### **TEX-MOX experiments:**

# final design of critical experiments to mimic MOX fuel in low moderation conditions

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#### [ INTRODUCTION

[ REPRESENTATIVITY OF INDUSTRIAL CASES USING THE K<sub>EFF</sub> SENSITIVITY TO NUCLEAR DATA

[ THERMO-MECHANICAL DESIGN



#### **TEX-MOX experiments**

#### MOX FUEL CYCLE

IRS

Criticality safety issue with low moderated **MOX powder** mixtures

General lack in **intermediate energy** range critical configurations

#### **DESIGN OF EXPERIMENTS**

- Collaboration with american NCSP (Nuclear Criticality Safety Programm)
- Neutronic optimisation to target the maximum sensitivity in the intermediate energy range using PUMN and PUMH fuel plates (from ZPPR experiments)
- Polyethylene selected as moderator and reflector

Fuel Name	Description	Alloy (wt% of Fuel)	<sup>240</sup> <b>Pu</b> (wt% of Pu)	<b>Pu</b> (wt% of U+Pu)	<sup>235</sup> U (wt% of U)
PUMN	Pu-U-Mo-NUMEC	2.5	11.6	28.8	0.2
PUMH	PUM-High Pu240 content	2.5	26.4	34.9	0.2







#### **3 TEX-MOX experiments planned at NCERC<sup>§</sup> for 2025**

Case	Mod. Thickness [cm]	Layers pattern	Reflector thicknesses axial/radial [cm]	Keff	Thermal fission rate (%)	Inter. fission rate (%)	Fast fission rate (%)	Expected exp. Uncertainty*
INTER1	0.36	25 full PUMN	7/1.5	1.00815	20.80	45.70	33.50	200 pcm
INTER2	0.7	4 full PUMN 10 partial <b>PUMH</b> 2 full PUMN	7.5/1.5	1.00972	37.54	37.87	24.59	167 pcm
THERM	2.6	2 full PUMN 4 partial <b>PUMH</b> 1 full PUMN	7.5/1.5	1.02146	68.38	18.11	13.51	126 pcm

- Thick axial reflector increased to cut the room effect
- Radial reflector: trade off between room effect and neutron thermalization
- Only limited number of PUMH (High Pu240 content) available -> in the center to maximize the sensitivity to Pu240

Designs selected as the most « representative » of industrial cases

- <sup>§</sup> NCERC : National Criticality Experiments Research Center (NCERC), Nevada, USA
- \* Fuel composition measurements are not yet satisfying, may increase the total uncertainty



#### **3 TEX-MOX experiments planned at NCERC for 2025**

Inter1

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**PUMN** layer







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#### **Representativity study**

Similarity coefficient C<sub>k</sub>, that represents the similarity between two cases for a given nuclear data covariance matrix, is calculated with the TSURFER tool from SCALE 6.2 suite using the 44 energy groups covariance data of ENDFB-7.0 library. It is defined as follows:

Summed as follows.  $C_{lm} \text{ is the similarity coefficient between case / and case } m: C_{lm} = \frac{S_{L}^{T}C_{\alpha\alpha}S_{m}}{\sigma_{l}\sigma_{m}}$  nuclear data covariance matrix  $C_{lm} = \frac{S_{L}^{T}C_{\alpha\alpha}S_{m}}{\sigma_{l}\sigma_{m}}$   $\text{uncertainty on the } k_{eff} \text{ on the case } l \text{ or } m \text{ due to nuclear data}$ 

**Shared sensitivity ratio (SS)** provides the part of the sensitivity profile of the application case that is also present in the experiment configuration.

 $SS_{12} = \frac{\sum_{i,r} \sum_{Eg} \left\{ if S_1^{i,r,Eg} S_2^{i,r,Eg} > 0: min(\left|S_1^{i,r,Eg}\right|, \left|S_2^{i,r,Eg}\right|) - \frac{else:0}{\sum_{i,r} \sum_{Eg} \left|S_1^{i,r,Eg}\right|} \right\}}{\sum_{i,r} \sum_{Eg} \left|S_1^{i,r,Eg}\right|}$ 

*SS independant of the nuclear data covariances current knowledge* 

 $S_1^{i,r,Eg}$  k<sub>eff</sub> sensitivity values for the isotope *i*, reaction *r*, energy group *Eg of the case 1* 

*If the sensitivities of the two cases have opposite signs, nothing is added to the ratio.* 

#### **Representativity study**

#### 4 application cases with PuO2 and/or MOX in the intermediate energy range

Analysis looking at integral indicators (	all isotopes and reactions
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SSR	INTER1	INTER2
General_sphere_puo2	0.63	0.59
Storage_mox_puo2	0.61	0.49
Storage_puo2	0.56	0.58
Container_mox	0.66	0.66

The highest SS ratios are in bold

Ck	INTER1	INTER2
General_sphere_puo2	0.87	0.84
Storage_mox_puo2	0.87	0.75
Storage_puo2	0.81	0.79
Container_mox	0.92	0.88
	C <sub>k</sub> > 0.8	

Analysis looking at main isotope-reaction indicators						
239Pu fission	SS ratio	C <sub>k</sub>	240Pu capture	SS ratio	C <sub>k</sub>	
	INTER1	INTER1		INTER2	INTER2	
General_sphere_puo2	0.95	0.99	General_sphere_puo2	0.76	0.91	
Storage_mox_puo2	0.85	0.91	Storage_mox_puo2	0.81	0.66	
Storage_puo2	0.94	0.98	Storage_puo2	0.94	0.99	
Container_mox	0.95	0.99	Container_mox	0.91	0.99	

Conclusion:

- INTER1 very representative for 4 intermediate appl. cases for **global Ck et SS ratio + Pu239 fission**
- INTER2 representative for Pu240 capture (especially for SS ratio)



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#### **Temperature challenge**

#### DECAY HEAT PRODUCED BY THE FUEL PLATES

#### Temperature increase in the stack $< \Delta T = 40^{\circ}C$ without any active cooling

- with T<sub>room</sub> ~20° C, stack @60°C
- OK for safety (polyethylene fusion temperature ~100°C)
- Not optimal for a clean benchmark (thermal gradient, thermal expansion, misalignment of elements

# Active cooling system was introduced to produce high-quality benchmarks

- Average temperature < 30 °C (or 40°C)</li>
- Thermal gradient within the assembly < 15°C</li>



1/4 of the fuel assembly : polyethylene temperature





#### Measure the temperature gradients

- 25 Fiber Bragg Grating (FBG) sensors
- To measure the temperature gradient within the assembly
- Sensitive length : 456 mm
- 10 FBG placements each 5 cm





#### **Perspectives**

#### **3 CRITICAL TEX-MOX EXPERIMENTAL CONFIGURATIONS ARE PLANNED TO BE EXECUTED IN FY2025 IN USA**

Next week a campaign of measurements will be performed on the prototype at LANL

- No nuclear material
- Heating source to mimic the decay heat
- To test cooling capacities and the measurement devices
- Participation of IRSN staff



Air entrance

4 air extraction tubes for 4 layers



Polyethylene moderator

Thank you for your attention

#### ご清聴ありがとうございました

## 質問はありますか

