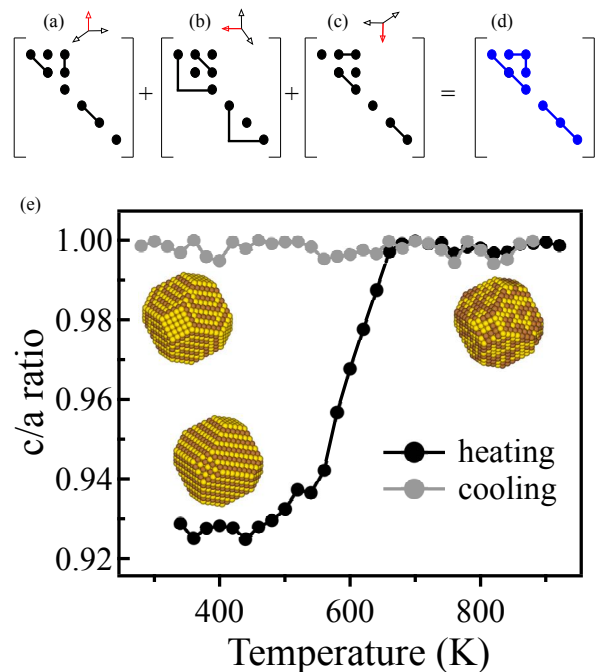


FIG. 5. The patterns of the elastic stiffness tensor for (a), (b) and (c) corresponding to the $L1_0$ structures with different orientations (the c axis is in red) and (d) the cubic system. Only the non-zero components are indicated and equal components are connected. (e) Evolution of the c/a ratio of the CuAu NP during MC simulations under heating and cooling.

consider the elastic stiffness tensor of the $L1_0$ structure in an orthonormal basis ($Oxyz$) where the 4-fold symmetry axis is chosen parallel to Oz (see Fig. 5a). Let us evaluate now this elasticity tensor in a new orthonormal basis obtained by a rotation by $\pi/2$ around Ox direction. This operation transforms the components x_1, x_2, x_3 of a vector into components $x'_1 = x_1, x'_2 = x_3, x'_3 = -x_2$. In this new axis coordinates, according to the rule of transformation of the tensor coefficients during a change of

orthonormal basis, the matrix representing the stiffness tensor in the Voigt's notation is modified as presented in Fig. 5b. Similarly, in a new basis obtained by $\pi/2$ around Oy direction, the elasticity tensor has the form shown in Fig. 5c. If we consider now a material formed by an equal volume fraction of the three $L1_0$ variants with their c axis perpendicular two by two, the mean elastic tensor of the material will take the form of a cubic material (see Fig. 5d), i.e. a more isotropic system. This is in agreement with numerical analysis showing that in case of multivariant domains, local stresses are zero or homogeneous. As a result, this macroscopic model based on the theory of elasticity (see details in Sec. IX. of the Supplemental materials), reveals that this mechanism can be generalized to any bimetallic systems with a low temperature $L1_0$ structure.

System	c/a ratio	A_U
CuAu	0.926	2.88
FePd	0.966	0.77
FePt	0.968	0.75
CoPt	0.973	0.57

TABLE I. **Descriptors of the anisotropy of the $L1_0$ tetragonal structure.** Values of the c/a ratios and the generalized Zener coefficient A_u and for the $L1_0$ -type materials: CuAu, FePd, FePt and CoPt [36, 37].

Regarding the literature, the formation of multivariants NPs was already observed in other $L1_0$ type systems like FePt [21–24], FePd [23, 25] and CoPt [26, 27]. However, the physical origin of the existence of such multivariants NP is not explained, or even not commented [24]. By comparing our results with the configurations shown in all these works, it appears that depending on the c/a ratio values of the $L1_0$ phase (Table I), and in agreement with the macroscopic demonstration given above, the extension of variants is more or less important. Indeed, for the CuAu system, the influence of the multivariants arrangement is clearly seen on the evolution of the mean c/a ratio calculated over the NP (Fig. 5e). Starting from a monovariant NP and upon heating, the c/a varies from 0.93 to 1 and allow to define the critical order/disorder transition temperature for a NP of 6 nm diameter. Upon cooling, the three variants nucleate and the mean c/a ratio in the whole NP is closed to 1, i.e. equivalent to a cubic structure. This result validates the simple demonstration given above using the equivalent stiffness tensor of a multivariants NP, together with the lowering of the total elastic energy obtained from the atomistic simulation when transiting from monovariant to multivariants NP. As a result, the degree of anisotropy of the $L1_0$ structure with respect to a cubic structure can be described by the c/a ratio of the tetragonal phase. Among the four systems, CuAu with a c/a of 0.926 is the most

anisotropic system and the volume extension of the variants is the most important in order to minimize the elastic energy and to tend to the one of an equivalent cubic system. Another more direct way to characterize the anisotropy of a material is looking at the stiffness components. Thus, Ranganathan *et al.* introduced a universal anisotropy index, A_U , which takes into account all the stiffness components of the elastic stiffness tensor instead of the ratio of individual stiffness coefficients to define anisotropy [28]. For the four alloys discussed here, the values of A_U , given in Table I, reflects perfectly the behavior of the c/a ratio justifying its use as a good descriptor of the anisotropy of the $L1_0$ tetragonal structure.

Bimetallic nanoparticles are fascinating materials whose unique properties are closely linked to their chemical order, i.e. core-shell, random, phase separation, Janus, ... [29, 30] Here, we have observed, demonstrated and explained the existence of a new mixing pattern corresponding to the presence of rotational antiphase boundaries persisting beyond a certain size (> 5 nm). Surprisingly, these ordered defects have never been discussed in the literature although HRTEM images have shown their presence. In addition to making an important contribution to the understanding of self-organization within a bimetallic NP, it is clear that such chemical ordering will have fairly unique impact on various properties that will need to be studied or even taken into consideration to revisit and reinterpret previous data. Typical example is the magnetocrystalline anisotropy characteristic of equiatomic binary alloys known to be due to an $L1_0$ order that alternates pure planes along one direction. Yet studies have often discussed the effect of size or the influence of annealing on the magnetic properties of $L1_0$ -type NPs [31–35], and the relationship with the presence or not of domain walls deserves to be considered. Furthermore, the present contribution on the metallurgy at the nanoscale has also raised the question of whether order defects such as domain walls exist in finite-sized bimetallic alloys. Despite extensive studies in the 1980s on those kind of defects, this fundamental question has never been addressed in NPs. This work then constitutes a major step forward in the NPs community, emphasizing once again that these nano-objects are a truly exceptional playground for tackling and highlighting unexpected physical singularities.

SUPPLEMENTAL MATERIAL : METALLURGY AT THE NANOSCALE: DOMAIN WALLS IN NANOALLOYS

Sec. I. Experimental details: synthesis and TEM analysis

Cu₅₀Au₅₀ and Co₅₀Pt₅₀ NPs were prepared by alter-

nated pulsed laser deposition (PLD) technique using a KrF excimer laser source in a high vacuum chamber under a pressure of 10^{-8} Torr [38]. The NPs were grown by epitaxy on a NaCl substrate and deposited on a TEM carbon grid by the carbon replica technique [39, 40]. The nominal thickness is 0.8 nm, the growth temperature is fixed at a temperature below the order/disorder phase transition in order to obtain NPs in the ordered phase ($L1_0$ phase), and the laser frequency is 5 Hz. The NPs were imaged by using a double aberration corrected electron microscope (JEOL ARM 200F cold FEG) in STEM mode using the High Angle Annular Dark Field (HAADF) technique. Chemical analysis of the NPs composition was performed by Energy Dispersive X-ray Spectroscopy (EDX) at the single particle level.

Sec. II. EDX spectra of CuAu NPs

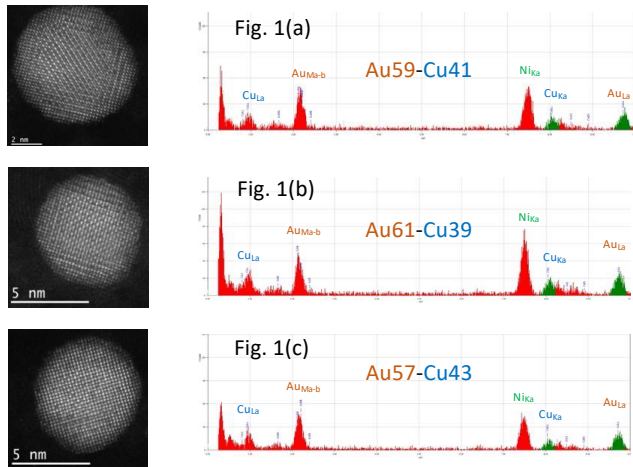


FIG. 6. EDX spectra acquired on the different NPs presented in the Figure 1 of the manuscript.

In Figure 6 are presented the EDX spectra measured on the NPs presented in Figure 1 of the manuscript. In all cases, the composition of the NPs by EDX gives a 60/40 composition in Cu and Au respectively.

Sec. III. Diffraction patterns of $L1_2$ and the $L1_0$ phases along different directions

The analysis presented in Figure 7 allows us to solve the enigma raised by the global diffraction of the particle shown in Figure 1 of the main manuscript. By superimposing the three diffraction patterns obtained for each $L1_0$ variant (which is equivalent to a global diffraction of the NP), we end up with reflections in all directions, making this diffraction identical to that of a $L1_2$ structure oriented according to $[100]$.

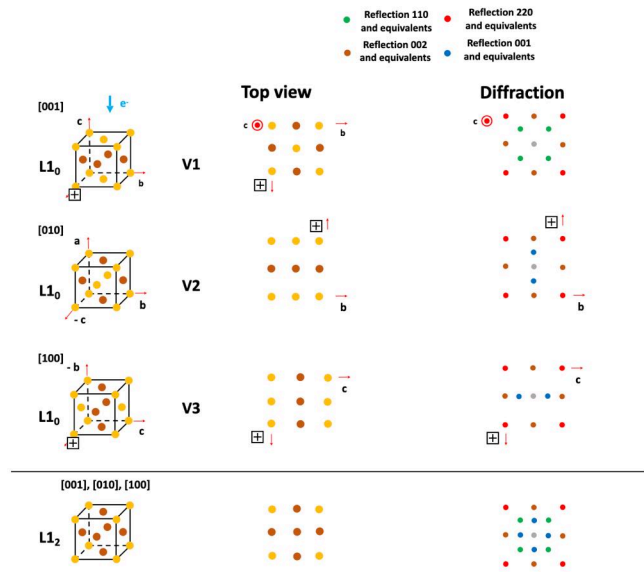


FIG. 7. Drawings showing the different configurations for the $L1_0$ phase according to $[001]$, $[010]$ and $[100]$ directions. A top view and the associated diffractions are also shown. Higher-order structural reflections are not shown.

Sec. IV. Structural and chemical analysis of $CuAu_3$ NP in a $L1_2$ ordered phase

In Figure 8 is presented the analysis of typical example of a Au_3Cu NP.

Sec. V. MC simulations based on a TB interatomic potential

The interatomic potential is included in a MC code in the canonical and semi-grand canonical ensembles to relax the structures at finite temperatures. The complete SMA model and parameter fitting procedure for pure metals and mixed interactions are detailed in Ref. [40] for Cu-Au and in Ref. [41] for Co-Pt.

MC simulations are based on the Metropolis algorithm carried out in the isothermal-isobaric ensemble (number of atoms of each species, temperature and pressure are conserved - zero pressure for NM in vacuum !) also called canonical ensemble. Two types of MC trials are applied: random atomic displacements and random atomic exchange between two atoms of different species at different sites. Each MC trial is accepted with the probability equal to 1 if the total energy of the system is lower after the trial, if not, the trial is accepted with a probability equal to $\exp(-\frac{\Delta E}{k_B T})$ where ΔE is the energy difference of the system after the trial, k_B the Boltzmann constant and T the temperature. For a NP of N atoms we typically run 2000 macrosteps after 800 of equilibration then the last 1200 macrosteps are used to calculate the ensemble averages. For each macrostep we apply N chemical exchanges for $20 \times N$ atomic displace-

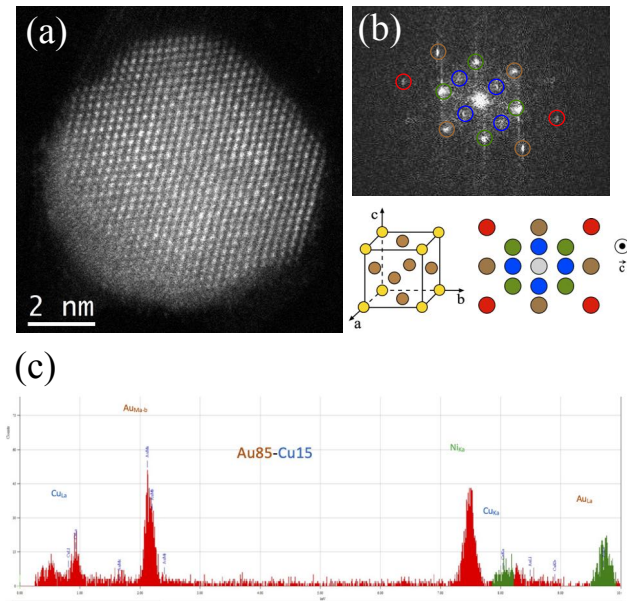


FIG. 8. (a) HR-STEM image of a CuAu_3 NP (mean size of 6 nm) oriented along the $[001]$ axis, (b) its global diffraction pattern corresponding to a $L1_2$ phase and (c) EDX spectra revealing the exact composition, $\text{Cu}_{15}\text{Au}_{85}$.

ments, randomly chosen respectively at each macrostep, which leads to about 30 millions to 120 millions of microsteps, depending on the size of the system (1289 or 6266 atoms). Heating and cooling starting from $L1_0$ ordered or disordered NP with a increment of temperature of 20 K, starting with the configuration obtained at the precedent temperature. Up to five different runs are performed in order to improve the statistic. This procedure ensures to get well converged equilibrium structures at low temperatures below the order/disorder temperature to be compared with experiment.

The analysed structures were obtained after a complete relaxation procedure by increasing the temperature above the critical order/disorder temperature up to a complete chemical disordering of the NP, and slowly decreasing the temperature down to $T = 150$ K.

Sec. VI. Parameter for the HRSTEM images

Simulated HRSTEM images of the nanoparticles were generated using the Dr. Probe software [42] based on the multislice algorithm. In order to have the simulated image as close as possible to the experimental ones, we need to set the parameters according to the characteristics of the microscope. In Table II are presented the mean values of the aberration coefficients corresponding to the objective lens of the JEOL JEM-ARM200F spherical-aberration- corrected electron microscope equipped with a cold field emission gun operated at 200 kV used for the

acquisition of the experimental images. The semi-angle of convergence and annular detector radii were given by JEOL. The electron probe radius was taken to be equal to the STEM resolution of the microscope with aberration correctors. The values of the aberration were taken from the measurement done by the STEM aberration corrector software.

Simulations Parameters	Value
Microscope energy	200 kV
Semi-angle of convergence	30 mrad
Electron probe radius	0.4 Å
Annular detector inner radius	68 mrad
Annular detector outer radius	280 mrad
Defocus (C1)	-1.2 nm
Spherical aberration (C3)	-1.95 μm

TABLE II. The parameters correspond to a JEOL ARM 200F cold FEG using a double aberration corrected electron microscope.

Sec. VII. Calculations of the local stress

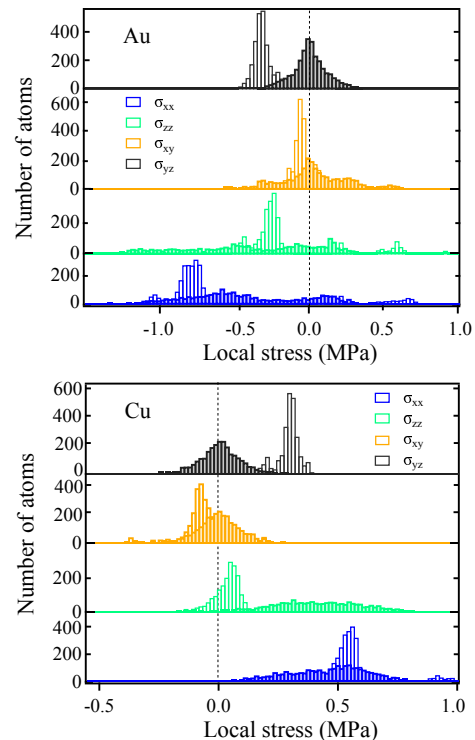


FIG. 9. Stress tensor in a histogram form (Cu and Au atoms) corresponding to the mono (empty) and multi-domain (filled) structures for the large NP.

Figure 9 depicts the four components of the stress tensor in a histogram form (Cu and Au atoms) corresponding to the mono and multi-domain structures for the 6 nm diameter NP. From this analysis, a number of conclusions can be drawn. First, Au and Cu atoms be-

have differently, inducing mainly compressive and tensile stresses, respectively. This is simply due to the difference in atomic radius, which is around 13% greater for Au. For both elements, the monovariant structure exhibits fairly sharp distributions for all components, typical of a structure under stress, with especially very high stress values of σ_{xx} around -0.80 MPa and 0.55 MPa for Au and Cu, respectively. For the multivariant structure, the analyzed landscape changes drastically. Hence, the distributions for the diagonal terms are no longer sharply defined but homogeneously distributed over a wide stress range of about 1 MPa. For the non-diagonal terms, we can clearly see that the presence of multi-domains significantly reduces their contribution with a distribution center of gravity close to zero. This is particularly well illustrated in the case of σ_{yz} which drops from 0.30 MPa (absolute value) to almost zero for both Cu and Au.

Sec. VIII. Multivariants in CoPt NPs

In Figure 10a. $\text{Co}_{50}\text{Pt}_{50}$ NPs microstructure exhibits the same feature as in CuAu with the coexistence of two orientational domains. The only difference with CuAu is the lateral expansion of the variant with *c* axis parallel to the substrate plane which is smaller. This is also confirmed by MC simulations coupled to HRSTEM images calculations. As seen in Figure 10b, the overall appearance of the NP does not reveal the multivariant structure, nor do cross-sectional views. Here again, the HRSTEM calculation is crucial, enabling the unambiguous demonstration of the coexistence of different orientational domains.

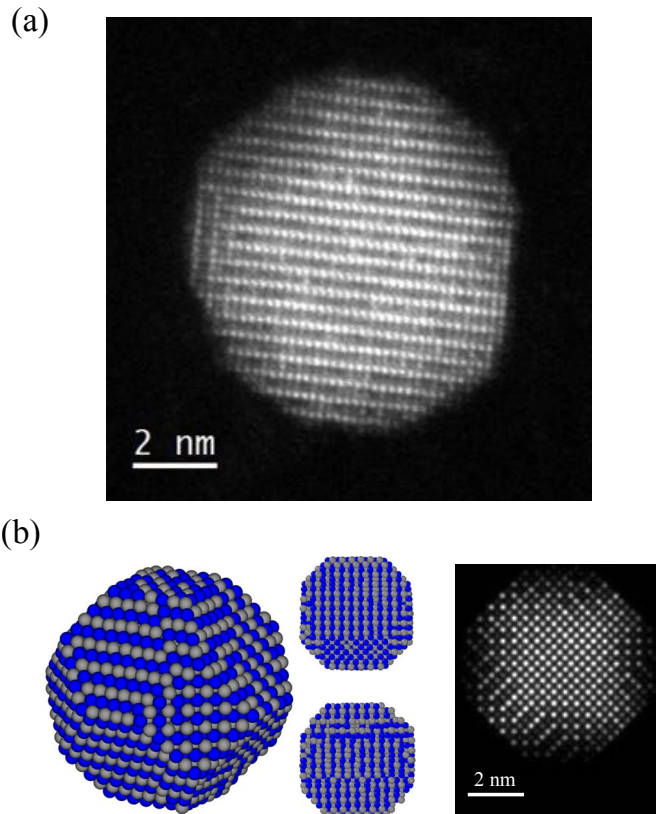


FIG. 10. (a) HRSTEM image of a CoPt NP exhibiting multivariant domains. (b) Equilibrium configurations of CoPt NPs after performing MC simulations and its calculated HRSTEM image. Global and cross-section views of a characteristic equilibrium configuration are presented for a NP containing around 3500 atoms. Co atoms are in blue and Pt atoms are in grey.

Sec. IX. Elasticity theory at the macroscopic scale

By comparison to the stiffness tensor of the cubic system which needs only three elastic components ($C_{11} = C_{22} = C_{33}$, $C_{12} = C_{13} = C_{23}$ and $C_{44} = C_{55} = C_{66}$) to describe its mechanical properties, the one of the tetragonal $L1_0$ structure has 3 more $C_{\alpha\beta}$ components, namely C_{33} , C_{13} and C_{66} in an orthonormal basis ($Oxyz$) where the 4-fold symmetry axis is chosen parallel to Oz leading to the following matrix where lines connecting some dots indicating that the corresponding coefficients are equal:

$$\begin{bmatrix} \bullet & & & & & \\ & \bullet & & & & \\ & & \bullet & & & \\ & & & \bullet & & \\ & & & & \bullet & \\ & & & & & \bullet \end{bmatrix}$$

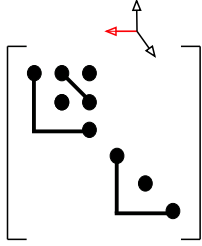
Let us evaluate now this elasticity tensor in a new orthonormal basis obtained by a rotation by $\pi/2$ around Ox direction. This operation, performed on the axis system transforms the components x_1, x_2, x_3 of a vector into components x'_1, x'_2, x'_3 such that:

$$\begin{cases} x'_1 = x_1 \\ x'_2 = x_3 \\ x'_3 = -x_2 \end{cases} \quad (1)$$

In this new axis coordinates, according to the rule of transformation of the tensor coefficients during a change of orthonormal basis, the new components of the stiffness tensor are written as:

$$\begin{cases} C'_{11} = C_{11} & C'_{22} = C_{33} & C'_{33} = C_{22} = C_{11} \\ C'_{12} = C_{13} = C_{23} & C'_{13} = C_{12} & C'_{23} = C_{23} \\ C'_{44} = C_{44} = C_{55} & C'_{55} = C_{66} & C'_{66} = C_{55} \end{cases} \quad (2)$$

In such a case, the elasticity tensor in this basis has a new form:



Similarly, in a new basis obtained by $\pi/2$ around Oy direction, the new components are written as:

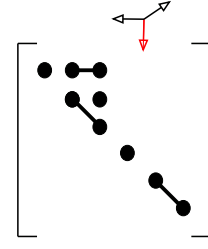
$$\begin{cases} x'_1 = -x_3 \\ x'_2 = x_2 \\ x'_3 = -x_1 \end{cases} \quad (3)$$

leading to the new components :

$$\begin{cases} C'_{11} = C_{33} & C'_{22} = C_{22} = C_{11} & C'_{33} = C_{11} \\ C'_{12} = C_{23} = C_{13} & C'_{13} = C_{13} & C'_{23} = C_{12} \\ C'_{44} = C_{66} & C'_{55} = C_{55} & C'_{66} = C_{44} = C_{55} \end{cases} \quad (4)$$

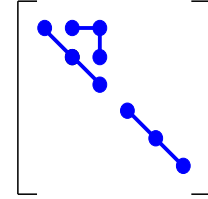
As a result, we finally obtain the following matrix :

If we consider now a material formed by an equal volume fraction of the three $L1_0$ variants with their \mathbf{z} axis perpendicular two by two, the mean elastic tensor of the material will take the form:



$$\begin{cases} C_{11}^* = C_{11} + C_{11} + C_{33} = 2C_{11} + C_{33} \\ C_{22}^* = C_{11} + C_{33} + C_{11} = 2C_{11} + C_{33} \\ C_{33}^* = C_{33} + C_{11} + C_{11} = 2C_{11} + C_{33} \\ \dots \end{cases} \quad (5)$$

This results in the corresponding matrix form:



which is exactly the form of the elasticity tensor for a cubic system.

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