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A Power Tower Control: A New Sliding Mode Control

Malek GHANES and Jean-Pierre BARBOT

Abstract—A control based power tower function at order 2 is proposed in this paper. This leads to a new sliding mode control, which allows employing backstepping technique that combines both guaranteed and finite time convergence. The proposed control is applied to a double integrator subject to perturbation d. Both guaranteed and finite convergence are ensured by the controller when d is considered constant and bounded, without knowing its upper bound. For the case, when d is variable and bounded with its upper bound known, only a finite time convergence is obtained. Simulation results are given to show the well founded of the proposed novel control.

Index Terms—Power tower, Backstepping, Guaranteed-finite time convergence, sliding mode.

I. INTRODUCTION

There are a large number of iterative techniques to built control or differentiator. These include: High order sliding mode [5], [14], [23], homogeneous [1], [17], [18], [20] backstepping [4], [12], [21], singular perturbation [11], [22], [24], high gain [2], [8], [9], ... In this article we study the possibility of constructing a finite-time control using the power tower function truncated to second order. Our original motivation was, similar to the case of the variable exponent "Homogeneous" differentiator, to propose a continuous variable exponent "Homogeneous" control. In the case of the differentiator the variation law of the homogeneity exponent is a function of the measurement noise [6] or of time to ensure guaranteed and finite convergence [7]. For the control, in order to ensure both guaranteed and finite time convergence with a continuous law exponential variation, theoretical obstructions prevented us from finding the control (see [25] for a discontinuous law) without a specific continuous power function. Indeed, for our best knowledge, a control combining guaranteed and finite time without singular problems has not yet been considered in the literature. Moreover, this kind of control has not been associated with the backstepping approach. To solve the problem of discontinuous control law when moving away from and approaching the sliding manifold, ensuring respectively guaranteed and finite time convergence, at least two different controllers are proposed in the literature (see [3], [15], [18], [19],...). In this paper we propose to fix the control discontinuity problem by using only one controller. For this purpose, a new control based on the power tower function [10] is introduced. This function, beyond its specific properties at the limits or on the fractal topology [16]

obtained the property of its derivative, allowed us to render possible the use of backstepping techniques for convergence with both guaranteed and finite time. By doing so, only two parameters are needed for the control tuning in absence of perturbation. In the presence of the latter, when it is variable, bounded with its upper bound known, one more parameter is needed. When the perturbation is constant and bounded, an integral action is necessary.

The remaining of the paper is organized as follows. Section II presents the main result, which render possible the use of backstopping technique that ensures a guaranteed-finite convergence by using only one controller. In Section III, the performances of the proposed control based power tower function, in absence and presence of perturbation, are put forward. A conclusion is given in section IV with some future works.

II. MAIN RESULT

Our control exploits the **power tower function** of order 2 allowing us to propose a new guaranteed-finite time backstepping based control. Before presenting this new idea, we need to introduce the following lemma:

Lemma 1: The time derivative of the function $\lceil a \rfloor^{|a|^{\alpha}}$ with a a function of time at least \mathbb{C}^1 and α a strictly positive constant is for $a \neq 0$:

$$\frac{d[a]^{|a|^{\alpha}}}{dt} = |a|^{|a|^{\alpha}} |a|^{\alpha-1} (1 + \alpha \ln(|a|))\dot{a} \qquad (1)$$
$$= |a|^{|a|^{\alpha} + \alpha - 1} (1 + \alpha \ln(|a|))\dot{a}$$

with $\dot{a} = \frac{d a}{d t}$.

Proof: As

$$[a]^{|a|^{\alpha}} = |a|^{|a|^{\alpha}} \operatorname{sgn}(a),$$

we first time derive

$$|a|^{|a|^{\alpha}}$$
.

In order to use the derivative of the composition of functions, we set

$$|a|^{|a|^{\alpha}} = e^{\ln(|a|)|a|^{\alpha}}$$

and we obtain

$$\frac{d \left|a\right|^{\left|a\right|^{\alpha}}}{dt} = e^{ln(\left|a\right|)\left|a\right|^{\alpha}} \frac{d \ln(\left|a\right|)\left|a\right|^{\alpha}}{d \left|a\right|} \dot{a}$$

or again

M. GHANES and J.-P. BARBOT are with Nantes Universite-École Centrale de Nantes-LS2N, UMR 6004 CNRS, Nantes, France malek.ghanes@ec-nantes.fr

J.-P. BARBOT is also with QUARTZ EA 7393, ENSEA, Cergy-Pontoise, France barbot@ensea.fr

$$\frac{d |a|^{|a|^{\alpha}}}{dt} = e^{\ln(|a|)|a|^{\alpha}} (|a|^{\alpha-1} + \ln(|a|) \alpha |a|^{\alpha-1}) \operatorname{sgn}(a) \dot{a}$$

which gives, multiplying both parts by sgn(a)

$$\frac{d\left\lceil a\right\rfloor ^{\left|a\right| ^{\alpha}}}{dt}=e^{ln(\left|a\right|)\left|a\right| ^{\alpha}}(\left|a\right| ^{\alpha-1}+ln(\left|a\right|)\alpha \left|a\right| ^{\alpha-1})\dot{a}.$$

This ends the proof.

Remark 1: If $\alpha > 1$ then we have

$$Lim_{a\to 0}|a|^{|a|^{\alpha}+\alpha-1}(1+\alpha \ln(|a|)) = 0$$
 (2)

which will be a guarantee of a bounded control law and therefore feasible in the vicinity of a = 0. This also ensures that for $\alpha > 1$ and \dot{a} bounded the equation (1) is also defined at a = 0 and is equal to zero.

Remark 2: An other property for $\alpha > 0$ of the proposed truncated power tower function is

$$Lim_{a\to 0}|a|^{|a|^{\alpha}}\operatorname{sgn}(a) = Lim_{a\to 0}\operatorname{sgn}(a).$$
(3)

Consequently the closed loop behavior obtained with such function refers to a sliding mode behavior.

Now, let us consider the following system:

$$\dot{x}_1 = x_2 \tag{4}$$

$$\dot{x}_2 = u + d$$

where u is the control input and d the disturbance.

Remark 3: To design a backstepping type control law in guaranteed-finite time we will refer to the lemma 1 and not to the derivative of $|a|^{\theta}$ which has an unbounded limit for $1 > \theta > 0$ and $a \to 0^+$.

Theorem 1: If d = 0, the following power tower control law:

$$u = -\lceil z_2 \rfloor^{|z_2|^{\gamma}} - \left(x_1 \qquad (5) + |x_1|^{|x_1|^{\beta} + \beta - 1} (1 + \beta \ln(|x_1|)) (-\lceil x_1 \rfloor^{|x_1|^{\beta}} + z_2) \right)$$

with $\beta > 1$, $\gamma > 0$ and $z_2 = x_2 + \lceil x_1 \rfloor^{|x_1|^{\beta}}$ ensures a guaranteed-finite time convergence of (4) to $x_1 = x_2 = 0$.

Proof: Based on the well known backstepping method [13], the proof is given in two steps.

First step. The first step consists on stabilizing x_1 by a fictive control x_2^* . For that, we define this control as a power tower control, that is

$$x_2^* = -\lceil x_1 \rfloor^{|x_1|^{\beta}} \tag{6}$$

with $\beta > 0$. Setting

$$V_1 = \frac{x_1^2}{2}.$$
 (7)

ŵ

The time-derivative of (7) reads

$$\dot{V}_1 = -|x_1|^{1+|x_1|^{\beta}} + x_1 z_2 \tag{8}$$

where

$$z_2 = x_2^* - x_2. (9)$$

If $x_2^* = x_2$, then the guaranteed-finite time convergence of x_1 to zero is achieved when d = 0. However, at this step, (9) is not converged to zero, that is why the following second step is important to design the real control.

Second step. Let first compute the time-derivative of (9). For that, we use the result of lemma 1 (see equation (1)). Then we obtain

$$\dot{z}_2 = u + |x_1|^{|x_1|^{\beta} + \beta - 1} (1 + \beta \ln(|x_1|)) \dot{x}_1.$$
 (10)

Now considering the Lyapunov function

$$V_2 = V_1 + \frac{z_2^2}{2} \tag{11}$$

. The time-derivative of (11) is:

$$\dot{V}_{2} = -|x_{1}|^{1+|x_{1}|^{\beta}} + x_{1}z_{2}$$

$$+ z_{2} \left(u + |x_{1}|^{|x_{1}|^{\beta} + \beta - 1} \right)$$

$$(1 + \beta \ln(|x_{1}|))(-\lceil x_{1} \rfloor^{|x_{1}|^{\beta}} + z_{2}) .$$
(12)

By setting u as proposed in (5) (including (6)), (12) becomes

$$\dot{V}_2 = -|x_1|^{1+|x_1|^{\beta}} - |z_2|^{1+|z_2|^{\gamma}}$$
(13)

From (13) the guaranteed-finite time convergence follows and this end the proof. $\hfill \Box$

From Theorem 1, we can set our first corollary:

Corollary 1: If d is bounded and its bound is know i.e. $|d| < D_{max}$, the following control law:

$$u = -K \operatorname{sgn}(z_2) - \left(x_1$$

$$+ |x_1|^{|x_1|^{\beta} + \beta - 1} (1 + \beta \ln(|x_1|)) (-\lceil x_1 \rfloor^{|x_1|^{\beta}} + z_2) \right)$$
(14)

with $K > D_{max}$, $\beta > 1$ and $z_2 = x_2 + \lceil x_1 \rfloor^{|x_1|^{\beta}}$ ensures a finite time convergence of (4) to $x_1 = x_2 = 0$.

Proof: By using the same Lyapunov function V_2 defined in (11), we obtain:

$$\dot{V}_2 = -|x_1|^{|x_1|^{\beta}} - z_2(-K \operatorname{sgn}(z_2) + d)$$
 (15)

and as $K > D_{max}$, we have a convergence in finite time but note in guaranteed time.

Corollary 2: If d is constant, bounded and its bound is unknown, the following control law:

$$u = w - [z_2]^{|z_2|^{\gamma}} - (x_1$$
(16)

+
$$|x_1|^{|x_1|^{\beta}+\beta-1}(1+\beta \ln(|x_1|))(-[x_1]^{|x_1|^{\beta}}+z_2))$$

= $-z_2$

with $\beta > 1$, $\gamma > 0$ and $z_2 = x_2 + \lceil x_1 \rfloor^{|x_1|^{\beta}}$ ensures a guaranteed-finite time convergence of (4) to $x_1 = x_2 = 0$.

Proof: By considering a new Lyapunov function as follows

$$V_3 = V_2 + \frac{(d-w)^2}{2},\tag{17}$$

where V_2 is defined in (11), we get:

$$\dot{V}_3 = -|x_1|^{1+|x_1|^{\beta}} - |z_2|^{1+|z_2|^{\gamma}}.$$
 (18)

From LaSalle theorem, we deduce that the system (4) controlled by the input (16) converges in guaranteed-finite time to the invariant set IS:

$$IS = \{x_1 = 0, x_2 = 0 \text{ and } w \in \mathbb{R}\}$$
 (19)

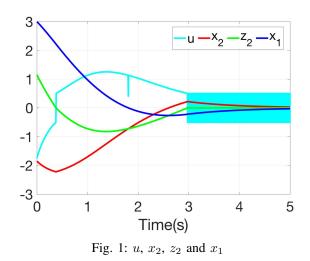
This ends the proof.

III. SIMULATIONS

To test the validity of the proposed power tower control, 4 simulations are presented. They are conducted using Matlab software, with a solver based on explicit Euler type where the sampling time is fixed to $50\mu s$. System (4) is considered with the following initial conditions: $x_1(0) = 3$, $x_2(0) = 1.8$. The control "gain" is very high when the initial conditions are far from zero, which requires very small sample step. As our sample step is limited to $10^{-6} \sec$ and our solver is an explicit Euler scheme, we have taken initial conditions not too far from zero. The parameters of the proposed controller (5) are selected as follows $\beta = 2$ and $\gamma = 1.5$. When the perturbation d is different from zero, controllers (16) and (14) are used, where $w_0 = 0$ in (16) and K = 10 in (14).

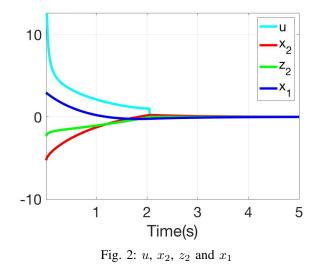
A. Results with d = 0 and with sign function

In this part, the controller (5) is applied to (4). The obtained results are depicted in Fig. 1. We can notice the very good performance of the proposed controller. The state x_1 converges to zero in a guaranteed-finite time. The same conclusion is stated for x_2 , which converges to zero in fixedfinite time. As z_2 is function of x_1 and x_2 , its convergence to zero is also achieved. For the behavior of the control (5), we can observe a chattering phenomena when $z_2 = 0$ at t = 3s. This behavior is natural and can be explained by the fact the tower term $|z_2|^{\gamma}$ in (5) goes to zero before the function z_2 , then the control u will depend only on the sign function of z_2 . This behaviour appears briefly also before, mainly at t = 0.4 s when z_2 crosses zero and at t = 1, 8 s when $x_1 = 0$ since the control depend also on the tower term $|x_1|^{\beta}$. At these two instants the control (5) depends directly on the sign function, which explains these two briefly discontinuities of the control. To overcome this behavior, we propose to replace the discontinuous function of this control by a continuous one when z_2 and x_1 reaches zero. This introduces the next subsection.



B. Results with d = 0 and with tanh function

In this part, the sign function used in (5) is replaced by the tanh function, where the gain of this function is fixed to 100000 to be more close to the behaviour of the sign function. The obtained results are depicted in Fig. 2. As excepted the same results about the guaranteed-finite time convergences of the states x_1 , x_2 and z_2 to zero are obtained. However, we can notice that the chattering disappeared in the control u, thanks to the tanh function. However, as it can be seen on Fig. 2, the control needs more effort at initial conditions.



C. Results with $d \neq 0$ constant and with tanh function

In this part, we test the performances of the controller defined in (16) when it is applied to system (4) in presence of a constant bounded perturbation d. We fixed d = 10 (any another value can be chosen) and the simulation results are shown in (3). In Fig. 3 we can show that the control (16) performs well in the sense that the perturbation d is exactly canceled (u = -d in steady state) thanks to the integral term

w in (16). The latter is replaced by the tanh function with high gain (100000) to avoid chattering phenomenon. Even if the *sign* function is approximated by the *tanh* function for avoiding the chattering, the convergence of the states x_1 and x_2 seems to be in guaranteed-finite time.

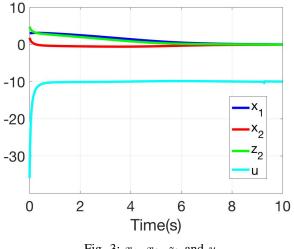


Fig. 3: x_1, x_2, z_2 and u

D. Results with d variable and with tanh function

In this part, we test the performances of the controller defined in (14) when it is applied to system (4) in presence of a variable bounded perturbation d where its upper bound is known. For that we took d as a sinus function: d = sin(t). The parameter K of the control (14) is fixed to 10, i.e. $K > D_{max}$, where $D_{max} = 1$ is the upper bound of the sinus function. The obtained results, plotted in Fig. (4), show very good performances of the control (14), the perturbation d is exactly canceled (u = -d) thanks to the sign function in (16), which is replaced by tanh function to avoid chattering phenomenon. In this case the convergence of the states x_1 and x_2 are in finite time and not in guaranteed time for the sign function.

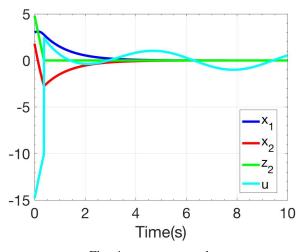


Fig. 4: x_1, x_2, z_2 and u

IV. CONCLUSION

In this paper, we propose a new control law on a power tower function truncated to order 2. This function makes it possible to use the backstepping technique in order to propose convergence in guaranteed and finite time. In a future work, the convergence finite times including the fixed one will be derived and the non-matching perturbations problem will be studied. The fixed-time will be assigned by the choice of some parameters $K_1 > 0$ and $K_2 > 0$ which multiply respectively the term $\lceil x_1 \rfloor^{|x_1|^{\beta}}$ and the term $\lceil z_2 \rfloor^{|z_2|^{\gamma}}$ in the control design. Moreover, the approach will be extended to higher dimensional systems. In a second step, the behavior of such law in an observer-based control scheme or with respect to noisy measurements or actuator saturation or again under sampling must be investigated.

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