

Stacked Intelligent Metasurface Performs a 2D DFT in the Wave Domain for DOA Estimation

Jiancheng An, Chau Yuen, Yong Liang Guan, Marco Di Renzo, Mérouane Debbah, H Vincent Poor, Lajos Hanzo

► To cite this version:

Jiancheng An, Chau Yuen, Yong Liang Guan, Marco Di Renzo, Mérouane Debbah, et al.. Stacked Intelligent Metasurface Performs a 2D DFT in the Wave Domain for DOA Estimation. ICC 2024 - IEEE International Conference on Communications, Jun 2024, Denver, United States. pp.3445 - 3451, 10.1109/icc51166.2024.10622963. hal-04734249v1

HAL Id: hal-04734249 https://hal.science/hal-04734249v1

Submitted on 20 Oct 2024 (v1), last revised 11 Nov 2024 (v2)

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers. L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

Stacked Intelligent Metasurface Performs a 2D DFT in the Wave Domain for DOA Estimation

Jiancheng An*, Chau Yuen*, Yong Liang Guan*, Marco Di Renzo[†], Mérouane Debbah[‡],

H. Vincent Poor[§], and Lajos Hanzo[¶]

*School of Electrical and Electronics Engineering, Nanyang Technological University, Singapore 639798

[†]CNRS, CentraleSupélec, Laboratoire des Signaux et Systèmes, Université Paris-Saclay,

91192 Gif-sur-Yvette, France

[‡]Center for 6G Technology, Khalifa University of Science and Technology,

P O Box 127788, Abu Dhabi, United Arab Emirates

[§]Department of Electrical and Computer Engineering, Princeton University, Princeton, NJ 08544 USA

[¶]School of Electronics and Computer Science, University of Southampton, SO17 1BJ Southampton, U.K.

E-mail: {jiancheng.an, chau.yuen, eylguan}@ntu.edu.sg, marco.di-renzo@universite-paris-saclay.fr,

merouane.debbah@ku.ac.ae, poor@princeton.edu, lh@ecs.soton.ac.uk

Abstract-Staked intelligent metasurface (SIM) based techniques are developed to perform two-dimensional (2D) directionof-arrival (DOA) estimation. In contrast to conventional designs, an advanced SIM in front of a receiver array automatically performs the 2D discrete Fourier transform (DFT) as the incident waves propagate through it. To arrange for the SIM to carry out this task, we design a gradient descent algorithm for iteratively updating the phase shift of each meta-atom in the SIM to minimize the fitting error between the SIM's response and the 2D DFT matrix. To further improve the DOA estimation accuracy, we configure the phase shifts in the input layer of the SIM to generate a set of 2D DFT matrices having orthogonal spatial frequency bins. Extensive numerical simulations verify the capability of a well-trained SIM to perform the 2D DFT. Specifically, it is demonstrated that a SIM having an optical computational speed achieves an MSE of 10^{-4} in 2D DOA estimation.

Index Terms—Stacked intelligent metasurface (SIM), directionof-arrival (DOA) estimation, reconfigurable intelligent surface, wave-based computing.

I. INTRODUCTION

D IRECTION-OF-ARRIVAL (DOA) estimation has long been a crucial task in applications such as astronomy, navigation, and radar sensing systems [1]–[4]. Traditionally, the DOAs have been estimated using beamforming relying on the fast Fourier transform (FFT) technique [5], [6]. However, beamforming has a limited angular resolution, which is fundamentally restricted by the Rayleigh criterion [7]. To address this problem, several super-resolution DOA estimation approaches have been developed such as MUSIC and ESPRIT [1]–[3]. While these methods provide significant performance advantages, they require potentially excessive computational and storage resources to carry out the eigenvalue decomposition of the spatial covariance matrix. Additionally, their performance erodes when only a small number of snapshots are available.

Moreover, practical systems generally face various imperfections such as station location errors, which are impervious to accurate modeling and calibration using conventional methods [8], [9]. Fortunately, advanced machine learning (ML) techniques are capable of accurately estimating the DOAs. In contrast to conventional model-based methods, data-driven ML-based approaches are more robust against practical array imperfections. Nevertheless, traditional DNNs rely on commercial processors or dedicated chips to perform computations, whose speed is limited by digital hardware. Motivated by advances in metasurface technologies and the radical wavebased computing paradigm [10]-[14], Liu et al. [15] fabricated a reconfigurable diffractive deep neural network (D^2NN) using a stacked intelligent metasurface (SIM) for large-scale parallel calculations and analog signal processing that is performed at the speed of light [16]. Specifically, a SIM employs an array of metasurface layers, each containing many programmable meta-atoms that can manipulate the EM behavior, as the waves pass through it. Adapting the bias voltage via a customized field-programmable gate array (FPGA) module allows each meta-atom to act as a reprogrammable artificial neuron having tunable weights.

Inspired by this advanced architecture, the authors of [17] harnessed SIM to implement holographic multiple-input multiple-output (MIMO) communications [18]. In contrast to conventional MIMO designs, a pair of SIMs deployed at the transmitter and receiver can automatically accomplish MIMO transmit precoding and receive combining as the EM waves propagate through them. This allows each spatial stream to be directly radiated and recovered from its corresponding transmit and receive ports, while significantly reducing the number of radio frequency (RF) chains needed. Furthermore, the authors of [19], [20] harnessed a SIM at the BS to facilitate the implementation of downlink multiuser beamforming in the EM wave domain. This eliminates the need for conventional

TABLE I LIST OF SYMBOLS AND THEIR MEANINGS

Symbols	Meanings
$d_{\rm x}, d_{\rm y}$	The element spacing in the x - and y -directions.
$N_{\rm x}, N_{\rm y}$	The number of meta-atoms in the x - and y -directions.
ϑ, φ	The elevation and azimuth angles of the DOA.
$\psi_{\rm x}, \psi_{\rm y}$	The electrical angles in the x - and y -directions.
$oldsymbol{a}\left(\psi_{X},\psi_{Y} ight)$	The steering vector.
$\xi_{l,m}$	The phase shift of the m -th meta-atom on the l -th layer.
$oldsymbol{v}_l$	The transmission coefficient vector for the <i>l</i> -th layer.
\mathbf{r}_l	The transmission coefficient matrix for the <i>l</i> -th layer.
$oldsymbol{W}_l$	The propagation matrix between adjacent layers.
G	The overall response of the SIM.
F	The 2D DFT matrix.
β	The scaling factor.

digital beamforming and for high-resolution digital-to-analog converters (DACs) at the BS.

Nevertheless, DOA estimation using an advanced SIM remains unexplored. Against this background, we design a new SIM-based physical DOA estimator. The philosophy behind the proposed estimator is that by optimizing the SIM, the incident EM waves can be transformed into the angular domain as they propagate through it. As a result, the direction of the signals can be readily estimated by detecting the energy levels at different receiver probes. This SIM-based system concept substantially simplifies the receiver hardware, since no analogto-digital converters (ADC) are required. Most remarkably, the calculation in the SIM occurs naturally as the waves propagate through it without incurring a processing delay.

II. SIM-BASED ARRAY SYSTEM MODEL

In this section, we present the system model for the SIMbased array used for DOA estimation. For the sake of convenience, Table I summarizes the main symbols used throughout this paper.

A. Incident Signal Model

As depicted in Fig. 1, we utilize a uniform planar array (UPA) placed on the ground (i.e., the x-y plane) for estimating the DOA parameters. In contrast to conventional array systems, a SIM consisting of (L + 1) metasurface layers is integrated with the UPA to transform the incident signal into its angular domain. We assume that the SIM is positioned horizontally, with all metasurface layers parallel to the x-y plane. To avoid ambiguity, the metasurface layers are labeled by $0 \sim L$ from the top to the bottom, as shown in Fig. 1. Let $\varphi \in [0, 2\pi)$ and $\vartheta \in [0, \pi/2]$ represent the physical azimuth angle and elevation angle of the DOA of the radiation source relative to the input layer of the SIM, which has $N = N_x N_y$ meta-atoms, with N_x and N_y representing the number of meta-atoms in the x-and y-directions, respectively. Additionally, the corresponding

element spacings are d_x and d_y . Therefore, the electrical angles ψ_x and ψ_y in the *x*- and *y*-directions are given by [21]

$$\psi_{\mathbf{x}} = \kappa d_{\mathbf{x}} \sin\left(\vartheta\right) \cos\left(\varphi\right),\tag{1}$$

$$\psi_{\mathbf{y}} = \kappa d_{\mathbf{y}} \sin\left(\vartheta\right) \sin\left(\varphi\right),\tag{2}$$

respectively, where $\kappa = 2\pi/\lambda$ represents the wavenumber, with λ being the wavelength.

Hence, the steering vector $\boldsymbol{a}(\psi_x, \psi_y) \in \mathbb{C}^{N \times 1}$ with respect to (*w.r.t.*) the input layer of the SIM is written as

$$\boldsymbol{a}\left(\psi_{\mathrm{x}},\psi_{\mathrm{y}}\right) = \boldsymbol{a}_{\mathrm{y}}\left(\psi_{\mathrm{y}}\right) \otimes \boldsymbol{a}_{\mathrm{x}}\left(\psi_{\mathrm{x}}\right),\tag{3}$$

and the elements of the vectors $\boldsymbol{a}_{x}(\psi_{x}) \in \mathbb{C}^{N_{x} \times 1}$ and $\boldsymbol{a}_{y}(\psi_{y}) \in \mathbb{C}^{N_{y} \times 1}$ are defined as follows:

$$\boldsymbol{a}_{\mathbf{x}}\left(\psi_{\mathbf{x}}\right)]_{n_{\mathbf{x}}} \triangleq e^{j\psi_{\mathbf{x}}(n_{\mathbf{x}}-1)}, \quad n_{\mathbf{x}}=1, 2, \cdots, N_{\mathbf{x}}, \qquad (4)$$

$$\left[\boldsymbol{a}_{\mathbf{y}}\left(\psi_{\mathbf{y}}\right)\right]_{n_{\mathbf{y}}} \triangleq e^{j\psi_{\mathbf{y}}(n_{\mathbf{y}}-1)}, \quad n_{\mathbf{y}} = 1, 2, \cdots, N_{\mathbf{y}}.$$
(5)

Let $s \in \mathbb{C}$ represent the signal transmitted from the radiation source, which is modeled as a circularly symmetric complex Gaussian (CSCG) random variable with zero mean and unit variance. Hence, the signal $x \in \mathbb{C}^{N \times 1}$ incident upon the input layer of the SIM can be expressed as

$$\boldsymbol{x} = \boldsymbol{a} \left(\psi_{\mathbf{x}}, \psi_{\mathbf{y}} \right) \boldsymbol{s}. \tag{6}$$

B. SIM Model

Fig. 1(b) shows the schematic diagram of a SIM device. For the sake of brevity, we assume that each of the L intermediate metasurface layers is modeled as a UPA obeying isomorphic arrangements. Additionally, we assume that the (L + 1) metasurfaces are evenly spaced. Let T_{SIM} represent the thickness of the SIM. Then, the vertical spacing between adjacent layers is $s_{\text{layer}} = T_{\text{SIM}}/L$. In practice, the SIM is enclosed in a supporting structure surrounded by wave-absorbing material to reduce the interference from undesired sources of diffraction and scattering [15]. Furthermore, each metasurface layer consists of $M = M_x M_y$ meta-atoms, where M_x and M_y are the number of meta-atoms in the x- and y-directions, respectively. Moreover, the corresponding spacings between the adjacent meta-atoms on the intermediate layers are denoted by s_x and s_y .

Moreover, each meta-atom is capable of adjusting the phase shift of the EM waves passing through it by controlling the bias voltage of the associated circuit [15], [17], [20]. Let $v_l = [v_{l,1}, v_{l,2}, \dots, v_{l,M}]^T \in \mathbb{C}^{M \times 1}, \ l = 1, 2, \dots, L$ represent the complex-valued transmission coefficient vector for the *l*-th layer, where $v_{l,m} = e^{j\xi_{l,m}}, \ m = 1, 2, \dots, M, \ l =$ $1, 2, \dots, L$ with $\xi_{l,m} \in [0, 2\pi)$ representing the phase shift of the *m*-th meta-atom on the *l*-th layer [17]. Furthermore, let $\Upsilon_l = \text{diag}(v_l) \in \mathbb{C}^{M \times M}$ represent the corresponding transmission coefficient matrix for the *l*-th layer. In particular, let $v_0 = [v_{0,1}, v_{0,2}, \dots, v_{0,N}]^T \in \mathbb{C}^{N \times 1}$ and $\Upsilon_0 = \text{diag}(v_0) \in$



Fig. 1. Illustration of a SIM-based radar system, where the SIM performs 2D DFT in the wave domain. The receiver array directly observes the angular spectrum of the incident signal.

 $\mathbb{C}^{N \times N}$ denote the complex-valued transmission coefficient vector and the corresponding matrix for the input layer, respectively, where we have $v_{0,n} = e^{j\xi_{0,n}}$, $n = 1, 2, \dots, N$ and $\xi_{0,n}$ denotes the phase shift of the *n*-th meta-atom on the input layer.

Furthermore, let $W_l \in \mathbb{C}^{M \times M}$, $l = 1, 2, \dots, L-1$ be the matrix that characterizes the EM wave propagation between adjacent layers in the SIM. Based on the Rayleigh-Sommerfeld diffraction equation [17], the attenuation coefficient $[W_l]_{m,\check{m}}$ from the \check{m} -th meta-atom on layer l to the m-th meta-atom on layer (l+1) is formulated as follows:

$$\left[\boldsymbol{W}_{l}\right]_{m,\breve{m}} = \frac{A_{\text{meta-atom}}s_{\text{layer}}}{2\pi d_{m,\breve{m}}^{3}} \left(1 - j\kappa d_{m,\breve{m}}\right)e^{j\kappa d_{m,\breve{m}}}, \quad (7)$$

where $A_{\text{meta-atom}}$ denotes the area of each meta-atom, and $d_{m,\tilde{m}}$ represents the corresponding propagation distance, which is calculated as follows:

$$d_{m,\breve{m}} = \sqrt{\left(m_{\rm x} - \breve{m}_{\rm x}\right)^2 s_{\rm x}^2 + \left(m_{\rm y} - \breve{m}_{\rm y}\right)^2 s_{\rm y}^2 + s_{\rm layer}^2}, \quad (8)$$

with m_y and m_x being defined as $m_y \triangleq \lceil m/M_x \rceil$ and $m_x \triangleq m - (m_y - 1) M_x$. Similarly, \breve{m}_y and \breve{m}_x are obtained by replacing m with \breve{m} .

Furthermore, let $W_0 \in \mathbb{C}^{M \times N}$ represent the attenuation coefficient matrix between the input layer and the first layer. The (m, n)-th entry of W_0 is obtained by replacing $d_{m,\tilde{m}}$ in (7) with the corresponding propagation distance $\tilde{d}_{m,n}$. The value of $\tilde{d}_{m,n}$ can be readily calculated according to the array layout seen in Fig. 1(a). Similarly, let $W_L \in \mathbb{C}^{N \times M}$ represent the attenuation coefficient matrix between the *L*-th metasurface layer and the output layer, i.e., the receive antenna array. The receiver is a UPA arranged in the same pattern as the input layer of SIM, and it is placed at a distance s_{layer} far away from the *L*-th layer. Because of the identical layer spacing and the isomorphic arrangement of the input and output layers, it is readily seen that $W_L = W_0^T$. As a result, the overall forward propagation through the SIM $G \in \mathbb{C}^{N \times N}$ is described as:

$$\boldsymbol{G} = \boldsymbol{W}_{L} \boldsymbol{\Upsilon}_{L} \boldsymbol{W}_{L-1} \cdots \boldsymbol{W}_{2} \boldsymbol{\Upsilon}_{2} \boldsymbol{W}_{1} \boldsymbol{\Upsilon}_{1} \boldsymbol{W}_{0}.$$
(9)

C. Received Signal Model

As mentioned earlier, the receiver has a UPA consisting of $N = N_x N_y$ receiver antennas. For a single source transmitting a waveform *s*, the complex signal vector $\boldsymbol{r} \in \mathbb{C}^{N \times 1}$ received at the array can be expressed as:

$$\boldsymbol{r} = \sqrt{\rho} \boldsymbol{G} \boldsymbol{\Upsilon}_0 \boldsymbol{x} + \boldsymbol{u} = \sqrt{\rho} \boldsymbol{G} \boldsymbol{\Upsilon}_0 \boldsymbol{a} \left(\psi_{\mathbf{x}}, \psi_{\mathbf{y}} \right) \boldsymbol{s} + \boldsymbol{u}, \qquad (10)$$

where ρ represents the signal-to-noise ratio (SNR), and $\boldsymbol{u} \in \mathbb{C}^{N \times 1}$ is the measurement noise vector at the receiver array, which is modeled as a CSCG random vector satisfying $\boldsymbol{u} \sim C\mathcal{N}(\boldsymbol{0}, \boldsymbol{I}_N)$. It is also assumed that *s* and *u* are uncorrelated.

Note that in contrast to a conventional array, the received signal in (10) is processed by a controllable analog transformation carried out by the SIM. By appropriately configuring the phase shifts applied by the meta-atoms in the SIM, the receiver antenna array has the potential to directly observe the angular spectrum of the incident signal.

III. SIM OPTIMIZATION FOR REALIZING THE 2D DFT

Achieving the expected DOA estimation capability requires configuring the SIM to output the angular spectrum of the incident signal. In this section, we formulate an optimization problem for using the SIM to implement the 2D DFT in the wave domain, and devise a gradient descent algorithm for finding a high-quality suboptimal solution for the phase shifts.

A. Optimization Problem

Specifically, for the 2D DFT matrix $F \in \mathbb{C}^{N \times N}$ having $N = N_x N_y$ grid points, its (n, \check{n}) -th entry is defined as follows:

$$f_{n,\breve{n}} = \left[\boldsymbol{F} \right]_{n,\breve{n}} \triangleq e^{-j2\pi \frac{(n_{x}-1)(\breve{n}_{x}-1)}{N_{x}}} e^{-j2\pi \frac{(n_{y}-1)(\breve{n}_{y}-1)}{N_{y}}}, \quad (11)$$

where n_y and n_x are defined as $n_y \triangleq \lceil n/N_x \rceil$ and $n_x \triangleq n - (n_y - 1) N_x$, respectively, while \breve{n}_y and \breve{n}_x are obtained by replacing n with \breve{n} .

To evaluate the similarity between the response of the SIM and the 2D DFT matrix, the loss function \mathcal{L} is defined as the Frobenius norm of the fitting error between the target entry and the EM response of the SIM, yielding

$$\mathcal{L} = \|\beta \boldsymbol{G} - \boldsymbol{F}\|_F^2, \qquad (12)$$

where $\beta \in \mathbb{C}$ represents a scaling factor required for helping the response of the SIM at the normalized value required.

Aiming at minimizing the loss function in (12), the optimization problem constructed for utilizing the SIM to fit the 2D DFT matrix is formulated as:

$$\min_{\{\xi_{l,m}\}} \quad \mathcal{L} = \|\beta \boldsymbol{G} - \boldsymbol{F}\|_F^2 \tag{13a}$$

s.t.
$$\boldsymbol{G} = \boldsymbol{W}_L \boldsymbol{\Upsilon}_L \boldsymbol{W}_{L-1} \cdots \boldsymbol{W}_2 \boldsymbol{\Upsilon}_2 \boldsymbol{W}_1 \boldsymbol{\Upsilon}_1 \boldsymbol{W}_0,$$
 (13b)

$$\boldsymbol{\Upsilon}_{l} = \operatorname{diag}\left(\left[e^{j\xi_{l,1}}, e^{j\xi_{l,2}}, \cdots, e^{j\xi_{l,M}}\right]^{T}\right), \qquad (13c)$$

$$\xi_{l,m} \in [0, 2\pi), \ m = 1, \cdots, M, \ l = 1, \cdots, L, \ (13d)$$

$$\beta \in \mathbb{C},\tag{13e}$$

where (13b) \sim (13d) characterize the constraints on the EM response of the SIM, while (13e) characterizes the scaling factor.

Note that due to the non-convex constant modulus constraint and the fact that the phase shifts associated with different metasurface layers are highly coupled, the optimization problem in (13) is non-trivial to solve. In the subsequent subsection, we customize a gradient descent method for efficiently finding a near-optimal solution of (13).

B. Proposed Gradient Descent Algorithm

The gradient descent algorithm iteratively adjusts the phase shifts of the SIM for minimizing the loss function in (13a). Specifically, the gradient descent involves two main procedures: *i*) calculating the derivative and *ii*) updating the parameters.

1) Derivative Calculation: For a tentative SIM model, the gradient of the loss function \mathcal{L} w.r.t. the phase shift vector $\boldsymbol{\xi}_l$ of the *l*-th layer of the SIM is calculated as follows:

$$\nabla_{\boldsymbol{\xi}_{l}} \mathcal{L} = \sum_{n=1}^{N} \nabla_{\boldsymbol{\xi}_{l}} \left\| \beta \boldsymbol{g}_{n} - \boldsymbol{f}_{n} \right\|^{2}, \ l = 1, 2, \cdots, L.$$
(14)

where $\boldsymbol{g}_n \in \mathbb{C}^{N \times 1}$, $n = 1, 2, \dots, N$ and $\boldsymbol{f}_n \in \mathbb{C}^{N \times 1}$, $n = 1, 2, \dots, N$ represent the *n*-th column of \boldsymbol{G} and \boldsymbol{F} , respectively.

Furthermore, the *m*-th entry of the gradient in (14) is obtained by taking the partial derivative of $\|\beta g_n - f_n\|^2$ w.r.t. $\xi_{l,m}$. Upon applying the chain rule to the derivatives, we have:

$$\frac{\partial \|\beta \boldsymbol{g}_{n} - \boldsymbol{f}_{n}\|^{2}}{\partial \xi_{l,m}} = 2\Re \left\{ \beta^{*} \frac{\partial \boldsymbol{g}_{n}^{H}}{\partial \xi_{l,m}} \left(\beta \boldsymbol{g}_{n} - \boldsymbol{f}_{n}\right) \right\}$$

$$\stackrel{(i)}{=} 2\Re \left\{ \beta^{*} \frac{\partial \left(\boldsymbol{P}_{l,n} \boldsymbol{v}_{l}\right)^{H}}{\partial \xi_{l,m}} \left(\beta \boldsymbol{g}_{n} - \boldsymbol{f}_{n}\right) \right\}$$

$$= 2\Re \left\{ \beta^{*} \frac{1}{j} v_{l,m}^{*} \boldsymbol{e}_{m}^{H} \boldsymbol{P}_{l,n}^{H} \left(\beta \boldsymbol{g}_{n} - \boldsymbol{f}_{n}\right) \right\}$$

$$= 2\Im \left\{ \beta^{*} v_{l,m}^{*} \boldsymbol{e}_{m}^{H} \boldsymbol{P}_{l,n}^{H} \left(\beta \boldsymbol{g}_{n} - \boldsymbol{f}_{n}\right) \right\}, (15)$$

for $m = 1, 2, \dots, M$, $l = 1, 2, \dots, L$, where e_m^H represents the *m*-th row of the identity matrix I_M and (*i*) holds due to the fact that $g_n = P_{l,n}v_l$, and $P_{l,n} \in \mathbb{C}^{N \times M}$, $n = 1, 2, \dots, N$, $l = 1, 2, \dots, L$ denotes the equivalent coefficient matrix associated with the *l*-th metasurface layer activating the *n*-th meta-atom on the input layer, which is defined as

$$\boldsymbol{P}_{l,n} = \boldsymbol{W}_{L} \boldsymbol{\Upsilon}_{L} \boldsymbol{W}_{L-1} \cdots \boldsymbol{W}_{l+1} \boldsymbol{\Upsilon}_{l+1} \boldsymbol{W}_{l} \text{diag} \left(\boldsymbol{q}_{l,n}\right), \quad (16)$$

with $q_{l,n} \in \mathbb{C}^{M \times 1}$ representing the complex signal component illuminating the *l*-th layer of the SIM from the *n*-th meta-atom in the input layer, defined as

$$\boldsymbol{q}_{l,n} = \boldsymbol{W}_{l-1} \boldsymbol{\Upsilon}_{l-1} \boldsymbol{W}_{l-2} \cdots \boldsymbol{W}_2 \boldsymbol{\Upsilon}_2 \boldsymbol{W}_1 \boldsymbol{\Upsilon}_1 \boldsymbol{w}_{0,n}, \quad (17)$$

for $n = 1, 2, \dots, N$, $l = 1, 2, \dots, L$, where $\boldsymbol{w}_{0,n} \in \mathbb{C}^{M \times 1}$ represents the *n*-th column of \boldsymbol{W}_0 .

By gathering the M partial derivatives in (15) into a vector, the gradient in (14) can be formulated as:

$$\nabla_{\boldsymbol{\xi}_{l}} \mathcal{L} = 2 \sum_{n=1}^{N} \Im \left\{ \beta^{*} \boldsymbol{\Upsilon}_{l}^{H} \boldsymbol{P}_{l,n}^{H} \left(\beta \boldsymbol{g}_{n} - \boldsymbol{f}_{n} \right) \right\}, \quad (18)$$

for $l = 1, 2, \cdots, L$.

2) Parameter Update: Once all the gradients w.r.t. the SIM's phase shift vectors are calculated, we simultaneously evolve the phase shift values ξ_l in the direction that decreases the value of the loss function. At each iteration, the update formula is as follows:

$$\boldsymbol{\xi}_l \leftarrow \boldsymbol{\xi}_l - \eta \nabla_{\boldsymbol{\xi}_l} \mathcal{L}, \tag{19}$$

where $\eta > 0$ represents the learning rate. To ensure a stable convergence, the learning rate η is decreased at each iteration according to a step-based schedule:

$$\eta \leftarrow \eta \zeta \pi / \max_{l=1,2,\cdots,L} \left\{ \max \nabla_{\boldsymbol{\xi}_l} \mathcal{L} \right\},$$
(20)

with ζ representing the step-size decay parameter.

In addition, the auxiliary scaling factor β has to be updated during each iteration to maintain the normalized level. Specifically, given a tentative SIM response matrix G, the optimal value of β can be readily obtained by utilizing the least squares (LS) method, yielding

$$\beta = \left(\boldsymbol{g}^{H}\boldsymbol{g}\right)^{-1}\boldsymbol{g}^{H}\boldsymbol{f}, \qquad (21)$$

where we have $g = \operatorname{vec}(G)$ and $f = \operatorname{vec}(F)$.

The phase shift values are updated repeatedly until either the loss function \mathcal{L} converges or the phase shift vectors of the SIM are updated for an affordable number of iterations. By employing the SIM to implement the 2D DFT in the wave domain, the system can directly generate the angular spectrum at the receiver array and provide a coarse on-grid estimate for the DOA parameters of the incident signal. However, the coarse estimate has limited estimation precision for a small value of N. Fortunately, the input layer provides an extra design degree of freedom (DoF), which can be exploited for generating a set of 2D DFT matrices associated with orthogonal frequency bins, thus substantially improving the DOA estimation performance of a moderate-size SIM, as it will be further detailed in the next section.

IV. SIM-BASED DOA ESTIMATION

In this section, we first introduce the proposed SIM-based DOA estimation protocol by appropriately configuring the phase shift values of the input layer, i.e., Υ_0 . We then present the specific DOA estimation procedure based on this configuration.

The proposed protocol divides the total observation time T into T_y blocks, each of length T_x , so that $T = T_x T_y$. The phase shift vectors for the first to the *L*-th layers are determined by employing the optimization process described in Section III-B and remain the same during T snapshots. By contrast, the phase shift vector for the input layer of the SIM is reconfigured at each time slot in order to generate a set of DFT matrices having orthogonal spatial frequency bins. Specifically, at the snapshot t, the phase shift of the *n*-th meta-atom imposed on the input layer is configured as:

$$\xi_{0,n,t} = -2\pi \frac{(n_{\rm x}-1)(t_{\rm x}-1)}{N_{\rm x}T_{\rm x}} - 2\pi \frac{(n_{\rm y}-1)(t_{\rm y}-1)}{N_{\rm y}T_{\rm y}}, \quad (22)$$

where n_y and n_x are as defined in (11), t_y and t_x represent the block index and the time slot index within that block, respectively, which are defined as $t_y \triangleq \lfloor t/T_x \rfloor$ and $t_x \triangleq t - (t_y - 1) T_x$, respectively.

Note that upon right-multiplying G (i.e., the well-fitted version of F) by $\Upsilon_{0,t}$, the SIM implicitly characterizes a set of 2D DFT matrices whose frequency bins are mutually orthogonal to each other. Under a noiseless received signal model, the EM waves propagating through the optimized SIM are automatically focused on the specific antenna and snapshot indices, returning the on-grid DOA estimate and the spatial frequency offset component of the incoming signal, respectively. As a result, the DOA parameters of the incoming signal can be readily estimated by measuring the energy

distribution across the receiver antenna array, which is in contrast to conventional DOA estimation algorithms relying on phase-sensitive receivers and array signal processing.

Specifically, let $r_{n,t}$ represent the signal received at the *n*-th probe in the *t*-th snapshot. After collecting the received signals over *T* snapshots, we search for the index of the strongest signal magnitude. The 2D index of the peak is inferred as follows:

$$[\hat{n}, \hat{t}] = \arg \max_{\substack{n=1,2,\cdots,N, \\ t=1,2,\cdots,T}} |r_{n,t}|^2.$$
 (23)

Therefore, the corresponding electrical angles of the incident signal are obtained as

$$\hat{\psi}_{\mathbf{x}} = \mod\left[2\left(\frac{\hat{n}_{\mathbf{x}}-1}{N_{\mathbf{x}}} + \frac{\hat{t}_{\mathbf{x}}-1}{N_{\mathbf{x}}T_{\mathbf{x}}}\right) + 1, 2\right] - 1,$$
 (24)

$$\hat{\psi}_{y} = \text{mod}\left[2\left(\frac{\hat{n}_{y}-1}{N_{y}} + \frac{\hat{t}_{y}-1}{N_{y}T_{y}}\right) + 1, 2\right] - 1,$$
 (25)

respectively, where \hat{n}_y and \hat{n}_x are defined in (11), while \hat{t}_y and \hat{t}_x are as in (22).

Based on the estimates in (24) and (25), the estimated azimuth and elevation angles $\hat{\varphi}$ and $\hat{\vartheta}$ are given by

$$\hat{\varphi} = \arctan\left(\frac{\hat{\psi}_{y}d_{x}}{\hat{\psi}_{x}d_{y}}\right),$$
(26)

$$\hat{\vartheta} = \arcsin\left(\frac{1}{\kappa}\sqrt{\frac{\hat{\psi}_{x}^{2}}{d_{x}^{2}} + \frac{\hat{\psi}_{y}^{2}}{d_{y}^{2}}}\right).$$
(27)

In conventional radar systems, the antenna arrays first receive signals and down-convert them to baseband signals before estimating the DOAs. However, the SIM operates in a fundamentally different way by directly processing the raw RF signals received, without the need for an individual RF chain and ADC at each antenna element. This substantially reduces both the hardware cost and energy consumption, which has great potential for onboard applications such as employing a SIM on a drone to identify the DOA of ground targets.

V. SIMULATION RESULTS

In this section, we conduct numerical simulations to evaluate the performance of the proposed SIM-based DOA estimator. Specifically, we consider the scenario of estimating the DOA of a single source, as shown in Fig. 1. The system operates at 60 GHz. The simulation parameters are the following: $N_x = N_y = 4$; the spacing between adjacent meta-atoms on the same layer is $d_x = d_y = \lambda/2$; the receiver antenna array is arranged as the input layer of the SIM, both with half-wavelength element spacing.

In Fig. 2, we evaluate the convergence behavior of the proposed gradient descent algorithm for optimizing a ninelayer SIM having the layer spacing equal to $d_{\text{layer}} = \lambda$. Each square metasurface contains $M = 12 \times 12 = 144$ meta-atoms.



Fig. 2. Convergence analysis of the proposed gradient descent algorithm.



Fig. 3. Normalized loss function versus the number of metasurface layers.

Three different decay parameters of $\zeta = 0.9, 0.95, 0.99$ are considered. It is demonstrated in Fig. 2 that as the iterations proceed, the proposed gradient descent method gradually converges for a moderate value of the decay parameter, such as 0.95. For a value of ζ close to 1, the algorithm may overshoot frequently and require more iterations to converge. Additionally, while the gradient descent algorithm may reduce the loss function rapidly at the early stage of less than 50 iterations for $\zeta = 0.9$, it may get trapped in a locally optimal point. In the considered case study, the decay parameter of 0.95 performs the best after running 200 iterations.

Furthermore, we evaluate the ability of the SIM to mimic the 2D DFT versus the number of metasurface layers L. Specifically, we consider four setups, namely M = 64, 100, 144, 196 meta-atoms on each layer. For each setup, the SIM phase shifts are optimized using the gradient descent method with a decay parameter of 0.95 over a maximum of 200 iterations. The simulation results of Fig. 3 demonstrate that a SIM having a small number of layers is unable to fit the 2D DFT matrix well. As the number of layers L increases, the SIM succeeds in better approximating the 2D DFT in the wave domain. Additionally, it is demonstrated that the fitting performance also improves, as the number of meta-atoms M on each layer increases. Specifically, Fig. 3 shows that increasing M from 64 to 196 improves the normalized fitting MSE by nearly an order of magnitude.



Fig. 4. MSE versus SNR.

Next, we examine the performance of the proposed SIMbased DOA estimator by evaluating its MSE versus the SNR, while the SIM parameters are kept the same as in Fig. 2. For brevity, we consider the electrical angles ψ_x and ψ_y instead of the physical angles, which are both uniformly distributed on the grid points in [-1, 1]. The simulation results shown in Fig. 4 are obtained by averaging 100 independent experiments. More specifically, we consider two different numbers of snapshots, namely $T_x = T_y = 25$ and 100. For comparison, we also plot the MSE when using the proposed estimation protocol associated with the digital 2D DFT. As expected, the MSE decreases as the SNR increases. Specifically, the MSE improves by 10 dB for every 10 dB increase in SNR. Additionally, increasing the number of snapshots per block from $T_x = 25$ to $T_x = 100$ provides an extra 2 dB performance gain, thanks to the finer granularity. It is demonstrated that the proposed SIM-based channel estimator achieves an MSE of approximately 10^{-4} when $T_x = 100$ snapshots in each block and the SNR is 10 dB. Moreover, the proposed SIM that operates in the wave domain provides the same performance as its digital counterpart.

Finally, we examine the ability of the SIM to compute the 2D DFT by analyzing the angular spectrum under four different setups. The spectrum is obtained by combining the outputs of $T_x \times T_y = 1024$ 2D DFTs over (4, 4) grid points. We first consider a random setup of $\bar{\psi}_x = -0.67$ and $\bar{\psi}_y = -0.48$, marked by the red cross. Observe from Fig. 5(a) that the highest energy matches both the corresponding antenna as well as the snapshot index. This means that the SIM could return a perfect estimate of the DOA parameters under noiseless conditions. Similarly, the angular spectra of the other three cases are shown in Figs. 5(c)-(d), where the energy peak is at the position corresponding to the incident signal's DOA. In a nutshell, the SIM results in a fundamental DOA estimation paradigm shift by directly observing the angular spectrum instead of the array signal.

VI. CONCLUSIONS

We proposed a novel SIM architecture for estimating the 2D DOA parameters. By appropriately training the SIM,



(a) Case I: $\bar{\psi}_x = -0.67$, $\bar{\psi}_y = -0.48$; (b) Case II: $\bar{\psi}_x = 0.53$, $\bar{\psi}_y = -0.34$;



(c) Case III: $\bar{\psi}_x = -0.52$, $\bar{\psi}_y = 0.41$; (d) Case IV: $\bar{\psi}_x = 0.44$, $\bar{\psi}_y = 0.33$;

Fig. 5. The angular spectrum of the incident signal after passing through the SIM.

the spatial EM waves can be directly transformed into their angular domain as they propagate through the SIM. Furthermore, we designed a protocol to generate an angular spectrum having orthogonal spatial frequency bins. Thus, one can easily read the DOA by searching for the index having the highest magnitude. Our simulation results indicate that the proposed SIM-based DOA estimator achieves good MSE estimates under moderate conditions, while allowing for a substantial enhancement in the computing speed at a moderate hardware complexity. As the first attempt in this area, we considered a single source in this paper, while DOA estimates of multiple sources using the SIM require future research efforts. Additionally, leveraging SIM for joint DOA estimation and MIMO precoding opens up opportunities for a new wavebased signal processing paradigm for integrated sensing and communication scenarios in future mobile networks [22], [23].

ACKNOWLEDGMENTS

This research is supported by the Ministry of Education, Singapore, under its MOE Tier 2 (Award number MOE-T2EP50220-0019) and A*STAR (Agency for Science, Technology and Research) Singapore, under Grant No. M22L1b0110. The research of Yong Liang Guan is supported by the Temasek Laboratories@NTU Signal Research Programme Phase 4 Grant.

REFERENCES

- [1] R. Schmidt, "Multiple emitter location and signal parameter estimation," IEEE Trans. Antennas Propag., vol. 34, no. 3, pp. 276-280, Mar. 1986.
- [2] R. Roy and T. Kailath, "ESPRIT-estimation of signal parameters via rotational invariance techniques," IEEE Trans. Acoustics Speech Signal Process., vol. 37, no. 7, pp. 984-995, Jul. 1989.
- [3] P. Stoica and A. Nehorai, "Music, maximum likelihood, and Cramer-Rao bound," IEEE Trans. Acoustics Speech Signal Process., vol. 37, no. 5, pp. 720-741, May 1989.

- [4] Z. Zheng, Y. Huang, W.-Q. Wang, and H. C. So, "Direction-of-arrival estimation of coherent signals via coprime array interpolation," IEEE Signal Process. Lett., vol. 27, no. 3, pp. 585–589, Mar. 2020. S. Haykin, "Array signal processing," Englewood Cliffs, 1985.
- [5]
- [6] H. Krim and M. Viberg, "Two decades of array signal processing research: the parametric approach," IEEE Signal Process. Mag., vol. 13, no. 4, pp. 67-94, Jul. 1996.
- [7] L. Godara, "Application of antenna arrays to mobile communications Part II: Beam-forming and direction-of-arrival considerations," Proc. IEEE, vol. 85, no. 8, pp. 1195-1245, Aug. 1997.
- [8] C. See and A. Gershman, "Direction-of-arrival estimation in partly calibrated subarray-based sensor arrays," IEEE Trans. Signal Process., vol. 52, no. 2, pp. 329-338, Feb. 2004.
- Z.-M. Liu and Y.-Y. Zhou, "A unified framework and sparse Bayesian [9] perspective for direction-of-arrival estimation in the presence of array imperfections," IEEE Trans. Signal Process., vol. 61, no. 15, pp. 3786-3798, Aug. 2013.
- [10] C. Xu, J. An, T. Bai, S. Sugiura, R. G. Maunder, L.-L. Yang, M. Di Renzo, and L. Hanzo, "Antenna selection for reconfigurable intelligent surfaces: A transceiver-agnostic passive beamforming configuration," IEEE Trans. Wireless Commun., vol. 22, no. 11, pp. 7756-7774, Nov. 2023.
- [11] J. An, C. Xu, Q. Wu, D. W. K. Ng, M. D. Renzo, C. Yuen, and L. Hanzo, "Codebook-based solutions for reconfigurable intelligent surfaces and their open challenges," IEEE Wireless Commun., pp. 1-8, 2022, Early Access
- [12] M. Di Renzo, A. Zappone, M. Debbah, M.-S. Alouini, C. Yuen, J. de Rosny, and S. Tretyakov, "Smart radio environments empowered by reconfigurable intelligent surfaces: How it works, state of research, and the road ahead," IEEE J. Sel. Areas Commun., vol. 38, no. 11, pp. 2450-2525, Nov. 2020.
- [13] J. An, C. Xu, L. Gan, and L. Hanzo, "Low-complexity channel estimation and passive beamforming for RIS-assisted MIMO systems relying on discrete phase shifts," IEEE Trans. Commun., vol. 70, no. 2, pp. 1245-1260, Feb. 2022.
- [14] T. J. Cui, M. Q. Qi, X. Wan, J. Zhao, and Q. Cheng, "Coding metamaterials, digital metamaterials and programmable metamaterials, Light: science & applications, vol. 3, no. 10, pp. e218-e218, Oct. 2014.
- C. Liu, Q. Ma, Z. J. Luo, Q. R. Hong, Q. Xiao, H. C. Zhang, L. Miao, [15] W. M. Yu, Q. Cheng, L. Li et al., "A programmable diffractive deep neural network based on a digital-coding metasurface array," Nature Electronics, vol. 5, no. 2, pp. 113-122, Feb. 2022.
- [16] A. Silva, F. Monticone, G. Castaldi, V. Galdi, A. Alù, and N. Engheta, "Performing mathematical operations with metamaterials," Science, vol. 343, no. 6167, pp. 160-163, Jan. 2014.
- J. An, C. Xu, D. W. K. Ng, G. C. Alexandropoulos, C. Huang, C. Yuen, [17] and L. Hanzo, "Stacked intelligent metasurfaces for efficient holographic MIMO communications in 6G," IEEE J. Sel. Areas Commun., vol. 41, no. 8, pp. 2380-2396, Aug. 2023.
- [18] J. An, C. Yuen, C. Huang, M. Debbah, H. Vincent Poor, and L. Hanzo, "A tutorial on holographic MIMO communications-part I: Channel modeling and channel estimation," IEEE Commun. Lett., vol. 27, no. 7, pp. 1664-1668, Jul. 2023.
- [19] J. An, M. Di Renzo, M. Debbah, and C. Yuen, "Stacked intelligent metasurfaces for multiuser beamforming in the wave domain," in Proc. IEEE Int. Conf. Commun. (ICC), Rome, Italy, May 2023, pp. 1-6.
- [20] J. An, M. Di Renzo, M. Debbah, H. V. Poor, and C. Yuen, "Stacked intelligent metasurfaces for multiuser downlink beamforming in the wave domain," arXiv preprint arXiv:2309.02687, 2023.
- [21] P. Heidenreich, A. M. Zoubir, and M. Rubsamen, "Joint 2-D DOA estimation and phase calibration for uniform rectangular arrays," IEEE Trans. Signal Processing, vol. 60, no. 9, pp. 4683-4693, Sep. 2012.
- [22] M. Hua, Q. Wu, W. Chen, Z. Fei, H. C. So, and C. Yuen, "Intelligent reflecting surface-assisted localization: Performance analysis and algorithm design," IEEE Wireless Commun. Lett., vol. 13, no. 1, pp. 84-88, Jan. 2024.
- [23] J. An, H. Li, D. W. K. Ng, and C. Yuen, "Fundamental detection probability vs. achievable rate tradeoff in integrated sensing and communication systems," IEEE Trans. Wireless Commun., vol. 22, no. 12, pp. 9835-9853, 2023.