

Low-cost Jacobian-free mapping for dynamic cell clustering in multi-regime reactive flows

Antoine Stock, Vincent Moureau, Julien Leparoux, Renaud Mercier

▶ To cite this version:

Antoine Stock, Vincent Moureau, Julien Leparoux, Renaud Mercier. Low-cost Jacobian-free mapping for dynamic cell clustering in multi-regime reactive flows. Proceedings of the Combustion Institute, 2024, 40 (1-4), pp.105287. 10.1016/j.proci.2024.105287. hal-04684711

HAL Id: hal-04684711 https://hal.science/hal-04684711v1

Submitted on 3 Sep 2024

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers. L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

Low-cost Jacobian-free mapping for dynamic cell clustering in multi-regime reactive flows

Antoine Stock^{*a*,*}, Vincent Moureau^{*a*}, Julien Leparoux^{*b*}, Renaud Mercier^{*b*}

^aCORIA, Normandie Univ, UNIROUEN, INSA Rouen, CNRS UMR6614, FRANCE

^bSafran Tech, Digital Sciences Technologies Department, Rue des Jeunes Bois, Châteaufort, 78114, Magny-Les-Hameaux, FRANCE

Abstract

Dynamic Cell Clustering (DCC), also referred as Cell Agglomeration, is an optimisation technique used to reduce the cost of finite-rate chemistry in reactive flows. It consists of three steps: i) grouping of elements with similar composition into clusters, ii) computation of a single element per cluster and iii) mapping of the computed elements to the remaining elements of the cluster through interpolation and extrapolation. The size of the clusters results from a compromise between cost reduction and desired accuracy. A new Jacobian-free mapping method (JFM) combined to Principal Component Analysis (PCA) is introduced in order to provide the accuracy of a higher-order mapping without the overhead of a Jacobian evaluation. The increased accuracy is obtained by creating a connectivity map between adjacent clusters. Along the cluster connections, composition and source term gradients are known enabling an approximation of the Jacobian. The JFM methodology is validated on a hydrogen-air triple flame, a multi-regime flame which covers a wide region in the species/temperature phase space. It is shown that for realistic clustering conditions the JFM method shows a similar accuracy to the explicit Jacobian. Compared to other mapping methods, an error reduction of up to 74% is observed while the cell agglomeration overhead remains less than 1% of the initial cost.

Keywords: Reactive flows; Dynamic Cell Clustering; Cell agglomeration; Principal Component Analysis; Jacobian-free mapping

Information for Colloquium Chairs and Cochairs, Editors, and Reviewers

1) Novelty and Significance Statement

A new mapping method for cell agglomeration is introduced. Prior methods have shown limitations in terms of efficiency or accuracy. The proposed Jacobian-Free Mapping (JFM) method combined with Principal Component Analysis for cell agglomeration is both accurate and efficient, no longer requiring a compromise between both properties. The method is original and performs very well for challenging multi-regime flames such as H2/air triple flames, which is of high interest for the decarbonation of the transport and energy sectors. As it is based on a Cartesian mapping and as it does not depend on the underlying chemical mechanism, it can be easily implemented in many codes and has a great potential for wide acceptance.

2) Author Contributions

- A. S. : performed research, implementation, paper writing
- V. M. : guided research, paper writing
- J. L. : guided research, paper writing
- R. M. : guided research, paper writing

3) Authors' Preference and Justification for Mode of Presentation at the Symposium

The authors prefer **OPP** presentation at the Symposium, for the following reasons:

- The presentation can focus on outcomes and results without requiring the inclusion of extensive background information
- · A room-audience-level discussion about the proposed method would be profitable
- The proposed cell clustering method can be implemented in many codes, deserving a wide audience

1. Introduction

Reactive flows are a prominent subject of study, 2 with applications spanning from combustion pro-3 cesses in engines to industrial reactors. Large-Eddy 4 Simulation (LES) and Direct Numerical Simulations 5 (DNS) have emerged as powerful tools for simulating 6 turbulent reactive flows, providing valuable insights 7 into the complex interactions between turbulence and 8 chemical reactions. One of the primary challenges in 9 unsteady modelling of reactive flows is the accurate 10 computation of chemical source terms. 11

12 Finite-rate chemistry (FRC) is the most direct approach in combustion simulations. It involves solving 13 a system of transport equations for each participating 14 chemical species and calculating the rates of chemi-15 cal reactions based on kinetic mechanisms. In reac-16 tion regions, chemical timescales can be several order 17 of magnitude smaller than the flow timescales, thus 18 requiring splitting approaches where chemistry is in-19 tegrated separately from the flow. As a result, FRC 20 offers precise representation of chemical processes 21 but can become prohibitively expensive, particularly 22 when increasing the size of kinetic schemes. 23

Several methodologies have been developed over 24 the years to enhance the efficiency of solving 25 chemistry. These methods include reducing ki-26 netic schemes through advanced techniques such as 27 DRGEP [1, 2], CSP [3], analytical reduction [4], and 28 virtual chemistry [5]. Additionally, dynamic adaptive 29 chemistry (DAC) [6, 7] offers the ability to perform 30 on-the-fly kinetic mechanism reduction. 31

For a given kinetic scheme further gain can be 32 achieved with chemistry tabulation [8]. Tabulation 33 34 techniques are very popular and efficient but rely on the flamelet hypothesis and necessitate to precompute 35 a look-up table based on canonical flames. Tabulation 36 reaches its limits when departing from the flamelet 37 regime or from the tabulated canonical flames. This 38 can be overcome by storage-retrieval techniques like 39 in-situ adaptive tabulation (ISAT) [9-11] or cell ag-40 glomeration techniques [12-17]. 41

Cell agglomeration, also called Dynamic Cell 42 Clustering (DCC) can be broken down into three 43 44 steps: i) grouping of cells with similar composition 91 into clusters, ii) computation of a single source term 45 per cluster and iii) mapping of the computed cells to-46 47 wards remaining cells of the same cluster. This paper focuses on the mapping step and presents a new 48 method that combines high accuracy and low compu-49 tational cost. The use of Principal Components Anal-50 ysis to create an optimal low-dimensional representa-51 tion of the composition is also discussed. Section 2 52 presents the methodology and Section 3 validates the 53 chosen approach on a H2/air triple flame. 54

2. Methodology 55

2.1. Cluster creation 56

Clustering methods aim at grouping similar com-57 105 putational cells together. Each cell acts as a chemical 106 58

reactor, therefore clustering has to consider each parameter defining the reactor's behaviour. A common state vector is $\phi = \{P, T, Y_1, ..., Y_{Nsp}\}$, comprising the pressure, temperature and mixture composition. Further parameters could be required according to the combustion model: partially stirred reactors (PSR) or turbulent combustion models for instance.

2.1.1. Dimensionality reduction

59

60

61

62

63

64

65

66

68

70

71

76

78

80

81

82

88

92

93

94

95

96

97

98

99

100

101

102

103

104

To ease the clustering process, dimensionality reduction is performed on the species fractions. The most basic approach consists in retaining the most relevant species and ignoring the others. This requires user knowledge and is likely to result in a sub-optimal clustering. An alternative is Principal Component Analysis (PCA) [18, 19], which automatically creates an optimal low-dimensional representation of a mixture [20-22]. PCA identifies the principal components, which are linear combinations of the state variables. These combinations can be related to known properties such as a progress variable or mixture fraction. Mathematically, PCA involves finding the eigenvectors and eigenvalues of the covariance matrix of the input data. These eigenvectors represent the directions in the high-dimensional space along which the data varies the most, while the eigenvalues indicate the variance explained along each eigenvector. The low-dimensional representation of ϕ is referred to as M. In the current context only mass fractions are considered in the reduction, individual Principal Components are expressed as:

$$PC_{i} = V_{i}Y$$

$$PC_{i} = \sum_{k=1}^{N_{species}} V_{i,k}Y_{k}$$
(1)

with V_i the ith eigenvector and $V_{i,k}$ the weight coefficients of individual species.

2.1.2. Clustering algorithm

K-Means [23] is one of the most popular and simplest clustering algorithms. It aims at partitioning data into K clusters, where each data point belongs to the cluster with the nearest mean value. It iteratively minimises the sum of squared distances between data points and their assigned cluster's centroid by moving the latter until an optimum is found. It has been used for cell agglomeration in [13]. An alternative approach is grid-based clustering [24]. This method divides the data space into a grid of cells. Each data point is then assigned to the grid cell that corresponds to its state coordinates. The goal is to group data points that fall within the same grid cell, effectively simplifying the clustering process and potentially making it more efficient for large datasets or



Fig. 1: Coarse clustering of data points along two dimensions of a H2-air triple flame

1 high cluster counts. A representation is given in fig-

² ure 1. This method has been used for cell agglomera-

³ tion in [12] and is chosen here for its efficiency.

4 2.2. Mapping

Once clusters have been formed and a single re-5 actor computed, the result has to be mapped to all 6 the elements within the cluster. As all elements have 7 slightly distinct states, inevitably, errors are intro-8 duced when mapping the compositions. However, ac-9 cording to the choice of the mapping method, this 10 error may be minimised. Backward mapping [14] 11 consists in redistributing source term relative to mass 12 fractions, while avoiding negative mass. This formu-13 14 lation is efficient but suffers from low accuracy and results in poor species gradients, as it will be shown 15 in the validation section. Conversely, Jacobian-based 16 mapping [16] has great accuracy but the computation 17 of the Jacobian of a time-integrated chemical reactor 18 is very expensive if not prohibitive. 19

This paper present a new mapping method, based on a Jacobian-free estimation. This estimation is designed to be low-cost while providing similar accuracy to an explicit Jacobian. Connectivity is created between the clusters, which is then used to approximate the Jacobian. Mapping is done based on those, while limiting degenerate cases.

27 2.2.1. Cluster connectivity

A connectivity map of adjacent clusters is created based on the cluster grid coordinates. Two clusters M_{C_1} and M_{C_2} are considered adjacent when they connect orthogonally:

$$|M_{C_{1},i} - M_{C_{2},i}| = 1, M_{C_{1},j} - M_{C_{2},j} = 0 \text{ for all } j \neq i.$$
(2)

An example of this connectivity, which can be computed efficiently using sparse matrices and sorting, is represented in Fig. 2. In this figure, the cluster center is the computed reactor, which is chosen as the one that minimizes composition difference $f(M_{\phi_i})$ to the other reactors:

$$f(M_{\phi_i}) = \sum_{j \neq i} \|M_{\phi_i} - M_{\phi_j}\|_2^2 .$$
 (3)



Fig. 2: Cluster connectivity based on computed reactor position based on Eq. 3

2.2.2. Jacobian-free mapping

Each edge of the connectivity graph allows to compute the Jacobian vector of the reaction rates within the reduced space M integrated along the edge. Let ϕ_{Ci} and ϕ_{Cj} , be the time-integrated reactors of two neighbour clusters C_i and C_j :

$$\phi_{Ci}^{t_0 + \Delta t} = \phi_{Ci}^{t_0} + \dot{\omega}_i \,, \tag{4}$$

with $\dot{\omega}$ the source term. The source term difference between two adjacent clusters *i* and *j* is expressed as:

$$\Delta \dot{\omega}_{j \to i} = \dot{\omega}_i - \dot{\omega}_j \,. \tag{5}$$

Similarly, composition difference between clusters i and j is expressed as:

$$\Delta M_{j \to i} = M_{\phi_{Ci}^{t_0}} - M_{\phi_{Cj}^{t_0}} \,. \tag{6}$$

The ratio of those differences is first-order approximation of the Jacobian J_M projected onto the unit vector $dM_{j\to i}$.

$$J_M dM_{j \to i} \approx \frac{\Delta \omega_{j \to i}}{\Delta M_{j \to i}} \,.$$
 (7)

39

40

41

42

43

45

46

47

48

49

Let ϕ_e be a reactor to be estimated within C_i , thus 1 $\Delta \omega_{i \to e}$ needs to be estimated from the know dis-2 placement $\Delta M_{i \to e}$. Based on the knowledge of the 3 Jacobian projected onto several known directions, the full Jacobian may be reconstructed and used to com-5

pute the change in the source terms: 6

$$\Delta \omega_{i \to e} = J_M \Delta M_{i \to e} \,. \tag{8}$$

37

38

39

40

41

42

43

44

45

46

47

7 However, degenerate cases can happen due to an insufficient number of projection directions or highly 8 co-linear directions (see Sec. 3). Rather than comput-9 ing the Jacobian at the cluster level, the source term 10 variation can be expressed as a weighted sum of vari-11 12 ations in known directions:

$$\Delta\omega_{i\to e} = \sum_{j=1}^{n} \alpha_j \Delta\omega_{i\to j} , \qquad (9)$$

with n the number of connected clusters and α_i the 13

interpolation coefficients to be determined from 14

$$\Delta M_{i \to e} = \sum_{j=1}^{n} \alpha_j \Delta M_{i \to j} = \mathcal{M} \alpha \,. \tag{10}$$

Eq. 10 can directly be inverted only if n = d, with 15 d the number of dimensions of subspace M: 16

$$\alpha = \mathcal{M}^{-1} \Delta M_{i \to e} \,. \tag{11}$$

The case n = 0 is very unlikely as chemistry 17 is continuous or is characteristic of an over-resolved 18 clustering. This case is shared with other mapping 19 methods. Solving for $1 \le n < d$ may be obtained by 20 a least square algorithm: 21

$$\alpha = \left(\mathcal{M}\mathcal{M}^t\right)^{-1} \mathcal{M}\Delta M_{i\to e} \,. \tag{12}$$

The least square returns α which minimises f: 22

$$f(\alpha) = \left\| \Delta M_{i \to e} - \mathcal{M} \alpha \right\|_2^2.$$
 (13)

The obtained solution is the best possible projection 23 of $\Delta M_{i \to e}$ given the insufficient amount of vectors 24 in M. This case is illustrated in Fig. 3a. 25

For d < n, Eq. 12 has an infinite number of so-26 lutions as there is an infinite number of vector com-27 binations from \mathcal{M} that are equal to $\Delta M_{i \to e}$. An ad-28 ditional constraint is set to obtain α with the smallest 29 norm, which is expected to introduce minimal error. 30 This is achieved with a least-square algorithm with 31 ridge regression [25]: 32

$$\alpha = \left(\mathcal{M}\mathcal{M}^t + \lambda I\right)^{-1} \mathcal{M}\Delta M_{i\to e} \,. \tag{14}$$

The ridge regression returns α which minimises f: 33

$$f(\alpha) = \left\|\Delta M_{i \to e} - \mathcal{M}\alpha\right\|_2^2 + \lambda \left\|\alpha\right\|_2^2 .$$
 (15)

 λ is chosen to be negligible compared to eigenvalues 34 of \mathcal{M} to not deteriorate the solution but way larger 35 36 than machine accuracy to break the super-colinearity of the system. The constraint minimising the norm of α is optimal as it reduces extrapolation and thus error magnitude. Once α is found, degenerate cases have to be handled. It can be shown that Eq. 9 is an interpolation and not an extrapolation if and only if:

$$\begin{cases} \sum_{j=1}^{n} \alpha_j \le 1, & (16) \\ \alpha_j > 0 & \text{for all } j \in \{1, ..., n\}. & (17) \end{cases}$$

$$\alpha_j \ge 0$$
 for all $j \in \{1, ..., n\}$. (17)

Illustrations of these special cases are given in Figs. 3c and 3b. It will be shown that extrapolation is beneficial to some extent in Sec 3, however avoiding excessive extrapolations remains crucial. Rescaling of α may be introduced with a user-defined limit α_{\lim} :

$$\alpha_{\text{rescaled}} = \frac{\alpha}{\max\left(1; \frac{\sum_{j=1}^{n} |\alpha_j|}{\alpha_{\text{lim}}}\right)}, \quad (18)$$

with typical values of α_{lim} ranging from 1 to 10.



(a) Projection due to n < d.



(b) Extrapolation due to violation of Eq. 16.



(c) Extrapolation due to violation of Eq. 17.

Fig. 3: Special cases for Jacobian-free mapping.

3. Validation

3.1. Simulation set-up

The implementation is done in YALES2 [26], which is a low-Mach number LES solver for massive unstructured meshes. Numerical methods are

49

50

51

4th-order in time and space and finite-rate chem-1 istry is integrated with CVODE [27] with analytical 2 Jacobian and full vectorization. PCA is performed 3 with PETSc [28] using dgesvd(). A H₂-air triple 4 flame [29, 30] in standard conditions is used as a ref-5 erence case. It is solved using the San Diego mecha-6 nism [31], which counts 21 species and 64 reactions 7 8 for H₂-air combustion with nitrogen chemistry. Inlet velocity is uniform and equal to $1m.s^{-1}$ and air-9 fuel equivalence ratio ranges from 0 to 24 to have 10 non flammable conditions on the sides. This set-



Fig. 4: Temperature field in the full simulation domain. Velocity streamlines are represented in white.



Fig. 5: Heat release rate (HRR) field in the full simulation domain with a HRR contour line to materialise the flame branches.

11

up is chosen as it spans a large region in the phase
space with lean-premixed, rich-premixed and diffusive flame regimes altogether. The mesh, represented
in Fig. 6, is refined within reactive areas thanks to
feature-based mesh adaptation to limit the cost and
the clustering of fresh gases.

18 3.2. Results

¹⁹ Error is measured on instantaneous quantities pro-²⁰ duced by the reactors: the Heat Release Rate (HRR)



Fig. 6: Triple flame mesh, made of 50'000 elements with smallest elements size of 20 microns.

and the species source terms $\dot{\omega}_k$ related by:

$$HRR = \sum_{k=1}^{N_{species}} \dot{\omega}_k H_{f,k}^0 , \qquad (19)$$

with $H_{f,k}^0$ the standard enthalpy of formation of species k. The analysis is focused on HRR here but the same conclusions are obtained for individual species. Within a solver iteration, reactors are solved twice, with and without clustering, computation is advanced based on the reference without clustering, Relative error is obtained based on the integrated difference:

$$E = \frac{\sum_{i=1}^{N_{\text{elem}}} |HRR_{\text{cluster},i} - HRR_{\text{ref},i}| V_i}{\sum_{i=1}^{N_{\text{elem}}} |HRR_{\text{ref},i}| V_i} .$$
 (20)

Measurement of the error is started from a quasisteady state of the triple flame. The error should tend to zero when the size of the clusters ε is reduced. Fig. 7 shows this behaviour when varying the clustering dimensions.



Fig. 7: Relative error on heat release rate relative to cluster resolution.

22

23

24

25

26

27

28 29

30

31 32













(d) PC4 field



Principal Components of the triple flame are shown
 in Fig. 8 and Fig. 9 and their variance, i.e. fluctuations

1

- in Fig. 8 and Fig. 9 and their variance, i.e. fluctuations
 of composition is given in Tab. 1.
- ⁵ Using only T or T + PC1 is insufficient as the rel-⁶ ative error on HRR remains higher than relative clus-
- 7 ter size. When advanced with clustering, these cases
- ⁸ diverge, unless cluster resolution is extremely high.



(a) PC1 coefficients



(b) PC2 coefficients



(c) PC3 coefficients



 10^{-2}

 10^{-1}

10

 -10^{-3} 10^{-3}



	Variance	Cumulated Variance
PC1	0.7526	0.7526
PC2	0.2454	0.9980
PC3	0.0015	0.9995
PC4	0.0004	0.9999

Table 1: Normalized variance along the 4 first principal components. All simulation points are considered here.

 -10^{0}

 -10^{-1}

 -10^{-2}

1 Using 2 PC or more is satisfactory, which is consis-

² tent as the two first PC hold most of the explained

³ variance. When advanced with clustering these cases

show great stability unless cluster resolution is ex tremely coarse.

6 Clustering along Principal Components with little

7 variance, like PC3 and PC4 is sub-optimal as way

more reactors need to be solved for a small error de crease. This is investigated by introducing a reduced

9 crease. This is investigated by
10 computational time:

$$RCT = \frac{\text{Wall clock time}(\mu s).N_{\text{cores}}}{N_{\text{elements}}.N_{\text{iterations}}} \,. \tag{21}$$

¹¹ Fig. 10 shows the relation between HRR error and

¹² RCT. As previously, T and T + 1PC have poor per-

13 formance. T + 2PC, T + 3PC and T + 4PC have

very similar behaviour. T + 4PC becomes slightly

¹⁵ more expensive at high cluster resolution due to some

16 excessive clustering.



Fig. 10: RCT of source term computation depending on the number of Principal Components. Dashed line represents the reference cost without cell agglomeration.

17 The Jacobian-free mapping is now considered using two Principal Components. An accuracy com-18 parison between backward, Jacobian and Jacobian-19 free mapping is performed in Fig. 11. As expected 20 Jacobian mapping is at all times more accurate than 21 backward mapping. On large clusters, the Jacobian-22 free mapping has a higher accuracy than the explicit 23 Jacobian. This is because it is computed based on 24 a variation of cluster size, thus filtering most of the 25 high-frequency non-linear species production rates. 26 On small cluster size the accuracy of the Jacobian-27 free mapping drops to the level of the backward map-28 ping due to a lack of connectivity. It should be noted 29 that clustering is most likely to be used with relatively 30 large cluster sizes. 31 Performance of the Jacobian-free mapping is given 32 33 by Fig. 12. Jacobian performance is not shown as

an efficient implementation is not trivial. In the cur-

³⁵ rent study its evaluation cost exceeds by far the source



Fig. 11: Accuracy comparison between backward, Jacobian and Jacobian-free mapping.





term computation cost. At equivalent RCT, error is diminished by up to 74% using Jacobian-free mapping. Best results are obtained when extrapolation is used at $\alpha_{lim} = 4$ but larger extrapolation deteriorate the solution. This is also clearly shown by HRR fields of Fig. 14. While $\alpha_{lim} = 4$ provides a smoother and more realistic solution than backward mapping, using extrapolation without a limiter can create extremely sharp local errors. Fig. 13 also stresses the need for a limiter by showing that a few elements can reach

37

38

39

40

41

42

43

44

prohibitive values of α , reaching a magnitude of over 1 1000. 2

Overhead induced by the cell agglomeration re-3

mains less than 1% of the initial source term cost and 4

is given in Tab. 2. Largest cost is associated with 5

PCA. It should be noted that this is the cost if PCA 6

was to be performed at every single iteration, which 7

8 is not needed in most combustion cases. The cluster

creation cost is negligible as it mainly relies on radix 9

sort, which is very efficient on integers. Mapping cost 10

consists mainly in solving the ridge regression while 11

creation of connectivity is negligible. 12











4. Conclusions 13

A new mapping method for cell agglomeration 14 has been introduced. Its accuracy and cost-reduction 15 has been demonstrated in a challenging hydrogen-air 16 17 triple flame. While the methodology parallelism has

Reference run	RCT	%
Source terms	440.0	100.00
Cell agglomeration	RCT	%
Source terms	122.1	27.80
+ PCA	1.8	0.41
+ Clustering	0.3	0.07
+ Mapping	1.1	0.25

Table 2: Source term cost and cell agglomeration overheads at $\epsilon = 0.01$.

18 not been discussed here, cell agglomeration can be easily performed in parallel for partitioned domains, 19 with each core having its own clusters. Future investi-20 21 gations should therefore be focused on massive DNS and LES of turbulent flames. 22

Declaration of competing interest 23

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Acknowledgments 28

24

25 26

27

29

31

32

37

38

39

40

41

42

43

44

45

46

47

48 49

50

51

52

53

54

55

56

57 58

59

60

61

62

This work has received funding from the European Union's Horizon 2020 research and innovation 30 programme under the CoEC project, grant agreement No 952181. Access to the HPC resources of TGCC and IDRIS was granted under the allocations 33 2023-A0142A11335 and 2023-A0152B06880 made 34 by GENCI. 35

36 References

- [1] T. Lu, C. K. Law, A directed relation graph method for mechanism reduction, Proceedings of the Combustion Institute 30 (1) (2005) 1333-1341. doi:10.1016/j.proci.2004.08.145.
- [2] P. Pepiot-Desjardins, H. Pitsch, An efficient error-propagation-based reduction method for large chemical kinetic mechanisms, Combustion and Flame 154 (1-2) (2008) 67-81. doi:10.1016/j.combustflame.2007.10.020.
- [3] M. Valorani, F. Creta, D. A. Goussis, J. C. Lee, H. N. Najm, An automatic procedure for the simplification of chemical kinetic mechanisms based on CSP, Combustion and Flame 146 (1-2) (2006) 29-51. doi:10.1016/j.combustflame.2006.03.011.
- Q. Cazères, P. Pepiot, E. Riber, B. Cuenot, [4] A fully automatic procedure for the analytical reduction of chemical kinetics mechanisms for Computational Fluid Dynamics applications, Fuel 303 (11 2021). doi:10.1016/j.fuel.2021.121247.
- [5] M. Cailler, N. Darabiha, D. Veynante, B. Fiorina, Building-up virtual optimized mechanism for flame modeling, Proceedings of the Combustion Institute 36 (1) (2017) 1251-1258. doi:10.1016/j.proci.2016.05.028.

- [6] D. A. Schwer, P. Lu, W. H. Green, An adaptive chemistry approach to modeling complex kinetics in reacting flows, Combustion and Flame
 133 (4) (2003) 451–465. doi:10.1016/S0010-5 2180(03)00045-2.
- [7] L. Liang, J. G. Stevens, J. T. Farrell, A dynamic adaptive chemistry scheme for reactive
 flow computations, Proceedings of the Combustion Institute 32 I (1) (2009) 527–534.
 doi:10.1016/j.proci.2008.05.073.
- [8] E. Knudsen, H. Pitsch, Capabilities and limitations of multi-regime flamelet combustion models, Combustion and Flame 159 (1) (2012) 242–
 264. doi:10.1016/j.combustflame.2011.05.025.
- [9] S. B. Pope, Computationally efficient implementation of combustion chemistry using in situ adaptive tabulation, Combustion
 Theory and Modelling 1 (1) (1997) 41–63.
 doi:10.1080/713665229.
- [10] L. Lu, S. B. Pope, An improved algorithm for
 in situ adaptive tabulation, Journal of Com putational Physics 228 (2) (2009) 361–386.
 doi:10.1016/j.jcp.2008.09.015.
- [11] B. J. Liu, S. B. Pope, The performance
 of in situ adaptive tabulation in computations of turbulent flames, Combustion Theory and Modelling 9 (4) (2005) 549–568.
 doi:10.1080/13647830500307436.
- [12] G. M. Goldin, Z. Ren, S. Zahirovic, A cell agglomeration algorithm for accelerating de-tailed chemistry in CFD, Combustion Theory and Modelling 13 (4) (2009) 721–739. doi:10.1080/13647830903154542.
- [13] F. Perini, High-dimensional, unsupervised
 cell clustering for computationally efficient
 engine simulations with detailed combustion chemistry, Fuel 106 (2013) 344–356.
 doi:10.1016/j.fuel.2012.11.015.
- [14] L. Liang, J. G. Stevens, J. T. Farrell, A 100 39 dynamic multi-zone partitioning scheme for 101 40 solving detailed chemical kinetics in reac-41 102 tive flow computations, Combustion Science 103 42 and Technology 181 (11) (2009) 1345-1371. 43 104 doi:10.1080/00102200903190836. 44 105
- 45 [15] A. Babajimopoulos, D. N. Assanis, D. L. Flow- 106 ers, S. M. Aceves, R. P. Hessel, A fully cou- 107 46 pled computational fluid dynamics and multi- 108 47 zone model with detailed chemical kinetics 109 48 for the simulation of premixed charge com- 110 49 pression ignition engines, International Jour- 111 50 nal of Engine Research 6 (5) (2005) 497-512. 112 51 doi:10.1243/146808705X30503. 52 113
- [16] Q. Xie, Y. Liu, M. Yao, H. Zhou, Z. Ren, 114
 A fully coupled, fully implicit simula- 115
 tion method for unsteady flames using 116
 Jacobian approximation and clustering, 117
 Combustion and Flame 245 (11 2022).
 doi:10.1016/j.combustflame.2022.112362.
- [17] A. Cuoci, A. Nobili, A. Parente, T. Grenga,
 Tabulation-based sample-partitioning adaptive
 reduced chemistry and cell agglomeration,

Tech. rep.

62

63

64

65

66

67

68

69

70

71

72

73

74

75

76

77

78

79

80

81

82

83

84

85

86

87

88

80

90

91

92

93

94

95

96

97

98

- [18] Jolliffe I. T., Principal Component Analysis, Springer New York, NY, 2002.
- [19] H. Hotelling, Analysis of a complex of statistical variables into principal components, Tech. rep. (1930).
- [20] J. C. Sutherland, A. Parente, Combustion modeling using principal component analysis, Proceedings of the Combustion Institute 32 I (1) (2009) 1563–1570. doi:10.1016/j.proci.2008.06.147.
- [21] K. Zdybał, G. D'Alessio, G. Aversano, M. R. Malik, A. Coussement, J. C. Sutherland, A. Parente, Advancing Reacting Flow Simulations with Data-Driven Models (9 2022).
- Y. Yang, S. B. Pope, J. H. Chen, [22] Empirical low-dimensional manifolds in Combustion composition space, and 160 1967-1980. Flame (10)(2013)doi:10.1016/j.combustflame.2013.04.006.
- [23] J. Macqueen, Some methods for classification and analysis of multivariate observations, Tech. rep., University of California, Los Angeles (1967).
- [24] Gan Guojun, Ma Chaoqun, Wu Jianhong, Grid-based Clustering Algorithms, Data clustering: Theory, Algorithms, and Applications 6 (12) (2017) 209–2017. doi:10.1137/1.9780898718348.ch12.
- [25] Arthur E. HOERL, Robert W. KENNAR, Ridge Regression: Biased Estimation for Nonorthogonal Problem, Tech. Rep. 1, University of Delaware and E. I. du Pont de Nemours & Co (2000).
- [26] V. Moureau, P. Domingo, L. Vervisch, Design of a massively parallel CFD code for complex geometries (2 2011). doi:10.1016/j.crme.2010.12.001.
- [27] Cohen D, Hindmarsh A, CVODE, A Stiff/Nonstiff ODE Solver in C, Computers in Physics 10 (2) (1996) 138–143.
- [28] Satish Balay, Shrirang Abhyankar, Mark⁻F. Adams, PETSc Web page (2023).
- [29] J. W. Dold, Flame Propagation in a Nonuniform Mixture: Analysis of a Slowly Varying Triple Flame, Tech. rep. (1989).
- [30] Veynante D, Vervisch L, Poinsot T, Linan A, Ruetsch G, Triple flame structure and diffusion flame stabilization, Center for turbulent research, Proceedings of the Summer Program (1994).
- [31] "Chemical-Kinetic Mechanisms for Combustion Applications", San Diego Mechanism web page, Mechanical and Aerospace Engineering (Combustion Research), University of California at San Diego.