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Next-Generation Tunable All-Fiber Mach-Zehnder Interferometers in Hollow Core Fibers

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*Abstract***— We demonstrate a new acousto-optic Mach-Zehnder interferometer (MZ) based on a hollow core fiber (HCF). The fabricated acousto-optic device excites two MZs in a 7.5 cm long HCF. In the first MZ, the HCF is attached in a centrally positioned acoustic driver, exciting two acoustically induced long period gratings. The second MZ induces two strong curvatures at the edges of the attached HCF-driver length. The MZs tune the free spectral range of the modulated multiwavelength spectrum by changing the driver's frequency in steps of 1 Hz while providing compactness, efficiency, and high sensitivity, suitable for dynamic filters and fiber sensors.**

Keywords—acousto-optic devices, long period gratings, Mach-Zehnder interferometers.

I. INTRODUCTION

Acousto-optic devices based on optical fibers enable highly sensitive dynamic sensors providing good resistance for the characterization of chemical, food, and biomedical applications [1], [2]. On the other hand, all-fiber Mach-Zehnder interferometers (MZs) are attractive for sensing strain, humidity, refractive index, temperature, fuel, and gases $[3]$, $[4]$, $[5]$, $[6]$). In MZs, the optical beam is split to travel distinct optical paths which are further recombined interfering at the fiber output. The interference fringes have the free spectral range (FSR) tuned by changing the beams' relative phase.

Optical fibers provide notable features to enable multiple optical path lengths by means of distinct guided modes. These path lengths can be altered in MZs by employing concatenated fibers with different cross sections. The input beams can be coupled or split by fabricating two-point perturbations changing the refractive index or structure of the fiber cross section, e.g., by employing tapering [7], [8] or two symmetric bends nearly separated along the fiber [6]. Besides, MZs including two inscribed or pressure-induced long period gratings (LPGs) have been reported in sensing applications [3], [5], [9]. MZs based on LPGs provide tunable notch wavelength and magnitude by changing respectively the grating period and modulated refractive index amplitude.

Alternatively, acoustically modulated MZs provide additional electrical tuning of LPG properties and its transmission spectrum. The acoustically induced LPGs are caused by bend-induced geometric deformation of the fiber changing the optical path length of the guided modes. The dynamic LPGs couple power between the fundamental and higher order modes at a resonant wavelength and depth defined respectively by the acoustic frequency and amplitude [10], [11]. The acousto-optic devices generally use tapered and etched fibers to reduce the fiber diameter and increase the modulation efficiency. Nevertheless, FSR tuning is usually limited to small variations induced by applied temperature or strain. Thus, relevant FSR tuning and generation of multiple fringes usually require replacing long fibers in between the two LPGs, resulting in the fabrication of additional MZs with distinct dimensions, which might increase the overall device size, consumed energy, switching time, and insertion losses [12].

We have recently numerically and experimentally demonstrated acoustically induced LPGs in tubular and hybrid-lattice HCFs [10], [11]. Here, we demonstrate a new all-fiber in-line dual MZ inside a hybrid kagome-tubular HCF. The fabricated acousto-optic modulator employs a centered-positioned acoustic driver, providing unique features to generate multiple resonant wavelengths by tuning the electrical frequency in 1 Hz steps. The results are analyzed and discussed for further sensing applications.

II. EXPERIMENTAL SETUP AND METHODS

Fig. 1(a) illustrates the experimental setup with the acoustooptic modulator (AOM), composed of an HCF segment of length *L*, a piezoelectric transducer (PZT), and a silica acoustic horn. The AOM is fabricated by employing a silicamade hybrid lattice HCF with a cross section formed by 800 nm thick Kagomé struts and 20 µm diameter tubes $(1.25 \mu m)$ thickness), as seen in Fig. 1(b). The HCF has a 34 µm diameter air core and is 240 µm in outer diameter, as described in detail in [13]. The PZT is 2 mm in thickness and 25 mm in diameter. The horn is 1.8 cm long and has the diameter tapered from 4.8 to 0.65 mm. The AOM connections are similar as in [10]. The HCF ends are fixed resulting in a total device length of $L = 7.5$ cm.

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Fig. 1. (a) Experimental setup and acousto-optic modulator (AOM) using a piezoelectric transducer (PZT), an acoustic horn and an HCF segment of length *L*. (b) Hybrid-lattice hollow core fiber (HCF) and (c) details of the Mach-Zehnder interferometers (MZs).

The HCF input is butt-coupled to a standard single-mode optical fiber (SMF) connected to a supercontinuum laser source (SC) using a lens. The HCF output is butt-coupled to a multimode optical fiber (MMF) connected to an optical spectrum analyzer (OSA). A signal generator (SG) is used to excite the PZT with a maximum 10 V voltage sinusoidal electrical signal.

Fig. 1(c) illustrates the two MZs in the AOM, indicating the connection of the horn and HCF. MZ-1 is assembled by placing the acoustic driver centered along the HCF and attaching the fiber with the horn along the length *d*, splitting the fiber into two equivalent lengths $({\sim} 3.7 \text{ cm})$. MZ-1 has a cavity length of $L_{MZ} \sim 3.9$ cm. The acoustically induced LPG-1 and LPG-2 couple power between the fundamental mode to higher order modes supported by the HCF air core [11, 13]. Fig. 1(c) indicates MZ-2 located in the separation region of $d \sim 1.6$ mm between the LPGs. The pressure caused by the LPGs in the fixed fiber *d* edges induces two strong curvatures coupling higher order modes in addition to those in MZ-1. Thus, MZ-2 curvatures work as a two-point coupler increasing the modes effective index *n*eff. The FSR is tuned as [14],

$$
\text{FSR} \approx \frac{\lambda^2}{\Delta n_{eff} L_{MZ}}.\tag{1}
$$

where, Δn_{eff} is the modes effective refractive index difference, λ is the optical wavelength and, L_{MZ} is the centerto-center LPGs separation.

The AOM modulates a notch at $\lambda_c = 1176$ nm in the HCF transmission spectrum at $f = 264.064$ kHz (although is not shown, other modulated notches could also be tuned from λ = 800 to 1200 nm). The fringes' FSR is tuned by adjusting the frequency from $f = 264.064$ to 264.066 kHz (1 Hz steps).

III. RESULTS AND DISCUSSION

We have measured the modulated transmission spectra of the HCF. Fig. 2(a) shows one predominant modulated notch in the spectrum, indicating that the variations of Δn_{eff} induced by MZ-2 are still negligible to generate multiple fringes. In this case, the two LPGs work as a unique grating with an induced phase shift caused mainly by the fixed length *d* [9]. The modulated notch approaches a nearly 2π -phase-shift at $f_0 = 264.064$ kHz. Fig. 2(b) shows the modulated spectrum under an externally induced strain (*d* changes are estimated in about $\Delta d = 100 \text{ }\mu\text{m}$). The modulated spectrum approaches a nearly π -phase-shift showing that the AOM has high sensitivity to monitor external measurands. Thus, minor variations of *d* changing the relative phase between the coupled modes might be useful to characterize strain in sensing applications.

In contrast, a multiwavelength spectrum is generated by increasing *f* to 264.065 kHz (Δf = 1 Hz) and 264.066 kHz $(\Delta f = 2 \text{ Hz})$, as shown in Fig. 2(c) and 3(d). We note in the modulated spectra that increasing modal coupling and Δ*n*eff reduce the fringes FSR. This is caused by the frequencytuning of MZ-2 edges curvatures coupling higher order modes. The reduced fringe FSR is followed by increasing fringes in the notch. The reduced fringe visibility (magnitude) in respect to the zero dB level implies that raising modal couplings might induce power losses (max. 2 dB). Overall, the fringe FSR could be tuned from $FSR = 1$ to 0.6 nm with a tuning slope of \sim 4 fringes/Hz (the spectra in Fig. 2(a) and 2(b) are not considered to estimate FSR).

Previous numerical and analytical studies show that the dual AOM-MZ couples favorably LP₀₁ and higher order modes propagating in the HCF air core (predominantly the higher order modes LP_{11} and LP_{21}) [11]. These modes have a relevant spatial overlap of electric fields over the fiber crosssection, providing efficient modal couplings as described in [11]. Nevertheless, other modes with low spatial overlap, such as tube modes, might also couple in with minor modulation efficiency. Overall, the modulated spectra show a 3-dB notch bandwidth of \sim 4 nm and a maximum modulation depth of 6.5 dB at $\lambda_c \sim 1176$ nm for the considered frequencies. The modulated notch shows asymmetric fringe distribution around λ_c caused by variation of the modes Δ*n*eff and beatlengths in the considered spectral range [11].

In summary, the demonstrated AOM shows relevant high modulation efficiency employing a maximum 10 V drive voltage and a 7.5 cm short fiber length. This improved efficiency is caused by the increased induced strain in the HCF tubes changing the propagation mechanism of optical modes in the air core [11]. Thus, HCFs with large diameters might be suitably used to increase the acousto-optic interaction, reducing requirements of reduced diameter or long fibers, high drive voltages, and use of power amplification. The AOM-MZ is promising to characterize external measurands as strain, temperature, density, and viscosity by exposing the induced LPGs in contact with fluid substances, which might change the acoustic period and amplitude [2]. Further studies might also explore HCFs with larger air holes or thinner tubes with distinct fiber structures, adjusting the spectral modal properties to improve the FSR sensitivity, fringes visibility, and modulated spectrum symmetry.

IV. CONCLUSION

We experimentally demonstrate a new all-fiber acoustooptic dual MZ enabling full reconfiguration of a multiwavelength filter by frequency-tuning the FSR. MZ-1 is fabricated with a centered positioned acoustic driver inducing

Fig. 2. Measured transmission spectra of the hollow core fiber for the frequency range of *f* = 264.064 - 264.066 kHz. (a) The AOM MZs induce a nearly 2πphase-shift in the modulated spectrum at *f =* 264.064 kHz. (b) The spectrum is modulated by an externally induced strain resembling π-phase-shift. MZs multiwavelength spectra by tuning the fringes FSR with (c)(d) increasing frequency respectively in steps of Δ*f* = 1 and 2 Hz.

simultaneously two acoustically induced LPGs. MZ-2 is formed by the attached HCF - driver length exciting two strong edge curvatures. The demonstrated AOM modulates a notch bandwidth of 4 nm with a maximum depth of 6.5 dB at 1176 nm. FSR is tuned from 1 to 0.6 nm by changing the frequency in steps of 1 and 2 Hz. Thus, the AOM-MZ provides high frequency-tuning sensitivity dynamically generating from 1 to 8 resonant wavelengths, due to increased modal couplings and Δ*n*eff. In additional, the preliminary results indicate high sensitivity to measure strain induced by external measurands. This sensitivity might be studied to measure temperature, density, refractive index, and viscosity by exposing the device to fluid substances [2]. Overall, the modulated notch width, fringe number, and FSR show a strong dependence on the induced HCF modal couplings, which can be adjusted by optimizing the HCF structure. The demonstrated AOM-MZ provides compactness, high modulation efficiency, and an in-line monolithic fiber setup, which is suitable for tunable filters and fiber sensors.

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