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# Maximization of inertial waves focusing in linear and nonlinear regimes

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## Abstract

We study the propagation of inertial waves generated by an axisymmetric torus oscillating at frequency  $\omega_f$  in a rotating fluid. Inertial waves (IW) are emitted from the torus and propagate at an angle  $\theta_f$  that depends on the ratio of the rotation frequency of the fluid to the forcing frequency of the torus. The waves focus in a neighbourhood of the apex of the propagation cone. Using direct numerical simulations, we characterize the flow in this region, within a linear approximation or in the regime where nonlinear interactions between waves produce a turbulent patch. Forcing by the torus is modeled in two ways. The first model represents the effect of the oscillating torus as a local volume force in the form of a Dirac delta function, called the Dirac ring. The second approach aims at a more realistic three-dimensional model of a torus represented by a volume penalization technique. We observe the appearance of a mean flow composed of a central vortex produced by the nonlinear interaction of the IWs. We show that this phenomenon is in agreement with the theory of Davidson *et al.* [1] for a rotating fluid. Using Dirac ring forcing in the linear regime, we obtain the dependence on the propagation angle of the vertical kinetic energy at the focal point, that reaches a maximum for  $\theta_f = 35^\circ$ , in agreement with the linear theory developed by Liu *et al.* [2]. A similar angle is observed in the 3D torus forcing case for both linear and nonlinear simulations: the angle  $\theta_f = 30^\circ$  maximizes the vertical velocity and dissipation, attesting of an optimal energy transfer from the oscillating source to the focal region. In the nonlinear regime, we obtain the detailed spectral distribution of the kinetic energy in the focal zone, and we develop a spatio-temporal analysis of the velocity field that shows a wide presence of IW in the flow. Moreover, we identify triadic resonances of IWs that lead to the production of the turbulent patch and of a large-scale mode similar to the geostrophic mean flow.

## I. INTRODUCTION

Geophysical and astrophysical flows are often submitted to a buoyancy force induced by stable stratification and/or to Coriolis force, respectively, induced by rotation, respectively leading to the appearance of internal gravity waves (GW), inertial waves (IW), or inertial gravity waves (IGW) when stratification and rotation are both present. In the dynamics of

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liquid cores of planets [3] or Earth’s equatorial atmosphere [4] IWs play an important role, whereas GWs are particularly present in the ocean even when coupled to large-scale motion due to rotation. In the ocean, the energy injected by the tides leads to internal gravity waves that propagate and dissipate through various mechanisms, such as wave breaking, that eventually produce three-dimensional turbulence and enhance mixing [5]. In addition, these waves contribute to the transport of heat and dissolved greenhouse gases, which are important phenomena for climate modelling [6]. The conversion of tidal forces into internal waves occurs when tidal currents encounter the topography of the seafloor and emit internal gravity waves. Several of these waves can then interact with each other at remote distance of the topography and eventually produce a local zone of turbulence that geophysicists call *remote turbulence* [7].

Remote turbulence is the result of local conversion of energy due to wave transport and wave breaking occurring at remote topography. Energy exchanges between waves of different scales and local eddies can then concentrate turbulent energy to varying degrees. But geometry also plays an amplifying role when the rays of the waves are concentrated in a localized region called the focal zone. Such geometric effects can be due to a horizontal curvature of the topography, as confirmed by in situ measurements in an oceanic canyon [8], in a strait [9], or in an enclosed crater [10]. Several studies have investigated the focusing of conical waves generated by an oscillating sphere in an inviscid stratified fluid [11], by vertical oscillations of a horizontal disc in a stratified fluid [12], by a librating disc in an inertial wave context [13, 14] or by periodic axial compression in a closed rotating cylinder of gas [15]. More complex shapes were also considered such as background topography in the form of a circular ring with a Gaussian cross-section or an elliptical ring [both by 16] or a horseshoe-shaped ring [17] under tidal forcing. In the case of circular ring with a Gaussian cross-section, the amplification rate of the waves when focusing was obtained using linear theory [16].

The configuration of a ring with a Gaussian cross-section can be geometrically idealized in a flow containing an oscillating torus-shaped solid ring, hence reproducing the focusing of waves at the apex of the propagation cone with an angle  $\theta_f$  (figure 1b). Many configurations are possible, from experiments with a single torus [18] to experiments with a wave generator containing multiple concentric tori which can be configured to focus the waves [19]. Several studies in stratified or rotating fluids have analyzed this torus configuration: numerical

simulations and experiments of IWs by Duran-Matute *et al.* [20], experiments of GWs [18, 21–23] and of IGW [22], analysis and linear theory of GWs [24], or linear theory of IWs [2]. Since GWs and IWs are both transverse waves with similar dispersion relations, their dynamics can be expected to be comparable, at least qualitatively. In particular for IWs waves in a rotating flow, if the axis of rotation is along the vertical direction  $z$  with the rotating rate  $\Omega_z$ , the relation between frequency  $\omega_{dr}$  and wave vector  $\mathbf{k} = (k_x, k_y, k_z)$  of a propagating inertial wave satisfy the following dispersion relation [25]

$$\omega_{dr}(\theta) = \pm 2\Omega_z \sin \theta \quad (1)$$

where  $\theta(\mathbf{k})$  is the angle between  $\mathbf{k}$  and the horizontal plane, called propagation angle, such that  $\sin \theta(\mathbf{k}) = k_z/|\mathbf{k}|$  (see figure 1a). For gravity waves, the dispersion relation is similar by replacing the sine dependence in  $\theta$  by a cosine function, and the rotation rate by the stratification intensity parameter (Brunt-Väisälä frequency).

The structure of the waves emitted by an oscillating object changes depending on the presence of viscous effects. For instance, uni- and bi- modality for the waves emitted by a sphere are discussed by Voisin *et al.* [26]. Large viscosity yields a unimodal form: the waves appear as a single wave beam with maximum wave amplitude in its center, and they form a single focusing region [18, 21]. At low viscosity a bimodal form is observed, with each section of the torus generating two rays tangential to its boundary that cannot merge into a single wave beam due to low viscous diffusion, so that they lead to four focusing regions [22]. In both unimodal or bimodal form, the conical structure of the wave beams for the torus configuration is geometrically confined.

In terms of dynamics, the flow motion is either in a regime of linear wave superposition, or in a nonlinear regime of wave interactions with possible local overturning of the density in the stably stratified case [18], depending on the ratio between the amplitude of forced oscillations and the large radius of the torus, quantified by the Keulegan-Carpenter non-dimensional number (see section II). For the linear regime of waves, based on the theoretical work available for an oscillating sphere [26] and for an oscillating torus [21], one finds a preferential propagation angle  $\theta_p$  at which the growth of the fluid velocity amplitude in the focal region is maximal for GWs. For IWs in a rotating fluid, this preferential angle was found to depend on the parameters of the configuration when the local forcing is modelled as a Dirac ring [2]. At the angle  $\theta_p$ , the maximum wave energy is transferred from torus

oscillations to the vertical velocity in the focal zone, hence triggering a localized turbulent state when nonlinearities eventually kick in.

In the present work we use direct numerical simulations (DNS) to investigate the existence of an optimal propagation angle, in a configuration close to the theoretical approach assuming localized ring forcing, or by considering a full 3D model of the torus. A second question concerns the nonlinear wave regime, in which resonant triads are a mechanism of energy redistribution between waves at different scales, as experimentally demonstrated in a unimodal form [21] for GW and in a bimodal form for GWs and IGWs (by the addition of rotation) [22]. In the review of Dauxois *et al.* [27] about the instability of an GW beam, there are two mechanisms that lead to the energy exchange between different scales. The first is resonant triads between waves. The second is the generation of a mean flow from internal gravity waves beams by a streaming instability due to nonlinear interactions of the oscillating wave beam with itself. Can similar mechanisms be observed for IWs focusing in a rotation flow such as resonant triads and generation of mean flow? Alternatively, is there an optimal propagation angle that amplifies the focusing to its maximum when varying the Rossby number and keeping all other flow parameters unchanged? Although this last question was discussed by Shmakova and Flór [21] for the stratification with GWs, it is still pending in the case of pure rotation with IWs.

In order to answer these questions, we use direct numerical simulations (DNS) of a vertically oscillating torus in a rotating fluid to reproduce the phenomenon of wave focusing at the apex of the wave propagation cone. We use a systematic comparison between the linear and nonlinear DNS to contrast the two regimes when possible and to better highlight effects that are inherently nonlinear. In what follows, we first present the governing equations and the numerical framework in section II. In this section, we also expose the method used in DNS to model the forcing by the oscillations of a 3D circular torus or of an idealized ring of Dirac with negligible size. In section III, we highlight the bimodal form of our flow as well as the streaming-like instability that generates a mean flow observed by time-averaging. In section IV, we evidence the presence of a propagation angle that maximizes the transfer of energy from the torus to the focal zone by computing both the vertical velocity and the kinetic energy dissipation. Finally, in section V, we show that the flow is largely dominated by the presence of inertial waves driven by resonant triads.

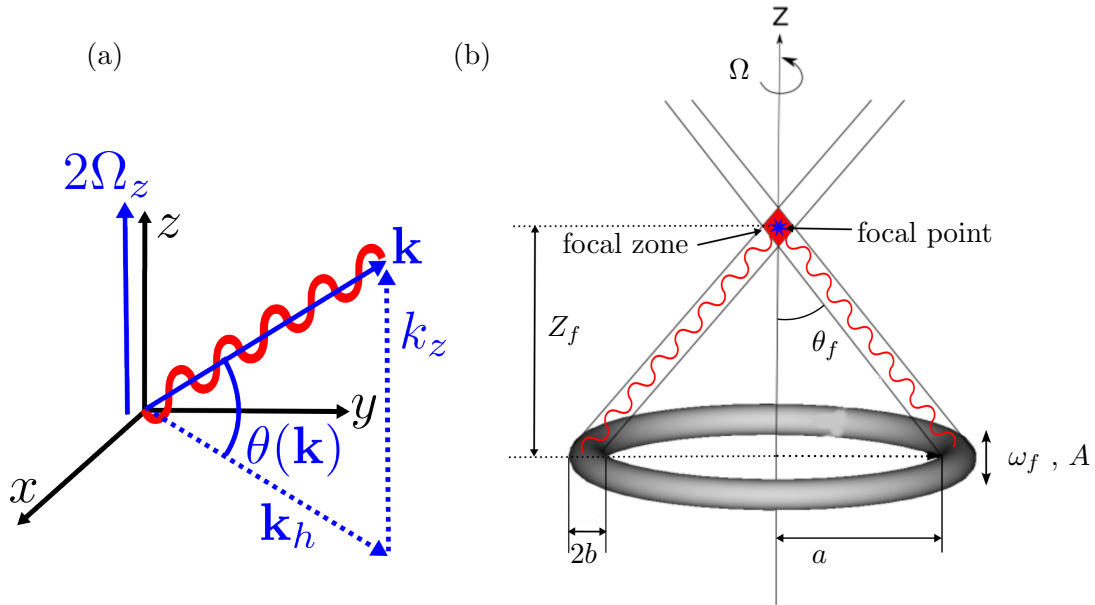


FIG. 1. (a) Illustration of a propagating inertial wave with wave vector  $\mathbf{k}$  and propagation angle  $\theta(\mathbf{k})$ . (b) Illustration of the conical focusing of inertial waves emitted by a torus vertically oscillating at frequency  $\omega_f$  with amplitude  $A$ .

## II. NUMERICAL SIMULATIONS

### A. Configuration and governing equations

We consider a rotating fluid submitted to a vertical oscillation of a torus at frequency  $\omega_f$  with amplitude  $A$  (figure 1b). The torus largest radius is  $a$  and its smallest radius  $b$ . It sends energy in the form of an inertial wave cone, that concentrates energy with maximum at the apex of the cone. The dynamics of this rotating incompressible flow is described by the Navier-Stokes equations in a rotating frame [25] with adequate forcing terms:

$$\frac{\partial \mathbf{u}}{\partial t} + \boldsymbol{\omega} \times \mathbf{u} = -\frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{u} - 2\boldsymbol{\Omega} \times \mathbf{u} + \mathbf{f} \quad (2)$$

$$\nabla \cdot \mathbf{u} = 0 \quad (3)$$

where  $\mathbf{u}$  is the velocity field,  $\boldsymbol{\omega} = \nabla \times \mathbf{u}$  is the vorticity,  $p$  is a modified pressure that includes the centrifugal hydrostatic pressure.  $\boldsymbol{\Omega} = [0, 0, \Omega_z]$  is the angular velocity with constant vertical rotation rate  $\Omega_z$ ,  $\rho$  is the density and  $\nu$  is the kinematic viscosity. The forcing term  $\mathbf{f}$  allows to model the effect of the oscillating solid body with a forced frequency  $\omega_f$  and amplitude  $A$  on the rotating fluid. For example, the classical Saint-Andrew's cross-

shaped pattern of propagation of inertial waves is obtained by a point-wise Dirac forcing oscillating with a frequency  $\omega_f$ , at a location  $\mathbf{x}_0$ , with  $\mathbf{f}(\mathbf{x}, t) = [0, 0, A \sin(\omega_f t) \delta(\mathbf{x} - \mathbf{x}_0)]$ . In this paper, we study the oscillations of a 3D solid circular torus and of an idealized Dirac ring model. The latter simplifies the torus as a circular ring with negligible size, whose effect is represented by a local volume force in the momentum equation mathematically expressed as a Dirac delta function. This permits to retrieve the analytical results of Liu *et al.* [2] and to study the maximization of the focusing effect. This configuration of the Dirac ring is a guide to the exploration of parameters in the case of the 3D solid torus. Therefore, the two configurations are obtained numerically by using two kinds of body forces with different characteristics:

1. The vertically oscillating Dirac ring of radius  $a$  is modelled by a volume forcing as

$$\mathbf{f} = \begin{bmatrix} 0 & 0 & A_0 \sin(\omega_f t) H_0^{\text{DR}}(\mathbf{x}) \end{bmatrix} \text{ with } H_0^{\text{DR}}(\mathbf{x}) = \delta(|\mathbf{x}| - a) . \quad (4)$$

where  $A_0$  is the inertial forcing amplitude.

2. The vertically oscillating 3D torus is modeled by using a volume penalization method [28, 29]. The penalization method was originally developed by Arquis *et al.* [30] to model the interface between a fluid and a porous medium with a ratio  $\eta$  between permeability and viscosity. In this method, the Navier-Stokes equation applies to both the porous medium and to the fluid, distinguished only by the forcing term that localizes the porous medium separately from the remaining fluid via a spatial mask function. Angot *et al.* [31] demonstrated that when  $\eta \rightarrow 0$  the penalized region of the porous medium represents adequately a solid and the global solution converges to a solution with no-slip boundary condition on the surface of the solid surrounded by fluid. The forcing term for penalization is thus

$$\mathbf{f} = \frac{1}{\eta} (\mathbf{u} - \mathbf{u}_s) H^{\text{T}}(\mathbf{x}, t) \quad (5)$$

where  $H^{\text{T}}(\mathbf{x}, t)$  is a mask function representing a torus-shaped solid body moving with vertical velocity  $\dot{z}(t) = A\omega_f \sin(\omega_f t)$ . Thus,  $\mathbf{u}_s = [0, 0, \dot{z}(t)]$  is the velocity of a point on the torus due to vertical oscillation. The mask function is based on a solid torus body with largest radius  $a$  and smallest radius  $b$  as indicated in figure 1(b), and is

defined at time  $t = 0$  as

$$H_0^T(\mathbf{x}) = \begin{cases} 0 & \text{if } \mathbf{x} \notin \text{torus,} \\ 1 & \text{if } \mathbf{x} \in \text{torus .} \end{cases} \quad (6)$$

In Fourier space, we denote by  $\hat{*}$  the Fourier coefficient for a wave number  $\mathbf{k} = (k_x, k_y, k_z)$ . The oscillating motion  $z(t) = -A \cos(\omega_f t)$  of the solid can therefore be represented as the following phase change of the Fourier modes [28]

$$\hat{H}^T(\mathbf{k}, t) = \hat{H}_0^T(\mathbf{k}) e^{-ik_z z(t)} . \quad (7)$$

In both torus and Dirac ring, the regions oscillating at forcing frequency  $\omega_f$  emit inertial waves propagating at an angle  $\theta_f$  if  $\omega_f$  satisfies the dispersion relation (1) of inertial wave *i.e.*  $\omega_f = \omega_{dr}(\theta_f)$ . This leads to

$$\theta_f = \sin^{-1}(\omega_f / 2\Omega_z) . \quad (8)$$

Inertial waves propagating at an angle  $\theta_f$  have no typical scale, so that their wavelength can range from large to small, in relation to the source size. Since the system is symmetric around the  $z$  axis and the waves form a cone of propagation, the main difference between the two configurations is that the Dirac ring produces a single focal point at height

$$Z_f = a \cot \theta_f \quad (9)$$

whereas the 3D torus produces a wider focal zone (figure 1b) whose size is related to the torus radius  $b$ .

The difference in the injected power from the Dirac ring and the 3D torus, particularly in terms of their spectral breadth, is discussed in Appendix A.

## B. Parameters and numerical setup

Equations (2) and (3) are solved using a standard pseudo-spectral method in a  $2\pi$ -periodic cubic domain, and using a spatial resolution of  $512^3$  points. In the 3D torus configuration with forcing (5), the penalization term is solved implicitly with  $\eta = 10^{-6}$  s [29, 32]. The oscillations close to the torus wall due to the discontinuity of the  $H_0^T$  function are filtered as in Kolomenskiy & Schneider 2009 ([28] Appendix A) with a gaussian smoothing function

DR DNS	1	2	3	4	5	. . . .	23	24	25
$2\Omega_z$	5.077	5.32	5.77	6.52	6.62	. . . .	9.7	10	14.61
$\theta_f$	80°	70°	60°	50°	49°	. . . .	31°	30°	20°
$Ro(\times 10^{-2})$	1.96	1.88	1.73	1.53	1.51	. . . .	1.03	1	0.68
$\omega_{\min}$	0.25	0.25	0.25	0.25	0.25	. . . .	0.25	0.25	0.25
$\omega_{\max}$	125	125	125	125	125	. . . .	125	125	125

T DNS	1	2	3	4	5	6	7	8	9	10
$2\Omega_z$	1.53	1.77	1.99	2.08	2.19	2.3	2.37	2.51	2.97	3.67
$\theta_f$	55°	45°	39°	37°	35°	33°	32°	30°	25°	20°
$Ro(\times 10^{-2})$	1.37	1.18	1.05	1	0.96	0.91	0.88	0.83	0.7	0.57
$\omega_{\min}$	0.126	0.126	0.126	0.126	0.126	0.126	0.126	0.126	0.126	0.126
$\omega_{\max}$	251	251	251	251	251	251	251	251	251	251

TABLE I. Simulation parameters for the case of Dirac ring, labeled DR, for which only linear DNS are run, and for the 3D torus configuration, labeled T, for which linear and nonlinear DNS are run. For the DR DNS runs numbered 4 to 24,  $\theta_f$  varies from 40° to 60° by increments  $\Delta\theta_f = 1^\circ$ . The tables show the following values for DR and T configurations: the frequency of the fastest IW is  $2\Omega_z$ , the forcing frequency is  $\omega_f = 5$  or  $\omega_f = 1.256$  and the corresponding respective Rossby numbers are  $Ro = \omega_f A / (a\Omega_z)$  for DR and  $Ro = \omega_f A / (2b\Omega_z)$  for T. The frequency  $2\Omega_z$  must be compared with the maximum pulsation  $\omega_{\max} = 2\pi/\Delta t$  and minimum one  $\omega_{\min} = 2\pi/T$  solved in the 4D Fourier transform for which the time series is characterized by its period  $T = N\Delta t$ , number of points  $N$  and interval  $\Delta t$  (same parameters as the DNS time discretization).  $N = 2000$ ,  $\Delta t = 0.025$  for the T configuration, and  $N = 500$ ,  $\Delta t = 0.05$  for the DR configuration.

$\hat{H}_0^T(\mathbf{k})e^{-C_s(k_x^2/N_x^2+k_y^2/N_y^2+k_z^2/N_z^2)}$  where  $C_s = 16$  and  $N_x, N_y, N_z$  the resolution in each direction. This gives a thicker mask function, and we note that Hester *et al.* [33] recently showed that it is possible to get second-order convergence with the penalisation method by using a carefully chosen adequate thickness of the mask function.

The flow produced by the oscillation of the 3D torus depends on several parameters: the geometry of the torus with radii  $(a, b)$ , the oscillation frequency  $\omega_f$  and amplitude  $A$ ,

the rotation rate  $\Omega_z$ , the kinematic viscosity  $\nu$ . By using  $T_0 = \omega_f^{-1}$ ,  $L_0 = 2b$ ,  $U_0 = A\omega_f$ ,  $\rho_0$  and  $P_0$  as characteristic time, length, velocity, density and pressure respectively, the non-dimensional form of (2) without forcing is

$$\frac{1}{Ke} \frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} = -E \nabla p + \frac{1}{Re} \nabla^2 \mathbf{u} - \frac{2}{Ro} \mathbf{e}_z \times \mathbf{u}$$

where  $Ke = A/2b$  is the Keulegan-Carpenter number that represents the ratio of the forcing amplitude to the minor radius of the torus where  $E = P_0/(\rho_0 U_0)$  is the Euler number,  $Ro = A\omega_f/(\Omega_z 2b)$  is the Rossby number and  $Re = A\omega_f 2b/\nu$  is the Reynolds number. Classically, the reference pressure  $P_0$  is not known and the default choice is  $E = 1$ . In that case,  $Ke$ ,  $Re$  and  $Ro$  characterize the flow. In a similar torus configuration in a stratified fluid, one can introduce the Stokes number  $St = Re/Ke = \omega_f b^2/\nu$  to study the linear waves. [18]

For Dirac ring forcing, the non dimensional numbers are obtained by changing  $2b$  into  $a$  and  $A$  into  $A_0/\omega_f^2$ . In this study, we focus on the search for the optimal propagation angle  $\theta_f$  that maximizes the energy focusing of the inertial waves, so that we restrict the parameter space by keeping constant the geometrical parameters of the 3D torus ( $a = 0.848$ ,  $b = 0.0942$ ) and of the Dirac ring ( $a = 1$ ). With these values, the focal point remains in the domain for all the forcing angles considered in our simulations in a cube of vertex length  $2\pi$ .

In addition, when exploring the angle dependence of the energy-focusing efficiency with  $\theta_f$ , we keep constant the three parameters  $Re \gg 1$ ,  $Ke \ll 1$  and  $St \gg 1$  by keeping constant  $\nu$ ,  $A$  and  $\omega_f$ . We vary only the rotation rate  $\Omega_z$  while ensuring  $Ro \ll 1$ . Note that inertial waves appear at low Reynolds and low Rossby numbers, whereas in the regime of high Reynolds and low Rossby numbers, wave-turbulence interactions are expected to occur [34].

Two sets of direct numerical simulations have been run for the two configurations. For the Dirac ring configuration, we run only linear simulations obtained by setting  $\boldsymbol{\omega} \times \mathbf{u} = \mathbf{0}$  in equation (2), for comparison with the analytical results of Liu *et al.* [2]. We choose  $\Delta t = 0.05$ ,  $\nu = 10^{-4}$ ,  $A_0 = 0.01$ ,  $\omega_f = 5$  so that  $Re = 100$ ,  $Ke = 0.0004 \ll 1$  and  $St = 50000 \gg 1$ . 25 linear simulations use propagation angles from  $\theta_f = 20^\circ$  to  $80^\circ$  adjusted by varying the rotation rate in the range  $2\Omega_z = 5.077$  to  $14.61$ ; therefore  $Ro \ll 1$  varies from  $0.0038$  to  $0.00136$  (see Table I). A tentative non linear DNS shows that most of the energy sent into the fluid feeds eddies that are close to the Dirac ring and not in the focal point, so with little influence in the focal region.

For the 3D torus configuration, the 10 simulations correspond to parameters detailed in Table I. They consist of a first linear simulation (again with  $\boldsymbol{\omega} \times \mathbf{u} = \mathbf{0}$ ) run for a sufficiently long time so that the wave network has time to establish in the geometrical domain. The network is a side effect of the periodic boundary conditions, but similar reflections exist in physical experiments in containers with plane walls. A sponge zone technique [35] could be implemented numerically to absorb waves, but with a high numerical cost due to the enlargement of the domain, an increase of dissipation due to the buffer zone and small wave reflection. As far as we know, laboratory experiments are obtained either in the presence of rigid walls or in the presence of free interfaces (water surface). We also tested the effect of a rigid horizontal wall using the penalization method on our results. It shows that dissipation and energy in the bulk flow are twice larger in the presence of the wall than with periodic conditions. However, the concentration in the focal zone (the ratio of the focal zone to the total) is about the same for energy and dissipation. In addition, these linear simulations can be compared to the linear simulations in the configuration of the Dirac ring. Starting with this linear flow state we then pursue fully nonlinear DNS with  $\boldsymbol{\omega} \times \mathbf{u} \neq \mathbf{0}$ , to study the nonlinear focusing of the inertial waves that produces local turbulence in the focal region. For the ten DNS, we choose  $\Delta t = 0.025$ ,  $\nu = 10^{-5}$ ,  $A = 0.0157$ ,  $\omega_f = 1.256$  so that  $Re = 372$ ,  $Ke = 0.083 \ll 1$  and  $St = 1115 \gg 1$ . The simulations differ by their forcing angles  $\theta_f$  from  $20^\circ$  to  $55^\circ$  adjusted by varying  $2\Omega_z \in [1.53, 3.67]$  and therefore  $Ro \in [0.057, 0.137]$ , again maintaining  $Ro \ll 1$  (see Table I). Figure 2 shows a time series of the vertical velocity including the linear and non-linear phases of the simulation. For the majority of DNS, convergence in the linear phase requires a duration of about  $150T_{\Omega_z}$  where  $T_{\Omega_z} = 2\pi/\Omega_z$  is the rotation period of the fluid.

Although we keep  $Ke$  and  $Re$  constant and vary only  $Ro$  in our simulations, one can also discuss the role of the Ekman number  $Ek = Ro/Re = \nu/(\Omega 2b)$  in relation with the presence of boundary layers on the torus. The wave beams originate from the oscillating torus due to the oscillating Ekman boundary layers that break at critical latitudes into inertial waves. One can estimate the transport velocities of the shear layer and therefore of the waves, which vary between  $Ek^{1/6}$  and  $Ek^{3/10}$  (see figure 1 in [36]). In our DNS, this means that velocities injected in waves vary from about  $\sim 15\%$  to  $\sim 30\%$  between low and high  $Ro$ .

Nevertheless, the viscous spreading of the wave beam (size and amplitude) and the associated decay of the velocity and vorticity envelopes depend on the distance  $x$  from the

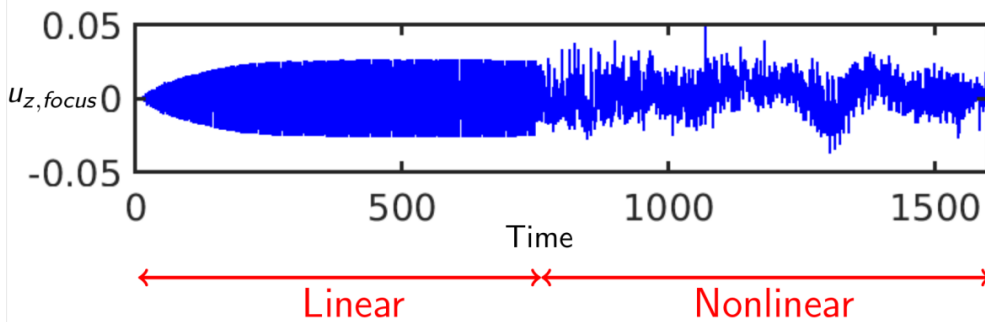


FIG. 2. Time series of vertical velocity  $u_{z,\text{focus}}$  at the focal point  $Z_f$  in the case  $\theta_f = 33^\circ$  from our DNS in the torus configuration.

source and on the viscous length  $l = (\nu/(2\Omega_z \sin \theta_f))^{1/2}$  [37, 38]. Hence, by varying only  $\Omega_z$  in the DNS and keeping  $\omega_f$  constant,  $l \simeq 2.8 \cdot 10^{-3}$  remains constant, all the beams undergo the same decay and arrive in the focal zone with the same energy loss whatever the  $Ro$ . This would not be the case if  $\Omega_z$  were kept constant and  $\omega_f$  varied in order to keep  $Ek$  constant and also the wave velocity. With the chosen values of  $\omega_f$  and  $\theta_f$  from  $55^\circ$  to  $20^\circ$ ,  $l$  variation is 55%. Our choice is to retain the same beam characteristics with a slight reduction in energy.

### III. ORGANISATION OF THE FLOW

#### A. Focal zone and wave structure

We analyse here the organisation of the flow for the 3D torus configuration for both the linear stage and the following nonlinear regime.

Due to the vertical axial symmetry of the torus, the velocity field in the linear case is expected to be also symmetric, since no symmetry-breaking mechanism is present. Therefore, in this regime, the superposition of all the propagating inertial waves results in zero horizontal velocity and maximal vertical velocity on the central axis of the focal zone. This is observed in figures 3(a) for the 3D distribution around the torus and 3(c) for the 2D vertical plane cut distribution of the instantaneous vertical velocity field from the linear simulation at propagation angle  $\theta_f = 33^\circ$ . Moreover, the inertial waves have the form of

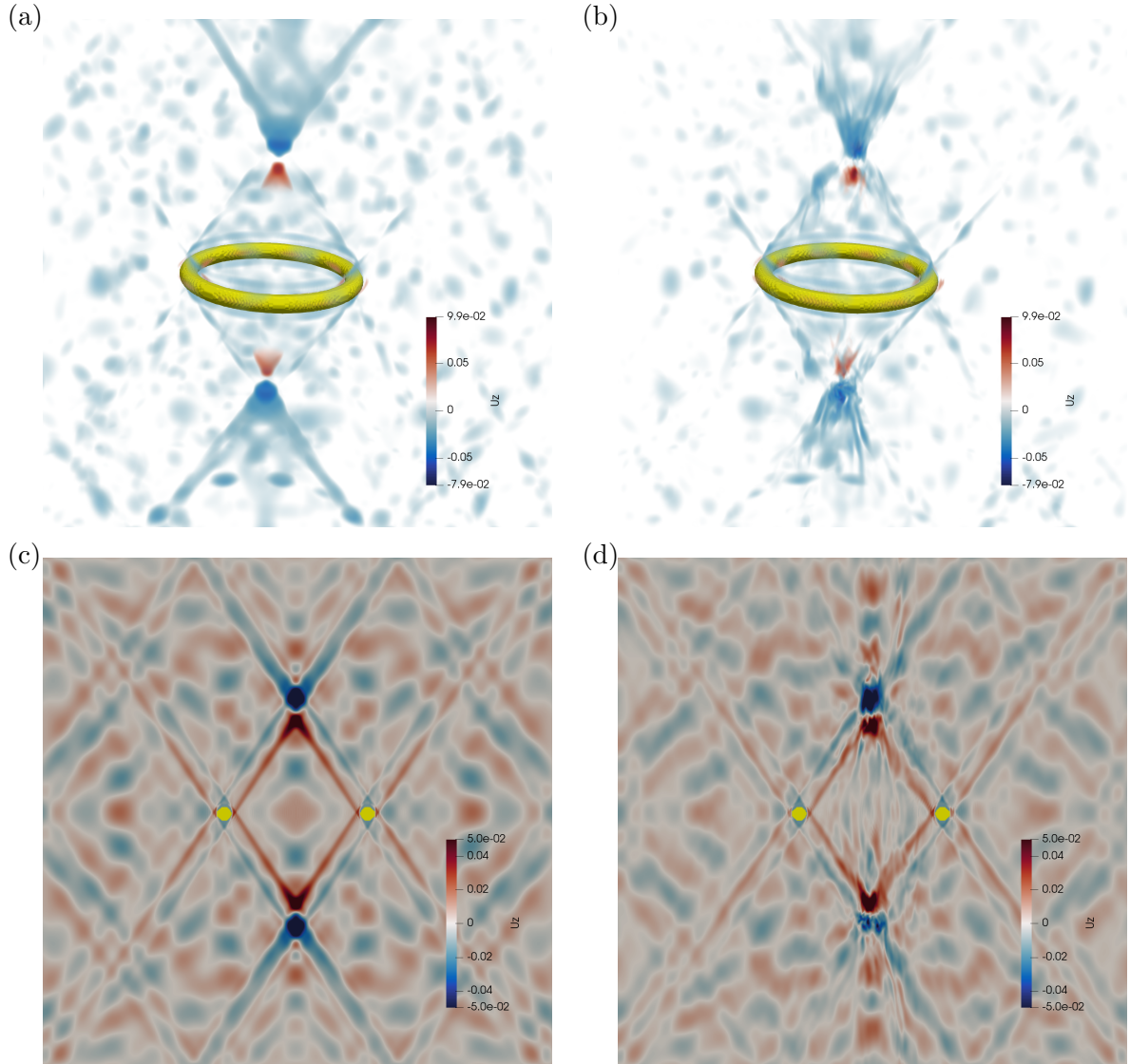


FIG. 3. Visualisation of the instantaneous vertical velocity  $u_z$  at a given time  $t$  from a numerical simulation with  $\theta_f = 33^\circ$  with oscillating 3D torus (shown in yellow). Linear simulation results with (a) 3D volume rendering (values of  $u_z$  close to 0 are transparent), and (c) in a 2D vertical  $(x, z)$  plane. Nonlinear simulation (b) for 3D volume rendering and (d) in a 2D vertical plane.

a bimodal beam since each section of the torus generates two rays tangential to the torus boundary. Figures 3(a) and (b) also show that these rays do not merge into a single wave beam by diffusion as in other cases [22] because the Stokes number  $St = 1115 \gg 1$  is too large for this to occur, as discussed in the Introduction.

Panels (b) and (d) of figure 3 show the vertical velocity distributions for the nonlinear

regime. They reveal that the initial concentration of vertical velocity in the focal zone due to linear superposition of waves eventually turns into non linear interactions that create a localized turbulent state. The 3D visualization of figure 3(b) shows that the overall organization of the flow has a conical shape consistent with the cylindrical symmetry, and the maximum velocity is located in the focal zone. The vertical section of figure 3(d) shows details of the flow organization inside the cone, with two main features: (i) secondary inertial waves emerging from the focal region and propagating at an intermediate propagation angle closer to vertical than the incoming waves; (ii) a vertical structure reminiscent of Taylor-like columns in rotating flows. Overall, the nonlinear flow is slightly different but not too far from the linear wave propagation flow. The corresponding regime is therefore that of weak wave turbulence, with the addition of a vertical mode that will be further commented in the next section III B.

## B. Main averaged flow

The main averaged flow is obtained by time-averaging the velocity field over  $N$  times, as

$$\bar{\mathbf{u}}(\mathbf{x}) = \frac{1}{N} \sum_{i=1}^N \mathbf{u}(\mathbf{x}, t_i) . \quad (10)$$

The main averaged flows in the linear and non linear regimes are shown in figure 4. In the linear DNS (figure 4a), inertial waves are linearly superimposed and disappear when averaged, even in the focal zone. All that remains is the main flow that contains two large-scale rotors in the form of two cylinders turning clockwise and counter-clockwise and elongated in the vertical direction (corresponding to a small vertical wavenumber  $k_z \simeq 0$ ) with a radius of the order of the large torus radius. Indeed, under the assumption of linearity and stationary, the linear Taylor-Proudman theorem [39] can be applied so that  $\partial u_z / \partial z = 0$ . The flow is therefore invariant along the  $z$ -axis and is two-dimensional with two (2D2C) or three velocity components (2D3C). The vertical displacement imposed by the torus is therefore reflected throughout the fluid column above the torus to ensure that  $\partial u_z / \partial z = 0$ . One concludes that the large scale observed in linear simulation appears as a classical Taylor column triggered by the displacement of a solid body in a rotating fluid.

An important question concerns the persistence of such Taylor columns in turbulent regimes. Large structures identified to geostrophic modes [40] are observed in rotating flows

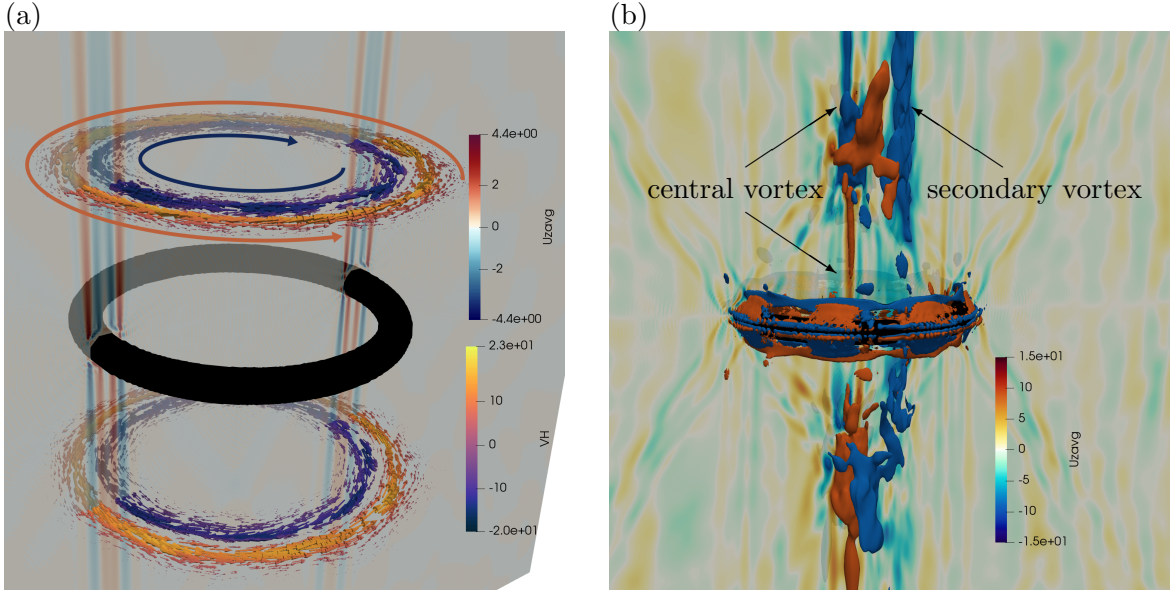


FIG. 4. Visualisation of the averaged velocity from DNS at  $\theta_f = 33^\circ$  (the 3D torus is in black). (a) 3D visualisation of averaged vertical velocity  $\bar{u}_z$  (blue to red) and velocity vector in two horizontal cuts coloured by the average horizontal velocity  $u_h^{avg}$  (black to yellow) in the linear simulation. (b) 3D visualisation of vertical average velocity  $\bar{u}_z$  (blue to red) in a vertical cut and two iso-surfaces of  $\bar{u}_z = \pm 9$  (chosen at 12.1% of the maximum of  $u_z$ ) in the non linear simulation.

in experiments by Brunet *et al.* [41] where the flow is forced by oscillating cylinders, by Boury *et al.* [42] where a trapezoidal domain is forced by a wave generator, or in simulations by Le Reun *et al.* [43] where the flow is excited by the elliptical instability. Geostrophic modes are similar in shape to Taylor columns, but with richer dynamics.

In our nonlinear simulations, the main averaged flow observed in figure 4b is rather different. First, we observe that the Taylor columns remain but are significantly weaker than a central and secondary vortex that appears along the vertical axis of the torus. This vortex appears to originate from the focal zone and to extend towards the central point of the torus. It was already observed in experiments and DNS by Duran-Matute *et al.* [20]. Second, as will be quantitatively confirmed in section V, the flow is dominated by waves, so that we expect that the central vortex energy comes from a conversion of wave energy due to nonlinear mechanisms.

In the context of rotating fluids, the theory of Davidson *et al.* [1], confirmed by the numerical experiments of Ranjan and Davidson [44], is the one that comes closest to our

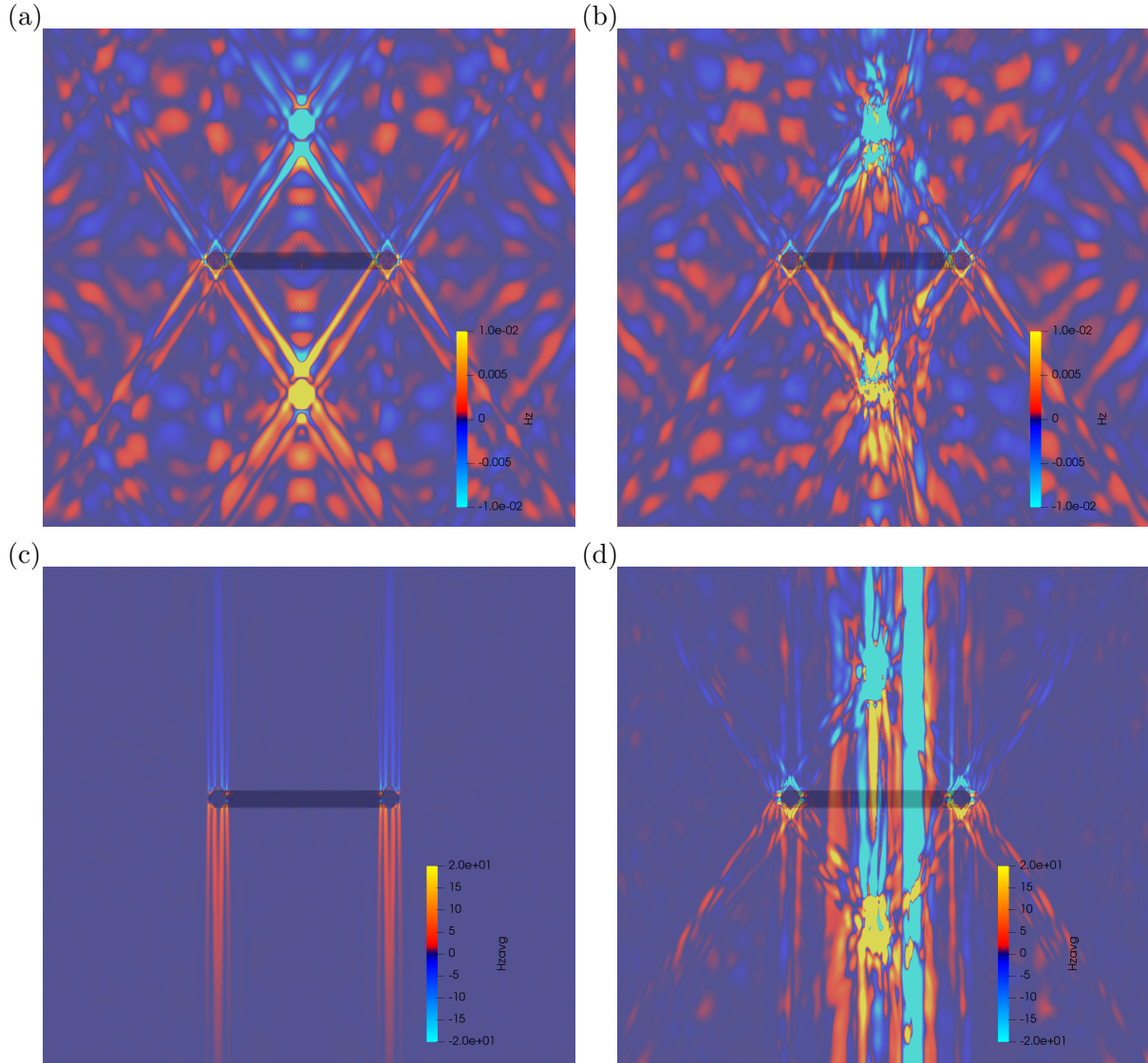


FIG. 5. Distribution of vertical helicity in a vertical plane containing the axis of symmetry, for  $\theta_f = 33^\circ$  in simulation for the 3D torus. Colors: red for positive helicity and blue for negative helicity. (a) linear and (b) non linear data for the instantaneous vertical helicity  $\mathcal{H}_z$ ; (c) linear and (d) non linear data for the averaged vertical helicity  $\mathcal{H}_z^{\text{avg}}$ . The shadow of the torus is shown in black. The domain shown is only 5/6-th of the size of the calculation box, which is  $2\pi$ .

configuration among the few theories that explain the emergence of columnar vortices. This theory is based on the linear emission of inertial waves by a localised patch or ‘blob’ of turbulence produced by nonlinear interactions. Inertial waves emitted from this blob propagate at faster group velocity for low frequency  $\omega \simeq 0$  in the vertical direction ( $\mathbf{k} \perp \boldsymbol{\Omega}$ ) than for

any higher frequency in other directions. They impose themselves on the flow, giving rise to columnar features. Non linear effects on inertial waves acting over longer periods of time are supposed to develop and maintain this structure. In the present non linear simulations, the focal zone can be considered as a blob resulting from non linear interactions of inertial waves, unlike the focal zone in the linear case which is a mere linear superposition of inertial waves. Helicity is in the following used as a diagnostic to confirm that these structures are formed by inertial waves, as proposed by [44], since inertial waves with negative helicity propagate upwards (relative to the axis of rotation), while waves with positive helicity propagate downwards.

In order to confirm this, we plot in figure 5 the distribution of the vertical helicity  $\mathcal{H}_z = u_z \omega_z$  of the instantaneous flow and helicity  $\mathcal{H}_z^{\text{avg}} = u_z^{\text{avg}} \omega_z^{\text{avg}}$  of the mean averaged flow in a vertical plane. The helicity for the instantaneous and averaged fields obtained by linear simulations are shown in figures 5(a) and (c) respectively. The distribution of instantaneous field helicity is directly related to the propagation of the inertial waves, and is concentrated along the rays of propagation of the waves and in the focal region. When averaged over several dozen periods, the (periodic) wave pattern disappears from the distribution of the flow helicity, while the Taylor column remains, having negative helicity above, and positive helicity below the ring. The flow has zero background helicity, and overall, the net helicity, obtained by summing over the domain, is zero.

Helicity in the nonlinear regime is shown in figures 5(b) and (d) for the instantaneous and averaged fields, respectively. The distribution of the instantaneous field reminds that of the linear case from the presence of the waves propagation pattern. However, the non linear interactions produce secondary waves emitted from the focal region, as well as a vertical mode in the vicinity of the axis of symmetry. We also note that the helicity amplitude is very similar in linear and non linear simulations, and this is true as well for the averaged flow helicity. The latter is plotted for the non linear DNS in figure 5(d). By definition, averaging a field means filtering the low frequencies  $\omega \simeq 0$  in the linear and non linear cases. Inertial waves such as  $\omega \simeq 0$  are then filtered out. In contrast to the linear case, the wave pattern of primary propagating waves emitted by the torus, is still present. Background helicity far from the centre region is small, if not zero.

Most striking is that the averaged helicity distribution (for the nonlinear DNS) reveals a maximum of concentration in and around the focal region, that extends throughout the

vertical extent of the fluid domain. The average shown in figure 5 (d) shows that the helicity  $\mathcal{H}_z^{\text{avg}}$  in the central vortex, is of sign opposite to the helicity in the wave cones, which seems to be a signature of the evolution of a turbulent cloud under rotation. The development of the central vortex observed here is in agreement with with the description by of Davidson *et al.* [1] and Ranjan and Davidson [44] for grid turbulence and DNS of homogeneous turbulence.

For the sake of a critical discussion of various theories, one can mention Greenspan’s 1969 [40] theorem that prohibits the formation of geostrophic modes (close to the columnar vortex) by exact resonant triadic mechanism in a rotating fluid. Two other mechanisms can bypass Greenspan’s theorem and transfer energy from wave interaction to columnar vortex such as quasi-resonant triadic interactions [45, 46] and quartetic interactions [41, 47]. In fully-developed rotating turbulence, it was shown that the geostrophic mode is largely dominated by wave/wave interactions [48] without identification of the precise mechanisms. It is note easy to isolate such wave/wave interactions in wave turbulence or in fully-developed turbulence, and all the more in our geometry where turbulence is confined and concentrated within a small region. Other theories may explain the generation of a main flow such as streaming instability observed in experiments of stratified fluid [27, 49], but it is yet to be adapted to rotating fluids. A possible hint is the role of helicity, which we have used as a diagnostic tool in the framework of Davidson’s theory, but helicity plays also an important role in the transition from three- to two-dimensional turbulence without the presence of waves [50–52]. In this transition, the level of helicity in spatial triads plays an important role (for further reading see [50] and [51]).

#### IV. MAXIMUM ENERGY TRANSFER IN THE FOCAL ZONE

In order to characterize the efficiency of the energy input by the forcing into the focal region, we investigate hereafter the evolution with  $\theta_f$  of the *rms* (root mean square) vertical velocity in this region — which amounts to evaluating the vertical kinetic energy —, and of the kinetic energy dissipation.

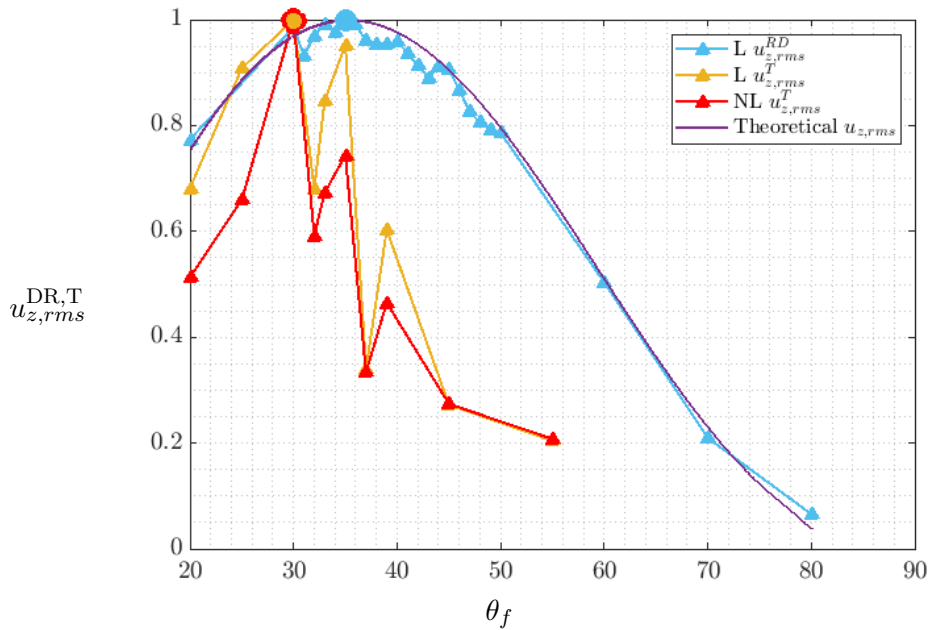


FIG. 6. Rms of vertical velocity  $u_z$  in the focal zone as a function of the propagation angle  $\theta_f$ : solid purple curve without symbols for the theoretical result of Dirac ring configuration adapted from Liu *et al.* [2]; cyan triangles for the linear numerical simulations for the ring of Dirac configuration (DR index); orange triangles for the 3D torus configuration (T index) in the linear simulation, and red symbols for the non linear simulation. The large circles in blue and red indicate the maximum of each curve.

### A. Vertical velocity in the focal zone

Due to axisymmetry, the linear superposition of waves at the focal point results in a concentration of vertical velocity and zero horizontal velocity. We investigate this property and compare it to the non linear regime obtained by DNS. For that, we start by defining a neighbourhood of the focal point in which we quantify the energy coming from the oscillating torus that feeds the vertical velocity. Both the 3D torus and the ring of Dirac configurations are considered in the numerical simulations.

For the ring of Dirac configuration, we compute the vertical velocity  $u_z$  in a small cube around the theoretical position of the focal point at altitude  $Z_f$  computed in equation (9). This cube is defined by the four grid cells surrounding the focal point and is denoted  $C^{\text{DR}}$ . For the 3D torus configuration, the focal zone is spread out, and we define it as the points

inside a sphere  $C^T$  of radius  $R = 0.5$  with a center at height  $Z_f$ . The location of  $C^T$  is shown in figure 7. For the two configurations, we compute the *rms* vertical velocity averaged over  $N$  times  $t_i$  and in space over the cube  $C^{DR}$  or the sphere  $C^T$ :

$$u_{z,rms}^{DR,T} = \sqrt{\frac{1}{NN^{RD,T}} \sum_{j=1}^{N^{RD,T}} \sum_{i=1}^N (u_z(\mathbf{x}_j, t_i) - \bar{u}_z(\mathbf{x}_j))^2} \quad (11)$$

where  $\bar{u}_z(\mathbf{x}_j)$  is the time average of  $u_z$  at point  $\mathbf{x}_j$  in  $C^{DR}$  or  $C^T$  and  $N^{RD,T}$  is the number of points within  $C^{DR}$  or  $C^T$ .

We characterize the transfer of energy to the vertical velocity by computing the velocity amplitude and its dependence on  $\theta_f$ . Figure 6 shows the dependence of  $u_{z,rms}^{DR}$  and  $u_{z,rms}^T$  on  $\theta_f$ . For the Dirac ring case, the linear numerical simulation result matches closely the theoretical result derived from Liu *et al.* [2]. For the simulation and the theoretical results, the maximum vertical velocity in the focal zone is observed at  $\theta_{DNS}^{DR} \simeq 35^\circ$ . For the 3D torus configuration, we observe larger oscillations of the curves  $u_{z,rms}(\theta_f)$  than in the Dirac ring case. We attribute this to the higher sensitivity of the forced wave packets to the topology of the flow in the vicinity of the torus. Nonetheless, on figure 6 for the 3D torus configuration (obtained with nonlinear DNS), the amplitude curve clearly indicates a maximum at  $\theta_{DNS}^T \simeq 30^\circ$ , *i.e.* close to the value for the Dirac ring case.

These data can be compared with those obtained in the literature for stratified fluids in similar forced propagation of internal waves. The latter's dispersion relation corresponds to propagation angles  $\theta_{GW} = \pm N \cos^{-1}(\omega_f/N)$ , where  $N$  is the Brunt–Väisälä frequency (the stronger the stratification, the larger  $N$ ), differing only by the cosine function instead of a sine in the dispersion relation of rotating fluids (equation (8)). Transposing our results, we therefore expect  $\theta_{GW} = 90^\circ - \theta_{IW} \simeq 60^\circ$  in the case of stratification, close to the preferential angle  $\theta_{GW} \simeq 55^\circ$  observed by Maffioli *et al.* [53] in DNS of stratified turbulence mixing GW, eddies and large-scale structures, also in good agreement with the linear theory that maximizes the horizontal energy flux of GW found by Maffioli *et al.* [53]. It disagrees however with other results by Dohan and Sutherland [54] ( $\theta_{GW} \simeq 35^\circ$  from linear theory maximizing the GW vertical energy), by Shmakova and Flór [21] ( $\theta_{GW} = 35^\circ$ ), or by Voisin *et al.* [26] (analytical theory for a sphere or a cylinder). Note that the shape of the oscillating object as well as the different body force (gravity, Coriolis) could be responsible for the observed differences.

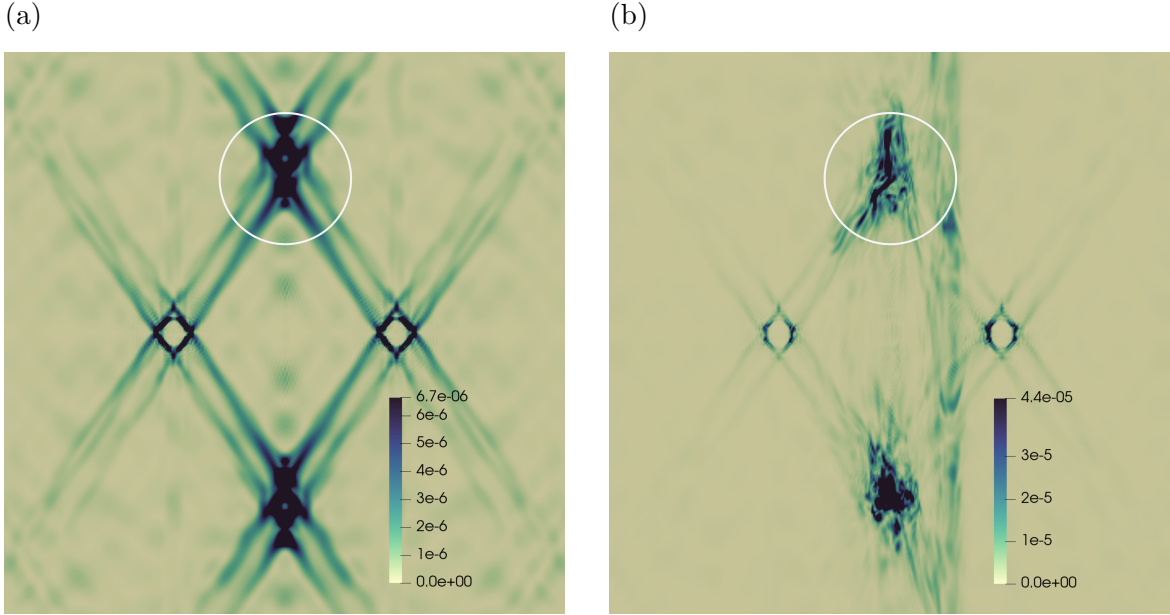


FIG. 7. Distribution of the instantaneous dissipation field  $\varepsilon(\mathbf{x}, t)$  in a vertical azimuthal plane, for the torus configuration, at  $\theta_f = 33^\circ$ . (a) linear simulation; (b) non linear simulation. The white circle delimitates the focal zone  $C^T$ .

## B. Dissipation in the focal zone

The energy sent by the torus and spatially propagated by the inertial waves is mainly dissipated in the focal zone. We compute the dissipation rate field in the fluid domain as  $\varepsilon(\mathbf{x}, t) = \nu (\nabla \mathbf{u}(\mathbf{x}, t))^2$  and plot its distribution in an azimuthal vertical plane in figures 7(a) and (b) for the linear and non linear simulations respectively, with  $\theta_f = 33^\circ$ . The strong concentration of dissipation in the focal zone  $C^T$  is clear, but the dissipation is concentrated in structures smaller in the non linear simulation than in the linear one, since the focal region appears as a turbulent patch. For the non linear simulation (figure 7b), the bottom focal zone exhibits a somehow more homogeneous concentration of dissipation than the top focal region. This is only due to the specific choice of azimuthal plane, which cuts through vertically elongated structures that rotate around the axis of symmetry and can be captured differently depending on their azimuthal location. In order to quantify the concentration of dissipation, we define a space- and time-averaged dissipation rate by grid point in a volume  $V$

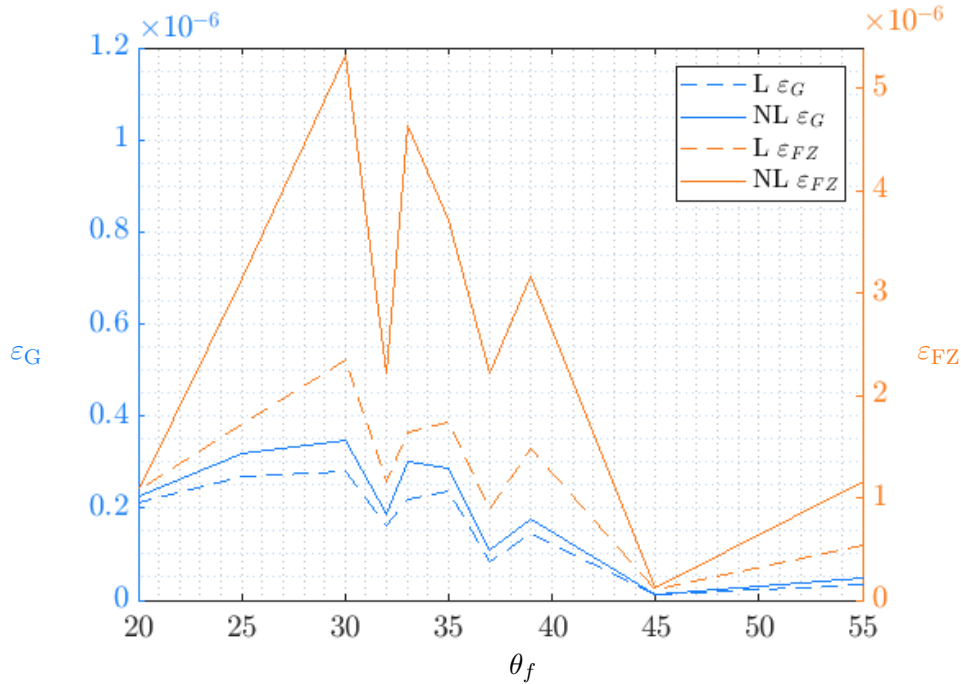


FIG. 8. Averaged dissipation rates  $\varepsilon_G$  in the whole fluid domain (blue curves) and  $\varepsilon_{FZ}$  in the focal zone (red curves), by numerical simulations for the 3D torus configuration. Solid lines for non linear simulation and dashed lines for the linear simulation, respectively noted NL and L.

as

$$\bar{\varepsilon} = \frac{1}{N(V)} \sum_{j=1}^{N(V)} \sum_{i=1}^N \varepsilon(\mathbf{x}_j, t_i) \quad (12)$$

where  $N(V)$  is the number of grid points in  $V$ ,  $\mathbf{x}_j \in V$  and  $N$  is the number of times for averaging. We compute the dissipation rate in the focal region named  $\varepsilon_{FZ}$  by applying the average (12) to the focal zone with  $V = C^T$ . Moreover, we compute the global dissipation in the whole domain named  $\varepsilon_G$  by applying (12) to the global fluid volume. We compare the two dissipation rates in figure 8 for different values of  $\theta_f$  for linear and non linear simulations of the flow forced by the torus. As expected, more energy is dissipated in non linear simulations than in linear ones, and the concentration of energy in the focal region  $\varepsilon_{FZ}$  in the non linear simulation is almost 10 times larger than  $\varepsilon_G$ . In other words, with the same oscillation (same frequency  $\omega_f$  and same amplitude  $A$ ), there is more power sent by the torus in the focal zone in the non linear case than in the linear case. The maximum dissipation is reached for  $\theta_{DNS}^T \simeq 30^\circ$ , which is consistent with the peak vertical energy observed at this angle in section IV A.

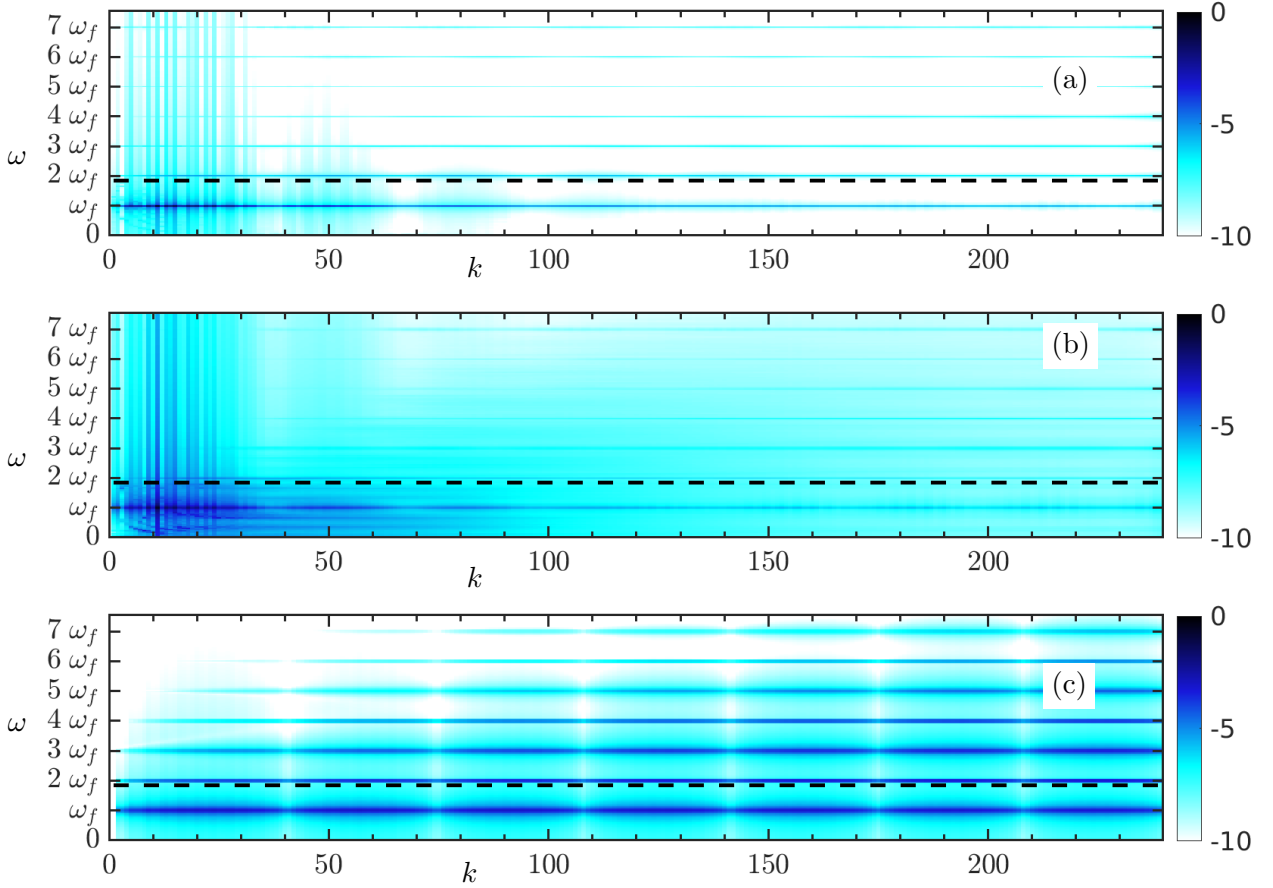


FIG. 9. Normalized spatio-temporal spectra: (a) linear simulation spectrum  $E^L(k, \omega)/E_{\text{tot}}^L$ ; (b) non linear simulation spectrum  $E^{\text{NL}}(k, \omega)/E_{\text{tot}}^{\text{NL}}$ ; (c) forced case spectrum  $E^f(k_0, \omega)/E_{\text{tot}}^f$ . The dashed line represents the rotating rate  $2\Omega_z$ . The colorbars indicate the log of the amplitude of the spectra.

Oscillations are observed on the *rms* vertical velocity (figure 6) and on the dissipation rate (figure 8) for linear and non linear simulations. They reflect a variation of forcing in terms of available inertial waves: in a confined domain, multiple wave reflections superimpose different waves, creating stationary waves, also called inertial modes. This phenomenon was also observed experimentally by Boury *et al.* [55], and we discuss it further in Appendix B.

## V. LINEAR AND NON LINEAR REGIMES FOR WAVES

### A. Spatio-temporal analysis of flow and harmonic forcing

We focus here on the 3D torus configuration with the propagation angle  $\theta_f = 33^\circ$  that maximizes vertical velocity and dissipation, as described in section IV. We analyse the spatio-temporal spectral content of the flow to quantify the injected energy and identify the resulting waves that are produced. The presence of inertial wave propagation is attested by the verification of the dispersion relation (1) applied to a 3D wave vector  $\mathbf{k}$  and a frequency  $\omega$ . We thus carry out a four-dimensional space-time Fourier transform of the velocity field  $\mathbf{u}(\mathbf{x}, t)$  in our simulation data to obtain the transformed spectral field  $\tilde{\mathbf{u}}(\mathbf{k}, \omega)$ .

This kind of analysis was used by Yarom and Sharon [56] in experimental data of rotating turbulence and extended to DNS of stratified turbulence by Lam *et al.* [57]. We apply the 4D transformation  $(\mathbf{x}, t) \rightarrow (\mathbf{k}, \omega)$  to fields of DNS in spectral Fourier space  $\hat{\mathbf{u}}(\mathbf{k}, t)$ , that are stored every 1 or 2 time steps depending on the case. In total, we use 1000 fields with a resolution of  $512^3$  points for the three velocity components. We then compute a temporal FFT with a Hann window to obtain  $\tilde{\mathbf{u}}(\mathbf{k}, \omega)$ . This completes the full 4D FFT transform. Compared to other methods — data reduction for a two-dimensional analysis as done in experiments by Yarom and Sharon [56] and Campagne *et al.* [58], and in simulations by Clark Di Leoni *et al.* [59], or by using statistical homogeneity assumptions in Maffioli *et al.* [53] —, our method requires larger memory storage and computational time, but with an evident gain of accuracy since a full detailed three-dimensional analysis is permitted. Although the homogeneity assumption seems to be available in fully turbulent flows, it is not applicable in our linear simulations for the reason that the phase correlation of velocity modes is not random (see Appendix in Maffioli *et al.* [53] for a detailed discussion about this assumption and a comparison with FFT4D).

We apply the 4D space-time analysis to obtain the fields  $\tilde{\mathbf{u}}^L(\mathbf{k}, \omega)$  of the 10 linear DNS, and the fields  $\tilde{\mathbf{u}}^{NL}(\mathbf{k}, \omega)$  of the 10 non linear ones. In Table I we report the minimum and maximum time frequencies  $\omega_{\min}$  and  $\omega_{\max}$  available in each case. Using these fields, we can successively compute the space-time spectrum of the kinetic energy density  $E^{L,NL}(k_0, \omega)$  at scale  $k_0$  and frequency  $\omega$ , the temporal spectrum  $E^{L,NL}(\omega)$  at frequency  $\omega$ , the spatial

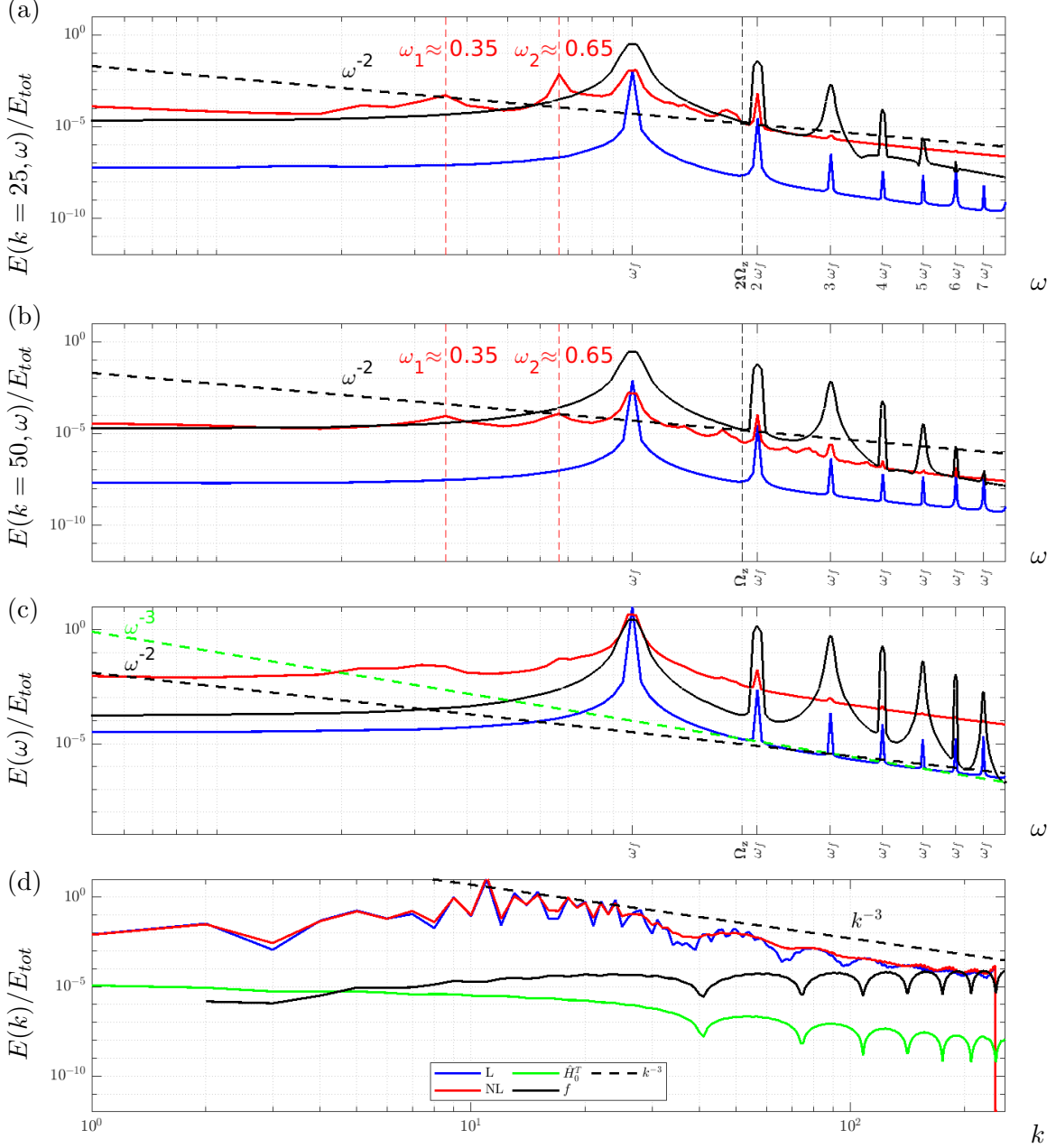


FIG. 10. Normalized spatio-temporal spectra  $E^{L,NL}(k, \omega)/E_{tot}^{L,NL}$  and  $E^f(k, \omega)/E_{tot}^f$  for: (a) slice at  $k = 25$ ; (b) slice at  $k = 50$ . (c) Normalized total temporal spectrum  $E^{L,NL}(\omega)/E_{tot}^{L,NL}$ ,  $E^f(\omega)/E_{tot}^f$ . (d) Normalized spatial spectrum  $E^{L,NL}(k)/E_{tot}^{L,NL}$ ,  $E^f(k)/E_{tot}^f$  and  $\hat{H}_0^T(k)$  from (19). The blue, red and black curves are, respectively, for linear, non linear and constant forcing term. The green curve for  $\hat{H}_0^T(k)$  has been shifted by  $\times 10^{-4}$  and black curve for  $E^f(k)/E_{tot}^f$  has been shifted by  $\times 10^{-2}$  for better comparison. The dashed black lines represent the power laws  $\omega^{-2}$  and  $k^{-3}$  suggested by Le Reun *et al.* [60].

spectrum  $E^{\text{L,NL}}(k_0)$  at scale  $k_0$  and the total energy  $E_{\text{tot}}^{\text{L,NL}}$ , as

$$E^{\text{L,NL}}(k_0, \omega) = \sum_{k_0-0.5 \leq |\mathbf{k}| < k_0+0.5} |\tilde{\mathbf{u}}^{\text{L,NL}}(\mathbf{k}, \omega)|^2, \quad (13)$$

$$E^{\text{L,NL}}(\omega) = \sum_{k_0} E^{\text{L,NL}}(k_0, \omega), \quad (14)$$

$$E^{\text{L,NL}}(k_0) = \sum_{\omega} E^{\text{L,NL}}(k_0, \omega), \quad (15)$$

$$E_{\text{tot}}^{\text{L,NL}} = \sum_{k_0, \omega} E^{\text{L,NL}}(k_0, \omega). \quad (16)$$

The spectra  $E^{\text{L,NL}}(k_0, \omega)$ ,  $E^{\text{L,NL}}(\omega)$  and  $E^{\text{L,NL}}(k_0)$  are normalized by the total energy  $E_{\text{tot}}^{\text{L,NL}}$  to facilitate comparison between different parametric cases. In equation (13) the averaging extends over the interval  $k_0 - 0.5 \leq |\mathbf{k} = (k_x, k_y, k_z)| < k_0 + 0.5$  due to the Cartesian grid discretization  $k_x, k_y, k_z = -N/2, \dots, -1, 0, 1, \dots, N/2$  where  $N$  is the resolution of the DNS, such that  $\mathbf{k}$  is rarely equal to  $k_0$ .

Figure 9 shows the distribution in  $(k, \omega)$  space of the kinetic energy density spectra  $E^{\text{L,NL}}(k_0, \omega)$  for the linear and nonlinear simulations. The dashed line in the plots also indicate the maximum frequency  $2\Omega_z$  available for IW from the dispersion relation. As expected, the spectral kinetic energy density is concentrated on the forcing frequency  $\omega_f$  in the linear (figure 9a) and non linear simulations (figure 9b). However, whatever the spatial scale  $k$ , there is more energy in the frequency domain around the peak at  $\omega_f$  in the non linear case than in the linear case. This spread is therefore linked to the redistribution of energy via non linear mechanisms. The concentration of energy along constant  $k$  lines shows that some scales are more energetic than others. In the linear and non linear simulations, we observe a global decrease of energy as the timescale related to the spectral modes decreases, *i.e.* when  $k$  increases. This phenomenon is more marked in the linear case beyond  $k = 50$ . Moreover, some harmonics of the form  $n\omega_f$ ,  $n = 2, 3, \dots, 7$  appear as a concentration of energy along constant  $\omega$  lines, that persist whatever the scale  $k$ . The origin of these harmonic frequencies is linked to the constant part of the forcing term that reflects the vertical displacement of the torus in equation (5). This term is  $-\frac{1}{\eta} \mathbf{u}_s \hat{H}^T(\mathbf{x}, t)$  in physical space, and  $-\frac{1}{\eta} \dot{z}(t) \hat{H}_0^T(k, \theta(\mathbf{k})) e^{-ik_z z(t)}$  in spatial Fourier space as discussed at Appendix A. When applying the temporal Fourier transform noted  $\mathcal{F}_t$ , the spatio-temporal spectrum of

forcing is

$$E^f(k_0, \omega) = \sum_{k_0-0.5 \leq |\mathbf{k}| < k_0+0.5} \left| \hat{H}_0^T(k, \theta(\mathbf{k})) \mathcal{F}_t [\dot{z}(t) e^{-ik_z z(t)}] (\omega) \right|^2. \quad (17)$$

As in equations (14), (15), (16) for the spectra of kinetic energy density, one defines in (17) similar spectra for the forcing: total temporal spectrum  $E^f(\omega) = \sum_k E^f(k, \omega)$ , total spatial spectrum  $E^f(k) = \sum_\omega E^f(k, \omega)$  and total forcing  $E_{\text{tot}}^f = \sum_{k, \omega} E^f(k, \omega)$ . Figure 9(c) for the normalized energy  $E^f(k_0, \omega)/E_{\text{tot}}^f$  shows that the forcing induces harmonic frequencies  $n\omega_f$  which are also visible in the linear and non linear spectra and, surprisingly, their energies do not decrease with scale. Harmonic forcing seems also to be found in experiments that generate the harmonics of waves, as in the case of a cylinder oscillating in a rotating fluid with a residual non-harmonic component of the oscillation profile of the wave generator [37]. The harmonics of inertial waves do not appear in our simulations wherein the condition  $n\omega \leq 2\Omega_z$  for their appearance is not met.

In order to analyse the spectra more precisely, we plot the spectra as functions of  $\omega$  for the linear and non linear simulations in figure 10. Panels (a) and (b) show the normalized energy density spectra  $E^{\text{L,NL}}(k_0, \omega)$  at  $k_0 = 25$  and  $k_0 = 50$ , respectively. Panel (c) shows the total temporal spectrum  $E^{\text{L,NL}}(\omega)$ . The corresponding forcing spectrum  $E^f$  is also shown in the three figures.

The power law  $\omega^{-2}$  found by Le Reun *et al.* [60] in wave turbulence for rotating fluid is shown in figures 10(a) and (b). For non linear simulations, the spectrum at large spatial scale  $E^{\text{NL}}(k = 25, \omega)$  in figure 10(a) is consistent with the  $\omega^{-2}$  scaling at frequencies smaller than the forcing one  $\omega_f$  with a large peak similar to that found in weak inertial-wave turbulence experiments (see Monsalve *et al.* [61]). The spectrum  $E^{\text{NL}}(k = 50, \omega)$  (figure 10b) at smaller spatial scale is steeper. The wave turbulence frequency scaling is not retrieved at all spatial scales.

As expected, all the spectra in figures 10(a), (b) and (c) have a frequency peak at forcing frequency  $\omega_f$ . As shown above in equation (17), the constant part of the forcing contains the displacement term  $\mathcal{F}_t [\dot{z}(t) e^{-ik_z z(t)}] (\omega)$  which triggers the harmonics  $n\omega_f$ . Moreover the associated amplitude of forcing decreases with  $\omega$  but not between scales when comparing the spectra at  $k = 25$  and  $k = 50$ . This constant part of forcing is therefore responsible for the peaks observed at harmonic frequencies for linear and non linear simulations in figures 10(a) and (b).

However, in non linear simulations, the peaks of energy spectrum are smoothed out by non linearities, with enlarged bandwidths around the harmonics  $n\omega_f$ . This is associated to local redistribution and a slightly off-resonant transfer of energy across scales. Moreover, for frequencies smaller than  $\omega_f$ , we observe a difference between linear and non linear regimes. In the latter, two secondary peaks are visible at smaller frequencies  $\omega_1 \simeq 0.35\omega_f$  and  $\omega_2 \simeq 0.65\omega_f$  in the spectra at  $k_0 = 25$  and  $k_0 = 50$  such that

$$\omega_1 + \omega_2 \simeq \omega_f . \quad (18)$$

This is a typical signature of wave turbulence based on the triadic resonant condition for IW, namely  $\omega_{dr}(\mathbf{k}) = \omega_{dr}(\mathbf{p}) + \omega_{dr}(\mathbf{q})$  and  $\mathbf{k} = \mathbf{p} + \mathbf{q}$  [62, 63], and was also recently observed by Shmakova *et al.* [22] for torus configuration in a stratified fluid. The total time spectrum  $E^{\text{NL}}(\omega)$  in figure 10(c) also contains the same two peaks although less marked than for the spectra at fixed  $k = 25$  and  $k = 50$ . Although triadic exchanges are a feature of spectral non linear terms in turbulence — expressed as a convolution integral over spectral modes satisfying  $\mathbf{k} = \mathbf{p} + \mathbf{q}$ —, they do not necessarily correspond to inertial wave resonance interactions, all the more so since the energy injection does not control which individual modes are forced. Nevertheless, in section VB we shall show that the spectrum is indeed dominated by IW in our simulations, so that the observed peaks at  $\omega_1$  and  $\omega_2$  are actual inertial waves.

The total spatial spectrum of the kinetic energy density  $E(k)$  is shown in figure 10(d). For linear and non linear simulations, it also contains periodic bumps at certain scales that are directly linked to the spectrum  $E^f(k)$  of the forcing term (black solid curve) and hence to the spectral trace of the mask function  $\hat{H}_0^T(k, \theta(\mathbf{k}))$  (equation (A2)) that represents the torus geometry. Averaging over all orientations of  $\mathbf{k}$  at a given scale  $k_0$  on a Cartesian grid, one gets

$$\hat{H}_0^T(k_0) = \sum_{|\mathbf{k}|=k_0} \hat{H}_0^T(k, \theta(\mathbf{k})) \quad (19)$$

which is plotted in figure 10(d) (green solid curve), and is at the origin of the bumps. The bumps are visible at small scale for linear and non linear simulations, but they are smoother in the non linear regime due to local turbulent diffusion. Figure 10(d) also shows the power law  $k^{-3}$  suggested in several studies [60, 64, 65], which is consistent with our numerical results.

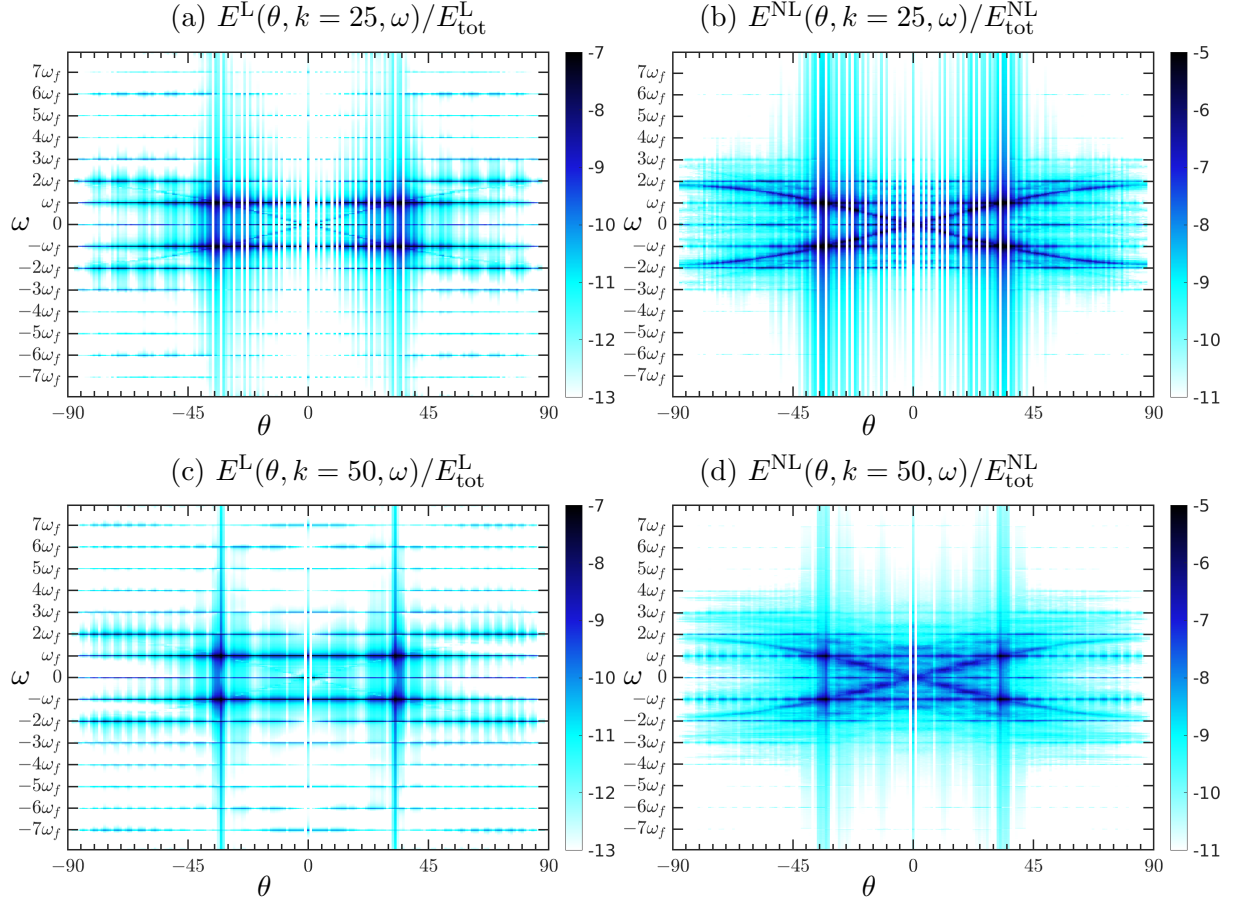


FIG. 11. Spectral kinetic energy density  $E^{L,NL}(\theta, k, \omega)/E_{\text{tot}}^{L,NL}$  for scales  $k = 25$  and  $k = 50$  for  $\theta_f = 33^\circ$ . Panels (a) and (b) for  $k = 25$ , (c) and (d) for  $k = 50$ ; (a) and (c) for linear simulations, (b) and (d) for non linear simulations. Color bar in log of amplitude.

## B. Signature of inertial waves

The above spectral analysis demonstrates the necessity to assess and quantify precisely the presence of IW in the torus configuration. A mere space-time spectrum function in  $(k, \omega)$  is not sufficient, because an angular space-time spectrum function in  $(k, \omega, \theta)$  is required to assign angles  $\theta$  to wavevectors and their dispersion relation (geometry in figure 1a). As in Lam *et al.* [57], we define angular spectra

$$E^{L,NL}(\theta_0, k_0, \omega) = \sum_{\substack{k_0 - 0.5 \leq |\mathbf{k}| < k_0 + 0.5 \\ \theta_0 - \Delta\theta \leq \theta(\mathbf{k}) < \theta_0 + \Delta\theta}} |\tilde{\mathbf{u}}^{L,NL}(\mathbf{k}, \omega)|^2. \quad (20)$$

We select spectral angles in the interval  $\theta_0 - \Delta\theta \leq \theta(\mathbf{k}) < \theta_0 + \Delta\theta$  with  $\Delta\theta = 0.5^\circ$ .

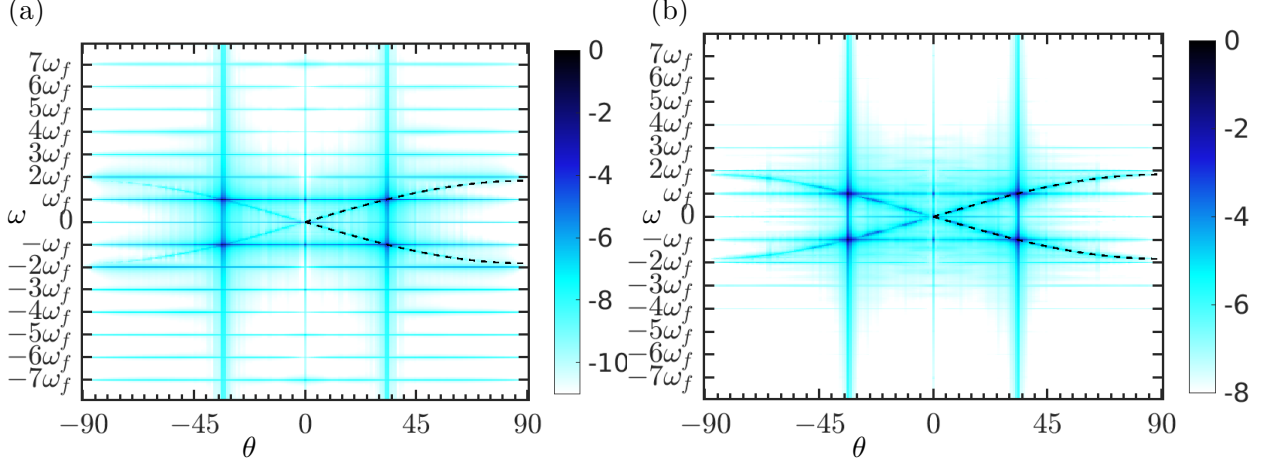


FIG. 12. Total angular spectral kinetic energy density  $E^{L,NL}(\theta, k_0, \omega)/E_{\text{tot}}^{L,NL}$  for  $\theta_f = 33^\circ$ . (a) for linear simulation spectrum (label L), (b) for non linear simulation spectrum (label NL). The color bar indicates the log of amplitude. The dashed line represents the dispersion relation  $\omega_{dr}(\theta)$  given by (1).

The normalized spectra  $E^{L,NL}(\theta, k, \omega)/E_{\text{tot}}^{L,NL}$  at scales  $k = 25$  and  $k = 50$  used in section V A are shown in figures 11. The color range is adapted to the maximum of each spectrum. Note that the stripey aspect of the plots is due to the forcing geometry, as explained in Appendix C.

In the linear case (see figures 11(a) and (c)), the energy is concentrated in the harmonics of the forcing, and the dispersion relation is observable for  $k = 25$  and less so for  $k = 50$ , showing that waves are present at smaller scales where the dissipation, although small, is significant with respect to the forcing. Note the presence of four peaks of energy density due to the resonance phenomenon when the frequency of the forcing  $\omega_f$  is equal to the natural frequency of the inertial wave associated to the propagation angle  $\theta_f$ , *i.e.* when  $\omega_f = \omega_{dr}(\theta_f)$ . In the non linear simulations in figures 11(b) and (d), the energy is less concentrated on the harmonics of forcing and more on the dispersion relation than in the linear simulations. We also observe a diffusion of the energy around the curve of the dispersion relation, as in stratified and rotating turbulence [66]. In both cases, at  $k = 25$  and  $k = 50$ , the waves are dominant compared to the linear case. Combined with the results of section V A, one concludes that the triadic resonance of IWs appears in the flow and maintains the presence of waves at different scales.

The total angular spectrum of all scales, is obtained by accumulating the angular spectrum of each scale (20) as

$$E^{\text{L,NL}}(\theta, \omega) = \sum_k E^{\text{L,NL}}(\theta, k, \omega) . \quad (21)$$

$E^{\text{L,NL}}(\theta, \omega)$  is shown in figures 12(a) and (b), with the same colour range for the linear and non linear simulations. In both cases, the energy distribution is concentrated along the dispersion relation of the inertial waves  $\omega = \omega_{dr}(\theta)$  given by (1) as a signature of IW, so that, overall, the kinetic energy seems to be contained mostly in IW. However, in the non linear simulation, the above-described harmonic frequencies due to forcing are limited to  $2\omega_f$  and to a lesser extent to  $3\omega_f$ , whereas in the linear case the higher harmonic frequencies  $3\omega_f, 4\omega_f, \dots, 7\omega_f$  are strongly persistent for any  $\theta$ . Moreover, the energy concentration around the dispersion relation is sharper in the linear case than in the non linear simulation where it is locally diffused. Again, this suggests that a nonlinear mechanism such as triadic resonance of IW enhances the presence of waves compared to linear phenomena. To explain this mechanism, quantitative theory would have to take into account triadic interactions, which are one of the key elements in our analysis of the flow.

### C. Nonlinear interaction in the focal zone

As shown in section IV, the focal zone is the most intense zone in terms of dissipation, and the bulk flow is practically dominated by inertial waves. We now need to link these two observations by studying the non linear interaction that takes place in the focal zone. For this, we rely on a bispectrum analysis of the vertical velocity field  $u_z$ .

We start by showing in figures 13(a) and (b) the time oscillations of  $u_z(\mathbf{x}_0, t)$  for linear and non linear simulations, respectively, at a point  $\mathbf{x}_0 = (0, 0, Z_f)$  in the focal zone. Velocity oscillations are regular in the linear case (figure 13a) but modulated in amplitude in the non linear one (figure 13b). As expected, a wide peak of energy at frequency  $\omega_f$  and secondary peaks at harmonic frequencies  $n\omega_f$  appear in figure 13(c) for the total time spectrum  $E_z(\omega)$  of  $u_z(\mathbf{x}_0, t)$  and for linear and non linear simulations. The spectrum of the non linear simulation (figure 13c) differs from that of the linear simulation by a much larger level of background vertical kinetic energy at all frequencies than in the linear simulation, attesting of non linear enrichment of the spectrum. The two time spectra obtained at the focal point

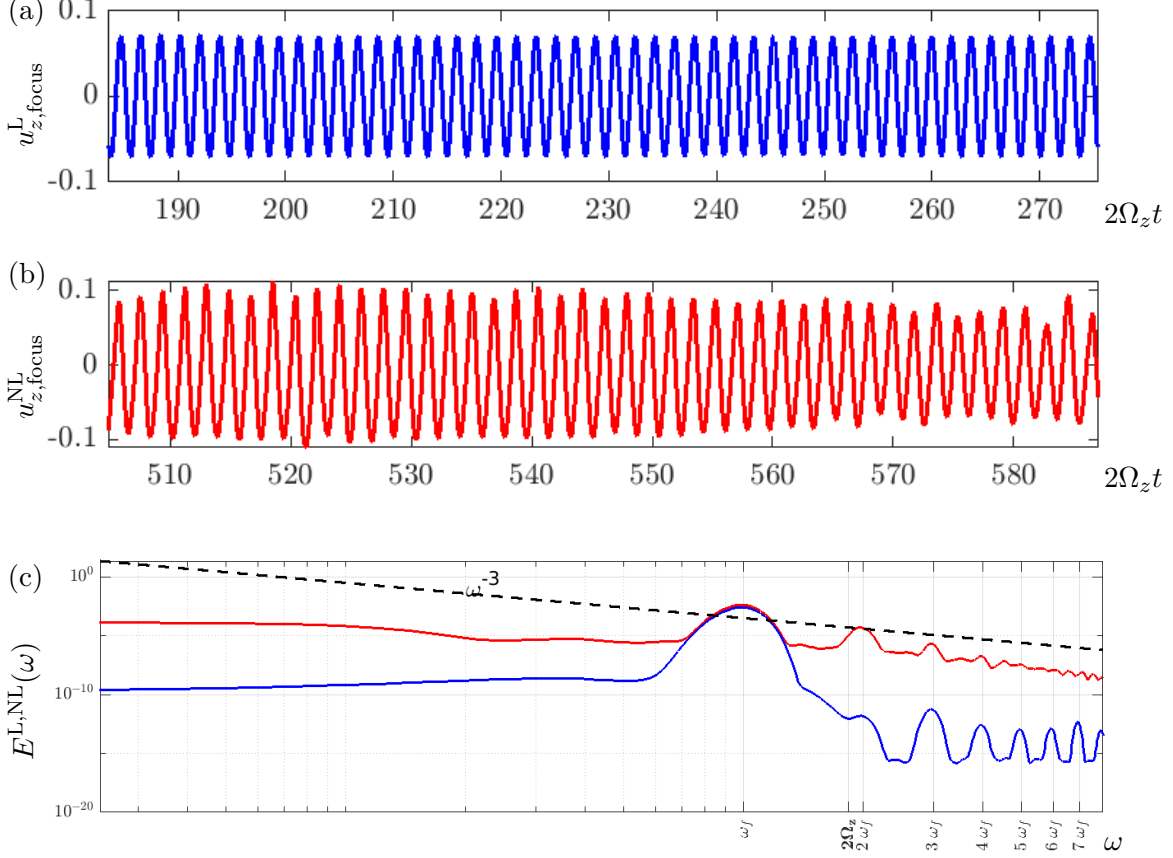


FIG. 13. Vertical velocity signal  $u_z(\mathbf{x}_0, t)$  as a function of normalized time  $2\omega_z t$  in the focal zone by the simulation of the torus configuration at  $\theta_f = 33^\circ$ : (a) linear simulation; (b) non linear simulation. (c) Temporal spectrum energy  $E(\omega)$  in blue for linear simulations, and red for the non linear ones.

$\mathbf{x}_0$  are consistent with the spectra obtained in the complete domain in the non linear and linear simulations in figure 10(c), although in the latter plot the peaks are sharper.

We characterize the spectral enrichment by non linear interactions in the focal zone using a bispectral analysis. For this, we consider the Fourier transform of the third-order cumulant function, which is the bispectrum that measures the statistical dependence between three spectral components  $(\omega_1, \omega_2, \omega_3)$  satisfying the resonance condition of the frequencies  $\omega_3 = \omega_2 + \omega_1$ , a condition deriving from the non linear terms in the energy balance equations [65]. We compute these statistics by using the HOSA Matlab toolbox proposed by Swami *et al.* [67]. The vertical velocity signal  $u_z(t)$  is decomposed into  $N = 379$  segments with 99%

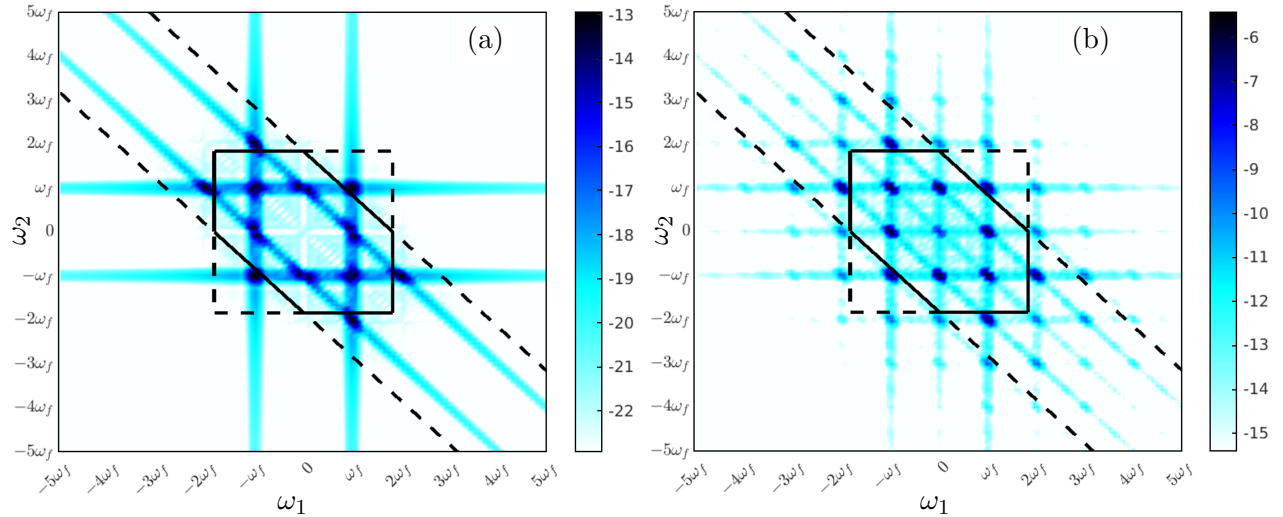


FIG. 14. Bicoherence contours obtained at  $\theta_f = 33^\circ$ : (a) linear simulation; (b) non linear simulation. Color bar indicates the log of amplitude. The hexagon (solid black line) represents the domain of non linear interaction of inertial waves. The dotted line represent highest frequencies ( $\pm 2\Omega$ ) of the inertial waves.

overlap between them, and we apply Hamming windowing on each segment containing the velocity  $u_z^i(\mathbf{x}_0, t)$ ,  $i = 1, \dots, N$ . The FFTs are computed with 2048 points. The bispectrum of the  $i$ -th segment is calculated as

$$b^i(\omega_1, \omega_2) = \hat{u}_z^i(\omega_1) \hat{u}_z^i(\omega_2) \overline{\hat{u}_z^i(\omega_1 + \omega_2)} \quad (22)$$

where  $\hat{u}_z^i$  represents the FFT on the  $i$ -th segment of  $u_z^i(\mathbf{x}_0, t)$  and  $\bar{*}$  is the complex conjugate. The power spectrum of  $b^i(\omega_1, \omega_2)$  is  $|b^i(\omega_1, \omega_2)|^2$ . The bispectrum is estimated by averaging all segments noted  $\langle * \rangle$ , as

$$\langle |b(\omega_1, \omega_2)|^2 \rangle = \sum_{i=1}^N |b^i(\omega_1, \omega_2)|^2. \quad (23)$$

The bicoherence is the normalized bispectrum

$$B(\omega_1, \omega_2) = \frac{\langle |b(\omega_1, \omega_2)|^2 \rangle}{\langle |\hat{u}_z(\omega_1)|^2 \rangle \langle |\hat{u}_z(\omega_2)|^2 \rangle \langle |\hat{u}_z(\omega_1 + \omega_2)|^2 \rangle}. \quad (24)$$

Note that  $\langle |\hat{u}_z(\omega_1)|^2 \rangle$ ,  $\langle |\hat{u}_z(\omega_2)|^2 \rangle$  and  $\langle |\hat{u}_z(\omega_1 + \omega_2)|^2 \rangle$  are the classical power spectra for the frequencies  $\omega_1$ ,  $\omega_2$  and  $\omega_1 + \omega_2$ .

Figure 14(a) is the map of bicoherence  $B(\omega_1, \omega_2)$  for the linear simulation and figure 14(b) for the non linear simulation (note the different scales). For the same resolution and same

numerical parameters, the non linear data are overall more concentrated around the peak than that in the linear case which reveals the importance of non linear interactions. For any fixed frequency  $\omega_3$  with a spectrum  $E(\omega_3)$  as in figure 13(c), the bicoherence function  $B(\omega_1, \omega_2)$  measures the statistical dependence of  $\omega_3$  on a combination of frequency pairs  $(\omega_1, \omega_2)$  such that  $\omega_3 = \omega_1 + \omega_2$ . The chosen frequency  $\omega_3$  appears on the maps of  $B(\omega_1, \omega_2)$  in figures 14(a) and (b) as an oblique line passing from top left to bottom right, defined by the affine equation  $\omega_2 = \omega_3 - \omega_1$ . For example, the highest frequencies resulting from the dispersion relation are  $\omega_3 = \pm 2\Omega$  and are represented as diagonal dashed black lines in figures 14(a) and (b). The highest frequencies of the waves are  $\omega_1 = \pm 2\Omega$  and  $\omega_2 = \pm 2\Omega$  (vertical and horizontal dashed black lines, respectively), meaning that an interaction between the waves produces a frequency  $\omega_3$  in the square  $\omega_1 = \pm 2\Omega$  and  $\omega_2 = \pm 2\Omega$ . If this frequency  $\omega_3$  is a frequency of waves, then this square is limited by the two oblique lines  $\omega_3 = \pm 2\Omega$ : the irregular hexagon drawn as a solid black line therefore represents the non linear interaction of inertial waves. Within this hexagon, the frequencies  $\omega_1$  and  $\omega_2$  and their interaction  $\omega_3 = \omega_1 + \omega_2$  satisfy the dispersion relation of inertial waves (1), namely  $\omega_3 = \omega_{dr}(\mathbf{k})$ ,  $\omega_2 = \omega_{dr}(\mathbf{p})$  and  $\omega_1 = \omega_{dr}(\mathbf{q})$  with  $\mathbf{k}$ ,  $\mathbf{p}$  and  $\mathbf{q}$  the wavevectors of waves satisfying the triadic resonant condition  $\omega_{dr}(\mathbf{k}) = \omega_{dr}(\mathbf{p}) + \omega_{dr}(\mathbf{q})$ .

In the linear simulations, the convective non linear term  $\boldsymbol{\omega} \times \mathbf{u} = \mathbf{0}$ , but there is still a non linear interaction due to the penalisation term (5), in particular for the torus forcing term  $-\frac{1}{\eta} \mathbf{u}_s H^T(\mathbf{x}, t)$  that produces harmonics from temporal nonlinear interactions due to multiplication in Fourier space, as seen in section V A (the term  $\mathcal{F}_t [\dot{z}(t)e^{-ik_z z(t)}](\omega)$  in equation (17)). According to  $B(\omega_1, \omega_2)$  (figure 14a), most of the interactions take place in the hexagon of the inertial waves, and three oblique lines corresponding to the frequencies  $\omega_3 = 0, \omega_f, 2\omega_f$  are visible. From  $B(\omega_1, \omega_2)$ , it can be deduced that

- stationary modes  $\omega_3 = 0$  are the geostrophic modes (see section III B) which are due to one interaction between the waves  $(\omega_1 = \omega_f, \omega_2 = -\omega_f)$  and its symmetric part  $(\omega_1 = -\omega_f, \omega_2 = \omega_f)$ ,
- the frequency  $\omega_3 = 2\omega_f$  (highest frequency out of the dispersion relation) is due to one interaction between waves  $(\omega_1 = \omega_f, \omega_2 = \omega_f)$ .

Note that the main frequency of the waves is imposed by the forcing at  $\omega_f$  (see section V B). For the frequency  $\omega_3 = \omega_f$ , there are two different interactions between the stationary

modes (geostrophic modes) and the waves ( $\omega_1 = 0, \omega_2 = \omega_f$ ) and between the waves ( $\omega_1 = -\omega_f, \omega_2 = 2\omega_f$ ) and their symmetric part.

In the non linear simulations (figure 14b), unlike linear ones, we observe many more interactions indicated by peaks of the bicoherence function, in particular in the hexagon. This means that triadic resonance-type interactions seem to dominate all other interactions. Moreover, the stationary mode at  $\omega_3 = 0$ , identified as central and secondary vortices in section III B, is due to other interactions such as those between waves ( $\omega_1 = 2\omega_f, \omega_2 = -2\omega_f$ ) and waves ( $\omega_1 = 3\omega_f, \omega_2 = -3\omega_f$ ). In addition, there are interactions between the higher harmonics  $\pm 2\omega_f, \pm 3\omega_f, \dots$  and the waves at  $\pm\omega_f$ , or in general with the higher harmonics  $\pm 2\omega_f, \pm 3\omega_f, \dots$ . This frequency enhancement between linear and non linear simulations is linked to the introduction of the non linear convective term and reflects a transfer between the waves and between the harmonics and the waves. This is not observed in the linear simulations (figure 14a).

## VI. CONCLUSION

Using direct numerical simulations, we study the focusing of inertial waves caused by the oscillation of a torus in a fluid with background rotation. Two models for representing the oscillating torus are considered: a Dirac ring configuration, which allows to compare the results with those from the linear theory developed by Liu *et al.* [2], and a three-dimensional solid torus representing closely the experimental realizations, and allowing to extrapolate the analytical results to a more complex configuration. For Dirac ring configuration, only linear simulations are considered, whereas for the 3D torus, linear and nonlinear simulations are performed to better understand the limits of the linear approach. For all the simulations, the frequency  $\omega_f$  of the torus oscillations was fixed but the rotation rate of the fluid background  $\Omega_z$  was varied to vary the angle of the waves emitted by the torus or by the ring of Dirac. In so doing, only the Rossby number  $Ro \ll 1$  varies with the propagation angle for forcings by the Dirac ring or by the 3D torus, and the other non-dimensional numbers — Reynolds  $Re$ , Keulegan-Carpenter  $Ke$  and Stokes  $St$  — are fixed. For the 3D torus configuration, since the Stokes number is large  $St \gg 1$ , the waves have a bimodal structure in agreement with the linear theory of Shmakova *et al.* [22] with a maximum of vertical velocity in focal zone.

Our first result concerns the averaged main flow for the 3D torus configuration. In the

linear case, the average main flow appears in the form of a flow invariant along  $z$  (axis of rotation) and could be assimilated to a geostrophic mode. The flow consists of two contra-rotating cylinders. In the non linear case, the averaged main flow is mainly dominated by a central vortex whose formation seems to be in agreement with the linear theory of Ranjan and Davidson [44]. We thus observe the generation of a mean flow with central vortex only due to the non linear focusing of the waves in agreement with the mechanisms related to a patch of turbulence described by these authors.

In addition, we have shown that the maximum of the vertical velocity in the focal zone is consistent with the linear theory for the Dirac ring configuration [2]. Indeed, the curves for the numerically measured and theoretically predicted vertical velocities overlap and reach a maximum at propagation angle  $\theta_f = 35^\circ$ . This ring of Dirac configuration serves as a guide and benchmark before considering the case of the 3D torus for which the maximum amplification is at around  $\theta_f = 30^\circ$ . Moreover, for this angle, the dissipation in the focal zone appears to reach a maximum which is always more important in the non linear than in the linear case.

Finally, using a four-dimensional spatio-temporal analysis, we have shown that the flow is dominated by inertial waves on a wide range of scales that we precisely identify. The observed wave scales can be smaller in the non linear case than in the linear case, suggesting the existence of a non linear transfer that reinforces the presence of inertial waves despite the presence of harmonics. This mechanism seems to be linked to triadic resonant interactions. The harmonic frequencies are induced by the torus oscillation on all scales. We have performed a bicoherence analysis in the focal area to identify non linear interactions. In the non linear case, it turns out that the triadic resonant interactions of the waves dominate all other interactions.

A possible extension of the present study to get even closer to the oceanographic context would involve the inclusion of the effect of local variations in topography on the production of waves of different phases and their focusing, by considering a torus with azimuthal variations of shape or radius. Our study also calls for the development of a weakly nonlinear theory to reach beyond existing linear theories, to take into account non linear interactions between waves and better predict mixing in the ocean that takes place in the presence of stratification. One question concerns the stability of the central vortex. In another way, the sub-critical or super-critical nature of the instability could be explored in order to determine the effects of

hysteresis around the threshold of the instability. We have simulated a wave regime, however, it will also be necessary to explore regimes with higher Reynolds numbers that are beyond the scope of this study. Our work falls within the scope of studies aimed at quantifying the intense events linked to wave focusing in order to make a significant contribution to the global energy balance.

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## Appendix A: Compared injected power by Dirac ring and 3D torus forcings

The two configurations do not inject the same energy distribution into the focal point or the focal zone. In first approximation, the energy sent by the forcing  $\mathbf{f}$  depends directly on the spatial functions  $H_0^T$  or  $H_0^{DR}$ . This comes from the physical space power equation at  $t$  and  $\mathbf{x}$  obtained by multiplying (2) by  $\mathbf{u}(\mathbf{x}, t)$ . Equivalently, the spectral power equation at  $t$  and  $\mathbf{k}$  is obtained by Fourier transforming (2) and multiplying it by the velocity Fourier component  $\hat{\mathbf{u}}(\mathbf{k}, t)$ , and adding the complex conjugate. This yields the Lin's equation for spectral energy density in isotropic homogeneous turbulence [68] when averaging on the set of wave vectors with the same modulus. The advantage of Fourier space is to interpret the power equation in terms of scale. Integrating these power equations over the entire physical or Fourier domain provides two ways of obtaining the same kinetic energy evolution equations. In Fourier space, the injected power forcing is given by the inner product

$\hat{\mathbf{f}}(\mathbf{k}, t) \cdot \overline{\hat{\mathbf{u}}(\mathbf{k}, t)} + CC$  where  $\bar{*}$  is the complex conjugate of  $*$ ,  $\hat{*}$  is spatial Fourier transform, and  $CC$  means that we add the complex conjugate of the previous expression. Since  $\hat{H}_0^T(\mathbf{k})$  and  $\hat{H}_0^{\text{DR}}(\mathbf{k})$  are the Fourier transforms of  $H_0^T$  and  $H_0^{\text{DR}}$ , the injected power includes terms as  $A_0 \sin(\omega_f t) \hat{H}_0^T(\mathbf{k}) \cdot \overline{\hat{\mathbf{u}}(\mathbf{k}, t)}$  in the Dirac ring case and  $-\frac{1}{\eta} \dot{z}(t) \hat{H}_0^T(\mathbf{k}) e^{-ik_z z(t)} \cdot \overline{\hat{\mathbf{u}}(\mathbf{k}, t)}$  in the 3D torus case.  $\hat{H}_0^T$  and  $\hat{H}_0^{\text{DR}}$  therefore act as transfer functions in Fourier space that spatially filter the velocity field.

Due to axisymmetry, we express  $H_0^T$  and  $H_0^{\text{DR}}$  in polar coordinates  $(k, \theta)$ , where  $k = |\mathbf{k}|$ ,  $\theta = \tan^{-1}(k_z/k_h)$  and  $k_h = (k_x^2 + k_y^2)^{1/2}$ . The expressions for  $\hat{H}_0^T$  and  $\hat{H}_0^{\text{DR}}$  are given in Liu *et al.* [2] and Beleggia *et al.* [69] as

$$\hat{H}_0^{\text{DR}}(k_h, \theta) = 2\pi J_0(k_h \cos \theta), \quad (\text{A1})$$

$$\hat{H}_0^T(k, \theta) = \frac{4\pi}{k \sin \theta} \int_{-b}^b J_0(k \cos \theta (a + x)) \sin(k \sin \theta \sqrt{b^2 - x^2}) (a + x) dx, \quad (\text{A2})$$

where  $J_0$  is the zeroth-order Bessel function of the first kind. In equation (A1), the geometrical parameter is the radius  $a = 1$  for the case of Dirac ring, and in equation (A2)  $a = 0.848$  and  $b = 0.0942$  for the 3D torus. The amplitude maps in  $(\theta, k)$  of  $|\hat{H}_0^T(k, \theta)|$  and  $|\hat{H}_0^{\text{DR}}(k, \theta)|$  from these equations are plotted in figure 15 by using explicit numerical integration for all  $\theta$  except for  $\theta = 0$  where the calculation diverges. The distribution of the mask functions show the dependence in Fourier space of the energy input in the system since their enter the definition of the forcing  $\mathbf{f}$ . Figure 15 therefore shows that  $|\hat{H}_0^T(k, \theta)|$  and  $|\hat{H}_0^{\text{DR}}(k, \theta)|$  let the energy pass to all angles  $\theta$  for both configurations, but also that, for the 3D torus configuration, energy is concentrated at large scales from small  $k$  up to  $k \simeq 30$ , while for the Dirac ring, it extends to all resolved scales. Moreover, the figure shows that, although energy at the forcing frequency  $\omega_f$  is sent to all angles and scales, only a small part goes into the wave vector  $\mathbf{k}$  that corresponds to the precise angle  $\theta_f$  from the dispersion relation (8).

## Appendix B: Source discretization effect on the energy transfer

As reminded by Boury *et al.* [55] in their experimental work, in a confined domain, whether in numerical simulations or in experiments, each wave vector allowed in such a confined geometry is quantified with a discrete collection of wave numbers in each direction. In a  $2\pi$ -periodic domain, the wave vectors  $\mathbf{k}$  are a set of integers  $\mathbf{k} = (l, m, n)$ . If small

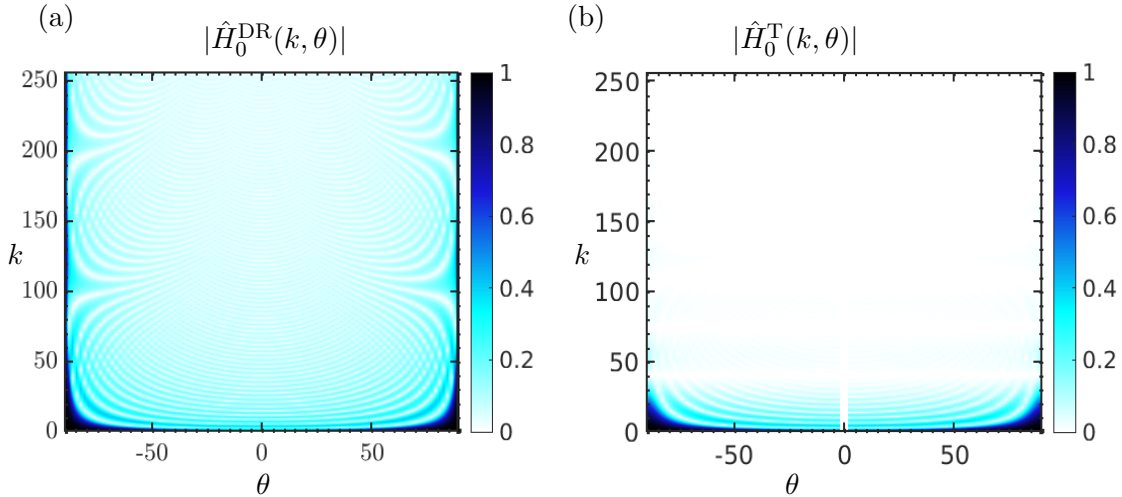


FIG. 15. Absolute value of forcing terms in Fourier space ( $k \equiv |\mathbf{k}|, \theta$ ): (a) ring of Dirac  $|\hat{H}_0^{\text{DR}}(k, \theta)|$ ; (b) 3D torus  $|\hat{H}_0^{\text{T}}(k, \theta)|$ . Both functions are normalized by their maximum value.

scales can be described by a multitude of wave numbers, this is no longer the case for large scales, where only a few wave numbers represents them. For instance, for a wavenumber  $k = 1$ , there are only 6 possible wave vectors  $\mathbf{k} = (\pm 1, 0, 0)$ ,  $\mathbf{k} = (0, \pm 1, 0)$ , ...

This quantification of the permitted wave numbers has a consequence on the spatial forcing by the 3D torus  $\hat{H}_0^{\text{T}}(\mathbf{k})$  or by Dirac ring  $\hat{H}_0^{\text{RD}}(\mathbf{k})$ . On the one hand, in figures 16(a) and (c) we have plotted the theoretical forcing of  $\hat{H}_0^{\text{T}}(\mathbf{k})$  and  $\hat{H}_0^{\text{RD}}(\mathbf{k})$ , based on formulas (A2) and (A1) respectively, with a continuous description of the wave vectors in terms of the modulus  $k = |\mathbf{k}|$  and the angle  $\theta$ . On the other hand, figures 16(b) and (d) show the numerical forcing  $\hat{H}_0^{\text{T}}(\mathbf{k})$  and  $\hat{H}_0^{\text{RD}}(\mathbf{k})$  based on the values of the wave vector in terms of modulus and angle discretized on the Cartesian grid such that  $\mathbf{k} = (l, m, n)$ ,  $(l, m, n) \in \{1, \dots, N_x\}^3$  with  $N_x$  the simulation resolution. When comparing the filters, the main difference between a continuous and a quantified grid comes from the large scales. Compared with the theoretical formulas for the two configurations, the energy contained in the small scales ( $k > 30$ ) is well evaluated by the Cartesian grid, but the energy contained in the large scales is underestimated, with energy gaps at several  $\theta$  angles. This numerical effect is more detrimental to the 3D torus configuration than to the Dirac ring configuration. Indeed, at fixed  $\theta$ , compared to the theoretical formula, in the Dirac ring configuration the energy of the small scales are of the same order of magnitude as the energy of the large scales, which compensates for the gaps. However, this is no longer the case in the 3D torus

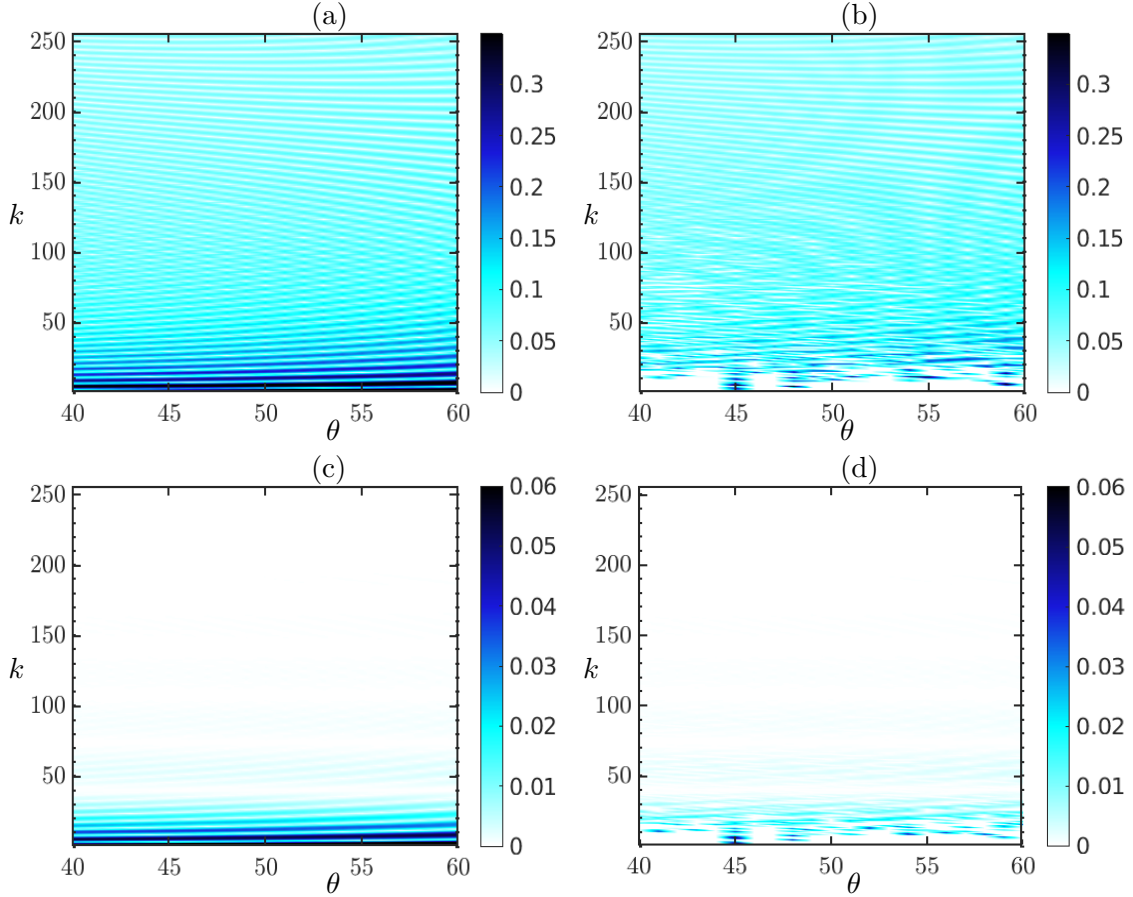


FIG. 16. Comparison of the modulus of the forcing of Dirac ring  $|\widehat{H}_0^{\text{RD}}(k, \theta)|$  as a function of wavenumber  $k$  and the angle  $\theta$  in the same range used in the simulations between: (a) theoretical value from (A1) and (b) numerical computation from a Cartesian grid. The same is for for 3D torus forcing  $|\widehat{H}_0^{\text{T}}(k, \theta)|$  between: (c) theoretical values from equation (A2) and (d) numerical results.

configuration, as the larger scales contain noticeably more energy and the smaller scales can no longer compensate for the gaps. For each angle, the total energies injected by the forcing terms  $\widehat{H}_0^{\text{T}}(\mathbf{k})$  and  $\widehat{H}^{\text{RD}}(\mathbf{k})$  therefore vary between the theoretical formula and the Cartesian grid, but these variations are less significant for the ring of Dirac configuration than for the 3D torus configuration. This has consequences for the vertical component of the velocity and the dissipation. Again, this phenomenon is observed equivalently in experiment and simulations whenever an enclosed fluid domain is considered.

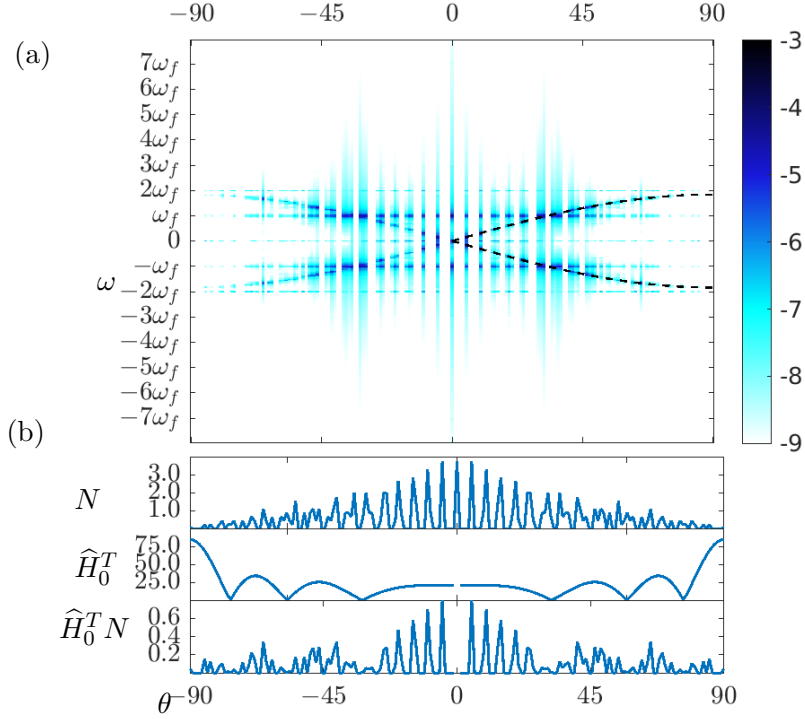


FIG. 17. (a) Angular spectral kinetic energy density  $E^{\text{NL}}(\theta, k_0 = 12, \omega)/E_{\text{tot}}^{\text{NL}}$  for  $\theta_f = 33^\circ$ . The dashed black lines represent the dispersion relation  $\omega_{dr}(\theta)$  defined in equation (1). The color bar indicates the log of the amplitude. (b) Dependence on  $\theta$  of  $\widehat{H}_0^T(k = 12, \theta)$  normalized by  $\max(H_0^T(k = 1, \theta))$  (middle panel),  $N(k = 12, \theta)$  normalized by  $\sum_{\theta} N(k = 12, \theta)$  (top panel),  $\widehat{H}_0^T(k = 12, \theta)N(k = 12, \theta)$ , plotted in percentage to indicate the injected power in different stripes.

### Appendix C: Frequency quantization due to the source geometry

Figure 17(a) shows the distribution in the  $(\theta, \omega)$  plane of  $E^{\text{L,NL}}(\theta, k, \omega)$  normalised by  $E_{\text{tot}}^{\text{L,NL}}$  for  $k = 12$  for non linear simulations in the torus configuration. The spectrum appears as concentrated energy along stripes, but the presence of the dispersion relation of IW is clear. The stripes appear for two reasons:

1. The quantization of the wave vectors since not all angles  $\theta$  are possible due to the discretisation on a Cartesian grid and bounded domain in particular at large scale (see section IV B and Appendix B) .

2. The spatial forcing of the torus. Upon defining the average  $\widehat{H}_0^T(k_0, \theta_0) = \sum_{|\mathbf{k}|=k_0, \theta(\mathbf{k})=\theta_0} \widehat{H}_0^T(k, \theta(\mathbf{k}))$  over all  $\mathbf{k}$  of norm  $k_0$  and angle  $\theta_0$ , we observe that the forcing term  $\widehat{H}_0^T(k_0 = 12, \theta_0)$  is zero for several angles  $\theta$  visible in figure 17(a), which is due to the Cartesian grid.

At fixed  $k$ , we compute the number  $N(k, \theta)$  of possible points on the grid for each  $\theta_0$ . Figure 17(b) shows these two sources of stripes,  $\widehat{H}_0^T(k_0, \theta_0)$  and  $N(k, \theta)$ , normalized respectively by  $\max_{\theta}(\widehat{H}_0^T(k = 1, \theta))$  and  $\sum_{\theta} N(k = 12, \theta)$ . Moreover, the product of the two sources of stripes  $\widehat{H}_0^T(k_0, \theta_0)N(k_0, \theta_0)$  is also plotted in the figure to identify the angles that form the stripes, based on the two previous reasons. The figure shows the coincidence of the zeroes and variations of this function of kinetic energy density with the modulation with  $\theta$  plotted on figure 17(a).

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