A MIXED APPROACH FOR SIMULATING ELASTIC RIBBONS

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MERCI code: gitlab.inria.fr/elan-public-code/merci

MERCI = Modèle d'Équilibre de Rubans avec Courbure Intrinsèque

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 $h \sim w \ll L$

Ribbon

Plate $h \ll w \sim L$

 $h \ll w \ll L$



Nematic Ribbons (Liquid Crystal Elastomers)



Gimenez-Pinto Scientific Reports 2017

Warner+Terentjev Liquid Crystal Elastomers Oxf Univ Press 2003



Sawa PRE 2013









Chebydesic Pavilion



Pr. O Baverel ENPC, FR thinkshell.fr





Lateral Torsional Buckling



Liang et al, J. Struct. Eng. (2022)



Edmonton bridge (Canada)

total span ~100 m

image: Bruce Edwards Edmonton Journal





Edmonton bridge (Canada)

3 buckled girders

March 2015

image: Bruce Edwards Edmonton Journal





V.Z. VLASOV

THIN-WALLED ELASTIC BEAMS





1-Mechanics of a ribbon

2-Numerical implementation (for statics)



BENDING AND TWIST CONSTITUTIVE RELATIONS



I : moment of inertia *E* : Young's modulus

filament	E
Microtubule	1 GPa
DNA	1 GPa
Actine	2 GPa
Collagen	2 GPa
Rubber	2 GPa
Steel	200 GPa



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SQUARE CROSS-SECTION (ROD)





w = h

$$G = \frac{1}{2} \frac{E}{1+\nu}$$

Bending and twist constitutive relations







typically w = 3h





WIDE RECTANGULAR CROSS-SECTION (RIBBON) : THE RIBEXT MODEL



 $w \gg h$

(typically w > 10h)

Rod behaviour if $\kappa_1^2 \ll 60 \frac{h^2}{w^4}$ Kirchhoff

Bending and twist constitutive relations $\nu = 0$

$$ZI_{1}\kappa_{1}\left(1-\left[\frac{\kappa_{3}^{2}}{60\frac{h^{2}}{w^{4}}+\kappa_{1}^{2}}\right]^{2}\right)$$

$$I_1 = \frac{1}{12}h^3w$$

Sano Wada PRL 2019 Audoly Neukirch JMPS 2021

$$M_3 = 2E I_1 \kappa_3 \left(1 + \frac{\kappa_3^2}{60\frac{h^2}{w^4} + \kappa_1^2} \right)$$

Ribbon behaviour if
$$\kappa_1^2 \gg 60 \frac{h^2}{w^4}$$

Sadowsky



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Kirchhoff equations for elastic rods

kinematics $n'_1 = n$ $n_2' = n_2$ $x'=d_{3x}$ $n'_3 = n$ $y' = d_{3y}$ $m'_1 =$ $z^\prime = d_{3z}$ $m'_2 =$ $egin{aligned} &d_{3x}' = u_2\,d_{1x} - u_1\,d_{2x} \ &d_{3y}' = u_2\,d_{1y} - u_1\,d_{2y} \end{aligned}$ $m'_3 =$ $d_{3z}' = u_2\, d_{1z} - u_1\, d_{2z}$ $d_{1x}' = u_3 \, d_{2x} - u_2 \, d_{3x}$ $d_{1y}' = u_3\, d_{2y} - u_2\, d_{3y}$ Darboux $d_{1z}' = u_3 \, d_{2z} - u_2 \, d_{3z}$ $egin{aligned} &d_{2x}' = u_1\,d_{3x} - u_3\,d_{1x} \ &d_{2y}' = u_1\,d_{3y} - u_3\,d_{1y} \end{aligned}$ $d_{2z}' = u_1 \, d_{3z} - u_3 \, d_{1z}.$

21 non linear PDE (arclength & time) equilibrium & stability BVP (collocation) numerical path following

$$\begin{array}{ll} h_{2}u_{3}-n_{3}u_{2}-f_{1}+\rho A\left(\ddot{x}\,d_{1x}+\ddot{y}\,d_{1y}+\ddot{z}\,d_{1z}\right)\\ h_{3}u_{1}-n_{1}u_{3}-f_{2}+\rho A\left(\ddot{x}\,d_{2x}+\ddot{y}\,d_{2y}+\ddot{z}\,d_{2z}\right)\\ h_{1}u_{2}-n_{2}u_{1}-f_{3}+\rho A\left(\ddot{x}\,d_{3x}+\ddot{y}\,d_{3y}+\ddot{z}\,d_{3z}\right)\\ m_{2}u_{3}-m_{3}u_{2}+n_{2}\\ m_{3}u_{1}-m_{1}u_{3}-n_{1}\\ m_{1}u_{2}-m_{2}u_{1}\end{array}$$

 $m_1 = K_1 u_1, \quad m_2 = K_2 u_2, \quad m_3 = K_3 u_3$ constitutive relations

Darboux
$$\begin{cases} kinematics \\ x' = d_{3x} \\ y' = d_{3y} \\ z' = d_{3z} \\ d'_{3x} = u_2 d_{1x} - u_1 d_{2x} \\ d'_{3y} = u_2 d_{1y} - u_1 d_{2y} \\ d'_{3z} = u_2 d_{1z} - u_1 d_{2z} \\ d'_{1x} = u_3 d_{2z} - u_2 d_{3x} \\ d'_{1y} = u_3 d_{2z} - u_2 d_{3x} \\ d'_{1y} = u_3 d_{2z} - u_2 d_{3z} \\ d'_{1z} = u_3 d_{2z} - u_2 d_{3z} \\ d'_{2z} = u_1 d_{3z} - u_3 d_{1z} \\ d'_{2z} = u_1 d_{3z} - u_3 d_{1z} . \end{cases}$$

$$m_1 = K \left(1 - \frac{u_3^4}{u_1^4} \right) u_1 \qquad \text{nonlinear constitutive} \\ m_3 = 2K \left(1 + \frac{u_3^2}{u_1^2} \right) u_3 \qquad \text{relations} \end{cases}$$

Faultione for plactic etrine

Dias & Audoly (JMPS) 2014

THE PUSH AND TWIST EXPERIMENT





THE PUSH AND TWIST EXPERIMENT



1-Mechanics of a ribbon

2-Numerical implementation

(for statics)

ENERGY APPROACH

$$V = \int_0^L F(\kappa_1, \kappa_3) \, ds + \int_0^L \rho h w g \, x(s) \, ds$$

Rod
$$F(\kappa_1, \kappa_3) = \frac{1}{2} EI_1 \kappa_1^2 + \frac{1}{2} (2I_1 \kappa_3)$$

Ribbon $F(\kappa_1, \kappa_3) = \frac{1}{2} EI_1 \kappa_1^2 + \frac{1}{2} (2I_1 \kappa_3)$
Ribbon $F(\kappa_1, \kappa_3) = \frac{1}{2} EI_1 \kappa_1^2 + \frac{1}{2} (2I_1 \kappa_3)$

 EEI_1) κ_3^2

Kirchhoff

 $2EI_{1}\kappa_{3}^{2} + \frac{1}{2}EI_{1}\frac{\kappa_{3}^{4}}{60\frac{h^{2}}{w^{4}} + \kappa_{1}^{2}}$ $(EEI_1)\kappa_3^2 + \frac{1}{2}EI_1\frac{\kappa_3^4}{\kappa_1^2}$

RibExt (formula with $\nu = 0$)

Sadowsky (limit)

(formula with $\nu = 0$)

ENERGY APPROACH: SUPER-HELICES CODE

$$V = \int_0^L F(\kappa_1, \kappa_3) \, ds + \int_0^L \rho h w g \, x(s) \, ds$$

High-order elements : uniform curvatures κ_1 and κ_3

Integration of *Darboux* system:

$$\mathbf{r}'(s) = \mathbf{d}_3 \text{ and } \begin{cases} \mathbf{d}_1'(s) = \kappa_3 \mathbf{d}_2 \\ \mathbf{d}_2'(s) = \kappa_1 \mathbf{d}_3 - \kappa_3 \mathbf{d}_1 \\ \mathbf{d}_3'(s) = -\kappa_1 \mathbf{d}_2 \end{cases}$$

 $V = V(\kappa_1^{(i)}, \kappa_3^{(i)})$ with $i \in (1, 2, ..., N)$

min V using IP-OPT

Lateral Torsional Buckling scenario

SUPER HELICES ==> SUPER CLOTHOIDS

$$V = \int_0^L F(\kappa_1, \kappa_3) \, ds + \int_0^L \rho h w g \, x(s) \, ds$$

Super Helices: uniform curvatures κ_1 and κ_3

Super Clothoids:
$$\begin{cases} \kappa_1(s) = as + b \\ \kappa_3(s) = cs + d \end{cases}$$

Casati Bertails SIGGRAPH 2013

CHAINED SUPER HELICES $V[\kappa_{1,3}^{(i)}] = \int_0^1 F(\kappa_1,\kappa_3) \, ds + \int_0^1 \Gamma x(s) \, ds$

$$\chi_{1}(S) = \frac{\kappa \mathbf{1}[1] \times \kappa \mathbf{3}[1] \left(s - \frac{\sin[s \sqrt{\kappa \mathbf{1}[1]^{2} + \kappa \mathbf{3}[1]^{2}}]}{\sqrt{\kappa \mathbf{1}[1]^{2} + \kappa \mathbf{3}[1]^{2}}} \right)}{\kappa \mathbf{1}[1]^{2} + \kappa \mathbf{3}[1]^{2}}$$

Bertails et al SIGRAPH 2006

N=3 Γ =18.46 θ =0. 0.0 Ζ 0.5 1.0 0.1 X _{0.0} -0.1 0.2 0.1 0.0 -0.1 Y

CHAINED SUPER HELICES
$$V[\kappa_{1,3}^{(i)}] = \int_0^1 F(\kappa_1, \kappa_3) \, ds + \int_0^1 \Gamma x(s) \, ds$$

$$\mathcal{X}_{2}(S) = \frac{1}{3 \left(\kappa 1 \left[1\right]^{2} + \kappa 3 \left[1\right]^{2}\right)} \left(\kappa 1 \left[1\right] \times \kappa 3 \left[1\right] \left(1 - \frac{3 \sin\left[\frac{1}{3} \sqrt{\kappa 1 \left[1\right]^{2} + \kappa 3 \left[1\right]^{2}}\right]}{\sqrt{\kappa 1 \left[1\right]^{2} + \kappa 3 \left[1\right]^{2}}}\right) \left(-3 \left(-1 + \cos\left[\left(-\frac{1}{3} + s\right) \sqrt{\kappa 1 \left[2\right]^{2} + \kappa 3 \left[2\right]^{2}}\right]\right) \sin\left[\frac{1}{3} \sqrt{\kappa 1 \left[1\right]^{2} + \kappa 3 \left[1\right]^{2}}\right) \left(-1 + 3 s\right) \kappa 1 \left[2\right] \left(\kappa 1 \left[1\right]^{2} + \cos\left[\frac{1}{3} \sqrt{\kappa 1 \left[1\right]^{2} + \kappa 3 \left[1\right]^{2}}\right] \times 3 \left[1\right]^{2}\right) \left(-1 + 3 s\right) \sin\left[\frac{1}{6} \sqrt{\kappa 1 \left[1\right]^{2} + \kappa 3 \left[1\right]^{2}}\right]^{2} \kappa 1 \left[1\right] \times \kappa 3 \left[1\right] \kappa 3 \left[2\right]^{2} - \kappa 1 \left[2\right] \left(\kappa 1 \left[1\right] \left(-\kappa 1 \left[2\right] \times \kappa 3 \left[1\right] + \kappa 1 \left[1\right] \times \kappa 3 \left[2\right]\right) + \cos\left[\frac{1}{3} \sqrt{\kappa 1}\right] \right)$$

CHAINED SUPER HELICES

$$V[\kappa_{1,3}^{(i)}] = \int_{0}^{1} F(\kappa_{1},\kappa_{3}) ds + \int_{0}^{1} \Gamma x(s) ds$$

$$x_{3}(s) = \frac{1}{2} \left[\frac{4|1| - 2|1|}{2} \left[\frac{4|1| - 2|1|}{2} \left[\frac{4|1|}{2} \left[\frac{4|1|}{2}$$

CHAINED SUPER HELICES

$$V[\kappa_{1,3}^{(i)}] = \int_{0}^{1} F(\kappa_{1},\kappa_{3}) ds + \int_{0}^{1} \Gamma x(s) ds$$

$$v_{3}(s) = \frac{1}{2} \begin{bmatrix} \frac{411-411}{10}[\frac{1386[\frac{1}{2}\sqrt{611}^{12}-611]^{2}}{10[1^{12}-611]^{2}} + \frac{1}{2}\sqrt{611}^{12}-611]^{2}}{10[1^{12}-611]^{2}} + \frac{1}{2}\sqrt{611}^{12}-611]^{2}} \\ \begin{bmatrix} \frac{411-411}{10}[\frac{1386[\frac{1}{2}\sqrt{611}^{12}-611]^{2}}{10[1^{12}-611]^{2}} + \frac{1}{2}\sqrt{611}^{12}-611]^{2}} \\ \begin{bmatrix} \frac{1}{10}[\frac{1}{10}(\frac{1}{10},\frac{1}{10},\frac{1}{10},\frac{1}{10}] \\ \frac{1}{10}(\frac{1}{10},\frac{1}{10},\frac{1}{10},\frac{1}{10},\frac{1}{10}] \\ \end{bmatrix} \\ \begin{bmatrix} \frac{1}{10}[\frac{1}{10}(\frac{1}{10},\frac{1}{10},\frac{1}{10},\frac{1}{10},\frac{1}{10}] \\ \end{bmatrix} \\ \begin{bmatrix} \frac{1}{10}[\frac{1}{10}(\frac{1}{10},\frac{1}{10},\frac{1}{10},\frac{1}{10}] \\ \frac{1}{10}(\frac{1}{10},\frac{1}{10},\frac{1}{10},\frac{1}{10},\frac{1}{10},\frac{1}{10},\frac{1}{10}] \\ \end{bmatrix} \\ \end{bmatrix} \\ \begin{bmatrix} \frac{1}{10}[\frac{1}{10}(\frac{1}{10},\frac$$

$$\begin{aligned} & \mathsf{CHAINED SUPER HELICES} \\ & V[\kappa_{1,3}^{(i)}] = \int_{0}^{1} F(\kappa_{1},\kappa_{3}) \, ds + \int_{0}^{1} \Gamma \, x(s) \, ds \\ & \mathsf{equilibrium} \quad \nabla \, V(\kappa_{1}^{(i)},\kappa_{3}^{(i)}) = 0 \\ & \mathsf{Hessian}_{(\mathsf{Jacobian})} \quad H_{ij} = \frac{\partial^{2} V}{\partial \kappa_{1,3}^{(i)} \, \partial \kappa_{1,3}^{(j)}} & \mathsf{Nu} \\ & N = 3 \\ & \mathsf{6 \ dofs} \quad H = \begin{bmatrix} 0.343101 & 0.301999 & 0.0081 \\ 0.301999 & 0.511598 & 0.249 \\ 0.0000260758 & 0.00486517 & 0.100 \\ 0.00136636 & 0.0349803 & 0.0025 \\ 4.8861 \times 10^{-7} & 0.000069284 & 2.67903 \end{bmatrix} \end{aligned}$$

Number dofs = 2 N

818523	0.0000260758	0.00136636	$4.8861 imes 10^{-7}$
49532	0.00486517	0.0349803	0.000069284
45727	0.10058	0.00255619	$2.67903 imes 10^{-7}$
10058	0.496799	0.0364329	0.0000684055
255619	0.0364329	0.334652	0.00917153
$03 imes 10^{-7}$	0.0000684055	0.00917153	0.493854

Full Hessian Matrix

THE MIXED APPROACH $V = \int_{0}^{1} F(\kappa_{1}, \kappa_{3}) \, ds + \int_{0}^{1} \Gamma x(s) \, ds$ $V = V(\kappa_1^{(i)}, \kappa_3^{(i)}, r^{(i)}, d_{123}^{(i)}) \text{ with } i \in (1, 2, \dots N)$ Minimize V under matching constraints Number dofs = 14 N

Banded Hessian matrix

THE MIXED APPROACH

H =

-0.44 0.19 -0.35 -0.66 0.23 -0.69 -0.12 -0.75 0 0.61 0.65 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	
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N = 8 elements => 112 dofs

Banded Hessian matrix

THE MIXED APPROACH

H =

0.12 -0.84 0.82 -0.63 0 -0.18 0.22 -0.64 0.37 0.86 -0.12 0 0 0 0 0 0 0.85 0.36 -0.83 0.22 -0.63 0 -0.81 -0.11		000 0 0 0 0 0 0
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-0.01 -0.76 0 -6.07 0 0 -1.8 0 0 0.11 0 0 0 0.01 0.03 0 4.41 0 0 2.57 0 0 -0.59 0 1 -0.11 0.05 0 0 -6.07 0 0 -1.8 0 0 0.11 0 0 -0.04 0.07 0 0 4.41 0 0 2.57 0 0 -0.59 0	0 0 0 0 0 0 -0.39 0 0 -2.05 0 0 0.11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000000000000 000000000000
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N = 8 elements => 112 dofs

Banded Hessian matrix

MOEBIUS

Charrondiere et al TOG 2024

Roger Fosdick Eliot Fried *Editors*

The Mechanics of Ribbons and Möbius Bands

1858 A. F. Moebius

2015 Journal of Elasticity special issue edited by R. Fosdick & E. Fried

MOEBIUS BAND

- 1858 Johann Benedict Listing (analysis situs => topology)
- 1929 M. Sadowsky (developable surface)
- 1962 W. Wunderlich (exact energy)
- 2007 Starostin+Heijden (numerics)

MOEBIUS BAND

Wunderlich energy 169 elements (resmeshing) w/L = 0.1approx. 1 second

MOEBIUS BAND: CONVERGENCE RATE

l/p0.020 0.050

MOEBIUS BAND: COMPUTATION TIME

p (nbr. seg.)

MOEBIUS BAND: EFFICIENCY

Lateral Torsional Buckling

0 0.05

Lateral Torsional Buckling

Lateral Torsional Buckling

$$w/L = 0.1$$

 $h/L = 0.001$
 $v = 0.35$

$$\Gamma = \frac{Mg}{Dw/L^2}$$

$$\Gamma_{\text{buck}} = 15$$

Lateral Torsional Buckling

$$w/L = 0.1$$

 $h/L = 0.001$
 $v = 0.35$

$$\Gamma = \frac{Mg}{Dw/L^2} = 20$$

FEniCS-Shell (Hale, Brunetti, Bordas, Maurini Comp. & Struct. 2018)

 $\eta(0) = 0$

Lateral Torsional Buckling

$$w/L = 0.1$$

 $h/L = 0.001$
 $v = 0.35$

$$\Gamma = \frac{Mg}{Dw/L^2} = 20$$

 $\eta(0) = 0$

Lateral Torsional Buckling

w/L = 0.1h/L = 0.001

 $\nu = 0.35$

harphi Sh = 10

 $\Gamma = \frac{Mg}{Dw/L^2} = 20$

 $\eta(0) = 0$

Lateral Torsional Buckling

w/L = 0.1h/L = 0.001v = 0.35

$$\Gamma = \frac{Mg}{Dw/L^2} = 20$$

Sh = 10

Lateral Torsional Buckling

Lat. disp.

 $\eta(0) = 0$

Ribbons: between (1D) rods and (2D) plates

(1D) high-order spatial discretisation

Mixed approach: curvature and position

Numerical implementation: MERCI code

Thank you

and $\frac{w}{L} = 0.01$.

(Left) the heavy Möbius ribbon stands up on a plane, or (right) the ribbon falls on its side, both solutions being stable. Parameters are $\Gamma = 0.1$

SUPER HELICES, SUPER CLOTHOIDS, AND DISCRETE ELASTIC RODS

Bertails et al 2006, Casati+Bertails 2013

Up to now: Inextensible Ribbon models

plate theory: extension is expensive

hypothesis: no extension at all ==> equilibrium: developable surface ==> presence of lines on the surface

Roger Fosdick Eliot Fried Editors

The Mechanics of Ribbons and Möbius Bands

Springer

1929 M. Sadowsky

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straight lines

The Ribext model: limits

 $\mu \gg 1 \qquad \psi \rightarrow 1 \qquad \text{Ribbon}$

depends on the equilibrium solution !!

The Ribext model: limits

μ

$$\psi(\mu) = 1 - \frac{2}{\sqrt{\mu/2}} \frac{\cosh\sqrt{\mu/2} - \cos\sqrt{\mu/2}}{\sinh\sqrt{\mu/2} + \sin\sqrt{\mu/2}}$$

$$\psi(\mu) = \frac{\mu^2}{720 + \mu^2}$$
Padé approximant
with $\mu[\kappa_1] = \sqrt{12(1 - \nu^2)}$

$$\left(\frac{w^2}{Lh}\right) \kappa_1 L$$
Shield
number

