

Fractional thermal model of the lungs using Havriliak-Negami function

Mathieu Pellet, Pierre Melchior, Youssef Abdelmoumen, Alain Oustaloup

► To cite this version:

Mathieu Pellet, Pierre Melchior, Youssef Abdelmoumen, Alain Oustaloup. Fractional thermal model of the lungs using Havriliak-Negami function. 7th ASME/IEEE International Conference on Mechatronic & Embedded Systems & Applications (ASME/IEEE MESA'11), Aug 2011, Washington DC, United States. pp.805-810, 10.1115/DETC2011-48095. hal-04649331

HAL Id: hal-04649331 https://hal.science/hal-04649331v1

Submitted on 26 Jan 2025 $\,$

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers. L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

FRACTIONAL THERMAL MODEL OF THE LUNGS USING HAVRILIAK-NEGAMI FUNCTION

Mathieu Pellet

IMS-UMR 5218 CNRS Université de Bordeaux 351 cours de la Libération F33405 Talence Cedex, France mathieu.pellet@ims-bordeaux.fr Pierre Melchior IMS-UMR 5218 CNRS Université de Bordeaux 351 cours de la Libération F33405 Talence Cedex, France pierre.melchior@imsbordeaux.fr Youssef Abdelmoumen

Hôpital du Haut-Lévéque, CHU de Bordeaux Avenue Magellan 33604 Pessac Cedex, France youssef.abdelmoumen@chu-bordeaux.fr

Alain Oustaloup

IMS-UMR 5218 CNRS Université de Bordeaux 351 cours de la Libération F33405 Talence Cedex, France alain.oustaloup@ims-bordeaux.fr

ABSTRACT

This paper is about fractional system identification of a thermal model of the lungs. Usually, during open-heart surgery, an extracorporeal circulation (ECC) is carried out on the patient. In order to plug the artificial heart/lung machine on the blood stream, the lungs are disconnected from the circulatory system. This may results in postoperative respiratory complications. A method to protect the lungs has been developed by surgeon and anesthetist. It is called: bronchial hypothermia. The aim is to cool the organ in order to slow down its deterioration. Unfortunately the thermal properties of the lungs are not well-known yet. Mathematical models are useful and needed in order to improve the knowledge of these organs. As proved by several previous works, fractional models are especially appropriate to model thermal systems (model compacity, accuracy) and the dynamic of fractal systems. Thus, fractional models of the lungs have been determined using time domain system identification with the Havriliak-Negami function. A comparison with integer order models was also carried out. The aim of this paper is to present the results of this study.

INTRODUCTION

Most of the time during open-heart surgery, it is necessary to stop the heart from beating to allow the surgeon to operate

properly. This is possible thanks to artificial heart/lung device. This device is called extracorporeal circulation (ECC). In order to connect the machine with the circulatory system, the heart and lungs are excluded from the blood stream. The lack of blood in the lungs during ECC, is recognized as a potential cause of postoperative pulmonary dysfunction. Thus, anesthetists are developing methods to protect the lungs. One of these methods is to cool down the lungs by insufflating fresh gas inside it. This method has shown results but is based on the assumption that the thermal insulation of the lungs increases during ECC. This assumption has not been verified yet. A possible solution to verify it, is to design a thermal model of the lungs during ECC and during standard condition, and to compare both models. This paper presents the first step of this study. Different models of thermal transfer inside the lungs are identified.

Fractional transfer functions are especially appropriate to model thermal [1] [2] [3] and biological systems [4] [5] and they are useful in system identification because they allow a few number of parameter (parametric compacity of the model) [6]. Among the fractional functions, the Havriliak-Negami function is not often used, though it showed interesting results in system identification [7].

This paper is composed of four parts. First, the approximations used for time simulation of fractional operator and Havriliak-Negami function are recalled. The second part

deals with the experimental protocol. The results of identification are presented in the third part. Finally, a conclusion considers the prospect.

TIME DOMAIN SIMULATION OF FRACTIONAL SYSTEMS

This part, recalls mathematical definition of non integer derivative, and then usual methods to simulate fractional systems.

Non integer derivative

The non integer derivative concept of any order (non integer),

_____(1)

was defined in the 19th century by Riemann and Liouville. Fractional derivative of a function f(t) is defined by the

order derivative ([.] is the floor operator) of a fractional order integral [8]:

₊, the Euler's function Γ is defined by :

(3)

(4)

(2)

The Laplace Transform of the order derivative (with +) of a function relaxed at the initial instant is such as [9]:

Frequency-bounded integro-differential operator synthesis

Because of the natural limits of a physical system and of the input/output signals (e.g. Shannon frequency and input signals spectrum), fractional operators s^{ν} are usually approximated with high rational order transfer function, over a frequency range $[\omega_A, \omega_B]$. Thus, the integro-differential operator and the rational transfer function have the same fractional behavior over this frequency range. The most commonly used approximation was suggested by Oustaloup [8]. It consists in a recursive distribution of poles and zeros over frequency range $[\omega_A, \omega_B]$. Such a method naturally induces a degradation of the approximation around the frequencies ω_A and B. This side-effect is known as "boundary effect". The approximation error is decreased over _B by widening the frequency range over which the v operator is synthesized, to [h], where

(5)

Boundary effect is considerably reduced by choosing [8]. The approximation of the integro-differential

operator over the $\begin{bmatrix} \\ B \end{bmatrix}$ frequency range is given by the relation :

where is an integer which is the number of pole-zero pair and where C_0 , and pulsations and are given by :



 $_0$ is calculated in order to obtain a unitary gain at the frequency 1 rad. s⁻¹.

Real parameters α and η are defined by the integrodifferential order ν , such as

Approximation and time simulation of Havriliak-Negami function

In this paper, the Havriliak-Negami function [10] [11]:

(11)

is used for identification and synthesized for $v_2 \in \mathbb{R}$, and $\frac{2}{4}$. The method used for the synthesis and time

simulation of the Havriliak-Negami function was developed by Sommacal in [7]. Because the details of the approximation are a bit complex, this part presents only the general idea. For futher explanations the reader should refer to [7].

It is shown that the function (11) can be written as :

with

(13)

(12)

and

(14)

where is the number of s-roots of function $_{HN}$.

Function F_1 is a product of classical Davidson-Cole functions which can be approximated using a recursive distribution of pole-zeros as presented above in the previous part of the paper. On the other hand, $\kappa(s)$ is approximated using a non recursive distribution of pole-zeros. Thus the Havriliak-Negami function is approximated on a frequency range as a product of pole-zeros.

EXPERIMENTAL PROTOCOL

Dr Youssef Abdelmoumen and his team are specialized in open-heart surgery. They provide the thermal data acquired on sheep. The experiment was carried out at the PTIB platform of Xavier Arnozan Hospital.

The general aim of this work is to study the variation of thermal characteristics of the lungs during extracorporeal circulation. Thus, the medical team recorded on a sheep the temperature of the lung during open-heart surgery before the ECC and during the ECC.

Lungs have a tree-like structure. From the trachea they are subdivided in series of bronchial tubes as shown in Fig. 1. The temperature inside the lungs is measured at the entry of the first three consecutive bronchial tubes (T_1, T_2, T_3) . The temperature of the body T_c is also measured. All these temperature are measured thanks to GI type thermocouple. These thermocouples are linked to a National Instruments PXI interface. A special software was designed with LABVIEW[®] and load into the PXI in order to acquire and record the signals.



Figure 1 Rough diagram of lungs, the black dots (●) show the approximate location of the thermal sensors

The measures are limited to these three locations because of the difficulty to accurately plant a sensor deeper into the lung.

SYSTEM IDENTIFICATION

If ones want to study the variation of the thermal characteristics of the lungs during ECC, then one can identify two different models of the thermal transfer in the lungs, during normal condition of the organ and during ECC, and finally compare both models. However this paper presents only the first step which is the result of the identification of the models.

In order, to simplify the problem and to limits the effect of the body temperature, the temperatures T_1 , T_2 and T_3 are normalized by T_c . Thus, two models are identified:

(15)

and

where

The transfer function chosen for and

(17)

is

it is identified with output error model. The vector of parameter is optimized using the non linear simplex optimization algorithm [12] [13].

The data are sampled at , thus the Havriliak-Negami function is approximated over the frequency range:

(19)

The data are also divided in two parts, one used to identify the model parameters (identification data) and the other to validate the value of the parameters (validation data).

The results of identification are shown on Fig. 2, 3, 4, 5, 6, 7, 8 and 9. On these figures the red curves are the model response, the blue curves are the input signals (ΔT_k) , and the black curves are the system response (ΔT_{k+1}) . One cans see that the model response is close to the system response on every diagram which means our model is able to reproduce accurately the dynamic behavior of the system.



Figure 2 System identification of error, before ECC.

and modeling

Accepted Manuscript







Figure 4 System identification of during





Figure 5 Validation data and modeling error of during ECC.



Figure 6 System identification of before ECC.

and modeling error,



Figure 7 Validation data and modeling error of before ECC.



Figure 8 System identification of during ECC.

and modeling error,

,

,



Figure 9 Validation data and modeling error of during ECC.

Results

Because the models are identified as black box, it is difficult to give a physical or physiological meaning to their parameters. However, Tables 1 and 2 show that the parameter is the one that varies the most in both models.

pre ECC	ECC	pre ECC	ECC
1.50	1.65	1.48	1.92
-0.32	1.20	1.31	-0.06
3.14	3.40	8.79	1.78
0.24	-1e-3	0.11	0.09
0.87	0.67	2.27	1.25
 1 -		-	

Table 1 Parameter values of and

Comparison between Havriliak-Negami models and integer models

In order to emphasize the interest of the Havriliak-Negami function, two integer models $H_{1i}(s)$ and $H_{2i}(s)$ are identified using the same data. The transfer function of these models is:

(20)

The vector of parameters $[b_1 f_1 f_2 f_3 f_4]$ is optimized using the *oe* function of MATLAB[®] which means an output error model is applied and the optimization algorithm is a gradient/hessian type. The values of the parameters identified are shown on table 3,4.

pre ECC	ECC	pre ECC	ECC
0.14	1.65	1.22	1.28
0.028	1.20	0.064	-0.15
-1.8	3.40	-1.6	-0.14
0.046	-1e-3	0.12	-0.16
0.97	0.67	0.95	0.34

Table 2 Parameters value of and

To compare the accuracy of the fractional and integer models the criterion J_e is defined

where N is the number of sample in which is the response of the system, and \tilde{Y} is the response of the model.

The values obtained for are presented on tables 3, 4, 5 and 6.

	Identification	Validation
	data	data
Fractional model		
Integer model		

Table 3 Values of
between ΔT_2 andcalculated for the model of the transfer
before ECC.

	Identification	Validation
	data	data
Fractional model		
Integer model		

Table 4 Values of
between ΔT_2 andcalculated for the model of the transfer
during ECC.

	Identification data	Validation data
Fractional model		
Integer model		

Table 5 Values of
between ΔT_3 andcalculated for the model of the transfer
before ECC.

	Identification data	Validation data
Fractional model		
Integer model		

Table 6 Values of
between ΔT_3 andcalculated for the model of the transfer
during ECC.

Tables 5 to 8 show that for each case, the criterion is minimized by the fractional model. Thus the accuracy of the fractional models are better for a same number of parameters than the integer models.

CONCLUSION

Four models of bronchial tubes thermal transfer are identified considering two different conditions ie with or without ECC. A significant variations in the parameters of the models is observed. For now, these variations are not linked with a physical meaning.

A comparison between an integer model and a fractional model is proposed, which shows the interest of the latter.

The main focus of the followings works will be to link the parameter of the model with a physical or physiological meaning.

REFERENCES

- [1] S. Victor, R. Malti, and A. Oustaloup, "Instrumental variable method with optimal fractionnal differentiation order for continuous-time system identification," in 15th IFAC Symposium on System Identification, SYSID, 2009.
- [2] J.-L. Battaglia, L. Le Lay, J.-C. Batsale, A. Oustaloup, and O. Cois, "Utilisation de modèles d'identification non entiers pour la résolution de problèmes inverses en conduction," *International Journal of Thermal Sciences*, vol. 39, no. 3, pp. 374 – 389, 2000.
- [3] M. Aoun, R. Malti, F. Levron, and A. Oustaloup, "Orthonormal basis functions for modelling continuous-time fractional systems," in *Sysid-IFAC*, 2003.
- [4] L. Sommacal, P. Melchior, J.-M. Cabelguen, A. Oustaloup, and A. Ijspeert, *Fractional Multimodels* of the Gastrocnemius Muscle for Tetanus Pattern, ch. 4, pp. 271–285. Advances in Fractional Calculus, 2007.
- [5] M. Pellet, P. Melchior, J. Petit, J.-M. Cabelguen, and A. Oustaloup, "Study of the peroneus digiti quarti muscle length effect on a motor unit fractional multimodel," in *IEEE/ASME International Conference on Mechatronics and Embedded Systems and Applications (MESA)*, July 2010.
- [6] A. Oustaloup, O. Cois, and L. Le Lay, *Représentations et identification par modèle non entier*. 2005.
- [7] L. Sommacal, Synthèse de la fonction d'Havriliak-Negami pour l'identification par modèle non entier et modélisation du système musculaire. Thèse de doctorat, Université Bordeaux 1, France, 2007.
- [8] A. Oustaloup, La dérivation non entière: théorie, synthèse et applications. Hermès, 1995.
- [9] K. Oldham and J. Spanier, *The fractional calculus*. New-York and London, 1974.
- [10] S. Havriliak and S. Negami, "A complex plane analysis of alpha dispersions in some polymers," *Journal Polymer Science*, vol. 14, no. B, pp. 99–117, 1966.
- [11] S. Havriliak and S. Negami, "A complex plane representation of dielectric and mechanical relaxation

processes in some polymers," *Polymer*, vol. 8, pp. 161–210, 1967.

- [12] M. Subrahmanyam, "An extension to the simplex method to constrained nonlinear optimization," *Journal of Optimization Theory and Applications*, vol. 62, no. 2, pp. 311–319, 1989.
- [13] D. J. Woods, An interactive approach for solving multi-objective optimization problems (interactive computer, nelder-mead simplex algorithm, graphics). Houston, tx, usa, Rice University, 1985.