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Original Research

A Multi-modal Computational Fluid Dynamics Model of Left Atrial Fibrillation Haemodynamics Validated with 4D flow MRI

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Abstract

Atrial fibrillation (AF) is characterized by rapid and irregular contraction of the left atrium (LA). Impacting LA haemodynamics, this increases the risk of thrombi development and stroke. Flow conditions preceding stroke in these patients are not well defined, partly due the limited resolution of 4D flow magnetic resonance imaging (MRI). In this study, we combine a high-resolution computed tomography (CT) LA reconstruction with motion and pulmonary inflows from 4D flow MRI to create a novel multimodal computational fluid dynamics (CFD) model, applying it to five AF patients imaged in sinus rhythm (24 ± 39 days between acquisitions). The dynamic model was compared with a rigid wall equivalent and the main flow structures were validated with 4D flow MRI. Point-by-point absolute differences between the velocity fields showed moderate differences given the sensitivity to registration. The rigid wall model significantly underestimated LA time-averaged wall shear stress (TAWSS) ($p=0.02$) and oscillatory shear index (OSI) ($p=0.02$) compared to the morphing model. Similarly, in the left atrial appendage (LAA), TAWSS ($p=0.003$) and OSI ($p<0.001$) were further underestimated. The morphing model yielded a more accurate mitral valve waveform and showed low TAWSS and high OSI in the LAA, both associated with thrombus formation. We also observed a positive correlation between indexed LA volume and endothelial cell activation potential (ECAP) ($R^2=0.83$), as well as LAA volume and LAA OSI ($R^2=0.70$). This work demonstrates the importance of LA motion in modelling LAA flow. Assessed in larger cohorts, LAA haemodynamic analysis may be beneficial to refine stroke risk assessment for AF.

46

Keywords: Atrial fibrillation, computational fluid dynamics, hemodynamics, multi-modal, fluid mechanics.

49 **Background**

50 Atrial fibrillation (AF) is a cardiac arrhythmia characterized by abnormal contraction of the
51 atrium. It is caused by the disturbed propagation of electrical signals across the atrial
52 myocardium.¹ Incidence of AF has been rising steadily with the worldwide prevalence
53 increasing by 33% since 2000.¹ AF patients are at a 3-5 fold increased risk of stroke^{2,3} as well
54 as elevated risk of heart failure and all-cause mortality.⁴ Over 90% of the thrombi responsible
55 for stroke in AF originate in the left atrial appendage (LAA) where haemodynamic conditions
56 are often pro-thrombotic.⁵ Low wall shear stress (WSS) and high oscillatory shear index (OSI)
57 resulting from stagnant, disordered and time-varying flow, are considered pro-thrombotic as
58 they interfere with normal endothelial function.⁶⁻⁸ Originally developed in the setting of
59 abdominal aortic aneurysms⁹, endothelial cell activation potential (ECAP), which combines
60 these two characteristics into a single metric (OSI/time-averaged WSS), has recently been used
61 to further characterize disturbed flow in the LAA.^{6,6,10} Treatment options for AF include
62 catheter ablation whereby the atrial wall is selectively scarred to interrupt stray electrical
63 signals and restore sinus rhythm. Anticoagulants are also usually prescribed to AF patients with
64 risk factors to mitigate stroke risk.¹¹

65

66 Magnetic resonance imaging (MRI) is well suited for tissue characterisation in the
67 diagnosis and monitoring of heart disease.¹² Further developments allowing the volumetric
68 encoding of intra-cardiac blood flow velocity in 3D and throughout the cardiac cycle (4D flow)
69 have made MRI a powerful tool in the assessment of cardiac flow.¹³⁻¹⁶ Although its use in
70 routine clinical practice is not widespread, 4D flow MRI has furthered our understanding of
71 the interplay between left atrial (LA) flow and AF.¹⁷⁻¹⁹ Whilst 4D flow MRI offers direct
72 measurement of blood flow velocities, the relatively low spatial resolution presents challenges.
73 WSS estimation requires accurate assessment of the near-wall velocity gradient. With 4D flow,

74 WSS must be approximated by interpolation between the wall and the noisy near-wall
75 velocities introducing significant error.^{20,21} Conversely, computational fluid dynamics (CFD)
76 meshes can provide highly-resolved WSS fields. Such models have been widely used in
77 vascular disease to predict disease progression.²²⁻²⁵ Increasingly, CFD methods are being
78 employed to characterize LA flows in AF.²⁶⁻²⁹ These studies have typically assumed the LA
79 wall to be rigid. Whilst some studies have applied multiphase computed tomography (CT) to
80 dynamically deform the LA in CFD simulations,³⁰⁻³² no CFD study has yet extracted LA
81 motion and pulmonary veins (PV) inflows from the same MRI acquisition.

82 The aim of this study was to develop a multi-modal, dynamic CFD model to produce
83 patient-specific LA haemodynamic data in higher temporal and spatial resolution than current
84 imaging methods offer. This model was then applied to a small cohort of AF patients to assess
85 existing theories and generate new hypotheses as to the genesis of stroke in these patients.

86

87 **Methods**

88 This study was based on retrospective analysis of five patients (Table 1) from the CTStrain-
89 AF Study (NCT04281329), an observational study administered by Assistance Publique -
90 Hôpitaux de Paris and approved by institutional review board. All participants were scheduled
91 for their first radiofrequency ablation in the next 6 months, were ≥ 18 years of age and gave
92 written informed consent for participation in the study. All patients analysed in the present
93 study were imaged at Centre Hospitalier Universitaire Pitié-Salpêtrière in Paris. In addition to
94 a routine cardiac CT scan, these patients received MRI with 4D flow, encompassing the whole
95 heart, prior to catheter ablation. These two datasets were used to create a multimodal model of
96 the LA (Figure 1). The patients were imaged whilst in sinus rhythm and the mean delay
97 between CT and 4D flow MRI acquisitions was 24 ± 39 days

98

99 **Table 1.** Patient characteristics.

Case	Sex	Age (yrs)	Weight (kg)	Height (cm)	BSA (m ²)	HR (BPM)	CO (L/min)	LAEF (%)	LA indexed volume (mL/m ²)	LAA volume (mL)
1	F	64	69	165	1.76	50	3.4	24.4	63.1	6.7
2	M	76	74	170	1.85	68	3.6	20.2	82.8	6.7
3	F	71	59	158	1.60	48	2.7	22.6	41.6	3.9
4	M	61	84	180	2.04	67	5.1	29.1	45.6	4.6
5	M	71	80	178	1.98	56	3.8	39.3	50.8	5.3

100 Note: BSA = body surface area, HR = heartrate, BPM = beats per minute, CO = cardiac output, LAEF = left atrial
 101 ejection fraction, LA = left atrium, LAA = left atrial appendage, F = female, M = male.

102

103 *3D geometric model reconstruction from CT data*

104 The 3D geometric models of the LA were based on the CT data given its high spatial resolution.
 105 Such data were acquired on a Siemens SOMATOM Force dual-detector CT scanner with a
 106 pixel spacing of 0.35-0.47 mm and slice thickness of 0.6 mm. Acquisitions were made either
 107 at peak systole (cases 1-4) or diastole (case 5). Reconstruction was then achieved via manual
 108 thresholding within 3D Slicer (Version 5.2.1). The stereolithography (.STL) file was then
 109 exported to Star CCM+ (Version 2022.1, Siemens, Munich) where local smoothing was used
 110 to remove any imaging or segmentation artefacts.

111

112 *4D flow MRI acquisitions*

113 MRI images were acquired on a 1.5T scanner (MAGNETOM Sola, Siemens Healthineers,
 114 Erlangen, Germany). Phase-contrast MRI with 3D velocity-encoding throughout the cardiac
 115 cycle was obtained for all patients using a 4D flow MRI research sequence.³³ Images were
 116 acquired during free-breathing with respiratory navigator and retrospective electrocardiogram
 117 (ECG) gating in a sagittal oblique volume encompassing the left heart, using the following scan
 118 parameters: echo time (TE) = 2-2.25 ms, repetition time (TR) = 4.33 ms, average temporal

119 resolution = 26.0 ms, views per segment = 2, flip angle = 7° , reconstructed pixel spacing = 2.4
120 x 2.4 mm², slice thickness = 3 mm, reconstructed 25-phase volumes, accelerated using
121 compressed sensing with an acceleration factor of R=7.7. Optimal single encoding velocity
122 (VENC) in all spatial directions is set according to scout in-plane velocity-encoded images
123 acquired in a 3-chamber view just before 4D flow scans. As such, VENC was 150 cm/s for
124 Cases 1-4. For Case 5 VENC was 300 cm/s due to the presence of aortic valve stenosis resulting
125 in high velocities and thus aliasing in the aortic root as revealed by scout images acquired at
126 VENC = 150 and then 200 cm/s.

127

128 *LA dynamic wall motion from MRI*

129 The SegmentRegistration module³⁴ available within 3D Slicer, which extends the previous
130 Elastix tool to temporal sequences,^{35,36} was used to generate a series of transforms describing
131 transient LA motion from 4D flow MRI magnitude images (Figure S1). The corresponding CT
132 reconstruction was then manually registered to the MRI (and transform sequence) coordinate
133 system. To implement these transforms in Star-CCM+, a grid of 125 control points was
134 generated in 3D Slicer across the spatial range of the LA and a time-position table for each of
135 these points was exported. Within Star-CCM+ these control points were implemented with B-
136 spline interpolation to morph the computational mesh. All cases were also simulated with rigid
137 walls, based on the original CT reconstruction, to assess the sensitivity of the haemodynamic
138 results to rigid vs. moving wall assumption.

139

140 *Extraction of PV inflow, mitral outflow and model validation from MRI*

141 PV inflows and mitral valve outflow were quantified in Medis Suite MR (version 4.0, Medis
142 Medical Imaging, Leiden) by re-slicing the 3D image stack into 2D planes perpendicular to
143 each PV and to the mitral valve, respectively, extracting the contour of interest and calculating

144 the time-resolved flow rate profile. PV flow rate profiles were then imported into Star-CCM+
145 where a spline interpolation was used to specify time dependant boundary flows. In parallel,
146 the raw 4D flow velocity images were post-processed in MATLAB into a series of velocity-
147 position tables for each phase of the cardiac cycle. Such tables were imported into Star-CCM+
148 to compare with the CFD velocity field and validate the major flow structures in the LA
149 throughout the cardiac cycle.

150

151 *CFD model*

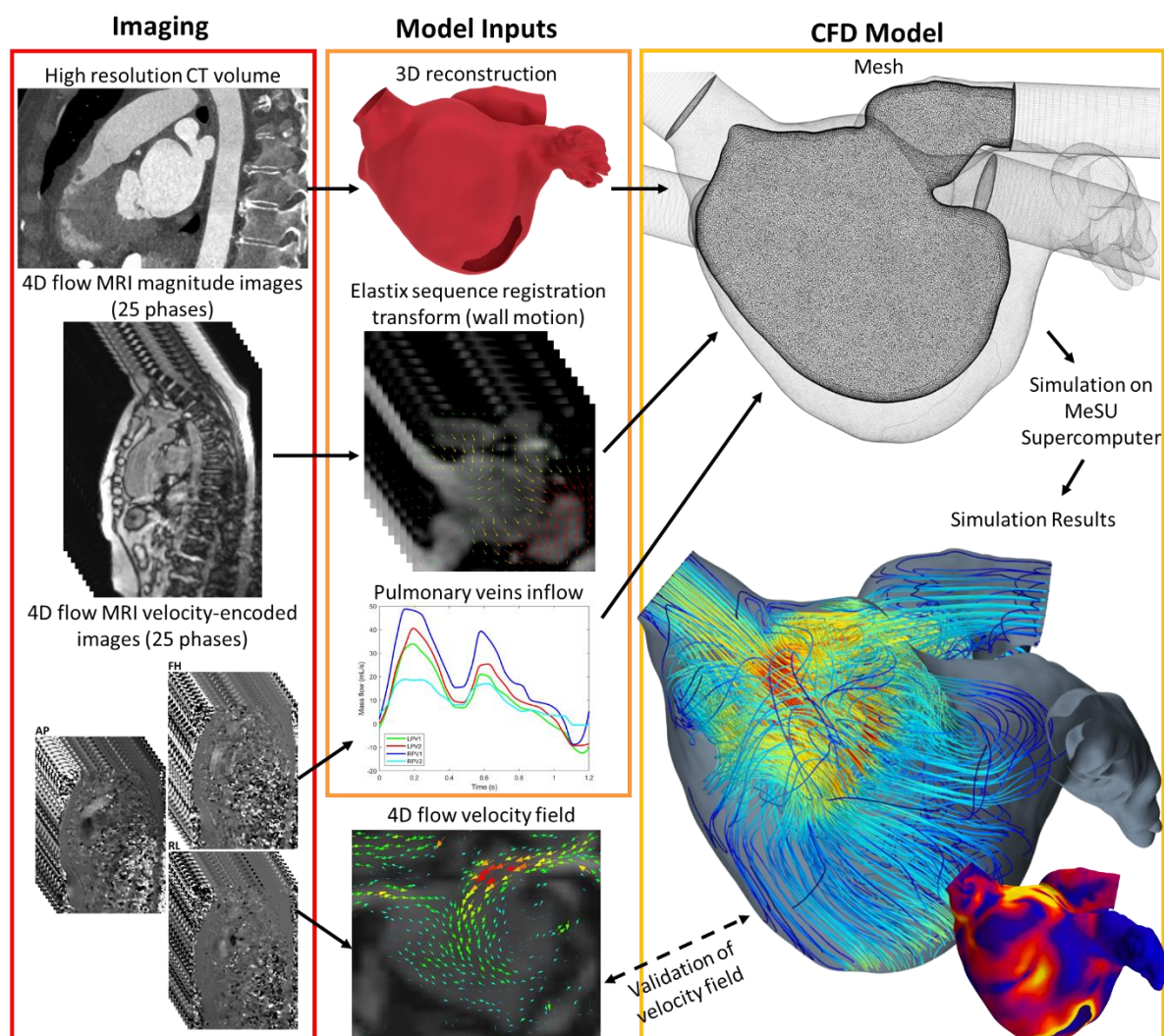
152 Second-order transient simulations were run with Star-CCM+'s laminar flow model and a
153 constant timestep of 0.001 s for a total of 5 cardiac cycles. The computational meshes were
154 based on the CT reconstructions and were constructed with a polyhedral core mesh and 12
155 prismatic boundary layers. Fifteen-cm extrusions were made to the inlets to create a fully-
156 developed flow profile. The mitral valve for all cases was modelled as fully open with zero
157 pressure. The outlet waveform was therefore a result of the total pulmonary inflow and the
158 change in LA volume. To assess mesh convergence, three meshes of varying densities (0.74M,
159 1.45M and 2.76M cells) were compared for Case 1. Once an appropriate degree of mesh
160 refinement was established (2.76M cells, mean mesh size = 0.4 mm, the same meshing
161 parameters were applied to all cases. Time-averaged velocity was assessed on two-line probes
162 of 50 points each spanning the LA/LAA horizontally and vertically (Figure S2) and throughout
163 the entire LA (Figure S3/S4). Time-averaged WSS (TAWSS) was assessed as a surface average
164 across the entire LA surface (Figures S5/6). TAWSS, OSI and ECAP were extracted from the
165 final cardiac cycle using a 100-sample sliding window. Blood density was 1050 kg/m^3 and a
166 non-Newtonian, Carreau-Yasuda blood viscosity model (haematocrit=45%) was used.³⁷ The
167 simulations were run on the MeSU supercomputer (Sorbonne Université) on 96 cores with a
168 mean simulation time of 7 hours and 10 mins. In our analysis of the haemodynamic data we

169 refer to indexed LA volumes which were calculated by dividing late systole (maximum) LA
170 volume by body surface area (BSA). BSA was calculated according to the Du Bois formula.³⁸

171

172 *Statistical Analysis*

173 Continuous variables were provided as mean (standard deviation, SD). To compare
174 haemodynamic differences between the LA and LAA as well as between rigid and morphing
175 models, a two-tailed paired t-test was performed with the normality of the data confirmed using
176 a Shapiro-Wilk test. Finally, associations of TAWSS, OSI and ECAP with LA and LAA
177 volumes were studied using linear regressions. R² Pearson correlation coefficients were
178 provided. Statistical analyses were performed using Real Statistics Resource Pack for Excel
179 (Microsoft, Redmond).



180

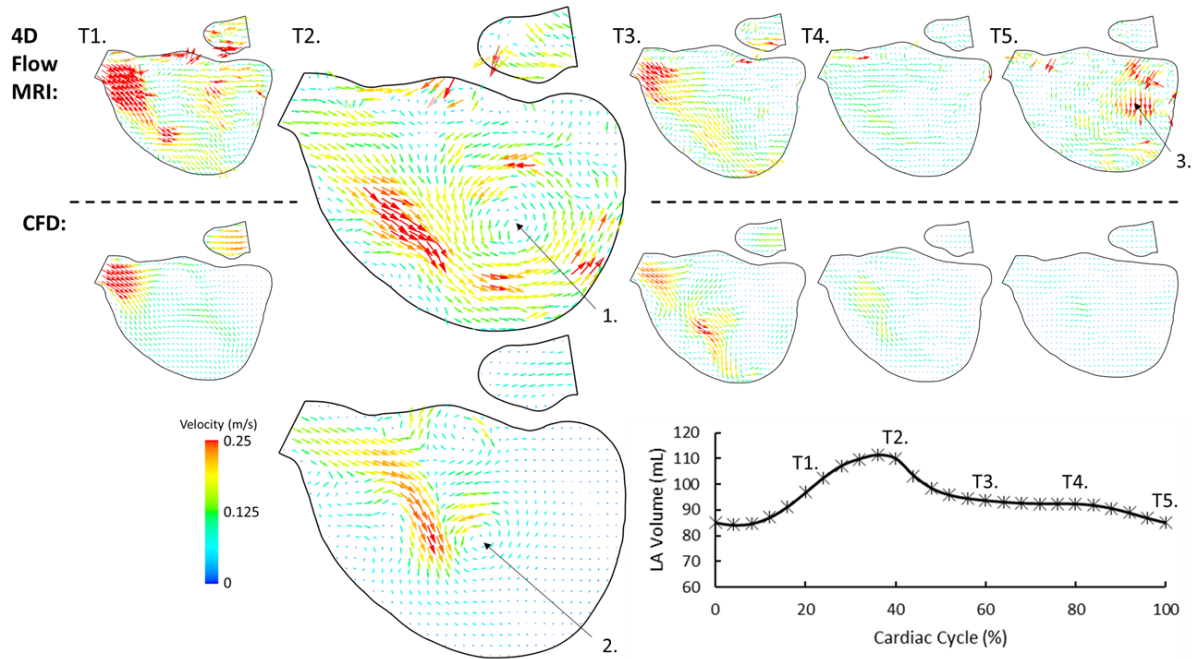
181 **Figure 1.** The workflow from imaging data to simulated haemodynamic results. AP: antero-
 182 posterior, FH: foot-head and RL: right-left directions.

183

184 Results

185 Grid convergence was acceptable for velocity (Figures S2 to S4) and TAWSS (Figures S5/6)
 186 on the finest mesh (2.76M cells, mean mesh size = 0.4 mm). Time-averaged velocity across
 187 the two-line probes and averaged across the entire LA volume differed by <1% when
 188 comparing the medium and fine mesh results, whilst TAWSS differed by 0.9% in the LA and
 189 3.0% in the LAA where TAWSS was very low.

190



191

192 **Figure 2. Validation of the CFD velocity field against 4D flow MRI data in Case 1.** 4D

193 flow MRI (upper row) and CFD (lower row)-derived instantaneous velocity vectors on a plane

194 through the left atrium (LA) for five temporal positions (T1-T5). These timepoints are indicated

195 on the left atrium volume curve (bottom right). Points 1 and 2 show a large vortex in the LA

196 whilst point 3 indicates noisy velocity vectors.

197

198 **Table 2.** Mean and standard deviation (SD) absolute velocity error (m/s) between CFD and 4D

199 flow MRI velocity fields in the left atrium for the five cases.

	Systole		Diastole	
	Mean	SD	Mean	SD
Case 1	0.07	0.05	0.05	0.05
Case 2	0.05	0.05	0.04	0.03
Case 3	0.05	0.04	0.06	0.05
Case 4	0.05	0.05	0.05	0.04
Case 5	0.08	0.07	0.05	0.05
Mean	0.06	-	0.05	-
SD	0.06	-	0.05	-

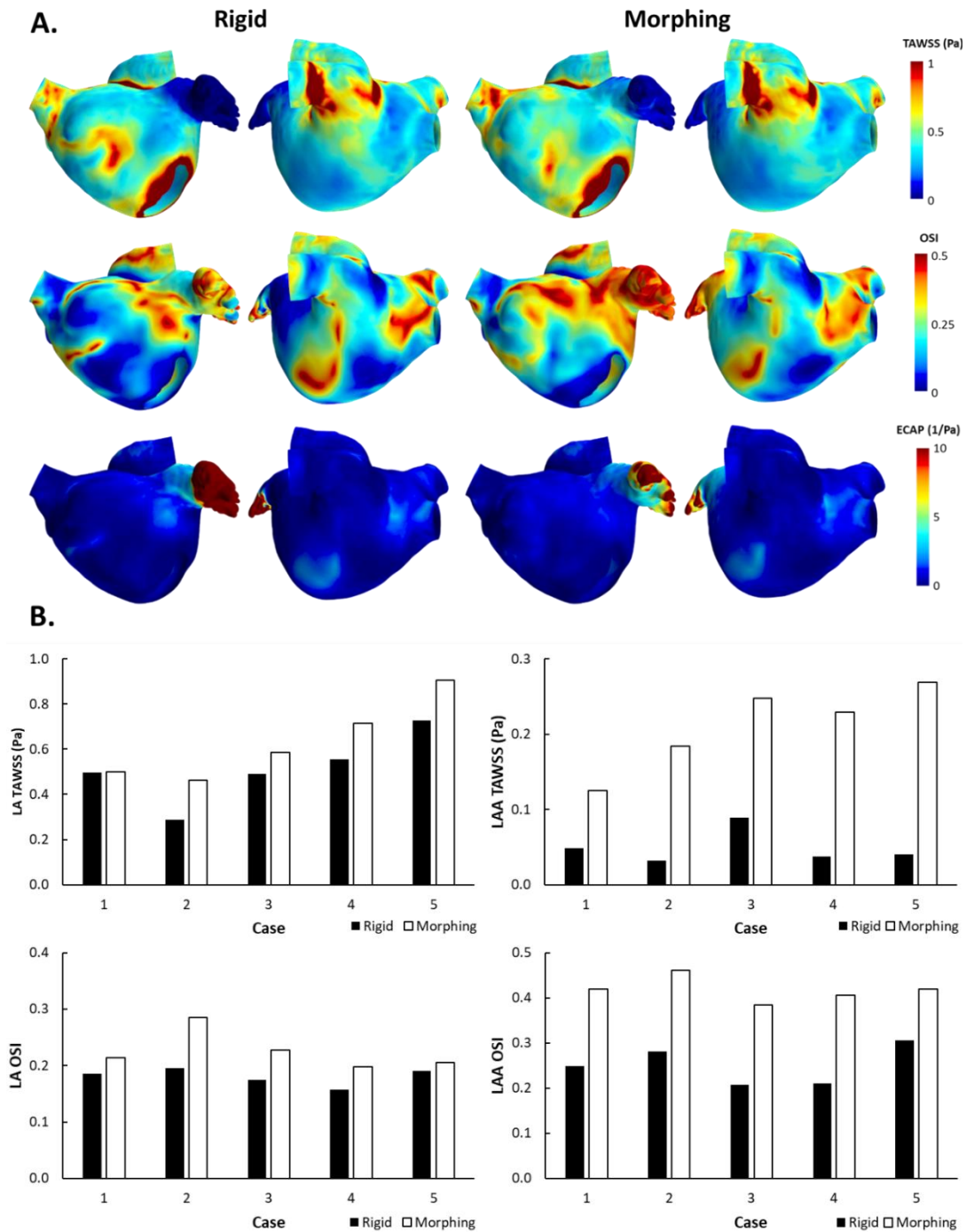
200

201 Comparison of the 4D flow and CFD temporal velocity fields for Case 1 shows good agreement
202 with the same large-scale structures observed in each (Figure 2, points 1 & 2). Towards time
203 point T5, when the LA empties and contracts towards its minimum volume, the 4D flow shows
204 some large, incongruous velocity vectors (Figure 2, point 3) likely arising from noise exterior
205 to the LA in the surrounding tissue. A visual comparison of the flow fields in all cases at systole
206 and diastole is shown in the supplemental material (Figure S7) with reasonable agreement.
207 Point-by-point absolute difference between the 4D flow MRI and CFD velocity fields are
208 reported in Table 2 for all five cases, revealing moderate differences given the sensitivity to
209 registration between the two fields. Of note, Case 5, which had a higher encoding velocity (300
210 cm/s), showed the highest systolic velocity errors.

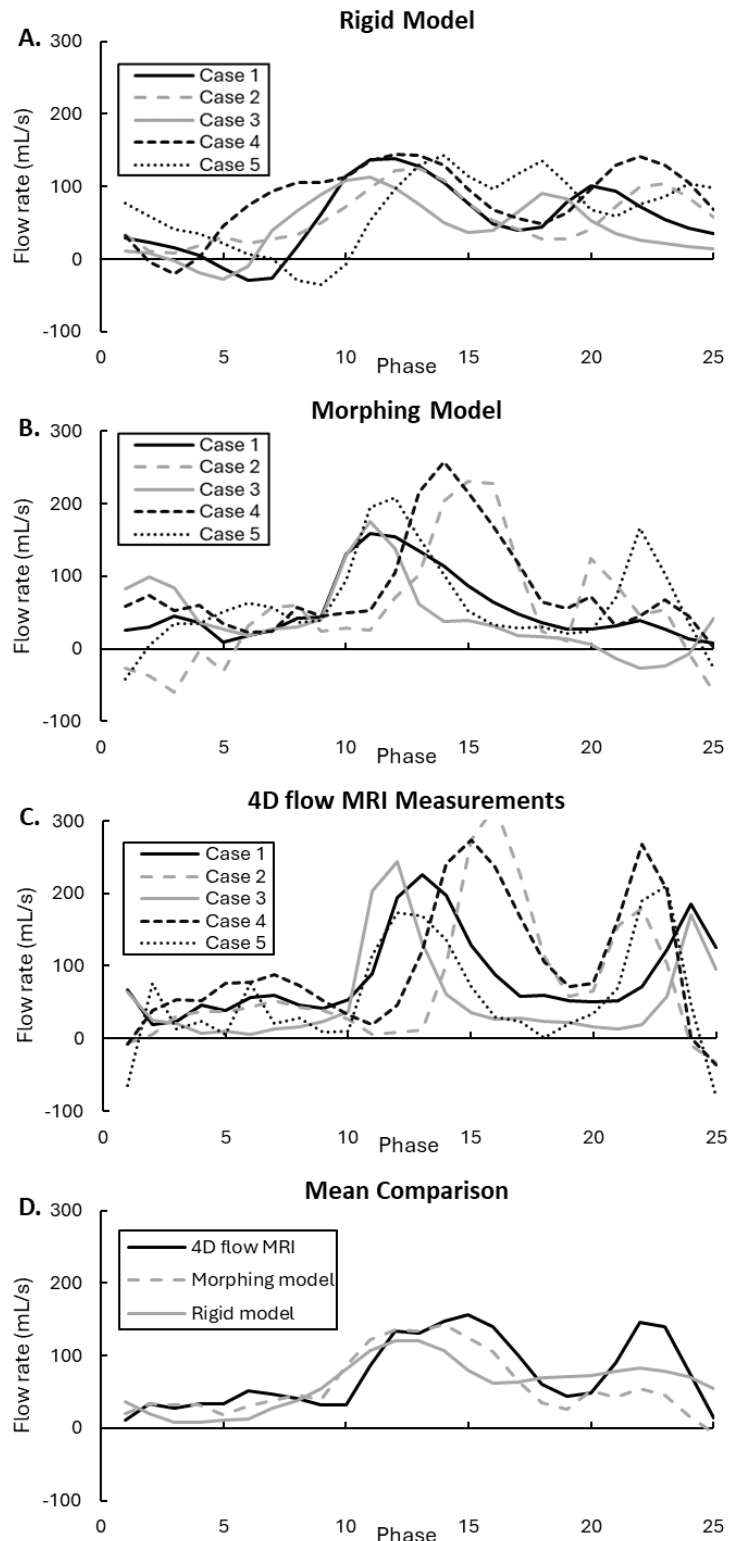
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212 Comparing the rigid and morphing models (Figure 3) revealed that the rigid model significantly
213 underestimated LA TAWSS (mean±SD=0.51±0.14 Pa vs. 0.63±0.16 Pa, p=0.02) and OSI
214 (mean±SD=0.18±0.01 Pa vs. 0.23±0.03 Pa, p=0.02) compared to the morphing model across
215 the five cases. In the LAA, TAWSS (mean±SD=0.05±0.02 Pa vs. 0.21±0.05 Pa, p=0.003) and
216 OSI (mean±SD=0.25±0.04 Pa vs. 0.42±0.03 Pa, p<0.001) were also underestimated though to
217 a far greater degree. Looking at the mitral valve outflow for all cases (Figure 4), the rigid wall
218 assumption decreased E and A wave amplitudes by an average of 44% and 46%, respectively,
219 when compared to the 4D flow MRI measurements. The morphing model also showed
220 decreases in E and A wave amplitude of 14% and 48%, respectively, indicating a considerably
221 improved E wave estimation (Supplemental material, Table S1) and slightly worse A wave.

222



224 **Figure 3. A.** Time-averaged wall shear stress (TAWSS), oscillatory shear index (OSI) and
 225 endothelial cell activation potential (ECAP) in the rigid and morphing models (Case 1). **B.**
 226 Quantitative comparison of surface-averaged TAWSS (top row) and OSI (bottom row)
 227 between rigid and morphing models in the left atrium (LA) and left atrial appendage (LAA)
 228 for the 5 cases analysed.



229

230 **Figure 4.** The mitral valve outflow obtained from the rigid computational fluid dynamics
 231 (CFD) model (**A.**), the morphing CFD model (**B.**) and as measured from 4D flow magnetic
 232 resonance imaging (MRI) (**C.**). **D.** Mitral outflows for the data in A, B and C averaged across
 233 all 5 cases. All waveforms are plotted across the 25 MRI time-phases.

234 The haemodynamic results from the morphing model (Table 3) show that the LAA exhibits
 235 substantially lower TAWSS ($-66\pm 6\%$, $p=0.003$), along with higher OSI ($87\pm 18\%$, $p<0.001$)
 236 and ECAP ($531\pm 192\%$, $p=0.01$) compared to the LA (Figure 5/6A). Haemodynamic metrics
 237 were plotted against indexed LA/LAA volume (Figure 6B), indicating that increased indexed
 238 end-systolic LA volume was correlated with decreased TAWSS ($R^2=0.35$) as well as increased
 239 OSI ($R^2=0.65$) and ECAP ($R^2=0.83$). Similarly, increased LAA volume was associated with
 240 decreased TAWSS ($R^2=0.61$) and increased OSI ($R^2=0.70$) and ECAP ($R^2=0.51$).

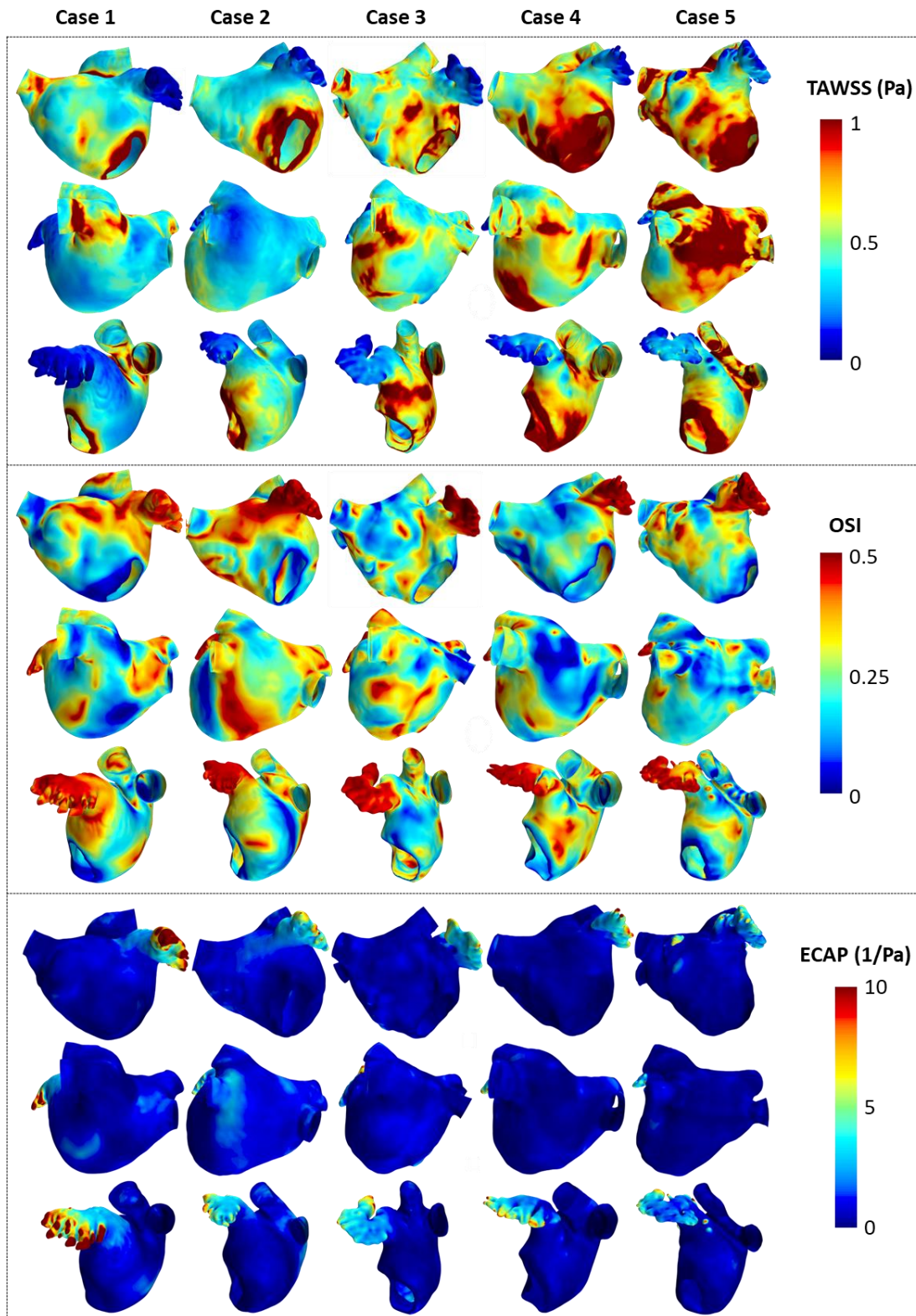
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242 **Table 3.** Surface-averaged haemodynamic results for the left atrium (LA) and the left atrial
 243 appendage (LAA).

Case	TAWSS (Pa)		OSI		ECAP (1/Pa)	
	LA	LAA	LA	LAA	LA	LAA
1	0.50 (0.38)	0.12 (0.09)	0.21 (0.11)	0.42 (0.05)	0.60 (0.46)	5.71 (4.34)
2	0.46 (0.40)	0.18 (0.10)	0.29 (0.11)	0.46 (0.03)	0.84 (0.50)	3.20 (1.62)
3	0.59 (0.25)	0.25 (0.15)	0.23 (0.12)	0.38 (0.12)	0.48 (0.34)	2.35 (1.72)
4	0.71 (0.40)	0.23 (0.12)	0.20 (0.10)	0.41 (0.09)	0.36 (0.27)	2.49 (1.79)
5	0.90 (0.68)	0.27 (0.15)	0.21 (0.10)	0.42 (0.07)	0.35 (0.47)	2.22 (1.72)
Mean (SD)	0.63 (0.18)	0.21 (0.06)	0.23 (0.03)	0.42 (0.03)	0.52 (0.20)	3.20 (1.46)

244 Note: TAWSS = time-averaged wall shear stress, OSI = oscillatory shear index, ECAP = endothelial cell
 245 activation potential, LA = left atrium, LAA = left atrial appendage, SD = standard deviation.

246



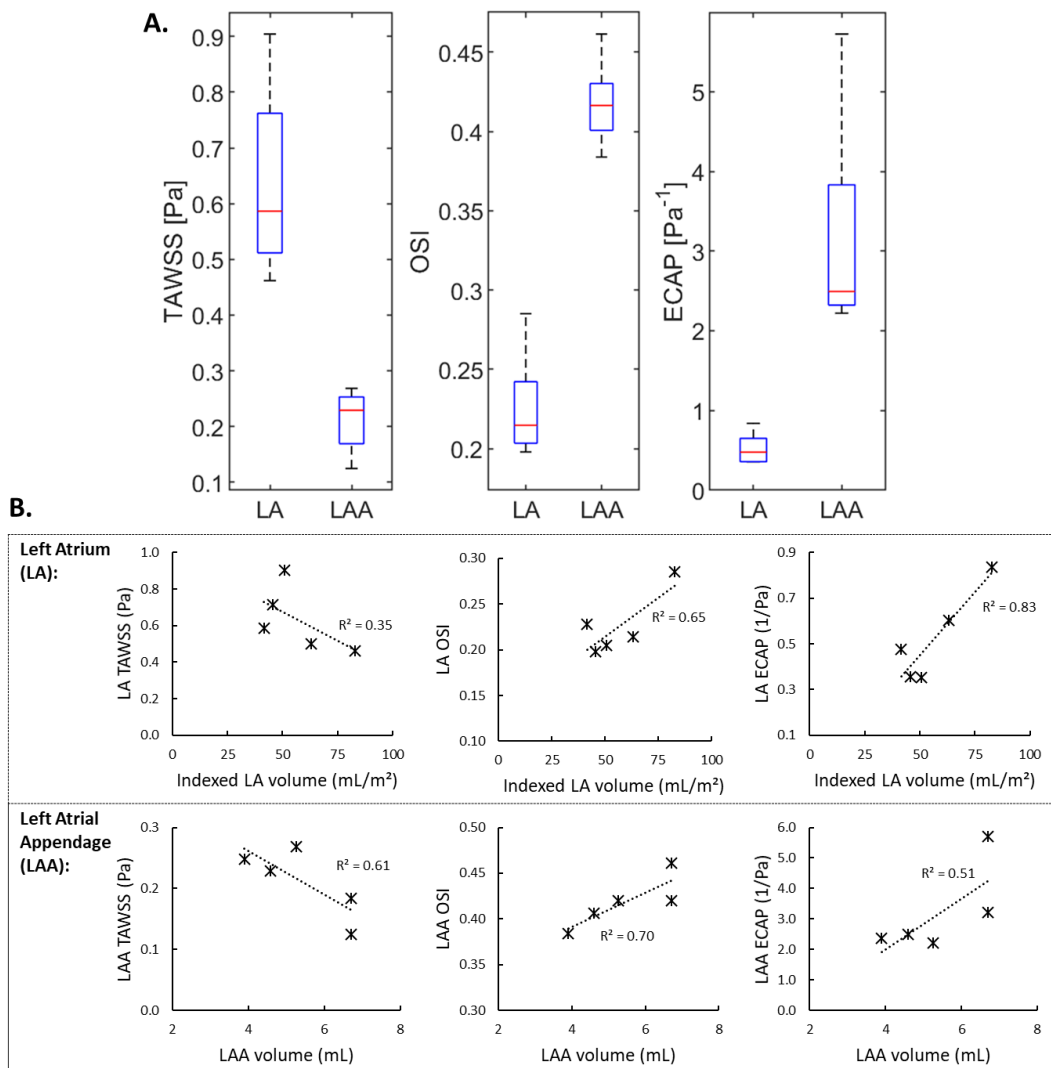
247

248 **Figure 5.** Left atrial time-averaged wall shear stress (TAWSS), oscillatory shear index (OSI)

249 and endothelial cell activation potential (ECAP) for cases 1-5 in the anterior (top), posterior

250 (middle) and lateral views (bottom).

251



252

253 **Figure 6. A.** Time-averaged wall shear stress (TAWSS), oscillatory shear index (OSI) and
 254 endothelial cell activation potential (ECAP) surface-averages for the left atrium (LA) and left
 255 atrial appendage (LAA). **B.** Linear regressions along with correlations between the
 256 haemodynamic metrics presented in A and indexed end-systolic LA volume (top) and LAA
 257 volume (bottom).

258

259 Discussion

260 In this study we present a novel multi-modal CFD model for the left atrium. The need for such
 261 a model comes from the relatively low resolution of 4D flow MRI, along with its implications

262 for WSS estimation³⁹ and the well-established link between WSS and thrombosis.^{40,41} This is
263 particularly important in the LAA where 4D flow analysis is challenging.⁴² We first outline the
264 accuracy and suitability of our novel CFD model of the LA. We then analyse results from a
265 small group of AF patients to examine existing hypotheses about thrombi formation and
266 describe potential new relationships between LA/LAA volumes and haemodynamic indices.

267

268 *Left atrium CFD model*

269 We present here, to the authors best knowledge, the first comparison of a LA CFD model with
270 4D flow MRI (Figure 2/S7, Table 2). Whilst these results are highly sensitive to cross-sectional
271 plane positioning, we see the same large-scale structures (Figure 2, pts 1. & 2). These results
272 are encouraging evidence that our CFD model accurately characterises such structures. Noisy
273 velocity vectors are a common issue with 4D flow MRI especially in enlarged LAs where the
274 velocity-to-noise ratio is lower. Such noise was observed in some cases (Case 1 Figure 2 pt. 3,
275 Case 5 Figure S7). This highlights another benefit of the CFD model which is free from
276 imaging noise and underpins the need to use the lowest practical encoding velocity.

277 The resolution offered by CT is critical to capture the intricate and highly patient-
278 specific morphology of the LA and especially of the LAA. For this reason it has been the basis
279 of the 3D reconstruction for the majority of CFD studies.^{31,43-45} The novel aspect of the present
280 study was to then register the CT geometric reconstruction to a MRI dynamic sequence
281 applying patient-specific PV inflows and LA wall motion. PV inflow distribution has been
282 previously shown to impact atrial flows,^{46,47}; whilst it is common to assume an even
283 distribution, here we applied unique patient-specific waveforms from 4D flow MRI to each
284 PV. Similarly, the vast majority of previous CFD studies have assumed a rigid wall boundary
285 condition, citing the reduced LA function in AF patients.^{48,49} Whilst LA ejection fraction may
286 be impeded in these patients it is not necessarily indicative of negligible local wall motion for

287 both the LA driven phases (reservoir and contraction) and the ventricular-driven phase
288 (conduit). Several CFD studies have however incorporated dynamic LA motion. Some applied
289 a generic or measured mitral valve annulus motion,^{27,50} a synthetic global displacement⁵¹ or a
290 similar approach to the present study, extracting local displacements from multiphase MRI or
291 CT.^{31,52} Our results show that haemodynamic indices vary significantly between rigid and
292 morphing models (Figure 3). The impact is greatest in the LAA, supporting recent findings,⁵³
293 where the rigid model fails to capture the oscillatory nature of the flow and records near-zero
294 TAWSS in some regions, the latter causing ECAP to be greatly overestimated. These results
295 make logical sense with wall motion being critical to flushing out stagnant pockets in the
296 intricate structure of the LAA.

297 Further to this, we have compared the impact on mitral valve outflows (Figure 4). Due
298 to conservation of mass (and volume for an incompressible fluid), mitral outflow is coupled to
299 changes in volume which are responsible for the characteristic E wave, occurring during LA
300 conduit phase, and A wave, occurring during LA contraction phase. An improved E wave
301 estimation was observed with the morphing model whilst A wave characterisation was slightly
302 worse. The consistent underestimation of the A wave may cause both models to underestimate
303 LA/LAA emptying and so overestimate the thrombogenicity. We see in the present study that
304 the amplitude and timing of the E wave is vastly improved when morphing the CFD model
305 (Figure 4B). Improvements to this registration algorithm will likely enhance the A wave. An
306 original feature of our approach is the inherent coupling of the wall motion and PV inflows,
307 both measured from the same MRI acquisition. Indeed, when motion and flow boundary
308 conditions are derived from separate acquisitions, like combining PV Doppler
309 echocardiography with dynamic CT, there is a greater risk of variability in the resultant mitral
310 valve outflow.

311

312 *Haemodynamics of the left atrium and left atrial appendage*

313 The model was applied to a small group of AF patients prior to ablation (Table 3, Figure 5).
314 The haemodynamic results showed in all patients lower TAWSS in the LAA compared to the
315 LA which has recently been associated with stroke.⁵⁴ Perhaps the most noteworthy result was
316 the systematically elevated OSI values in the LAA, suggesting a stagnant LAA with no
317 consistent flush-out. Such conditions, as per Virchow's triad, are pro-thrombotic.⁴¹ Being a
318 dynamic model, the LAA moves considerably throughout the cardiac cycle. As observed by
319 Koizumi et al., high frequency fibrillation may increase LAA OSI.²⁷ These results might also
320 explain why models which implement motion only via mitral valve longitudinal displacement
321 have not reported increased OSI in the LAA of stroke patients.⁵⁰
322 In our cohort, we saw a strong relationship between LAA volume and haemodynamics. Higher
323 LAA volume was associated with pro-thrombotic conditions. LAA volume has previously been
324 associated with stroke risk⁵⁵ and increased ECAP.⁵⁶ Like Lee et al.,⁵⁵ we also observed a strong
325 relationship between orifice area and pro-thrombotic conditions (low TAWSS, $R^2=0.93$, Supp
326 material Figure S8) though this may simply be emblematic of a larger LAA. Low WSS within
327 the LAA is to be expected given its unique anatomy and has been observed in healthy
328 subjects.⁵⁷ What the present study highlights, by comparing rigid wall and dynamic models, is
329 that LAA OSI is closely related to motion. This motion may be unique to AF patients whereby
330 the LAA is 'rattled' during fibrillation, increasing OSI and the occurrence of thrombosis in
331 these patients.

332

333 *Limitations*

334 There are several limitations of this study. The registration of the 3D model reconstructed from
335 CT to the MRI coordinate system is performed manually. As these are two separate
336 acquisitions, there is never a perfect registration of the two datasets. The applied motion model

337 fixes the PV inlets in space throughout the cycle. This neglects the slight translation or change
338 in dimension of these veins. 4D flow MRI signal-to-noise ratio (SNR) is lower than other
339 sequences that may be better suited to motion quantification. The 4D flow field itself is also
340 more prone to errors arising from low velocity-to-noise ratio (VNR), breathing motion
341 artefacts, undersampling artefacts and heart cycle variations. For Case 5 the encoding velocity
342 was higher than the remaining cases (300 cm/s vs. 150 cm/s). Results from this case are
343 therefore more susceptible to errors arising from a low VNR, as VNR is proportional to
344 $1/VENC$.⁵⁸ Whilst 4D flow MRI provides validation of the flow in the LA itself, the resolution
345 is too limited to provide a meaningful comparison in the LAA. 4D flow MRI measurements at
346 the mitral valve used for validation are sensitive to motion tracking.⁵⁹ All patients were imaged
347 whilst in sinus rhythm; analysis of patients during AF may be required to reveal the
348 mechanisms of AF-related thrombus formation in the LAA. Acquiring 4D flow MRI during
349 AF is challenging and 5D flow techniques, which further encodes the heart rhythm, may offer
350 insights into such mechanisms.⁶⁰ Finally, the mitral valve is modelled as constantly open.
351 Whilst the coupling of the PV inflows and wall motion (volume change) ensures a realistic
352 transient flow through the valve, the shape of the valve is not distinguishable in the dynamic
353 MRI and as this is an outlet it is likely to have very little impact on LA flow.

354

355 **Conclusion**

356 In this study we present a novel model of LA flow. We combine high-resolution CT with 4D
357 flow MRI to create a high-resolution patient-specific dynamic model with PV inflows,
358 validated against 4D flow MRI. We compare the performance of this model with results from
359 a rigid wall simulation, revealing that the rigid model underestimates TAWSS and OSI, whilst
360 substantially overestimating ECAP. We then apply this model to a group of five AF patients
361 and show in the LAA the low TAWSS and high OSI/ECAP associated with thrombosis. Left

362 atrial volume appears to correlate with pro-thrombotic conditions in the LAA. Whilst rigid wall
363 models are capable of capturing the low TAWSS in the LAA, we show here the advantage of
364 a dynamic model in capturing high OSI which may, if confirmed in a large cohort, become an
365 important clinical predictor of thrombosis.

366

367 **Declarations**

368 *Compliance with Ethical Standards*

369 Patients in the CTStrain-AF (NCT04281329) gave written informed consent for participation
370 in the study.

371

372 *Consent for publication*

373 All participants provided consent for publication.

374

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378

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382

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