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# <sup>1</sup>**Repeated lidar acquisitions in an underground salt gallery in the**

# <sup>2</sup>**Alsatian potassic basin (France): monitoring and geomechanical**

## <sup>3</sup>**modelling**

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#### 8 **Abstract**

9 In the Alsatian potassic basin, located northwest of Mulhouse (eastern France), the 10 deformation of an underground salt gallery is monitored from April 2017 to April 2019 using 11 repeated static lidar acquisitions. This monitoring aims to characterize the rheology of the rock salt. 12 The gallery is situated at 550 m deep in a 20 m thick rock salt layer. At this depth traditional 13 referencing tools such as GPS are not available; and the salt is creeping, which prevents the 14 referencing of the measurements with respect to a stable area. First, we develop a specific 15 acquisition protocol to precisely monitor the deformation affecting the gallery walls over time. After 16 two years, we measure a horizontal deformation between 0.10 and 0.30% all along the gallery with a 17 mean uncertainty of 0.08%. From the low horizontal deformation, a new methodology is developed 18 to set the point clouds in the same coordinate system. By doing so, the gallery closure, or volumetric 19 deformation, is calculated. Then, the horizontal deformation time series of the gallery is used to 20 parametrize the mechanical behaviour law of the rock salt, consistent with parameters from 21 laboratory work on this rock salt. Through our work, in addition to the new methodology, the lidar 22 device is shown to be a useful and polyvalent tool to monitor underground cavities and to 23 mechanically characterize the surrounding medium.

- 24
- 25 **Keywords:** Lidar, rock salt, underground cavity, geomechanical modelling, methodology

26

#### 27 **1. Introduction**

28 Underground galleries might undergo severe deformation induced by the ambient stress 29 state, especially for deep excavations in materials susceptible to creep. Thus, the measurement of 30 the deformation of those galleries is necessary to monitor their stability through time. It also allows 31 improved determination of the rheology of the surrounding medium. Traditional tools, such as an 32 extensometer or a sliding ruler, offer precise values of deformation. However, those values only 33 concern specific points. Unlike traditional tools, *LIght Detection And Ranging* (lidar) devices offer the 34 possibility to measure the distance between a large number of points, allowing the determination of 35 the deformation over a larger spatial extent. During an acquisition or scan, a lidar device derives a 36 volume depiction using laser technology. By measuring the distance from the sensor to many targets, 37 the acquisition collects a set of data forming a point cloud in 3D, representing the scanned volume. 38 Lidar devices have become essential tools for remote sensing and 3D modelling studies, and their 39 fields of application have widened considerably over the last two decades (Eitel et al., 2016; Telling et 40 al., 2017; Wang et al., 2014).

41 The use of lidar acquisitions to monitor underground galleries is justified by the millimetric 42 accuracy of the measurements (Lichti and Licht, 2006). For superficial excavations such as open-pit 43 mines geo-referencing tools such as GPS are available (Grenon et al., 2017), although not for deep 44 galleries. When the device cannot be set up in the galleries to achieve continuous acquisitions 45 (Cecchetti et al., 2017), the referencing of the acquisitions becomes crucial. In some cases, reflective 46 or optical targets are installed as reference points in a stable area (Kukutsch et al., 2015; Pejić, 2013). 47 In other cases, the point clouds are set in a same coordinate system with a processing based either 48 on cross-correlation methods (Han et al., 2013) or on the Iterative Closest Point (ICP) method 49 (Errington et al., 2010). Moreover, methods based on point clouds cross-correlation result in high 50 accuracy (Lynch et al., 2017). In particular cases, despite the depth, the position of the lidar for the 51 acquisition can be geo-referenced with precision (Delaloye et al., 2015). However, these methods

52 might be time consuming due to the point cloud processing or to the protocol of acquisition. In order 53 to limit the time spent on these geo-referencing issues, 'global fitting approach' methods have been 54 developed. These methods are based on the comparison of 2D or 3D shapes coming from two point 55 clouds representing the same area (Walton et al., 2018).

56 The "Mines Domaniales de Potasse d'Alsace" (MDPA) extracted potash from 1910 to 2002 57 northwest of Mulhouse (eastern France). Due to the depletion of the resource, an underground 58 waste storage site was then created in 1998 to maintain economic activity in the region. The site is 59 located at 550 m deep, in a 20 m thick rock salt layer. Several galleries have been dug both in and 60 around the site to allow the transport and the storage of waste materials. The activity ceased in 2002 61 due to a fire. The site is currently under observation and is the subject of many studies. Since its 62 creation, the deformation of the site's gallery has been regularly monitored using sliding rulers. This 63 monitoring indicates that the galleries of the waste storage site are slowly closing as a result of rock 64 salt creeping.

65 Reconnaissance visits have determined that the surface of the rock salt galleries was 66 delaminating. This is explained by the halokinesis. Inside the rock salt layer, salt crystals develop 67 within the natural cracks of the layer. In some cases these new crystals press against the crystals on 68 the surface of the gallery, causing their fall. Thus, we have opposing phenomena: the creeping of the 69 rock salt (decreasing the distance between opposite walls) and the delamination of the superficial 70 salt (increasing the distance). As a consequence, we have chosen to work with specific reflectors, 71 about 70, in order to isolate and measure only the rock salt creeping.

72 Due to both the creeping and the delamination, we have chosen to avoid the use of cloud 73 point processing in our study such as ICP method (Errington et al., 2010) or 'global fitting approach' 74 methods (Walton et al., 2018). The first phenomenon modifies the position of the points in respect 75 to each other and the second in respect to the roughness of the surfaces. The creeping of the rock 76 salt however prevents the determination and the use of a reference area. Rock salt creeping 77 therefore makes it difficult to implement a common coordinate system for all acquisitions over time.

78 In this study, we analyse the deformation of an underground salt gallery from April 2017 to 79 April 2019 connected to the waste storage site. This gallery has been monitored by regular static lidar 80 acquisitions, every two to three months. From these repeated lidar acquisitions, precise time series 81 of horizontal deformation or convergence are obtained. Those results are also compared to 82 measurements realized in the neighbouring waste storage site, attesting to the quality of the results. 83 Due to the small amplitude of the deformation after two years, a new methodology has been 84 developed to set the point clouds in the same coordinate system. Thus, the gallery closure, or 85 volumetric deformation, is computed. These time series are then used to parametrize the mechanical 86 behaviour law of the rock salt with a geomechanical model. Through this study, in addition to the 87 new methodology, a lidar device is shown to be a useful and polyvalent tool to monitor underground 88 cavities and mechanically characterize the surrounding medium.

#### 89 **2. Data acquisition**

90 The monitored gallery, oriented N008°W, is 100 m long, 4 m wide, and 2.2 to 3 m high. In 91 order to enable the determination of the deformation, reflective targets are installed every 10 m 92 along the gallery (Figure 1.a). These targets are 2.5 cm radius disks glued to aluminium cubes, which 93 are themselves fixed with a thick vice to the walls and the roof (Figure 1.b-d). For each wall and roof, 94 three cubes are fixed at one-quarter, at half, and at three-quarters of the length and the height 95 (Figure 1.e). Unfortunately, the cubes could not be fixed to the floor, making the monitoring of the 96 vertical deformation more complex.



98 **Figure 1 (color) - Schematic drawing of the gallery (a) and pictures of both the reflectors with their** 99 **cube (b-d) and the gallery (e)** (Modeste, 2020)**.** Blue points indicate the three positions of acquisition 100 and brown arrows the direction of the scan. The acquisition numbers are in red. The reflectors are 101 set up in arcs, each arc containing 9 of them and being numbered in green from 1 (entrance of the 102 gallery) to 8 (waste storage site).

97

103 From April 2017 to April 2019, ten campaigns of static lidar acquisitions have been 104 conducted, every two to three months. Only one campaign was not undertaken, in August 2018, due 105 to the unavailability of the instrument. The lidar device used is a Riegl VZ-2000 (Petrie and Toth, 106 2018). This device can scan targets that are at least 2.5 m apart. Each campaign consisted of four 107 acquisitions: one at each end and two at the centre, one in both directions (Figure 1.a). A 360° 108 acquisition at the centre of the gallery was not possible, since the walls were too close to the device.

109 No area could be considered as stable due to the salt creeping, preventing the presence of a 110 reference point reliable for each acquisition. Therefore, at each acquisition campaign, the lidar was 111 placed vertically below a hook set up on the roof at the beginning of our experiments. The distance 112 between the lidar and the roof is constant over time for each acquisition time. Thus, the lidar is not 113 at the exact same position every time, but at a similar position.

#### 114 **3. Methodology**

115 As indicated in the previous section, the point clouds of each acquisition are not in the same 116 coordinate system at each campaign. In order to monitor the gallery elsewhere than at the location 117 of the reflectors, it is necessary to set the point clouds in the same coordinate system. We have 118 developed a new method for this, which requires two assumptions: point clouds acquired from a 119 similar point and small displacement of the reflectors between the two acquisition times.

120 In this section, the acquisition realized at the time t<sub>i</sub> is associated with the coordinate system 121 i. To transform the coordinates of a point M from the coordinate system i into j, we use the Equation 122 1:

123  
\n
$$
\begin{pmatrix} x_i \\ y_i \\ z_i \\ 1 \end{pmatrix} = s \times \begin{pmatrix} R_{\theta\theta} & R_{\theta\varphi} & R_{\theta\omega} & \frac{T_x}{s} \\ R_{\varphi\theta} & R_{\varphi\varphi} & R_{\varphi\omega} & \frac{T_y}{s} \\ R_{\omega\theta} & R_{\omega\varphi} & R_{\omega\omega} & \frac{T_z}{s} \\ 0 & 0 & 0 & \frac{T_z}{s} \end{pmatrix} \times \begin{pmatrix} x_j \\ y_j \\ z_j \\ 1 \end{pmatrix} \tag{1}
$$

124 with  $(x_j, y_j, z_j)$  the coordinates of the point M in the coordinate system j,  $(x_i, y_i, z_i)$  the coordinates of 125 the point M in the coordinate system i, s a scaling factor,  $(T_x, T_y, T_z)$  the components of the vector 126 translation,  $R_{ii}$  the component of the rotation matrix,  $\theta$  the angle of rotation around the x-axis,  $\varphi$  the 127 angle around the y-axis and  $\omega$  the angle around the z-axis.

128 Assuming similar orthonormal coordinate systems, s is equal to 1. This is consistent with test 129 measurements giving a value of 1.0003 ± 0.0010 (Habib, 2018). The translation and the rotation are 130 geometrical transformations which preserve the distance between two points. Thus, the distance 131 measured during an acquisition campaign is comparable to a distance from another acquisition 132 campaign.

133 The distance between two points can be written:

134 
$$
(AB)_j = \sqrt{(x_{bj} - x_{aj})^2 + (y_{bj} - y_{aj})^2 + (z_{bj} - z_{aj})^2}
$$
 (2)

135 with (AB)<sub>j</sub> the distance between the points A and B at the time  $t_j$ , ( $x_{aj}$ ,  $y_{aj}$ ,  $z_{aj}$ ) the coordinates of the 136 point A in the coordinate system j at the time  $t_j$  and  $(x_{bj}$ ,  $y_{bj}$ ,  $z_{bj}$ ) the coordinates of the point B in the

137 coordinate system j at the time t<sub>i</sub>. Using the law of conservation of the distances between two points, 138 Equation 2 can be written with the coordinates of the coordinate system i and the displacement 139 vectors (displacements of the reflectors between the acquisition times  $t_i$  and  $t_i$ ):

$$
140 \qquad (AB)_j
$$

141 = 
$$
\sqrt{(x_{bi} - x_{ai} + dx_{bij} - dx_{aij})^2 + (y_{bi} - y_{ai} + dy_{bij} - dy_{aij})^2 + (z_{bi} - z_{ai} + dz_{bij} - dz_{aij})^2}
$$
 (3)

142 with dx<sub>aii</sub> and dx<sub>bii</sub> the displacement along the x-axis of the points A and B between the times t<sub>i</sub> and t<sub>i</sub>, 143 dy<sub>aij</sub> and dy<sub>bij</sub> the displacement along the y-axis of the points A and B between the times t<sub>i</sub> and t<sub>j</sub>, dz<sub>aij</sub> 144 and dz<sub>bij</sub> the displacement along the z-axis of the point A and B between the times t<sub>i</sub> and t<sub>i</sub>. Here, the 145 vector displacement is expressed in the coordinate system i. In the case of low deformation, with 146 variation of distance of a few millimetres, the displacement difference is small compared to the 147 coordinate difference. Thus, we can assume that the square of the displacement difference can be 148 neglected (Equation 4, 5 and 6):

149 
$$
(dx_{bij} - dx_{aij})^2 \sim 0 \quad (4)
$$

150 
$$
(dy_{bij} - dy_{aij})^2 \sim 0 \quad (5)
$$

151 
$$
(dz_{bij} - dz_{aij})^2 \sim 0 \quad (6)
$$

152 By using and developing Equations 3 to 6, we have:

153 
$$
(AB)^2_j = (x_{bi} - x_{ai})^2 + 2(x_{bi} - x_{ai})\left(dx_{bij} - dx_{ai}\right) + \left(dx_{bij} - dx_{ai}\right)^2 + (y_{bi} - y_{ai})^2
$$

154 
$$
+ 2(y_{bi} - y_{ai})(dy_{bij} - dy_{aij}) + (dy_{bij} - dy_{aij})^{2} + (z_{bi} - z_{ai})^{2}
$$

155 
$$
+ 2(z_{bi} - z_{ai}) (dz_{bij} - dz_{aij}) + (dz_{bij} - dz_{aij})^2
$$

156 
$$
\Leftrightarrow \frac{1}{2} \big[ (AB)^2_j - (AB)^2_i \big]
$$

157 = 
$$
(x_{bi} - x_{ai})(dx_{bij} - dx_{aij}) + (y_{bi} - y_{ai})(dy_{bij} - dy_{aij})
$$

158 
$$
+ (z_{bi} - z_{ai}) (dz_{bij} - dz_{aij}) + o [(dx_{bij} - dx_{aij})^2] + o [(dy_{bij} - dy_{aij})^2]
$$

$$
+ o\left[\left(dz_{bij} - dz_{aij}\right)^2\right] \tag{7}
$$

160 Equation 7 can be written with matrix:

161 
$$
\left(\frac{1}{2}\left[ (AB)^2_j - (AB)^2_i \right]\right) = \left(-\Delta x_{abi} - \Delta y_{abi} - \Delta z_{abi} \Delta x_{abi} \Delta y_{abi} \Delta z_{abi}\right) \times \begin{pmatrix} dx_{aij} \\ dy_{aij} \\ dz_{aij} \\ dy_{bij} \\ dy_{bij} \\ dz_{bij} \end{pmatrix}
$$
 (8)

162 with Δx<sub>abi</sub> the coordinates difference along the x-axis between points A and B in the coordinate 163 system i, Δy<sub>abi</sub> the coordinates difference along the y-axis between points A and B in the coordinate 164 system i, Δz<sub>abi</sub> the coordinates difference along the z-axis between points A and B in the coordinate 165 system i. This is repeated for each combination of reflectors and the matrix is concatenated. Thus, 166 from Equation 8 and for M points, we have:

167 
$$
\begin{pmatrix} \frac{1}{2} \left[ (AB)^2 - (AB)^2 \right] \\ \vdots \\ \frac{1}{2} \left[ (LM)^2 - (LM)^2 \right] \end{pmatrix} = \begin{pmatrix} -\Delta x_{abi} & -\Delta y_{abi} & -\Delta z_{abi} & \cdots & 0 & 0 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \vdots \\ 0 & 0 & 0 & \cdots & \Delta x_{lmi} & \Delta y_{lmi} & \Delta z_{lmi} \end{pmatrix} \times \begin{pmatrix} dx_{aij} \\ dy_{aij} \\ dz_{aij} \\ \vdots \\ dx_{mij} \\ dy_{mij} \\ dy_{mij} \end{pmatrix}
$$
(9)

168 Equation 9 has the form: D = GM, with D the data, G the transfer matrix and M the model. In our 169 case, M is the reflector displacements to be estimated. We can use Equation 10 to solve Equation 9 170 (Tarantola, 2005):

171 
$$
M = M_0 + (G^T C_D^{-1} G + C_M^{-1}) G^T C_D^{-1} (D + G M_0) \quad (10)
$$

172 with M<sub>0</sub> the a priori model, C<sub>D</sub> the covariance matrix of the data and C<sub>M</sub> the covariance matrix of the 173 model. By solving Equation 10, we obtain the reflectors displacement between the two acquisitions 174 in the coordinate system of our choice. The estimated displacement vectors are in the coordinate 175 system i in the previous equation sequence.

176 This method requires the use of at least seven distinct reflectors. These reflectors might be 177 placed either within the same arc or all along the gallery. For each reflector, we have three 178 unknowns, the three associated components of the displacement vector. We need at least the same 179 number of unknowns and distances to have a well-defined system. Thus, with seven reflectors, we 180 have 21 unknowns for 21 distances.

181 By applying the displacement to the reflectors at the time  $t_i$ , we obtain the position of the 182 reflectors at the time  $t_i$  in the coordinate system i. Thus, at the time  $t_i$ , we have the position of the 183 reflectors in both coordinate systems i and j. By concatenating Equation 1 for each reflector, we get 184 Equation 11:

185 
$$
\begin{pmatrix} x_{ai} & x_{mi} \\ y_{ai} & \cdots & y_{mi} \\ z_{ai} & \cdots & z_{mi} \\ 1 & 1 & 1 \end{pmatrix} = \begin{pmatrix} R_{\theta\theta} & R_{\theta\phi} & R_{\theta\omega} & T_x \\ R_{\phi\theta} & R_{\phi\phi} & R_{\phi\omega} & T_y \\ R_{\omega\theta} & R_{\omega\phi} & R_{\omega\omega} & T_z \\ 0 & 0 & 0 & 1 \end{pmatrix} \times \begin{pmatrix} x_{aj} & x_{mj} \\ y_{aj} & \cdots & y_{mj} \\ z_{aj} & \cdots & z_{mj} \\ 1 & 1 & 1 \end{pmatrix}
$$
 (11)

186 By solving Equation 11 with a least-square method, the transfer matrix between the two 187 coordinate systems can be estimated and then used to set the point clouds in the same coordinate 188 system.

189 Thus, in this method the point clouds are set into the same coordinate system from 190 reference points whose position has been corrected for the displacement occurring between the two 191 acquisition times. Thus far such a correction was not envisaged to set the point clouds in the same 192 coordinate system. This method is less time consuming than methods based on point clouds cross-193 correlation since we do not need to work with the whole point clouds (Lynch et al, 2017). However, 194 our method requires installing reflectors to recognize and locate specific points completely during 195 each acquisition, in contrast to 'global fitting approach' methods (Walton et al., 2018).

#### 196 **4. Results**

197 This section is divided into two main parts. First, the uncertainty of distances between 198 reflectors and of deformations is determined. Second, the horizontal deformation time series are 199 analysed. Due to the small amplitude of the deformation, we can set the point clouds in the same 200 coordinate system. Lastly, the closure of the gallery is calculated using the open source software 201 CloudCompare (Girardeau-Montaut, 2011).

#### 202 **a. Uncertainty of distances between reflectors and of deformations**

203 The scan acquisition 1 is repeated twice during the first campaign of acquisitions (case 1, 204 Table 1). Between the two acquisitions, the lidar device is uninstalled and then reinstalled. Each

205 installation followed the described protocol. The aim is to compare the distances between reflectors 206 inside both collected point clouds. The coordinates of the center of each reflector are extracted from 207 the first point cloud. The distance between each reflector is then calculated from these coordinates. 208 This is repeated for the second point cloud. Lastly, both distance sets are compared; i.e., each 209 distance between reflectors obtained in the first point cloud is compared to its equivalent in the 210 second point cloud.

211 In this study, the uncertainty is defined as the difference between two distance sets coming 212 from two different point clouds acquired the same day. Thus, the uncertainty reflects the error 213 related to the acquisition of the point cloud and the extraction of the reflector coordinates. The 214 uncertainty is chosen to be greater than 90-92% of the absolute differences between both distance 215 sets. The uncertainty is low, about 3 mm (Table 1). Then we estimate the uncertainty by using only 216 reflectors located within a distance smaller than 40 m of the lidar. This distance corresponds to the 217 maximum distance between each reflecting target and the lidar when it is set up at the centre of the 218 gallery (Figure 1.a). The uncertainty is lower, about 2 mm (Table 1).

219 In order to assess the importance of the protocol, we realize during the second campaign an 220 additional acquisition 1 without respecting the protocol (case 2, Table 1). The device is shifted by  $\sim$  50 221 cm away from the protocol position. This time the uncertainty is 3 times higher, 9 mm with all 222 reflectors and 6 mm with reflectors located at less than 40 m from the lidar (Table 1). This result 223 highlights the importance of respecting the protocol by replacing the device approximately a few 224 centimetres from the original position.

225 In order to assess the stability of the uncertainty over time, we also repeat the acquisition 1 226 twice during the tenth campaign in April 2019 (case 3, Table 1). We follow the same procedure for 227 the comparison. The uncertainty is similar to the one obtained for the first campaign (Table 1). Thus, 228 the uncertainty is stable over time and we keep a value of 2.1 mm for the uncertainty on the 229 distance.

230

#### 231 **Table 1** - Estimation of the uncertainty on the measured distance from lidar acquisitions



232 In order to estimate the uncertainty on deformations, we use Equation 12, derived from 233 metrology (JCGM, 2008):

234 
$$
\Delta \varepsilon (L_i, L_f) = \sqrt{\left(\frac{\partial \varepsilon (L_i, L_f)}{\partial L_i} \times \Delta L_i\right)^2 + \left(\frac{\partial \varepsilon (L_i, L_f)}{\partial L_f} \times \Delta L_f\right)^2} \quad (12)
$$

235 with ε the deformation, Li and L<sub>f</sub> the initial and final distances, Δ refers to the uncertainty. Assuming 236 that the uncertainty on distances is constant over time, Equation 12 can be written as follow:

237 
$$
\Delta \varepsilon (L_i, L_f) = \frac{\Delta L}{L_i} \times \sqrt{1 + \frac{L_f^2}{L_i^2}}
$$
 (13)

238 Taking into account an uncertainty of 2.1 mm on the distances measured with the lidar, the 239 uncertainty on the deformation ranges from 0.05 to 0.10%.

#### 240 **b. Horizontal deformation**

241 After two years, the horizontal deformation develops between 0.10 and 0.30% all along the 242 gallery (Figure 2.a-b). To obtain the amplitudes of the horizontal deformation, we look at the 243 variation of distance between two reflectors on opposite walls, at the same height and inside the 244 same arc. These values are higher than the uncertainty which has a mean value of 0.08%. Thus, the 245 monitored deformation is significant and appears linear over two years. Considering a width of 4 m, 246 the variation of distance between two opposite reflectors ranges from  $\sim$ 4 to 12 mm. Hence, the 247 displacement of each reflector can be considered small.

248 To assess the quality of the results, we compare ours to available measurements of 249 horizontal deformation in three neighbouring galleries (Figure 2.c). These measurements were 250 carried out by the MDPA with a sliding ruler at reference points marked by nails from June 2007 to 251 June 2013. For the comparison, we use the results from arc 8 (Figure 1.a), which is the arc closest to 252 the waste storage site. In the manual time series (ruler), we note the presence of offsets due to the 253 loss of the initial reference point, the nail falling from the wall. Measurements have been made with 254 a point close to the initial reference point. As shown on Figure 2.c, both measurement types are 255 consistent.



256 257 **Figure 2 (color) - Horizontal deformation time series from lidar campaigns (a and b) compared to**  258 **manual available measurements (c)** (Modeste, 2020)**.** The plotted measurements correspond to arc 259 3 (a), 7 (b) and 8 (c). The positive values correspond to a decrease of the distance between the 260 reflectors. 'Top' indicates the pair of reflectors fixed at three-quarters height, 'Middle' at halfway, 261 and 'Bottom'" at one-quarter height. The MDPA data are ruler measurements in three neighbouring 262 galleries, associated with the names "Bloc 11 – LXW". The two distinct reference dates of April 2017

263 and June 2007 have been chosen for the lidar measurements and for the ruler measurements, 264 respectively.





# 275 **Figure 3 – Flowcharts to compute the reflector displacement between April 2017 and April 2019**

#### 276 **(a), and then to deduce the transfer matrix between the two coordinate systems (b)**

277 In order to estimate the quality of the inversion, displacement vectors are applied to the 278 position of their respective reflectors in the point cloud acquired in April 2017. We calculate the 279 distance between each reflector with their new coordinates. Then, we calculate the distance 280 between each reflector in the point cloud acquired in April 2019. Lastly, the two distance sets are 281 compared. The differences between the two distance sets are small, at the order of micrometres 282 (Table 2). Thus, these comparisons validate our methodology. Figure 4 shows reflectors coming from 283 both point clouds before and after being set in the same coordinate system.

284 **Table 2** – Difference of reflectors distance in April 2019 between the original and the adjusted data







286 **Figure 4 (color) – Reflectors (arcs 1, 2 and 3) from the April 2017 and the April 2019 point clouds**  287 **before (a) and after (b) having set them in the same coordinate system**. The point clouds have been 288 acquired from acquisition point 2. Yellow is associated with the April 2017 point cloud and red with 289 the April 2019 point cloud.

#### 290 **ii. The closure of the gallery**

291 On the open-source software CloudCompare, we study the closure, or volumetric 292 deformation, of four sections of the gallery between the first campaign in April 2017 and the last one 293 in April 2019. To do so, we work only with the point clouds acquired at the centre of the gallery 294 (acquisitions 2 and 3, Figure 1.a). Having the point clouds in a same coordinate system allows us to 295 cut the same section of the gallery at different times. By adding vertical planes on both sides of the 296 selected section, a continuous volume with triangular mesh is created by solving Poisson's equation 297 (Figure 5.a) (Kazhdan et al., 2006). Then, we compute the volume of the retained section. The April 298 2017 and April 2019 results are finally compared to each other. We repeat this process with three 299 other sections along the gallery (Figure 5.b).

300 Thus, we obtain four values ranging from 0.34 to 0.55% after two years (Figure 5.b). These 301 values are higher than the horizontal deformation results. As the gallery also deforms vertically 302 (closure), the volumetric deformation is greater than the horizontal deformation. These results are 303 close to the estimations based on the measured displacement of the reflectors. We compare the 304 computed deformation to the variation of the surface of the opening of the gallery, corresponding to 305 a rectangle. To the initial width of 4 m, we subtract the mean reflector displacement of each 306 opposing wall. To the initial height of 2.5 m, we subtract two times the mean reflector displacement 307 of the roof, since we do not have reflectors on the floor. Then, the product of the initial width and 308 height is compared to the product of the reduced width and height. From this comparison, we 309 estimate the volumetric deformation from the displacements of the reflectors. The estimated values 310 range from 0.44% to 0.52% (Figure 5.b).



## 312 **Figure 5 (color) - Created volume from the point cloud (a) and its volumetric deformation after two**

313 **years (b)** (Modeste, 2020)**.** Positive values correspond to a closure or a loss of volume. Numbers in 314 brown are the computed results on CloudCompare while numbers in green refer to the estimation 315 based on the displacement of the reflectors.

### 316 **5. Geomechanical modelling**

311

317 In this section, the time series of horizontal deformation are geomechanically modelled. The 318 model is first set up according to the mechanical characteristics of the Alsatian potassic basin. Then,

319 the deformation of the gallery is modelled to parametrise the mechanical behaviour law of the 320 medium.

321 **1. Model setup** 

322 The deformation of two rock salt samples from the Alsatian potassic basin has been studied 323 in the laboratory under different conditions of temperature and deviatoric stress. Ghoreychi (1991) 324 shows that the elasto-visco-plastic behaviour of the rock salt follows Norton's Law (Equation 12, 13, 325 14):

$$
\dot{\varepsilon}_{ij}^{\nu} = \left(\frac{3}{2}\right) \dot{\varepsilon}_{cr} \left(\frac{\sigma_{ij}^a}{\bar{\sigma}}\right) (12)
$$

327 where

328 
$$
\dot{\varepsilon}_{cr} = \begin{cases} A\bar{\sigma}^n & \bar{\sigma} \ge \sigma_1^{ref} \\ 0 & \bar{\sigma} < \sigma_1^{ref}(13) \end{cases}
$$

329 and

$$
A = \frac{A_s}{\sigma_0^n} \exp\left(-\frac{B}{T}\right) \tag{14}
$$

331 where  $\dot{\varepsilon}_{ij}^v$  is the creep strain-rate tensor,  $\dot{\varepsilon}_{cr}$  the creep rate,  $\sigma_{ij}^d$  the deviatoric stress,  $\bar{\sigma}$  the Von Mises 332 stress,  $\sigma_1^{ref}$  the Von Mises stress threshold, n the stress exponent, A<sub>s</sub> the rate of reference, T the 333 temperature, B the ratio between the activation energy and the universal gas constant, and  $\sigma_0$  the 334 normalization stress. Norton's law and modified versions are commonly associated with the 335 mechanical behaviour law of rock salts (Khaledi et al., 2016; Wang et al., 2010). For rock salts, the 336 threshold is null, creep occurring as soon as deviatoric stresses are present in the medium (Carter et 337 al., 1993). Empirical parameters are summarised in Table 3. Previous studies (Camusso and Billaux, 338 2013; Laouafa et al., 2010) focused on the modelling of the horizontal deformation time series 339 coming from the ruler measurements. In these studies, the authors used other values of reference 340 velocity  $A_s$ , between 0.015 and 0.022 %/day instead of 0.005%/day, to retrieve the measurements.





342 In this work, we use Flac3D, which is commercial software developed by Itasca that allows 343 the study of the mechanical behaviour of a continuous three-dimensional medium (Itasca, 2002). 344 This modelling aims to determine which value of the reference velocity  $A_s$  in Norton's Law is relevant. 345 To model the gallery, a rectangular parallelepiped at 26.4 m high, 24 m wide and 52 m long is drawn 346 with rectangular parallelepipeds at 0.6 m high and 0.8 m long and wide (Figure 6). With those 347 dimensions, the gallery is made up of five parallelepipeds wide and four in height, either a node at 348 0.6, 1.2 and 1.8 m of height. These positions are equivalent to those of the reflectors in the gallery. 349 Since the height of the model (26 m) is similar to the thickness of the salt layer (about 20 m), a single 350 layer is modelled. In the modelling, the density, the Young's modulus and the Poisson's ratio used are 351 2.31 gm.cm<sup>-3</sup>, 28.3 GPa and 0.25, respectively (Table 4). The Young's modulus is different from the 352 laboratory results, 25 GPa (Ghoreychi, 1991), to account for the presence of anhydrite and marls, 353 which have a Young's modulus of 61 and 5.9 to 7 GPa, respectively (Nguyen-Minh and Bergues, 1995; 354 Trippetta et al., 2013). These values and the mechanical behaviour law have been estimated 355 experimentally in laboratory tests on small samples. These results are used here without taking into 356 account potential scale effects.





364 The gallery is nearly oriented along the maximum horizontal stress direction, which is the 365 North-South axis (Baumann and Illies, 1983; Larroque, 1987). According to in-situ stress 366 measurements in the Alsatian potassic basin (Cornet and Burlet, 1992), the vertical stress  $\sigma_v$  is nearly 367 equal to the maximum horizontal stress  $\sigma_H$  and the minimum horizontal stress  $\sigma_h$  is equal to 0.95 $\sigma_v$ .

#### 368 **2. Comparisons with the model**

369 After setting up the stress field, the closure of the gallery is then modelled. The centre of the 370 parallelepiped, along the Y-axis/N-S direction, is excavated to model the gallery. Norton's Law with 371 the experimental and geomechanical parameters (Table 3 and 4) are associated with each element. 372 In the model, the temperature is set to 298 K, which is the temperature measured during the lidar 373 campaigns. The modelling is carried out with different values of  $A_s$ . A twenty-year period is first 374 modelled, which is approximately the time between the excavation of the gallery and the beginning 375 of our lidar measurement campaigns. Then, the modelling is pursued over a two-year period that 376 corresponds to our monitoring period. Over this two-year period the distance evolution between 377 each opposite node of the gallery is extracted from the model. The horizontal deformation is then 378 deduced and compared to our lidar time series (Figure 7). The comparison is done between the pair 379 of reflectors fixed at one-quarter height and the pair of nodes at 0.6 m, the pair of reflectors fixed at 380 half height and the pair of nodes at 1.2 m and so on. Thus, only three pairs of reflectors per arc are 381 selected for the comparison between the model and the data. With seven arcs, a total of 21 382 comparisons are made. A  $R<sup>2</sup>$  determinant, reflecting the similarity of the model to the 383 measurements, is calculated for each comparison (Table 5). We used the point clouds coming from 384 acquisitions 2 and 3 to produce the horizontal deformation time series (Figure 1.a). However, with 385 these acquisitions, it is not possible to get the time series of arc 5, for it is too close to the lidar. A 386 mean value of  $R^2$  is obtained for each modelling carried out with a different value of  $A_s$ . The 387 modelling carried out with a value of 0.005 %/day for As seems to fit our measurements best (Table 388 5). Here we retrieve results from laboratory experiments, which is 0.005 %/day.



390 **Figure 7 (color) - Comparison between the results from campaigns of lidar acquisition and the**  391 **geomechanical model** (Modeste, 2020)**.** The plotted results correspond to arc 3 (a-c) and arc 7 (d-f). 392 The reflectors are associated with the nodes in the model. The horizontal deformation time series of 393 the pair of reflectors fixed at three-quarters height is compared to the pair of nodes at 1.8 m (a and 394 d), the pair of reflectors fixed at half height to the pair of nodes at 1.2 m (b and e) and the pair of 395 reflectors fixed at one-quarter height to the pair of nodes at 0.6 m (c and f).







#### 397 **6. Conclusion**

398 The deformation of a 500 m deep salt gallery has been monitored from April 2017 to April 399 2019 by repeated static lidar acquisitions. After two years, the horizontal deformation is estimated 400 and ranges from 0.10 to 0.30% along the gallery. The detected deformation is higher than the 401 uncertainty, which has a mean value of 0.08%. The comparisons of measurements conducted in the 402 waste storage are consistent with our measurements. The horizontal deformation time series are 403 then used to parametrize the mechanical behaviour law of the surrounding medium in a 404 geomechanical model. The results confirm the values obtained in laboratory tests.

405 Despite the absence of a stable reference site, the acquisitions have been successfully 406 referenced to each other. A new methodology was developed for this purpose. At least seven specific 407 reflectors have to be used as markers and must remain at the same location for the duration of the 408 monitoring. The methodology relies on two assumptions: point clouds acquired from a similar point 409 and small displacement of the reflectors between the two campaigns.

410 Through our work, the lidar device is shown to be a useful and polyvalent tool to monitor 411 underground cavities and to mechanically characterize the surrounding medium. In addition, the new 412 methodology offers a new way to monitor the deformation of underground galleries, to coincide 413 with the many existing methods.

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- 419 geomechanics he accomplished over the course of his entire career.

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