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MOF-derived metal oxide (Cu, Ni, Zn) gas sensors with excellent selectivity towards H₂S, CO and H₂ gases

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ABSTRACT

Metal-organic framework (MOF)-derived metal oxides blend the sensing properties of metal oxides with MOF porosity, enhancing gas sensing capabilities. In this study, M-MOFs (M = Cu, Ni and Zn) were synthesized and then calcined at different temperatures to obtain their corresponding metal oxides (CuO, NiO and ZnO). The synthesis method incorporated novel approaches to enhance sensor performance, such as optimizing calcination temperatures for improved selectivity. Structural and morphological analyses confirmed the high surface area and porosity of the metal oxide materials, facilitating efficient gas adsorption and promoting enhanced sensor response. Gas sensing studies revealed significantly enhanced performance of MOF-derived metal oxides over M-MOFs, strongly influenced by calcination temperature. Moreover, CuO, NiO and ZnO MOF-derived metal oxides showed improved selectivity towards H_2S , CO and H_2 gases, respectively. This study demonstrates that tuning MOF and calcination parameters can tailor sensor selectivity effectively.

1. Introduction

Hydrogen (H₂) is an important gas and has a wide range of applications in different industries, such as food processing, medical treatments, aerospace, and energy storage. It is also one of the cleanest and most environmentally friendly sustainable energy sources due to its abundance, cleanliness, and recyclability [1–3]. Furthermore, H₂ monitoring in exhaled breath can be used as a gauge to examine intestinal conditions. For instance, a hydrogen breath test is widely used to diagnose small intestinal bacterial overgrowth syndrome and carbohydrate (fructose, lactose, and sorbitol) malabsorption [4]. However, it is a highly explosive gas (4–75 vol%) with high combustion heat (142 kJ g^{-1}), low ignition energy (0.02 mJ), and high flame propagation velocity [5]. In case of leakage, which is facilitated by H₂ small molecule size (0.289 nm) and high diffusion coefficient (0.61 cm²/s), the risk of disasters is high [6]. Unfortunately, H₂ gas leakages cannot be easily detected due to H₂ absence of color, odor and taste [7]. Hence, reliable H₂ gas sensors with high sensitivity and robustness are needed to avoid leakage-related accidents and explosions [8].

 $\rm H_2S$ gas is a colorless, corrosive, water-soluble, highly toxic, and flammable gas in the range of 4–44 vol% with an unpleasant rotten egglike smell. At low concentrations, it is highly irritant to eyes, skin, nose and throat and at concentrations above 100 ppm, it paralyzes the olfactory nerves, and the sense of odor disappears, which gives the false

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impression that exposure to the gas was finished. At concentrations higher than 1000 ppm it can be lethal [9,10]. In addition, H_2S is a known biomarker for Down syndrome, Alzheimer's disease, ischemia, asthma, and halitosis [11] Therefore, reliable detection of H_2S is also of importance.

CO is odorless, tasteless and colorless with a highly toxic nature, which is mainly emitted from the incomplete burning of fossil fuels. It is known as the silent killer and since human red blood cell hemoglobin (Hb) is a major target site for CO, it combines with hemoglobin to form carboxyhemoglobin, a molecule that is incapable of carrying oxygen to tissue sites, resulting in tissue hypoxia [12,13]. Nausea, headache and dizziness are observed with CO-Hb levels over 10 %, and when the amount of CO-Hb increases to 30–50 %, severe health issues like increases in respiratory and heart rates, syncope, motor paralysis and confusion are observed. In higher levels of poisoning death is likely [14]. Therefore, reliable detection of CO gas is also vital from our safety point of view.

Different H₂ gas sensors, such as electrochemical [15], catalytic [16], optical [17], surface acoustic wave [18], metallic thin film [19], gasochromic [20] and resistive-based sensors [21], have been developed. Also, various gas sensors for the detection of CO and H₂S gases have been reported in the literature [22–27]. Resistive gas sensors, which rely on semiconducting metal oxides (SMO), such as SnO₂ [28], In₂O₃ [29], ZnO [30], NiO [31], and CuO [32] display good response and stability, fast dynamics, small size, simple operation and low price [33]. However, in their pristine form, they generally show poor selectivity towards a specific gas.

Metal-organic frameworks (MOFs) are porous materials in which metal clusters and organic ligands are connected through coordination bonds [34]. Due to their high specific surface area, tunability and high stability, they are ideal materials for potential applications such as gas adsorption and separation [35], drug delivery [36], gas sensors [37], water treatment [38], catalysis [39] and energy storage [40]. MOFs can also be used as precursors for the preparation of different functional nanostructures (*i.e.* SMOs) [41] that are exploited in many different fields, including electrochemical energy storage [42], catalysis [43] and sensing [44]. Specifically, MOF-derived SMOs have been used as electrically-transduced gas sensors, such as chemiresistors, chemicapacitors and electrochemical gas sensors [45–49].

However, control of high temperature pyrolysis procedure is one of most challenging issues to successfully maintain the original high porosity and surface areas of MOFs, so that the MOF-derived materials could achieve excellent performance as gas sensor [50].

Several groups have investigated the use of MOFs and the derived SMOs for gas detection due to their large specific surface area, tunable pore sizes, low density, and ordered crystal structure. For instance, Nguyen et al. tested Co-MOF-74, Ni-MOF-74 and Mg-MOF-74 and found that Co-MOF-74 was the best H₂ gas sensor due to the presence of two oxidation Co states (+2 and + 3) in the cluster [51]. Also, regarding CO gas sensing by MOFs, Nguyen et al. [52], reported fabrication of a Ni-incorporated MOF gas sensor. However, it showed a low response of only 1.7–50 ppm CO gas. Aykanat et al. [53], reported MOFs with metallophthalocyanine (MPc, M = Co and Ni) units for CO gas sensing. Surya et al. [54] reported Ag-decorated UiO-66 (Zr) MOF-based capacitive sensor for the detection of H₂S gas. However, overall, MOF gas sensors have poor sensing performance due to their low conductivity and stability.

However, overall, MOF gas sensors have poor sensing performance due to their low conductivity and stability. However, MOFs, in combination with metal oxides show promising sensing properties. For example, Drobek et al. increased the selectivity of pristine ZnO nanowires by growing a thin layer of zeolitic imidazolate frameworks (ZIF)-8 onto the nanowire surface. This led to a response of 1.44–50 ppm H₂ gas at 300 °C and a very small response to other gases, such as toluene and benzene [55]. Following a similar approach, Weber et al. combined ZnO nanowires decorated with Pd nanoparticles (NPs) and ZIF-8 as porous material. This led to a response of 9–50 ppm H₂ gas at 200 °C. The addition of Pd NPs increased the electron depletion layer depth at the Pd–ZnO contact area, leading to higher resistance than with the ZnO NW sensor. In the presence of H₂ gas, Pd and part of the ZnO surface were converted into PdH_x and metallic Zn, respectively, which contributed to the increase in the conductivity, influencing the sensor response [56].

Interestingly, MOFs can be easily transformed into SMOs with a large surface area and controlled shape by using the appropriate heat treatment [57,58]. In fact, MOF-derived SMOs combine the good intrinsic sensing properties of metal oxides and the highly porous structure of MOFs, which can boost the sensing performance [59]. For example, DMello et al. recently reported the preparation of a MOF-derived Co–ZnO gas sensor anchored on nitrogen-doped carbon that could detect H₂ (1 % of concentration) at room temperature [60]. Hussain et al. reported enhanced sensitivity of CuO-decorated ZnO polyhedral nanostructures towards H₂S gas [61]. In another study, Chen and co-workers, reported MOF-derived Co₃O₄ NPs over direct grown ZnO nanoflowers for selective sensing of CO gas [62].

In this work, to tune the selectivity of MOF-derived SMOs towards different gases, we synthesized three different MOFs based on Cu, Ni and Zn metals and their nanostructured SMOs counterparts (*i.e.* CuO, NiO and ZnO) by calcination in air at different temperatures (400, 500 and 600 °C). The gas sensing test results showed enhanced sensing performance of MOF-derived CuO, NiO and ZnO compared with their original MOF counterparts. Furthermore, the three MOF-derived SMO gas sensors showed improved selectivity towards H_2S , CO and H_2 gases, respectively. Therefore, the selectivity of the resulting SMO gas sensor can be finely adjusted through the strategic selection of MOF precursors and specific calcination temperatures. Our study introduces a fresh perspective by investigating how variations in calcination temperatures influence the gas sensing properties of MOF-derived metal oxides, thus improving their practical utility.

2. Experimentation

2.1. Materials

All used chemicals were commercially available and were used as purchased. The chemicals 4-carboxypyrazole (4-cpz, 95 %), 1,4-benzenedicarboxylic (1,4-bdc, 97 %), 1,4-diazabicyclo [2.2.2] octane (DABCO, \geq 99 %), copper nitrate trihydrate (Cu(NO₃)₂·3H₂O, \geq 99 %), nickel acetate tetrahydrate (Ni(AcO)₂·4H₂O, \geq 99 %), zinc nitrate hexahydrate (Zn(NO₃)₂·6H₂O, \geq 99 %) were from Merck. The solvents *N*,*N*-dimethylformamide (DMF, \geq 99 %), ethanol (\geq 99 %), diethyl ether (\geq 99 %) and dichloromethane (DCM, \geq 99 %) were from Fisher Scientific.

2.2. MOF and MOF-derived SMO synthesis

 $NH_4[Cu_3-(\mu_3-OH)(\mu_3-4-cpz)_3]$, (Cu-MOF) was obtained following a previously described procedure [63]. Briefly, 222 mg 4-cpz (2 mmol) and 480 mg Cu(NO_3)_2·3H_2O (2 mmol) were dissolved in 30 mL of an aqueous ammonia solution (1:15, NH_3/H_2O) giving rise to a blue solution. After incubation for 3 days, the obtained dark blue crystals were filtered and rinsed in ethanol and diethyl ether. Before use, crystals were reduced to powder in an agate mortar.

 $[Ni_8(OH)_4(H_2O)_2(cpz)_6]$, (Ni-MOF) was synthesized using the approach described in [64]. After dissolving 33.3 mg 4-cpz (0.3 mmol) in 16 mL DMF and 99.2 mg Ni(AcO)_2·4H_2O (0.4 mmol) in 4 mL H_2O, they were mixed for 6 h. The obtained green solid was filtered, rinsed in ethanol and diethyl ether, followed by DMF exchange with DCM.

[Zn₂(bdc)₂(dabco)] (Zn-MOF) was obtained following a previously described protocol [65]. After dissolution of 500 mg Zn(NO₃)₂·6H₂O (1.68 mmol) and 280 mg 4-bdc (1.68 mmol) in 14 mL DMF and 0.0935 mg DABCO (0.84 mmol) in 6 mL DMF, the two solutions were stirred at 120 °C for 48 h. The product was washed with DMF and DCM.

The obtained Cu-, Ni- and Zn-MOFs were then calcined at 400, 500, $600 \,^{\circ}$ C in air for 2 h to obtain porous nanostructured CuO, NiO and ZnO, respectively.

2.3. Gas sensor fabrication

Photolithography and SiO₂–Si (100) were used to fabricate bilayered and patterned-interdigital electrodes. A Ti (~50 nm) layer was deposited to improve the adhesion between the SiO₂ substrate and electrode, and Pt (~200 nm) was used as electrode. To prepare the gas sensors, 10 mg of the synthesized MOFs and MOF-derived SMOs in powder form and 0.5 μ L α -terpineol were mixed in a mortar and the obtained paste was coated onto the electrode layer and dried at 70 °C in air for 1 h. The obtained gas sensors were annealed at 350 °C for 1 h to remove the organic species and stabilize their baseline electrical resistance. The thickness of sensing layer over the substrate was ~6 μ m (Fig. S1).

2.4. Gas sensing measurements

The fabricated gas sensors were put into a gas chamber inside a horizontal tubular furnace with possible temperature control. In the chamber, the concentration of the gas to be tested was obtained by adjusting the gas and dry air ratio using mass flow controllers (total flow rate = 500 sccm). Each sensor response was calculated using $R=R_a/R_g$ or $R=R_g/R_a$, in function of the sensor type and tested gas, where R_g and R_a were the resistance in the presence of gas and air, respectively. The response time and recovery time were defined as the times needed to reach 90 % of the change in resistance after injection and removal of the tested gas, respectively.

2.5. Characterizations

Shape and elemental composition were characterized using scanning electron microscopy (SEM; Hitachi S4800 microscope, Japan), transmission electron microscopy (TEM; JEOL 2200FS, 200 kV, and JEOL ARM-200F, 200 kV) and energy-dispersive X-ray (EDX) spectroscopy (Zeiss EVO HD15 microscope with an Oxford X-MaxN EDX detector). The crystal phases were determined by X-ray diffraction (XRD; PAN-Alytical Xpert-PRO diffractometer) using Cu-K_{a1} radiation ($\lambda = 1.5406$ Å) and a 2 θ range from 10 to 80°. Raman spectra were measured by dispersive Raman spectroscopy (Horiba XploRA), using a 659.55 nm laser and a 100x objective. The surface elemental composition and the different surface areas were assessed by X-ray photoelectron spectroscopy (XPS) with a monochromatic X-ray source (Al-K α ; h ν = 1486.6 eV) and by N₂ adsorption-desorption at 77 K. For elemental mapping, a Zeiss EVO HD15 microscope and an Oxford X-MaxN energy-dispersive X-ray (EDS) detector was used.



Fig. 1. XRD patterns of (a) Cu-MOF (b) Ni-MOF and (c) Zn-MOF materials calcined in air at 500, 600 and 600 °C, respectively. Raman spectra of (d) Cu-MOF (e) Ni-MOF and (f) Zn-MOF materials calcined in air at 500, 600 and 600 °C, respectively. XPS core-level spectra of (g) Cu 2p for Cu-MOF after calcination at 500 °C, (h) Ni 2p for Ni-MOF after calcination at 600 °C, and (i) Zn 2p for Zn-MOF after calcination at 600 °C.

3. Results and discussion

3.1. Morphological and structural analyses

The Cu- and Ni-MOFs were based on the same pyrazolate organic ligand, while the Zn-MOF was based on the 4-bdc and DABCO organic ligands. Then, these MOFs were calcined to obtain oxide-based materials, the structure of which was assessed by XRD and Raman measurements. XRD analysis of MOF-derived CuO (obtained by calcination at 500 °C) (Fig. 1a) highlighted sharp peaks at 32.6°, 35.6°, 38.7°, 48.9°, 53.5° and 58.3° that were assigned to the (100), (002), (111), (202), and (020) crystalline planes of single phase monoclinic CuO (JCPDS Card No.48-1548), respectively. No peak related to impurities, such as Cu, Cu₂O or Cu(OH)₂, was detected, implying the successful synthesis and high purity of the starting materials. The XRD analysis of MOF-derived NiO (calcination at 600 °C) (Fig. 1b) highlighted diffraction peaks at 37.4° , 43.4° , and 63.0° that were assigned to the (111), (200) and (220) crystalline planes of NiO with NaCl structure (JCPDS Card No. 47–1049), respectively [66,67]. Two other diffraction peaks at 44.6° and 51.9° were observed, suggesting the presence of the Ni₂O₃ phase due to calcination in air. The XRD analysis of MOF-derived ZnO (calcined at 600 °C) (Fig. 1c) showed that all peaks matched the typical Wurtzite crystal structure of ZnO (JCPDS No. 36-1451) [68,69]. Moreover, the absence of other peaks demonstrated the successful formation of a pure ZnO phase.

Similarly, Raman measurements were carried out after calcination at 500 °C (Cu-MOF) and 600 °C (Ni-MOF and Zn-MOF). Cu-MOF (Fig. 1d) displayed one peak at 285 cm⁻¹ (assigned to the Ag mode of the CuO phase) and two peaks at 333 and 620 cm^{-1} (assigned to the B_g modes of the CuO phase) [70,71], in agreement with previous studies. In the Ni-MOF Raman spectrum (Fig. 1e), five Raman peaks at 210, 370, 530, 690 and 1055 cm^{-1} were observed. The peaks at ~200 and 370 cm^{-1} and the peak at 530 cm⁻¹ corresponded to the first order transverse optical (TO) and to the longitudinal optical (LO) phonon modes of NiO, respectively. The peaks at 700 and 1055 cm⁻¹ were assigned to the 2TO and 2LO combinations, respectively [72,73]. All Zn-MOF peaks (Fig. 1f) matched those described in the literature and the peak at \sim 1144 cm⁻ contained contributions from $2A_1(LO)$ and $2E_1(LO)$ [68]. The first- and second-order Raman modes, due to ZnO monocrystals, were in line with the XRD findings. Then, XPS was used to obtain more information on the chemical compositions and states after calcination. The high-resolution Cu 2p spectra for Cu-MOF (obtained by calcination at 500 °C) displayed the specific Cu $2p_{3/2}$ (933.9 eV) and Cu $2p_{1/2}$ (953.6 eV) peaks and also satellite peaks, from 941.4 to 943.7 eV, indicative of Cu²⁺ presence (Fig. 1g). This confirmed the XRD results and the successful synthesis of CuO without any impurity, such as Cu, Cu₂O or Cu(OH)₂. The high-resolution Ni 2p spectra of Ni-MOF (obtained by calcination at 600 °C) (Fig. 1h) included binding peaks (~851.7 and 872.1 eV), assigned to Ni 2p_{3/2} and Ni 2p_{1/2} respectively, and satellite peaks (861.1 and 879.7 eV). Deconvolution revealed that the Ni $2p_{3/2}$ and Ni $2p_{1/2}$ peaks included two peaks/each: two peaks at 853.7 and 871.0 eV (assigned to Ni²⁺, confirming NiO synthesis) and two peaks at 855.5 and 872.5 eV (assigned to Ni³⁺ [74,75] indicating Ni₂O₃ formation during calcination in air). The high-resolution Zn 2p spectra for Zn-MOF after calcination at 600 $^{\circ}$ C revealed binding peaks at \sim 1021.6 and 1044.7 eV, corresponding to Zn 2p_{3/2} and Zn 2p_{1/2}, respectively (Fig. 1i). This strongly suggests the presence of zinc ions in a divalent state (Zn^{2+}) [76, 77], in line with the ZnO phase observed by XRD. Fig. S2 shows the high-resolution O1s and C1s spectra. The deconvolution of the C1s spectrum revealed three peaks that corresponded to the C=C bond of phenyl carbons, the C–O bond, and the C=O bond. This indicated that residual carbon was still present in all samples. The O1s region of all samples was fitted in two curves related to lattice oxygen (O-M) and adsorbed oxygen (-OH), in accordance with the literature. The peaks at 529.6, 529.2, and 530.1 eV were assigned to Cu-O, Ni-O, and Zn-O bonds, respectively.

SEM and TEM analysis were employed to investigate the morphology and microstructure of the materials. Then, MOF-derived CuO after calcination at 500 °C showed the presence of some agglomerations among NPs (SEM; Fig. 2a) and of spherical NPs with a mean size of ~50-60 nm (TEM; Fig. 2b). High-resolution (HR)-TEM analysis indicated that the inter-planar lattice distance was 0.22 nm, which belongs to the (111) crystal plane of CuO (Fig. 2c). Similarly, SEM and TEM analysis of the MOF-derived NiO (calcined at 600 °C) showed some agglomeration among NPs (SEM; Fig. 2d) and the presence of NiO NPs of almost spherical shape with a mean size of \sim 25 nm (TEM; Fig. 2e). HR-TEM (Fig. 2f) revealed an inter-planar lattice distance of 0.23 nm, which belongs to the (002) crystal plane of NiO [78,79]. MOF-derived ZnO (calcined at 600 °C) was composed of small interconnected NPs with homogeneous size (SEM; Fig. 2g), in line with previous results [80]. The ZnO NPs were almost spherical with a mean size of \sim 35–45 nm (TEM; Fig. 2h). The inter-planar lattice distance was 0.24 nm, which belongs to the (101) crystal plane of ZnO (HR-TEM; Fig. 2i).

The elemental composition was assessed by EDS (Table 1). In MOFderived CuO (calcined at 500 $^{\circ}$ C), the concentrations of Cu and O elements were 76.9 and 23.1 wt%, respectively. In MOF-derived NiO (calcined at 600 $^{\circ}$ C), Ni and O elements represented 77.3 and 22.7 wt%, respectively. In MOF-derived ZnO (calcined at 600 $^{\circ}$ C), Zn and O elements were 79.1 and 20.9 wt%, respectively.

The N₂ adsorption-desorption curves of the different samples are in Fig. 3. The BET surface areas of MOF-derived CuO (calcined at 500 °C), NiO (calcined at 600 °C), and ZnO (calcined at 600 °C) were 5.48, 12.65, and 8.36 m²/g, respectively. Therefore, NiO had the highest surface area.

3.2. Gas sensing studies

3.2.1. Gas sensors based on Cu-MOF and Cu-MOF-derived CuO

After exposure to 1, 5 and 10 ppm H_2S gas (a reducing gas) at 100, 150 and 200 °C, the Cu-MOF gas sensor resistance increased (Fig. 4a). This indicates that Cu-MOF behaves like a p-type sensor. Conversely, the baseline resistance was decreased by the sensing temperature, highlighting Cu-MOF semiconducting nature. Plotting Cu-MOF response in function of the temperature (Fig. 4b) showed that at all temperatures, the response increased with the concentration of H_2S gas because more gas molecules can be adsorbed onto the sensor surface. The highest response was observed at 150 °C: 5.05, 6.12 and 7.33 in the presence of 1, 5 and 10 ppm H_2S gas, respectively.

At 100 °C, H₂S gas did not have sufficient energy to overcome adsorption barrier on the sensing surface. Also, at 200 °C, the sensor response was decreased relative to 150 °C, it can be surmised that the desorption rate was higher than the adsorption rate, leading to a decrease of the gas response [81].

The net adsorption rate was maximized at the optimal temperature, and consequently, the gas response was increased. Following exposure to 1, 5 and 10 ppm H₂S, CO or NO₂ gas at 150 °C, Cu-MOF resistance diminished in the presence of CO gas (as expected because it is a reducing gas like H₂S gas) and also of NO₂ gas (oxidizing gas) (Fig. 4d). Moreover, the Cu-MOF gas sensor response was higher when exposed to H₂S compared with CO and NO₂ gases at all three tested concentrations (Fig. 4d). For example, the responses to 10 ppm H₂S, CO and NO₂ gases were 7.33, 2.23, and 1.86, respectively.

Then, the dynamic resistance curves of CuO (obtained by calcination at 500 °C) following exposure to 1, 5 and 10 ppm H₂S at different temperatures (250–400 °C) (Fig. 5a and b) indicated that the sensor performed best at 300 °C: 14.25, 16.79, and 20.92 to 1, 5, and 10 ppm H₂S gas, respectively. This also showed that calcination at 500 °C increased the sensing activity of this sensor. In the next step, three CuO gas sensors calcined at different temperatures (400, 500 and 600 °C) were compared. Upon exposure to 1, 5 and 10 ppm H₂S gas at 300 °C (Fig. 5c and d), the best response was observed with the gas sensor calcined at 500 °C. The response to 10 ppm H₂S gas of the sensors



Fig. 2. (a), (d) and (g), SEM (b), (e), (h) TEM and (c), (f), (i) HR-TEM images of MOF-derived CuO (calcined at 500 °C), NiO (calcined at 600 °C) and ZnO (calcined at 600 °C), respectively.

Table 1

Result	ts c	of tl	he	EDS	anal	lvsis	of	MOF-d	lerived	SMOs.
						~				

Sample	Calcination temperature (°C)	Element	Amount (wt %)
MOF-derived CuO	500 °C	Cu	76.9
		0	23.1
MOF-derived NiO	600 °C	Ni	77.3
		0	22.7
MOF-derived ZnO	600 °C	Zn	79.1
		0	20.9

calcined at 400, 500 and 600 °C were 14.09, 20.92 and 12.15, respectively. Lastly, the selectivity of the CuO gas sensor calcined at 500 °C was investigated in the presence of 1, 5 and 10 ppm H₂S, CO, C₆H₆, C₂H₅OH or NO₂ gas at 300 °C (Fig. 6a and b). The responses to 10 ppm H₂S, CO, C₆H₆, C₂H₅OH and NO₂ gases were 20.92, 5.18, 2.93, 2.51 and 2.05, respectively, indicating that this sensor is highly selective towards H₂S

gas.

3.2.2. Gas sensors based on Ni-MOF and MOF-derived NiO

Then, the Ni-MOF gas sensor was exposed to 1, 5 and 10 ppm CO gas at 50–200 °C (Fig. 7a). The resistance in the presence of increasing concentrations of CO gas revealed the p-type nature of this gas sensor. In addition, the baseline resistance and resistance variations were limited. Exposure to different concentrations of CO gas and at different temperatures (Fig. 7b) showed that the best responses were obtained at 100 °C: 2.22, 2.47 and 3.02 with 1, 5 and 10 ppm CO gas, respectively. Then, selectivity was evaluated by exposure to increasing concentrations of CO, H₂S, ethanol or NO₂ gases at 100 °C (Fig. 7c and d). This experiment showed that the Ni-MOF gas sensor was more selective for CO gas. For instance, the responses were 3.02, 1.27, 1.39 and 1.33–10 ppm CO, H₂S, ethanol and NO₂ gases, respectively.

Ni-MOF samples calcined at 400, 500 and 600 $^\circ$ C in air for 2 h were used for the next experiments. First, the NiO sensor calcined at 600 $^\circ$ C



Fig. 3. N_2 adsorption-desorption curves of MOF-derived (a) CuO after calcination at 500 °C, (b) NiO after calcination at 600 °C, and (c) ZnO after calcination at 600 °C.



Fig. 4. (a) Cu-MOF gas sensor dynamic resistance curves following exposure to 1, 5 and 10 ppm H_2S gas at 100 °C, 150 °C and 200 °C. (b) Response to different H_2S concentrations in function of the temperature. (c) Cu-MOF gas sensor resistance curves following exposure to 1, 5 and 10 ppm H_2S , CO or NO₂ gas at 150 °C. (d) Response in function of the gas type and its concentration.

was exposed to 1, 5 and 10 ppm CO gas at various temperatures (250–400 °C) (Fig. 8a and b). The sensor displayed a p-type behavior, and the best response was observed at 350 °C: 6.5, 8.66 and 10.49 in the presence of 1, 5 and 10 ppm CO gas, respectively. Comparison of the responses (CO gas at 350 °C) of the three NiO gas sensors calcined at different temperatures (Fig. 8c and d) indicated that the best response was obtained with the sensor calcined at 600 °C. For instance, the responses to 10 ppm CO gas were 4.76, 5.57 and 10.49 for the sensors calcined at 400, 500 and 600 °C, respectively. Lastly, exposure of the NiO sensor calcined at 600 °C to various concentrations of CO, H₂S, H₂, ethanol and NO₂ gases at 350 °C (Fig. 9a and b) highlighted its higher sensitivity towards CO gas. For instance, the responses were 10.49, 1.54, 1.13, 1.11 and 1.22–10 ppm of CO, H₂S, H₂, ethanol and NO₂ gas, respectively.

3.2.3. Gas sensors based on Zn-MOF and MOF-derived ZnO

The Zn-MOF gas sensor was first exposed to 1, 5 and 10 ppm H_2 gas at 50–200 °C (Fig. 10a). The decrease in resistance upon exposure to H_2 gas indicated that the Zn-MOF sensor displayed an n-type behavior. The best responses were obtained at 150 °C (Fig. 10b): 3.45, 4.76 and 5.88 to 1, 5 and 10 ppm H_2 gas, respectively. Exposure to H_2 , CO and NO₂ gases at 150 °C (Fig. 10c and d) showed the higher sensitivity of the Zn-MOF gas sensor for H_2 gas (responses to 10 ppm H_2 , CO and NO₂ gases: 5.88 and 1.39 and 1.38, respectively).

Calcination of Zn-MOF at 400, 500 and 600 °C was used to obtain ZnO gas sensors. First, the gas sensor calcined at 600 °C was exposed to 1, 5 and 10 ppm H₂ gas at various temperatures (Fig. 11a). The sensor showed an n-type behavior. Then, the response curve of the gas sensor in function of the sensing temperature and H₂ gas concentration (Fig. 11b) indicated that the best response was obtained at 350 °C (10.52, 17.25 and 34.48 to 1, 5 and 10 ppm H₂, respectively). Therefore, calcination significantly increased the response to H₂ gas. Then, comparison of the response of the ZnO sensors calcined at various temperatures to different

concentrations (1, 5 and 10 ppm) of H₂ gas at 350 °C (Fig. 11c and d) indicated that calcination at 600 °C gave the best performing gas sensor (Fig. 11d). For instance, the response to 10 ppm H₂ gas were 15.04, 29.23 and 34.48 with the ZnO gas sensors obtained by calcination at 400, 500 and 600 °C, respectively. Lastly, the sensor calcined at 600 °C was exposed to 1, 5 and 10 ppm H₂, CO, ethanol, C_6H_6 and NO₂ gases at 350 °C (Fig. 12a and b). This showed that the ZnO gas sensor was more selective towards H₂ gas. For instance, the responses to 10 ppm H₂, CO, ethanol, C_6H_6 and NO₂ gases were 34.38, 2.37, 1.41, 1.31 and 1.6, respectively.

3.3. Gas sensing mechanism

When resistive gas sensors are exposed to fresh air, the oxygen gas in air with high electron affinity is adsorbed on their surfaces and takes electrons, as described in the following reactions [82]:

$$O_2(g) \rightarrow O_2(ads)$$
 (1)

$$O_2(ads) + e^- \rightarrow O_2^- T < 150 \ ^{\circ}C$$
 (2)

$$O_2^- + e^- \to 2O^- \ 150 \le T < 400 \ ^\circ C$$
 (3)

$$O^{-} + e^{-} \rightarrow O^{2-} T > 400 \ ^{\circ}C$$
 (4)

Generally, equation (2) is dominant at low operation temperatures (T < 150 °C) and equations (3) and (4) at higher temperatures, namely, $150 \le T < 400$ °C and T > 400 °C, respectively. Depending on their compositions, the gas sensors tested in this study displayed different optimal sensing temperatures (Table 2).

Therefore, the dominant oxygen species were O_2^- for MOF-based sensors because their optimal sensing temperature was 150 °C or lesser, while dominant oxygen species were O^- for MOF-derived SMO-based gas sensors. In the presence of air and electron abstraction by



Fig. 5. (a) Dynamic resistance curves of the MOF-derived CuO gas sensor (obtained by calcination at 500 °C) in the presence of 1, 5 and 10 ppm H₂S gas and the indicated temperatures; (b) Response of the gas sensor in function of the sensing temperature and H₂S concentration. (c) Resistance curves and (d) response to 1, 5 and 10 ppm H₂S gas at 300 °C of CuO gas sensors obtained by calcination at 400, 500 or 600 °C.



Fig. 6. (a) Dynamic Resistance curves of the MOF-derived CuO sensor (obtained by calcination at 500 °C) in the presence of 1, 5 and 10 ppm of the indicated gases at 300 °C. (b) Corresponding selectivity graph.



Fig. 7. (a) Dynamic resistance curves of the Ni-MOF gas sensor in the presence of 1, 5 and 10 ppm CO gas at the indicated temperatures. (b) Response curves in function of the temperature and CO gas concentration. (c) Dynamic resistance of the Ni-MOF gas sensor in the presence of 1, 5 and 10 ppm of CO, H_2S , ethanol and NO_2 gases at 100 °C. (d) Corresponding selectivity graphs.

oxygen ions, an electron depletion layer is formed on the surface of ntype sensors (Table 2), in which the amount of electrons is lower than that in the core regions, and accordingly, the sensor resistance is higher compared with the vacuum condition [83]. For p-type gas sensors (Table 2), as a result of the abstract of electrons, a hole accumulation layer is formed on the sensor surface, resulting in the formation of a hole-rich layer that ultimately leads to lower resistance in air compared with the vacuum condition [84]. Upon exposure to reducing gases such as CO, H₂S and H₂, the following reactions are expected [85]:

$$CO + O^{-} \rightarrow CO_{2} + e T = 100 \ ^{\circ}C \tag{5}$$

 $2CO + O_2^- \rightarrow 2CO_2 + e T = 350 \ ^\circ C$ (6)

 $2H_2 + O_2 \rightarrow 2H_2O + e T = 150 \ ^{\circ}C$ (7)

$$H_2 + O^- \rightarrow H_2O + e T = 350 \ ^{\circ}C$$
 (8)

 $2H_2S + 3O_2^- \rightarrow 2SO_2 + 2H_2O + 3e T = 150 \ ^\circ C$ (9)

 $H_2S+3O^- \rightarrow SO_2+H_2O+3e T = 300 \ ^{\circ}C$ (10)

Although MOF-based sensors had a larger surface area compared with SMO-derived gas sensors, their sensing performance was weaker, possibly due to the lower charge carrier mobility. Also, as all tested MOF-based gas sensors had low baseline resistance values in air (<20 $k\Omega$), no significant resistance variation was occurred in the presence of target gases, resulting in a low response. In addition, the non-covalent interactions gases occurring on the surface of MOF-based gas sensors (*i.e.* van der Waals forces, hydrogen bonding, and π - π interactions) led to minimal electrical resistance change [86] In SMO-based gas sensors, the higher charge carrier mobility and baseline resistance values led to larger resistance variations upon exposure to gases and consequently higher responses were observed.

Each SMO-based sensor exhibited selectivity towards a specific gas (Table 2). The high selectivity towards H_2S gas observed for the MOFderived CuO sensor can be mainly related to conversion of CuO to CuS in the presence of H_2S , as follows [87].

$$CuO + H_2S \rightarrow CuS + H_2O(g) \tag{11}$$

According to the above reaction, H_2S can directly react with semiconducting CuO and convert it to CuS with high metallic-like conductivity. Previously, the formation of CuS upon exposure of CuO to H_2S gas has been demonstrated by theoretical models or experimental evidence [88–91]. Therefore, in the presence of H_2S gas, the electrical resistance significantly changes, explaining the higher selectivity towards this gas. It should be noted that equation (9) is valid when other SMOs, such as NiO, are exposed to H_2S gas; however, for CuO, the main reaction can be assumed to be the one described in equations (9) and (10).



Fig. 8. Resistance changes of the NiO gas sensor calcined at 600 $^{\circ}$ C to 1, 5 and 10 ppm CO gas at 250, 300, 350 and 400 $^{\circ}$ C. (b) Response curves in function of the sensing temperature and CO concentration. (c) Resistance curves and (d) response of the NiO gas sensors in function of the calcination temperature and CO gas concentration at 350 $^{\circ}$ C.



Fig. 9. (a) Resistance curves of the MOF-derived NiO sensor obtained by calcination at 600 °C to the indicated gases at 350 °C. (b) Corresponding selectivity graph.

The MOF-derived ZnO sensor displayed high selectivity towards H_2 gas that can be related to the highly reducing nature of H_2 gas and the formation of metallic Zn with higher conductivity compared with Zn on

the surface of ZnO at the sensing temperature [92]. ZnO + H₂ \rightarrow Zn(s) + H₂O(g)

(12)



Fig. 10. (a) Resistance curves of the Zn-MOF gas sensor upon exposure to 1, 5 and 10 ppm H_2 gas at the indicated temperatures. (b) Response curve in function of H_2 gas concentration and temperature. (c) Resistance curves of the Zn-MOF gas sensor to the indicated gases at 150 °C. (d) Corresponding selectivity graphs.

This explains the higher selectivity towards H_2 gas compared with other gases.

Also, the MOF-derived NiO sensor was more selective towards CO gas, mainly due to the good catalytic activity of NiO towards CO gas [93] and easy oxidation of CO to CO_2 gas on NiO surface at the sensing temperature.

Although some surface residual carbons were detected by XPS, their effects on the sensing mechanism were not significant because they did not form a major phase in the XRD profiles. However, the oxygen species attached to residual carbons could participate in the sensing reactions.

Table 3 compares the H_2S , H_2 , and CO gas sensing properties of the present work with those reported in the literature. Overall, it can be seen that the response values obtained in the present study are comparable and even, in most cases better than those reported in the literature.

4. Conclusions

M-MOFs (M = Cu, Ni and Zn) and MOF-derived CuO, NiO and ZnO SMOs were synthesized for gas sensing studies. The morphological and structural analyses confirmed the synthesis of metal oxides with the desired morphology, chemical composition and phases. The gas sensing studies revealed the better performance of the MOF-derived metal oxides compared with their MOF templates, but at higher optimal sensing temperatures. Moreover, the MOF-derived metal oxide sensing performance was influenced by their calcination temperature. Indeed, the best selectivity towards H_2S , CO and H_2 gases were obtained with CuO, NiO and ZnO gas sensors calcined at 500, 600 and 600 °C, respectively. This

research represents a significant advancement in the field of gas sensor technology, offering innovative MOF-derived metal oxide sensors with tailored properties for precise and reliable gas detection in various industrial and environmental settings. Future studies should investigate the fabrication of sensor arrays to easily detect the different gases present in a gas mixture.

CRediT authorship contribution statement

Carmen Montoro: Writing - original draft, Validation, Investigation, Formal analysis, Data curation, Conceptualization. Jin-Young Kim: Writing - original draft, Methodology, Investigation, Formal analysis, Data curation. Ali Mirzaei: Writing - original draft, Validation, Methodology, Investigation, Formal analysis, Data curation, Conceptualization. Jae-Hyoung Lee: Writing - review & editing, Validation, Methodology, Investigation, Formal analysis, Data curation, Conceptualization. Syreina Sayegh: Writing - review & editing, Validation, Methodology, Formal analysis, Data curation. Elissa Makhoul: Writing - review & editing, Validation, Methodology, Investigation, Formal analysis, Data curation. Igor Iatsunskyi: Writing - review & editing, Validation, Methodology, Investigation, Formal analysis, Data curation. Emerson Coy: Writing - review & editing, Validation, Methodology, Investigation, Formal analysis, Data curation. Mikhael Bechelany: Writing - review & editing, Validation, Supervision, Resources, Project administration, Methodology, Funding acquisition, Conceptualization. Hyoun Woo Kim: Writing - review & editing, Validation, Supervision, Resources, Funding acquisition, Conceptualization. Sang Sub Kim:



Fig. 11. Resistance changes of the MOF-derived ZnO gas sensor obtained by calcination at 600 °C to 1, 5 and 10 ppm H₂ gas at the indicated sensing temperatures. (b) Response curve in function of the sensing temperature and H₂ concentration. (c) Resistance curves and (d) Response of the ZnO gas sensors obtained by calcination at 400, 500 and 600 °C to 1, 5 and 10 ppm H₂ gas at 350 °C.



Fig. 12. (a) Resistance curves of the MOF-derived ZnO sensor obtained by calcination at 600 °C to 1, 5 and 10 ppm H₂, CO, ethanol, C₆H₆ and NO₂ gas at 350 °C. (b) Corresponding selectivity graph.

Table 2

Optimal sensing temperature, selectivity and conductivity type of the different gas sensors tested in this study.

Sensor	Optimal temperature (°C)	Selectivity	Conductivity
Cu-MOF	150	H ₂ S gas (low selectivity)	p-type
MOF-derived CuO calcined at 500 °C	300	H ₂ S gas (high selectivity)	
Ni-MOF	100	CO gas (low selectivity)	
MOF-derived NiO calcined at 600 °C	350	CO gas (high selectivity)	
Zn-MOF	150	H_2 gas (low selectivity)	n-type
MOF-derived ZnO calcined at 600 °C	350	H ₂ gas (high selectivity)	

Table 3

Comparison of H_2S , H_2 and CO gas sensing properties of present work with those reported in the literature.

Material	Gas and conc. (ppm)	T (°C)	Response (R_a / R_g) or (R_g / R_a)	Ref.
MOF-derived CuO calcined	H ₂ S (10)	300	20.92	This work
MOF-derived ZnO–CuO composite	H ₂ S (10)	350	~12	[94]
MOF-derived Ru-doped Fe ₂ O ₃ hollow nanobox	H ₂ S (10)	200	~11	[95]
MOF-derived CuFe ₂ O ₄ NPs	H ₂ S (50)	210	210	[96]
MOF-derived Co ₃ O ₄ / NiCo ₂ O ₄	H ₂ S (50)	~6	225	[97]
MOF-derived Co ₃ O ₄ /ZnO	H ₂ S (10)	5	250	[<mark>98</mark>]
MOF-derived ZnO calcined	H ₂ (10)	350	34.48	This
at 600 °C				work
MOF-derived WO ₃ -C/In ₂ O ₃ heterostructures	H ₂ (200)	250	4.19	[99]
Au-decorated ZnO	H ₂ (100)	230	37.6	[100]
Pt-decorated ZnO	H ₂ (15)	250	~6 (I _g /I _a)	[101]
Ag-decorated ZnO	H ₂ (300)	250	~5	[102]
ZnO nanorod arrays	H ₂ (2000)	225	~25	[103]
MOF-derived NiO calcined	CO (10	350	10.49	This
at 600 °C	ppm)			work
MOF-derived NiO/SnO ₂	CO (10 ppm)	25	2.5	[104]
MOF-derived porous In ₂ O ₃ / Fe ₂ O ₃ core–shell nanotubes	CO (200 ppm)	260	33.7	[105]
MOF-derived SnO ₂ /MoSe ₂ composite	CO (200 ppm)	25	10 % [($R_a - R_g$)/ $R_a \times 100$ %]	[106]
Co_3O_4 $@$ TiO ₂ nanocomposite	CO (100 ppm)	140	16	[107]
CuO/TiO ₂ heterojunction	CO (800 ppm)	250	~9	[108]

Writing – review & editing, Validation, Supervision, Resources, Methodology, Funding acquisition, Conceptualization.

Declaration of Competing interest

We declare no interest.

Data availability

Data will be made available on request.

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Appendix A. Supplementary data

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