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Article

# Battery Passports for Second-Life Batteries: An Experimental Assessment of Suitability for Mobile Applications

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**Abstract:** End-of-life electric vehicle (EV) batteries can be reused to reduce their environmental impact and economic costs. However, the growth of the second-life market is limited by the lack of information on the characteristics and performance of these batteries. As the volume of end-of-life EVs may exceed the amount of batteries needed for stationary applications, investigating the possibility of repurposing them in mobile applications is also necessary. This article presents an experimental test that can be used to collect the data necessary to fill a battery passport. The proposed procedure can facilitate the decision-making process regarding the suitability of a battery for reuse at the end of its first life. Once the battery passport has been completed, the performance and characteristics of the battery are compared with the requirements of several mobile applications. Mobile charging stations and forklift trucks were identified as relevant applications for the reuse of high-capacity prismatic cells. Finally, a definition of the state of health (SoH) is proposed to track the suitability of the battery during use in the second-life application considering not only the energy but also the power and efficiency of the battery. This SoH shows that even taking into account accelerated ageing data, a repurposed battery can have an extended life of 11 years at 25 °C. It has also been shown that energy fade is the most limiting performance factor for the lifetime and that cell-to-cell variation should be tracked as it has been shown to have a significant impact on the battery life.

**Keywords:** second life; circular economy; lithium-ion battery; battery passport; state of health; remaining useful life; mobile applications; battery life cycle; electric vehicle



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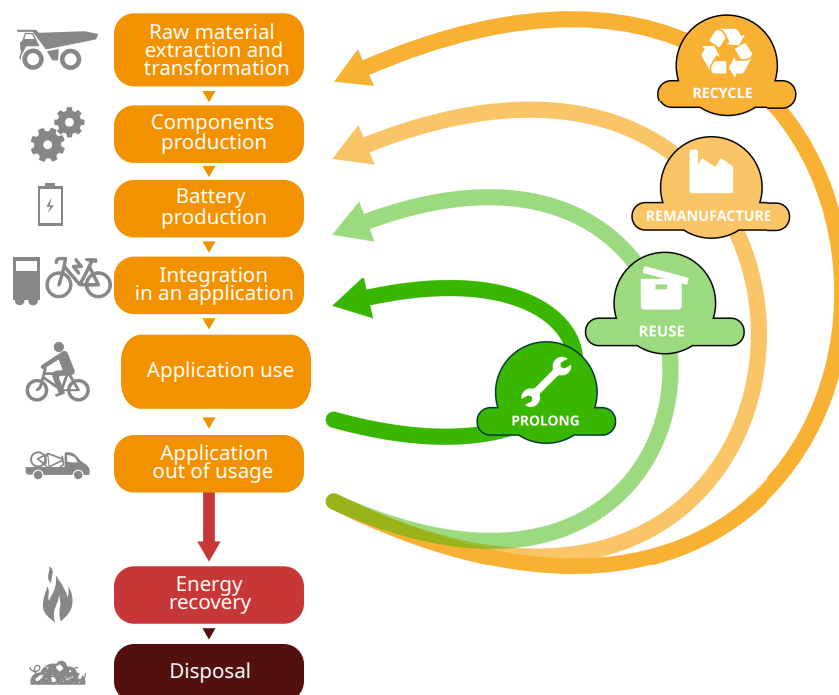


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## 1. Introduction

Policies to promote electric vehicles and renewable energy are being adopted around the world [1,2]. Lithium-ion batteries are becoming the ubiquitous energy storage technology due to their high energy density, low self-discharge rate and long cycle life [3]. In 2017, Sun et al. showed that batteries are mostly used to power consumer electronics applications, with electric mobility accounting for only a quarter of annual battery consumption [4]. The prominence of electronic batteries and the limited amount of energy they can store may explain why the linear economic approach of 'take, make and dispose' has been largely favoured. The recent growth of electric mobility and renewable energy provides an opportunity to move towards more sustainable practices [5].

The principles of the circular economy provide valuable guidance by promoting actions to maintain the value of products for as long as possible while minimising the generation of waste [6]. Figure 1 illustrates the different actions promoted by the circular model.



**Figure 1.** Technical cycles of the circular battery. The notion of second life can refer to reuse or remanufacture. Reproduced with permission from Guilhem Grimaud [7].

The most preferable action to take is to extend the lifespan of the application for which the battery was produced as much as possible. Thermal management [8,9] and optimal charging strategies [10,11] are some solutions that can help to prolong battery lifetime [12]. When the battery is no longer suitable for its first application, the possibility of giving the battery a second life should be systematically considered. Battery second life can be defined as the complete (referred to as reuse in Figure 1) or partial (referred to as remanufacture in Figure 1) reuse of the battery for the original purpose for which it was designed [13].

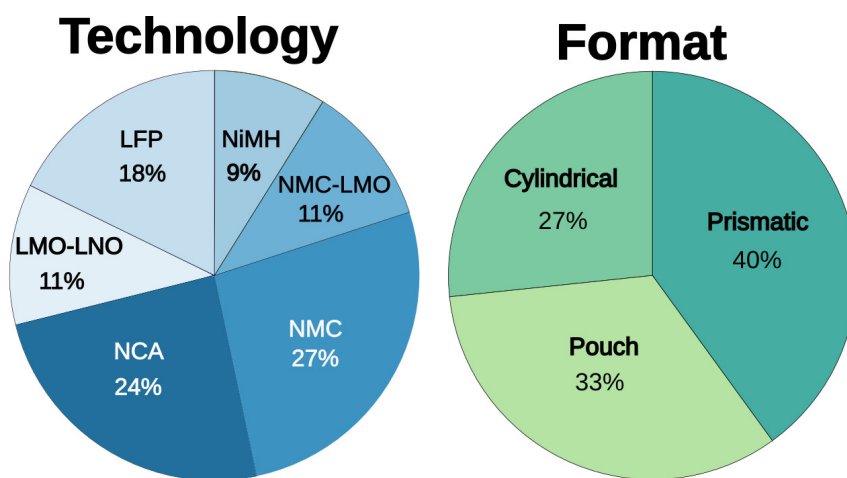
In 2018, Martinez-Laserna et al. highlighted the economic, legal and technical barriers hindering the development of such a second-life market [14]. Since then, significant progress has been made. Economic uncertainty about the future viability of this market appears to be limited, as companies such as Groupe Renault and Daimler have announced the creation of second-life battery factories [15,16]. Despite these encouraging announcements, a number of key challenges remain.

First, reuse brings a paradigm shift in the way the battery market is organised: from a stock-based economy to a flow-based economy. When new batteries are used, product design involves drawing up a system specification and then determining the specifications and quantities of batteries required to power the system [17,18]. In this system, the main limiting factor is the cost of the batteries, which is directly related to the level of raw material reserves that can be economically extracted [19]. One solution to reduce the environmental impact of batteries is to reuse them. However, the second-life market faces a major constraint. A company wishing to reuse batteries has to adapt to the flow of end-of-life vehicles, i.e., those available at a given time and in a given geographical area. The use of such batteries means that the design of the system must be adapted to the batteries available at the end of their first life. The performance of these batteries will also limit the performance of the designed system and its possible uses.

Despite the growth of electric mobility, the market for end-of-life electric vehicle batteries remains small. In France, only 3864 electric or hybrid vehicles reached the end of their life over the entire period from 2014 to 2020, compared to more than 8.6 million internal combustion vehicles [20,21]. These vehicles were distributed among the 1680 car dismantling centres in France responsible for dismantling and recycling vehicles. On average, over the period 2014–2020, a car dismantling centre collected 1 electric or hybrid

vehicle every 2 years and 5 months, compared to 14 internal combustion engine vehicles per day. This average should be treated with caution as there are large geographical differences in the distribution of end-of-life vehicles across the country. Nevertheless, this estimate highlights the small quantities of end-of-life electric and hybrid vehicles available.

The diversity of their technologies is another important barrier to the near-term growth of a reuse market. The wide variety of automotive battery designs is a major challenge, as they differ in size, electrode chemistry, configuration and state of health, making reuse complex [22]. Different battery cells within the same vehicle can also experience different degradation modes, resulting in different internal impedances, capacities and self-discharge rates [23]. Table A1 shows the characteristics of the world’s best-selling vehicles between 2012 and 2022. Figure 2 shows a synthesis of the different battery technologies and formats used in the most sold vehicles between 2012 and 2022.



LFP : Lithium Fer Phosphate    LMO : Lithium Manganese Oxide    LNO : Lithium Nickel Oxide  
 NCA : Nickel Cobalt Aluminium    NiMH : Nickel-Metal Hydride    NMC : Nickel Manganese Cobalt

**Figure 2.** Diversity of batteries technologies and formats used in the most sold vehicles from 2012. Made from data in Table A1. Shares are based in figures weighted by the number of sales.

This delay before a significant increase in the volume of end-of-life EV batteries can help to anticipate an important challenge: determining the applications that can be powered by reused batteries. To date, stationary uses are very popular in the literature on battery reuse [24]. Table 1 provides some examples of work on the use of second-life batteries in stationary storage applications.

**Table 1.** Examples of work on the use of second-life batteries in stationary storage applications.

Stationary Storage Application	Reference
Fixed charging station	[25,26]
Grid frequency regulation	[27,28]
Micro grid	[29,30]
Residential storage	[31,32]
Utility-scale storage	[33,34]

Stationary applications are often seen as ideal for second-life batteries, as they generally tolerate lower energy densities than electric vehicles [35]. They allow the use of modules or packs, which avoids prohibitive reconditioning costs [36]. Batteries reused for stationary applications are also subject to stresses comparable to those for mobility applications [37]. However, as the ageing process of degraded batteries is not yet well understood, they

should not be used in applications critical to the stability of the grid or human health, for example, for emergency power supply in hospitals.

The French electricity transmission grid operator RTE has expressed concern about the limited volumes of second-life batteries that could be reused in stationary applications. In its most optimistic scenario, up to 100 GWh, i.e., 22% of the volume of French batteries in 2050, could be reused in stationary applications in France [38].

Because of the diversity of battery technologies and applications, it is necessary to define a generic procedure for the experimental assessment of the performance of a battery at the end of its first life. The battery passport foreseen in the European Battery Regulation defines a set of minimum characteristics to be provided by the sellers of used batteries [13]. This information on the characteristics and performance of the battery can help determine whether a battery can be reused.

This information needs to be updated throughout the life of the battery as it plays a key role in determining the economic value of the battery and its suitability for reuse [39]. Walden et al. have highlighted some of the challenges of battery passports [40]. In particular, the following locks are mentioned:

- To standardise the format for different product types;
- To standardise performance indicators and how they are measured;
- To clearly define the data to be included in the passport;
- To protect intellectual property and confidential information;
- To allow access to the data by repairers, recyclers and consumers.

Standardisation of information measurement is essential in the field of batteries, where several experimental techniques and definitions coexist to measure the same performance indicators [41,42]. Berger et al. propose to extend the battery passport concept beyond the requirements of the new Battery Directive recently proposed by the European Commission. They define the battery passport as a valuable and comprehensive source of data for the sustainable management of products [43,44]. This article favours this definition. As the digital product passport can help to promote circular practices, any information deemed useful to facilitate decision making on possible reuse is included, in addition to the requirements of the European regulation [45,46].

The scientific literature on the battery passport and the assessment of its suitability for a second life in a particular application is sparse. Montes et al. [47] and Michelini et al. [48] have proposed lists of information that could be useful in making a decision on the suitability of a battery for a particular application, without however describing methods for obtaining this information. Beckers et al. presented an algorithm for determining the efficiency of an end-of-life automotive battery [39]. Thus, despite the growing number of experimental studies on end-of-life automotive batteries, none have presented a comprehensive methodology based on experimental work to assess the suitability of batteries for reuse in specific applications.

### 1.1. Contributions

This article aims to fill three gaps in the literature.

#### 1. Experimental evaluation to fill the battery passport

A simple test that can be used to fill a battery passport is described in detail. The capacity, resistance and open circuit voltage of all the battery cells from a second life module are measured and the key performance indicators of the battery are assessed. This experimental work contributes to the existing literature on second-life batteries as it proposes an experimental framework for assessing the suitability of a certain battery type for repurposing.

#### 2. Matching with second-life application needs

Based on the experimental results, the suitability of EV batteries for a second life is assessed by comparing measurements to the performance requirements of several applications. This

study contributes to the existing literature as it proposes an experimental assessment of the suitability of a second-life battery for several second-life applications.

### 3. Definition of the state of health and estimation of the remaining useful life according to the second-life application

A state of health is defined according to the new usage requirements. The different possible performances and end of life thresholds are also presented and used to estimate the remaining useful life. This study contributes to the existing literature as it proposes adapted definitions of state of health and remaining useful life according to second-life application.

#### 1.2. Layout

This article is organised as follows: The introduction presents the context and the objective of the article. Section 2 presents the experimental evaluation of key performance indicators for second-life battery selection. In Section 3, the suitability of the tested second-life batteries for powering different mobile applications is assessed. Conclusions are drawn and an outlook is given in the final section.

## 2. Experimental Evaluation of Battery Suitability for Reuse

This section presents a procedure for establishing a battery passport, as required by the European directive [13], which can then be used to assess whether reuse is possible. This protocol is intended to be generic. It can be used for any type of battery. Each characteristic of the battery is first assessed and then the experimental measurements are used to complete a battery passport that will guide the decision on the battery's eligibility for a second life.

#### 2.1. Visual Inspection of the Battery

The first stage of the procedure involves a visual inspection of the battery. In this study, a module extracted from a BMW i3 electric vehicle has been used. This checks that the battery has no defects such as traces of impact or swelling on the cells [49]. The various indications shown in Figure 3 show that the module was extracted from a vehicle produced in April 2017.

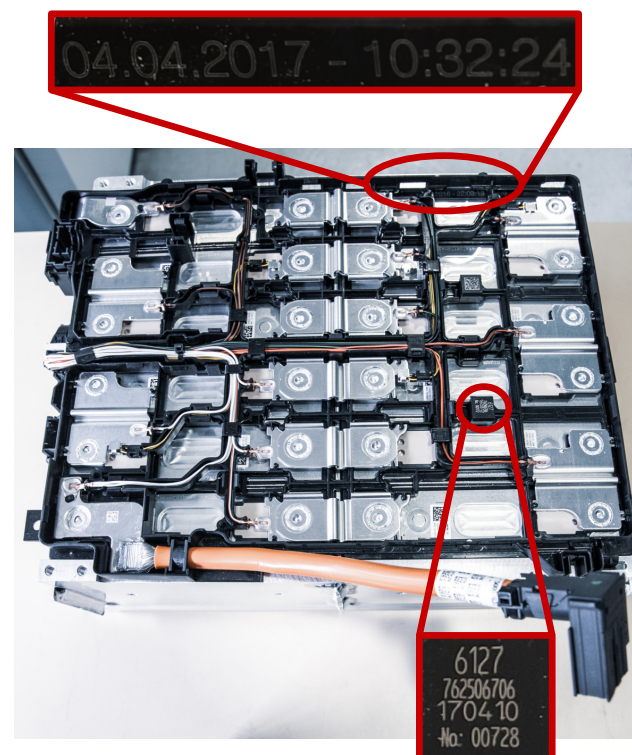
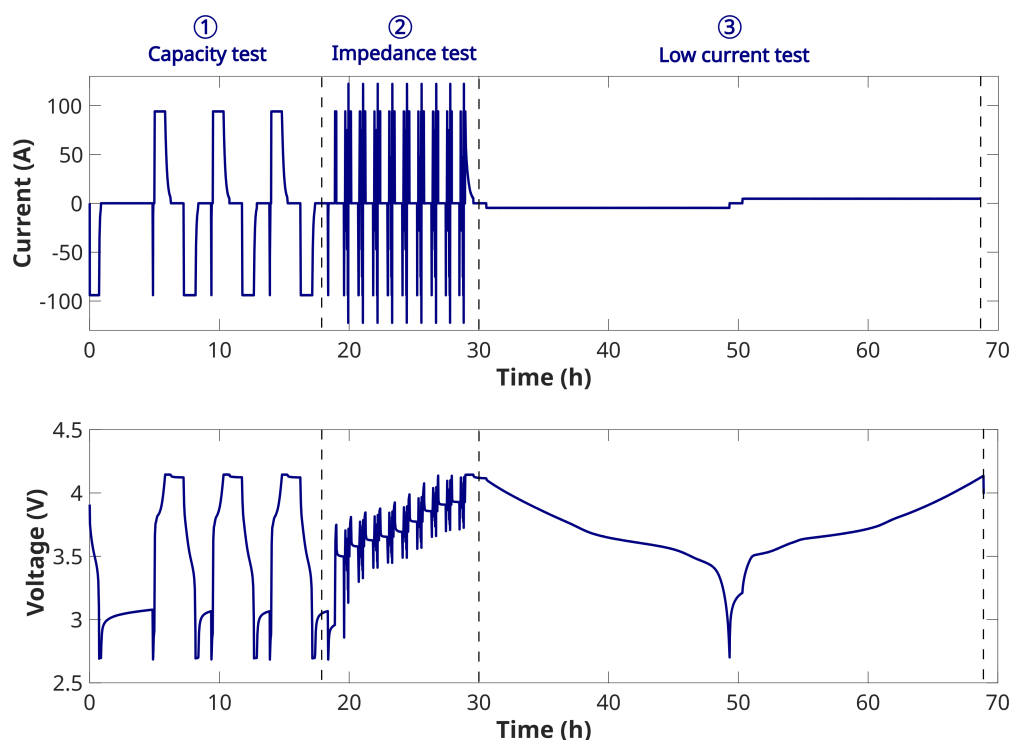


Figure 3. BMW i3 module production date.

The QR codes available on this module can also be used to obtain the battery model. This information is particularly useful for obtaining the product datasheet and collecting information on this technology. To complete this visual inspection, the module was measured for mass and dimensions. It weighs 28 kg and measures 410 mm by 300 mm by 150 mm, which corresponds to a volume of 18.4 L. It is made up of 12 lithium-ion cells connected in series, each weighing 2.1 kg and having a volume of 1 L. A BMW i3 vehicle is composed of eight modules connected in series.

## 2.2. Experimental Characterisation of the Second-Life Module

To complete the battery passport, a test consisting of a measurement of capacity, impedance and open circuit voltage is required. Figure 4 shows the current and voltage profiles for this test. Each cell of the module was tested separately.



**Figure 4.** Current and voltage evolution during the characterisation test.

Table 2 shows the different steps of the characterisation test and their approximate duration.

**Table 2.** Protocol of the characterisation test.

Step	Test	Estimated Duration (h)	Estimated Duration For a Short Test (h)
1	Capacity test	18	1.5
2	Impedance test	8	1
3	Low current test	42	4

Capacity measurements are the first stage of the test. They begin with a discharge to minimum cell voltage, followed by a four-hour rest. The initial rest ensures that the temperature in the climatic chamber corresponds to the set temperature. This is followed by a sequence of three complete CC-CV charge/CC discharge cycles. Before each charge, a short discharge is performed to restore the battery to its minimum voltage level. Next, charging is carried out between the cell's minimum and maximum voltage thresholds,

applying a constant current (DC) of 94 A (1 C). The maximum voltage is then maintained by reducing the current to 4.7 A (C/20). This constant voltage phase is commonly referred to by the acronym CV. Discharge takes place between the same voltage thresholds at a current of  $-94$  A ( $-1$  C). This is followed by maintenance of the minimum voltage until the current reaches  $-4.7$  A (C/20). This sequence is repeated three times. The first sequence is used as a preparation cycle to ensure that the cell temperature is close to that of the climatic chamber. This is useful when the cell has been used at a temperature other than the characterisation temperature. The following two cycles ensure measurement repeatability. The variation between measurements over these two cycles is less than 0.5%.

The second step in the complete characterisation test is an impedance measurement. Impedance is measured using a time-domain approach, with current pulses at different states of charge (10, 20, 30, 40, 50, 60, 70, 80 and 90%) and current regimes (0.3 C, 0.5 C, 0.8 C, 1 C and 1.3 C). Three types of current pulses are used. State-of-charge pulses last 6 min and are performed at a current of 94 A (1 C). They increase the state-of-charge by 10%. One-minute pulses are implemented in charge and discharge at a current of  $\pm 94$  A ( $\pm 1$  C). They are used to characterise the impedance and evaluate the influence of time variation  $\Delta t$ . Short pulses last 10 s and are performed at different current regimes: 0.3 C, 0.5 C, 0.8 C, 1 C and 1.3 C. They enable us to evaluate the influence of current on impedance. Each pulse is followed by a rest period five times longer than the pulse duration, e.g., 30 min rest after the 6 min pulses.

Step 3 is a pseudo-open circuit voltage measurement. This test begins at the end of charge and maintenance of the maximum voltage by reducing the current to 4.7 A (C/20). This charge brings the cell to a state of charge of 100%. This is followed by a 1 h 30 rest before a full discharge at a current of  $-4.7$  A (C/20). At the end of the discharge, a 30-min rest is performed. This is followed by a full charge at a current of 4.7 A (C/20). Finally, in step 4, cycles representative of automotive use and a mobile charging station are used.

The measurement conditions should be adapted to the battery and its intended use. For example, the voltage thresholds and current rates must be adapted to the battery technology being tested. The datasheet defines the safety limits for voltage, current and temperature [50]. Table 3 shows this information for the battery being tested. Obtaining this datasheet is therefore a prerequisite for carrying out this procedure. The load on the battery can also be adjusted according to the intended use in its second life. The performance of the battery must be measured in a way that is as close as possible to the conditions of use in the second-life application.

**Table 3.** Samsung SDI 94Ah main characteristics. Data from [51].

Characteristics	Values
Format	Prismatic
Rated capacity [Ah]	94
Positive electrode material	NMC111
Negative electrode material	Graphite
Rated voltage [V]	3.68
Maximal voltage [V]	4.15
Minimal voltage [V]	2.7
Specific energy [Wh/kg]	165
Size L × W × H [mm]	173 × 125 × 45
Weight [kg]	2.1

The test setup consisted of a Bitrode battery test system and a Vötsch VT 3050 climate chamber. To characterise the 12 cells at 25 °C, the authors measured the power consumption during the experiment. During the 11 days and 18 h of testing, the climate chamber consumed 141 kWh and the cycler 212 kWh, giving a total consumption of 353 kWh. In France, at the time of the experiment, this electrical consumption would have cost

approximately 24.7 kg CO<sub>2</sub> eq and EUR 95 [38]. In order to minimise the impact of this research, the data will be made open access. The authors hope that this data will benefit future research and allow a reduction in the number of experiments conducted.

The structure of this test could be adapted to reduce the test duration and its associated cost and impact. The capacity test could be reduced to a single cycle under nominal conditions. Impedance and low current tests could be measured only at nominal conditions and at 20 and 80% state of charge. This shorter test could reduce the energy consumed and the cost of the test by a factor 10. It would also be possible to make such measurements at the module level to avoid a time-consuming disassembly of the battery.

### 2.3. Capacity Measurements and Estimation of Energy

Capacity is the amount of charge a battery can store or deliver at a given current rate and temperature. In this article, capacity is measured in discharge at a current of 1 C during the constant current phase of the first step of the test shown in Figure 4. Data analysis was carried out using the open and free software DATTES 23.05 [52]. Figure 5 shows the capacities of the 12 cells in the second-life module considered. Measurements were made on each cell individually.

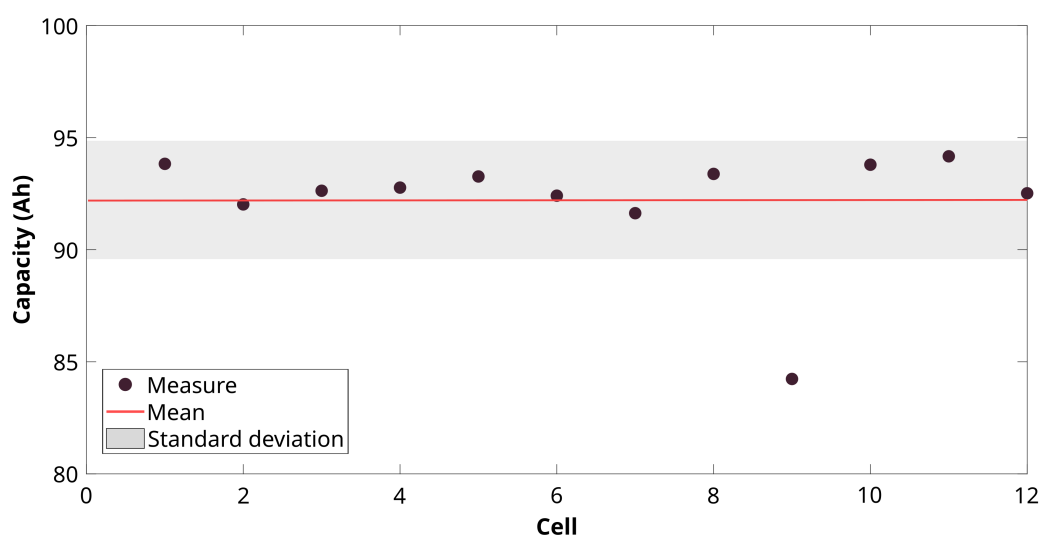
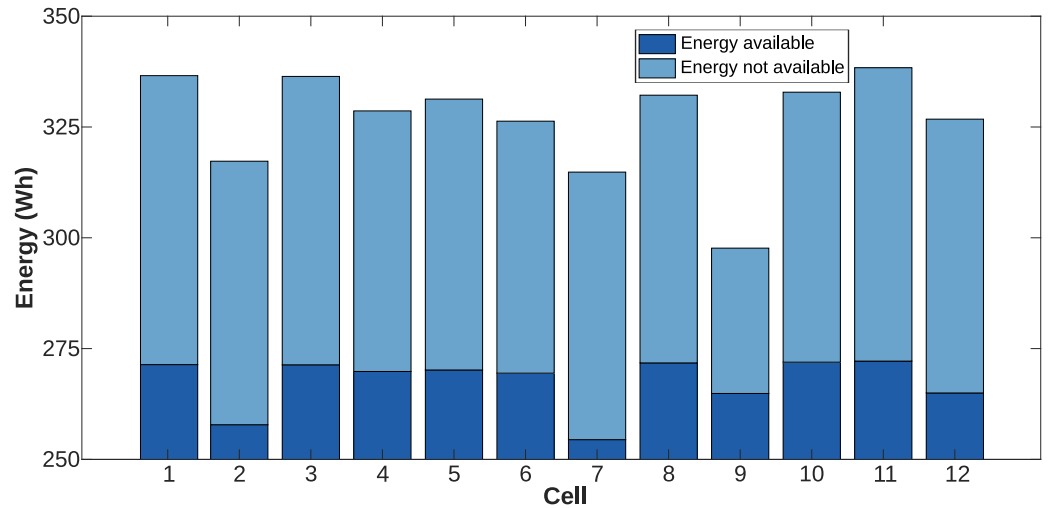


Figure 5. Capacity dispersion of cells in a second-life module.

The most degraded cell is significantly outperforming. As the module tested is a series assembly, its performance is limited by this degraded element.

The energy of a battery is a quantity that characterises the duration and intensity of the power it can deliver [53]. This quantity depends on the temperature and the current during the test and the degradation of the battery [54]. The measurement of the maximum available energy is necessary whatever the intended use. This value must be known in order to size the battery according to the requirements of the application. For mobile applications, the energy density of the battery must also be considered as the volume and mass available for the battery is generally limited. In this procedure, the energy available in each cell of the module is measured during step 1 of the characterisation test shown in Figure 4. The energy is calculated using Equation (A6) at a current rate and temperature representative of the intended use. In this study, a discharge current of 1 C (94 A) and a temperature of 25 °C were chosen, but these can be adapted in the case of an evaluation for a specific second-life application. Figure 6 shows the energy of the cells tested. The light blue area indicates a loss in energy due to differences in cell performance.

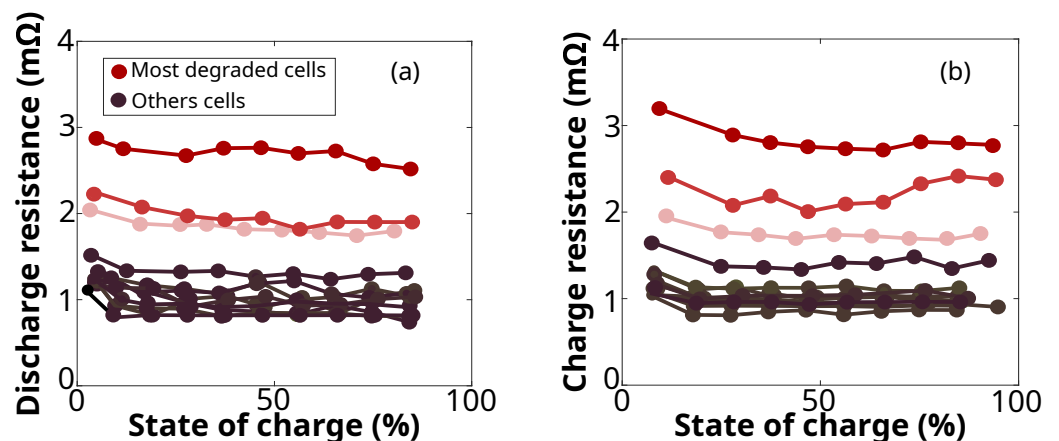


**Figure 6.** Energy of the tested cells; light blue area shows energy not available due to performance dispersion. Measurements were made at 25 °C and 1 C and the third measurement from step 1 is considered.

In an series assembly, the energy in blue light is not available because of the performance dispersion among cells. Reducing the current rate is one of the solutions to reduce the amount of this energy loss.

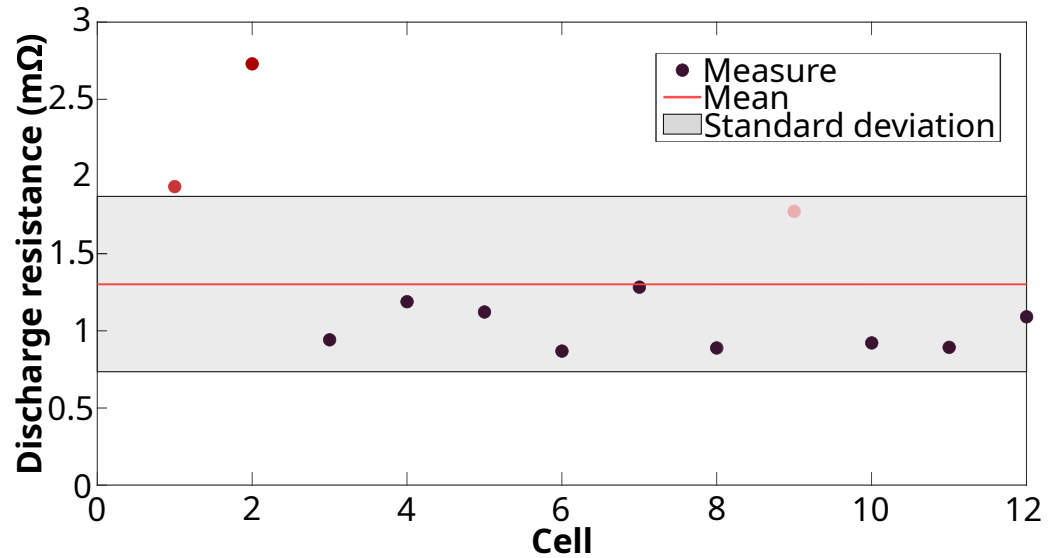
#### 2.4. Resistance and Power

The resistance and open circuit voltage are determined in steps 2 and 3, respectively, of the characterisation test shown in Figure 4. The resistance is measured at a temperature and using current pulses representative of mobile use. Current pulses of 10 s in duration measured at a current rate of 1 C (94 A) and a temperature of 25 °C were used. These conditions can be adapted as part of an evaluation for a specific second-life application. Figure 7 shows the results of the charge and discharge resistance measurements as a function of the state of charge on the elements making up this module.



**Figure 7.** Discharge resistance (a) and charge resistance (b) as a function of the state of charge for the various cells in the module.

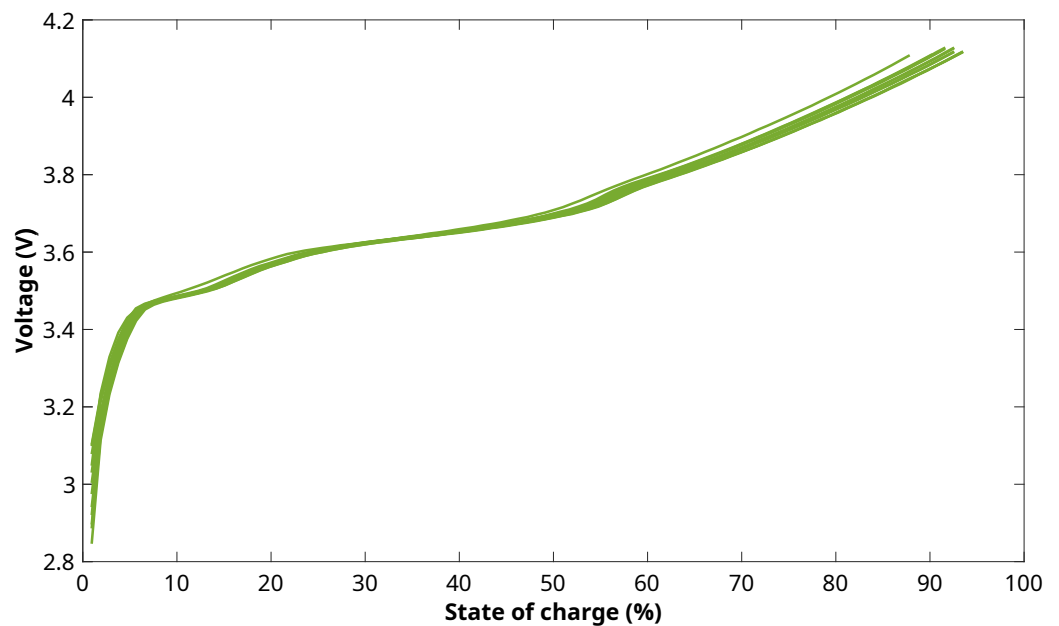
This figure shows that the majority of cells have a resistance on the order of 1 mΩ. Three cells have a higher resistance than the others; they are different from the outlier capacity cell. The most degraded cell has a resistance of around 3 mΩ. The discharge and charge measurements are consistent, since the most degraded cells are the same in charge and in discharge. Figure 8 shows the dispersion of discharge resistance measurements for the 12 cells in the module.



**Figure 8.** Resistance dispersion of cells in a second-life module. Resistance is measured in discharge with current pulses with a current rate of 1 C and at a state of charge of 50%.

This graph shows that three cells have above-average resistance. The most degraded cell has a resistance value of almost two standard deviations above the mean.

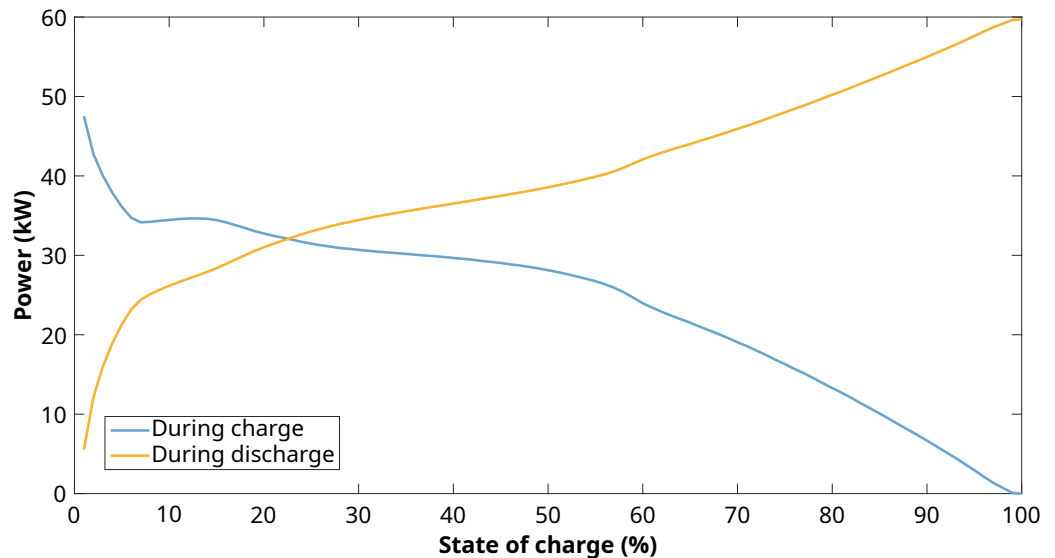
The power of a battery is a measure of the amount of energy it can supply or receive per unit of time. For any application, it is important to take power into account because it determines the speed of charging and discharging. Since the power of batteries decreases as they age, it is necessary to measure it to assess their suitability for a second life. The power that each cell can deliver is quantified according to the Equation (A3) for the discharge power [55]. To determine the power deliverable by a battery, its open circuit voltage must be known. The pseudo-open circuit voltage was measured at a current rate of C/20 and a temperature of 25 °C during the third stage of the characterisation test presented in Figure 4. Figure 9 shows the open circuit voltage as a function of the state of charge.



**Figure 9.** Open circuit voltage as a function of the state of charge of the individual cells in the module.

This figure shows that all cells behave very similarly. The variations in deliverable power can therefore be explained mainly by the dispersion of the resistances. Figure 10

shows the power that can be stored at charge and delivered at discharge by the module under test.



**Figure 10.** Power capability versus state of charge estimated for the different cells of the module.

This figure shows that deliverable power is particularly sensitive to state of charge. An accurate estimate of the state of charge is therefore necessary to determine the deliverable power at any given time. The deliverable power during charging is also lower than that during discharging for most of the state of charge range (between 20% and 100%). This result has been observed in several other works [56,57].

### 2.5. Efficiency and Energy Losses

Energy efficiency is a parameter whose quantification is essential in all applications, as energy losses must be kept under control. Knowing the efficiency of the battery and the factors that influence it can therefore help to optimise the sizing and use of this energy storage system. The efficiency of each cell in the module is measured in step 1 of the characterisation test shown in Figure 4. For this test, a current rate of 1 C (94 A) and a temperature of 25 °C have been chosen, but these can be adapted in the case of an evaluation for a specific second-life application. The use of constant current phases makes it possible to calculate the efficiency at a given current rate. However, this choice reduces the range of variation in the state of charge. Cell efficiency as a function of the state of charge is calculated using Equation (A4) [58]. The method used in this article was favoured because it allows for the calculation of the efficiency at a specific current rate, which is a necessity to construct a comparable measure. The authors would also like to highlight the fact that by calculating the mean of the efficiency over the state of charge, as presented in the article, an equivalent result to the more conventional method of calculating energy efficiency is obtained, which is based on a ratio between the discharged and charged energy. Figure 11 shows their evolution.

Efficiency develops in two phases. Over the range of state of charge from 0 to 20%, efficiency increases and then stabilises at a higher state of charge. The three cells with the highest resistances are clearly visible in this graph, as their efficiencies are severely degraded. The module efficiency is shown by a dashed line; it was calculated using Equation (A5) by dividing the sum of these cell voltages during discharge by the sum of the voltages during charge. This calculation is based on the constant current phase. Discharge ends when one of the cells reaches the minimum voltage threshold, while charging ends when one of the cell reaches the maximum voltage threshold. This graph shows that the range of states of charge accessible when operating at constant current is limited between a 20% and 85% state of charge due to the degraded cells. In order to minimise the effect of

these elements, current reduction and the use of balancing are two methods that can be implemented [59,60]. The module efficiency can also be used to estimate energy losses. The difference between the ideal efficiency at the start of the battery’s life and that at the time of the laboratory measurement is used to quantify losses in the form of heat from the module. The datasheet does not indicate the efficiency at the beginning of the battery’s life. Assuming an ideal efficiency of 97% for a new battery, the loss of efficiency over one cycle is 6% at a module level. For the module tested in this article, 216 Wh is lost. The cooling system must therefore be sized to dissipate this thermal energy.

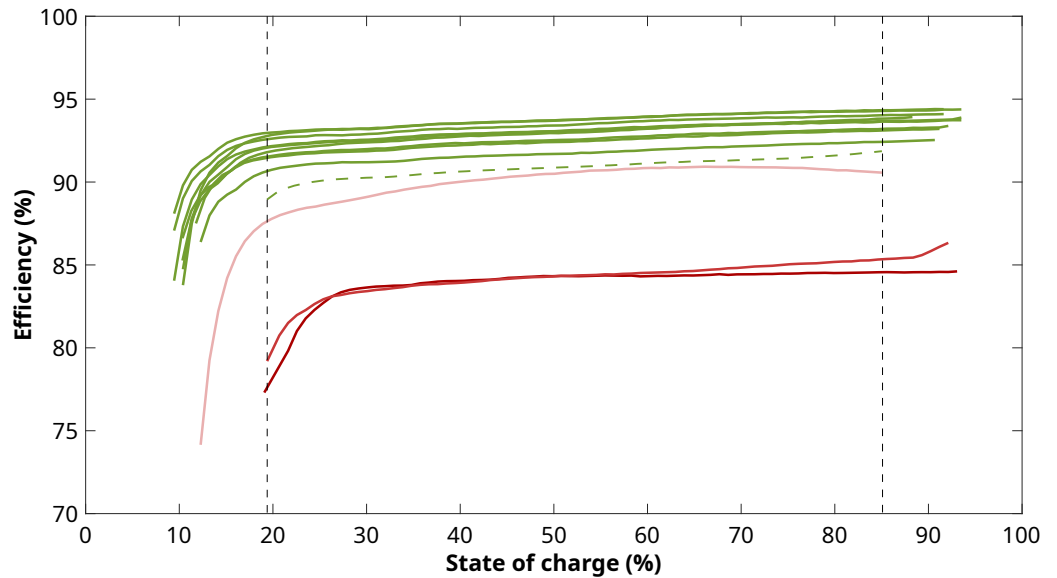


Figure 11. Cells efficiencies versus state of charge. Measurement is made at 25 °C and 1 C.

Figure 12 shows the spread of the average efficiency in the module. The average efficiency is calculated by averaging the efficiency over the swept state of charge range for each cell.

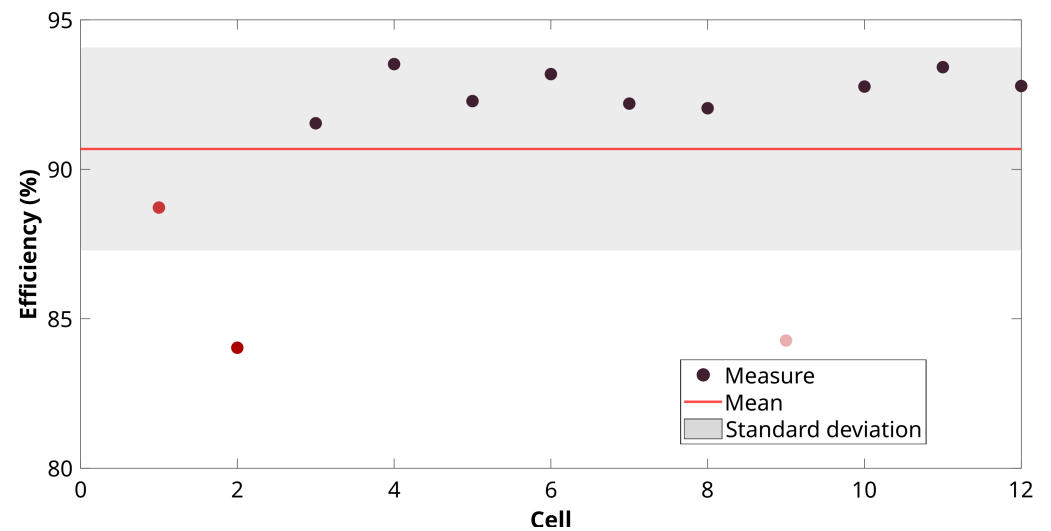


Figure 12. Mean efficiency dispersion of cells in a second-life module.

This figure shows that three cells have a below average efficiency. The low efficiency of cells 1, 2 and 9 can be partly explained by their high resistance.

European battery regulations also require the self-discharge rate to be estimated. For mobile use, self-discharge is not an essential characteristic as its effect is slow and limited to periods of less than a month. For the tested battery, the datasheet indicates that the self-discharge

rate at 25 °C will reach up to 3.3% loss of state of charge after 200 days of rest [51]. In addition, previous work has shown that when the battery is used in non-extreme conditions, the rate of self-discharge slows down as the battery degrades [58].

### 2.6. Performance Dispersion Inside the Module

Table 4 shows some statistical indicators of the performance distribution in the second-life battery module tested.

**Table 4.** Spread of performance measurements in a second-life battery module.

	Mean Value	Median Value	Standard Deviation	Worst Cell	Relative Dispersion
Q (Ah)	91.8	92.4	2.6	84.2	2.8
E (Wh)	267.5	269.9	5.9	254.4	2.2
R(t) (mΩ)	1.30	1.11	0.57	2.73	43.3
$\eta$ (%)	90.7	92.2	3.4	84.0	3.7

The performance dispersion is calculated from Equation (A1). For this module, the relative dispersion of capacity, energy and efficiency are, respectively, 2.8%, 2.2% and 3.7%. This level of dispersion corresponds to the order of magnitude of capacity measurements carried out in other studies involving batteries from electric vehicles [61–66]. These experimental results show that even four years after production, a battery can maintain excellent performance. At the beginning of their lives, the cells had a nominal discharge energy of 345 Wh when measured at 25 °C with a current rate of C/3 (31 A). After the first lifetime, the median energy available in the cells is 269.9 Wh. At the module level, the total energy available is 3.2 kWh, which represents a loss of 22% compared with the 4.1 kWh available in the new module. The relative dispersion of resistance is 43.3%. This level of dispersion is much higher than for capacity, energy and efficiency measurements. This trend is observed in several works on batteries from electric vehicles [61–63,65,67].

### 2.7. Filling the Battery Passport

European legislation requires that any battery produced from 2026 with a capacity greater than 2 kWh must be associated with its battery passport [35,68–70]. In order to support decisions on resale or reuse, the passports will contain information on battery composition, performance and remaining useful life [71]. This digital document will be useful for second-life service providers and recyclers to save money, time and reduce environmental impact by not having to test batteries to determine suitability for reuse [42,72]. Table 5 presents the information mentioned in the regulations. This information has been supplemented with elements considered useful to facilitate decision making on possible reuse.

This table has been filled in partly through a visual inspection of the module and some measurements on the module. The rest of the information was obtained from the manufacturer’s datasheet [51] or from the scientific literature of the battery in question. One of the advantages of reusing batteries several years after their introduction on the market is that it allows us to benefit from the scientific literature presenting experimental results on this battery technology. Publications describing electrochemical and ageing tests are particularly interesting for determining the chemical composition of the battery and estimating the number of cycles it is likely to be able to perform. Data shared under open licenses and processed with open software are also valuable as they enable us to produce more reproducible results and may help to limit the cost, impact and time spent on experimentation [42].

Table 5. Battery passport.

	Information	General Information	
		Value	Source
Annexe VI	Name and brand of battery	BMW i3 SAMSUNG 94 Ah	Section 2.1 Visual inspection
	Battery identification number	6127 762506706	Section 2.1 Visual inspection
	Batch or serial number	170410 00728	Section 2.1 Visual inspection
	Place of manufacture	Germany	Section 2.1 Visual inspection
	Date of manufacture	04/2017	Section 2.1 Visual inspection
	Weight	28 kg	Section 2.1 Visual inspection
	Rated capacity	94 Ah	[51]
	Chemistry	NMC111/C	[73]
	Hazardous substances present in the battery	Cobalt, Manganese, Nickel, Carbon, Polyvinylidene fluoride, Aluminium, Copper	[74]
	Usable extinguishing agent	Water	[75]
	Critical raw materials present in the battery	Lithium, Cobalt, Copper, Nickel, Manganese, Graphite	[74]
Other	Size	410 × 300 × 150 mm	Section 2.1 Visual inspection
	Volume	18.4 L	Section 2.1 Visual inspection
	Configuration	12s1p	Section 2.1 Visual inspection
	Temperature range	[−40; 60 °C]	[51]
	Voltage range	[32.4; 49.8 V]	[51]
	Rated voltage	44.2 V	[51]
	Date end of first life	07/2021	Seller
<b>Energy- and capacity-related information</b>			
Annexes IV and VII	Rated capacity	94 Ah	[51]
	Remaining capacity	91.8	Section 2.3 Capacity and energy
	Capacity lost	2.3%	Section 2.3 Capacity and energy
Other	Rated energy	4.1 kWh	[51]
	Remaining energy	3.6 kWh	Section 2.3 Capacity and energy
	Rated energy densities	146 Wh/kg; 222 Wh/L	[51]
	Measured energy densities	114 Wh/kg; 174 Wh/L	Section 2.3 Capacity and energy
	Energy/capacity of the worst cell	254.4 Wh/84.2 Ah	Section 2.3 Capacity and energy
	Dispersion of energy/capacity	2.2%/2.8%	Section 2.3 Capacity and energy
<b>Power-related information</b>			
Annexes IV and VII	Ohmic resistance (SoC 50%, 10 s, 1 C)	15.69 mΩ	Section 2.4 Resistance and power
	Rated power (SoC 50%, 10 s, 1 C)	42 kW	[51]
	Measured power output (SoC 50%, 10 s, 1 C)	38.6 kW	Section 2.4 Resistance and power
	Overall power loss	8%	Section 2.4 Resistance and power
	Charging power at SoC 80%	50.6 kW	Section 2.4 Resistance and power
	Discharging power at SoC 80%	12.7 kW	Section 2.4 Resistance and power
	Charging power at SoC 20%	31.5 kW	Section 2.4 Resistance and power
	Discharging power at SoC 20%	32.5 W	Section 2.4 Resistance and power
Other	Power/resistance of the worst cell	1488 W/2.7 mΩ	Section 2.4 Resistance and power
	Dispersion of rated power	24.4%	Section 2.4 Resistance and power
	Dispersion of rated resistance	43.3%	Section 2.4 Resistance and power
<b>Efficiency-related information</b>			
Annexes IV and VII	Round trip efficiency	90.7%	Section 2.5 Efficiency and energy losses
	Energy round trip fade	9%	Section 2.5 Efficiency and energy losses
	Cooling need	216 Wh	Section 2.5 Efficiency and energy losses
	Evolution of self-discharging rate	3.3%/200 days	[51]

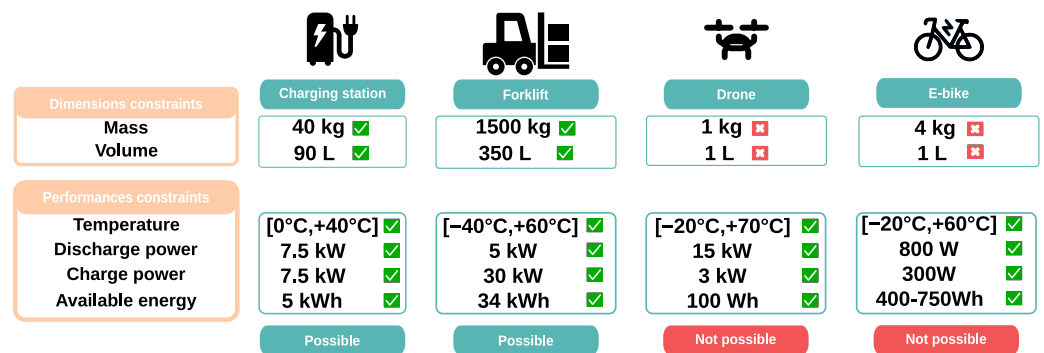
### 3. Suitability Assessment of the Battery for a Mobile Application

The purpose of this paragraph is to determine whether the battery under test can power different mobile applications. Mobile usages are defined as movable systems powered by batteries. Table 6 presents some examples of work on the use of second-life batteries in mobile applications.

**Table 6.** Examples of work on the use of second-life batteries in mobile applications.

Mobile Application	Reference
Boat	[76]
Electric golf cart and motorcycle	[77]
Heavy duty	[78]
Mobile charging station	[79]

Compared to stationary ones, a limited number of articles have presented performance requirements for mobile uses [48,80]. To fill this gap in the literature, the requirements for certain uses were estimated on the basis of usage profiles shared in the literature [81]. By comparing the battery passport with the requirements of each application, we can conclude whether the battery is eligible for a second life. Figure 13 shows the conclusions of this comparison.



**Figure 13.** Conclusions of the matching assessment between the battery passport and several mobile application needs. Data from [48,79–81].

This figure shows that the prismatic format of the SAMSUNG 94 Ah cell is incompatible with the needs of small applications. For applications such as drones or electric bicycles, cylindrical or pouch cells would be more suitable. The characteristics and performance of the BMW i3 battery make it suitable for reuse in a mobile charging station and in a forklift truck. To complete this result, two important pieces of information should be defined. First, a state of health should be defined based on the new application requirements. Secondly, the critical performance criteria should be identified to enable the definition of health indicators that could be used for rapid sorting of aged BMW i3 batteries.

When a battery is eligible for second-life use, it is necessary to monitor its performance in its new application. State of health is an indicator that can be used to characterise the battery’s ability to power a particular application in its current degraded state. In this work, a definition of this indicator adapted to a mobile charger is given by Equation (1).

$$SoH = \min(SoH_E, SoH_{P_{ch}}, SoH_{P_{dch}}, SoH_\eta) \tag{1}$$

with

- $SoH_E$  as the state of health for energy in %;
- $SoH_{P_{ch}}$  as the state of health for charge power in %;
- $SoH_{P_{dch}}$  as the state of health for discharge power in %;
- $SoH_\eta$  as the state of health for efficiency in %.

In this definition, the state of health for energy is defined according to Equation (2).

$$SoH_E = \frac{E(t) - E_{EoL}}{E_{BoL} - E_{EoL}} \times 100 \quad (2)$$

with

- $SoH_E$  as the state of health energy in %;
- $E(t)$  as the maximal energy available in the battery at instant  $t$  in watt-hours;
- $E_{EoL}$  as the end-of-life performance threshold related to the energy available in the battery in watt-hours;
- $E_{BoL}$  as the maximal energy available in the battery at the beginning of its life in watt-hours.

The state of health for charge power is defined according to Equation (3).

$$SoH_{Pch} = \frac{Pch(t) - Pch_{EoL}}{Pch_{BoL} - Pch_{EoL}} \times 100 \quad (3)$$

with

- $SoH_{Pch}$  as the state of health charge power criteria in %;
- $Pch(t)$  as the maximal charge power that the battery can receive at instant  $t$  in watts;
- $Pch_{EoL}$  as the end-of-life performance threshold related to the charge power the battery can receive in watts;
- $Pch_{BoL}$  as the maximal charge power that the battery can receive at the beginning of its life in watts.

The state of health for discharge power is defined according to Equation (4).

$$SoH_{Pdch} = \frac{Pdch(t) - Pdch_{EoL}}{Pdch_{BoL} - Pdch_{EoL}} \times 100 \quad (4)$$

with

- $SoH_{Pdch}$  as the state of health discharge power criteria in %;
- $Pdch(t)$  as the maximal discharge power that the battery can provide at instant  $t$  in watts;
- $Pdch_{EoL}$  as the end-of-life performance threshold related to the discharge power the battery can provide in watts;
- $Pdch_{BoL}$  as the maximal discharge power that the battery can provide at the beginning of its life in watts.

The state of health for efficiency is defined according to Equation (5).

$$SoH_\eta = \frac{\eta(t) - \eta_{EoL}}{\eta_{BoL} - \eta_{EoL}} \times 100 \quad (5)$$

with

- $SoH_\eta$  as the state of health efficiency in %;
- $\eta(t)$  as the mean efficiency of the battery at instant  $t$  in %;
- $\eta_{EoL}$  as the end-of-life performance threshold related to mean efficiency of the battery in %;
- $\eta_{BoL}$  as the mean efficiency of the battery at the beginning of its life in %.

In these definitions, the various end-of-life thresholds must be adapted to the potential use [82]. For a mobile charging station, these thresholds are determined on the basis of average daily journeys and the energy consumption of electric vehicles.

Based on simulation work, Tepe et al. have shown that an electric vehicle consumes between 0.18 and 0.3 kilowatt-hours per kilometre [37]. This consumption varies significantly according to vehicle size, since a vehicle with a 79.5 kWh battery consumes on average 20% more than a vehicle with a 45 kWh battery. To define the charger's end-of-life threshold, a

consumption of 0.18 kWh/km is considered in this work. This value corresponds to the consumption of a vehicle with a smaller battery. The distance covered daily by a vehicle is used to determine the minimum energy required from a mobile charging station. In France, 80% of daily car journeys are less than 55 km [83]. In a study analysing a database of 19,000 daily journeys, Plotz et al. showed that a distance of 55 km exceeds the median daily distance in countries such as Sweden, Germany and the USA [84]. Based on these figures, the notion of end-of-life energy is defined as when the charger can no longer supply the energy required for a vehicle with a consumption of 0.18 kWh/km to travel 55 km. The minimum energy to be stored therefore corresponds to 10 kWh for a mobile charging station made of four modules, i.e., 2.5 kWh per module.

The notion of end of life for charging and discharging power is defined as when the mobile charger cannot receive or supply a power of 7.4 kW, which corresponds to the standard vehicle charging power. Each of the four modules of the mobile charging station must therefore be able to receive or supply 1.85 kW.

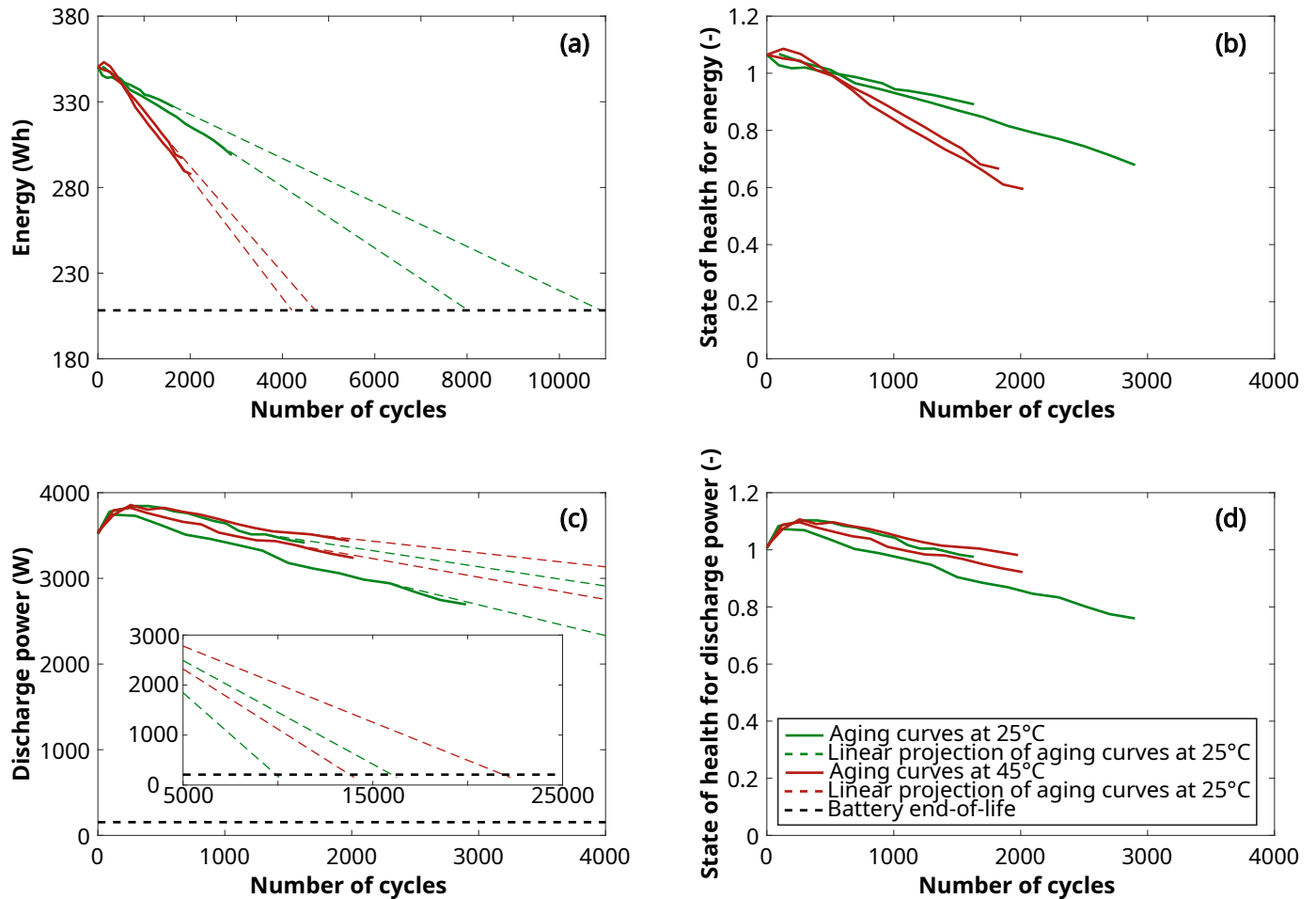
Finally, the notion of end of life in terms of energy efficiency is defined as when the average efficiency is less than 50%, based on an assumption. A different threshold could be chosen, taking into account economic and environmental criteria appropriate to the proposed use. These figures lead to the end-of-life performances presented in Table 7.

**Table 7.** Data used to calculate a module's state of health.

	Energy	Discharge Power	Charge Power	Efficiency
Beginning of life	4.1 kWh	42 kW	42 kW	97%
Measure	3.6 kWh	38.6 kW	28.1 kW	91%
End of life	2.5 kWh	1.85 kW	1.85 kW	50%
State of health	44%	91%	65%	87%

In this table, the data at the beginning of the module's life are based on strong assumptions. The energy at the beginning of a module's life is calculated by multiplying the nominal energy of a cell by the number of cells in a module. This assumes a perfectly homogeneous battery. Discharge power is calculated on the same assumption by multiplying the nominal power of a cell by the number of cells in a module. The datasheet does not provide any measurements of the charging power. The value for the discharging power is therefore adopted. Finally, the datasheet does not indicate any efficiency measurement either. An ideal efficiency of 97% is therefore assumed. Based on these assumptions, the battery's state of health is limited by the available energy. The minimal value is 44% for the state-of-health energy. It is important to note that based on this definition of the state of health, the end of life is reached at zero. This result also suggests that capacity is the measurement that should be used to define the health indicators used for the fast sorting of end-of-automotive-life batteries.

European battery regulations also call for an estimate of the number of cycles before the battery's end of life in its new application. This estimate can hardly be generic, since the load on the battery depends greatly on its use. For this work, the results shown in the datasheet are exploited. Data are collected using the software Webplotdigitizer. Estimating the remaining useful life involves determining the number of cycles that can be performed before reaching one of the end-of-life thresholds. In the datasheet, efficiency and charge power measurements over ageing are not shared. The remaining useful life is then only defined based on the energy and discharge power. Two ageing campaigns were conducted by the manufacturer. Degradations in the capacity and discharge resistance were measured during a cycling campaign at 25 °C and 45 °C [51]. Cycles were defined with a current rate of C/2 during charging and 1 C during discharging at 25 °C, while charge and discharge were performed at 1 C at 45 °C. Cycles were full voltage windows, which is known to be an ageing stress factor for lithium-ion batteries [85]. Two cells were tested in each experimental condition. Figure 14 shows the evolution of available energy and state of health for energy as a function of the number of cycles at 25 °C and 45 °C for the two cells tested by the manufacturer.



**Figure 14.** Energy (a), state of health for energy (b), discharge power (c) and state of health for discharge power and (d) evolution curves as a function of the number of cycles at the cell level and for temperatures of 25 °C (green lines) and 45 °C (red lines). End-of-life thresholds are shown as black dotted lines. Data were collected from a datasheet using the software Webplotdigitizer.

Figure 14a,b show the evolution of energy and state of health for energy as a function of the number of cycles at the cell level. A linear extrapolation of the curves is used to predict the remaining useful life. This extrapolation is used to obtain a first estimation of the number of cycles that could be reached during a second life. Using linear extrapolation is only a reasonable method for the first approach; this method was favoured as the ageing behaviour of second-life batteries is not yet well understood and modeled. Linear extrapolation is a reasonable assumption considering the already published results regarding second-life battery ageing [86–88]. Estimation could be later improved by using experimental data to create second-life battery ageing models. As expected, cells aged at 45 °C show faster degradation. This figure also shows the effect of cell-to-cell variations on lifetime, as two fresh cells aged under the same conditions can have significantly different lifespans. In a system, the first cell to reach end of life will end the life of the whole system. For discharge power, Figure 14c,d show that a cell aged at 25 °C has a significantly shorter life. The influence of temperature on the discharge power is unclear as the other cell aged at 25 °C and 45 °C performed comparably. Further experiments would be required to investigate the influence of temperature on power fade. Cell degradation in this accelerated ageing campaign helps to estimate the remaining lifetime. Estimations are presented in Table 8.

**Table 8.** Lifetimes in number of cycles for the tested cells.

	Energy 25 °C/45 °C	Power 25 °C/45 °C
Cell 1	8026/4710	10,062/14,010
Cell 2	10,901/4205	16,268/22,235

Lifetimes are given in numbers of cycles. The results at 25 °C are significantly better, as for the best-performing cell, the end of life should be reached after 8026 cycles, compared to 4710 cycles at 45 °C. Assuming two full voltage window cycles are made per day, this would lead to a minimal lifetime of 6.5 years at 45 °C and 11 years at 25 °C. It is important to point out that these results probably underestimate the actual battery life, given that extrapolation was based on accelerated ageing curves. A better estimation of the lifespan could also be given by using cycles representative of real usage. These results show the impact of dispersion on battery life. The most degraded cells significantly reduce the assembly life. This study also tends to confirm the fact that energy fade is a more limiting factor than power fade [89,90]. This work also suggests that the selection of batteries eligible for repurposing can consequently be based mainly on capacity health indicators. This supports a commonly proposed hypothesis [87,91–93].

#### 4. Conclusions and Outlook

This article has presented a procedure for evaluating the performance of a battery, filling a battery passport and determining its suitability for being repurposed in a mobile application. Assessing the possibility of reusing batteries in non-stationary uses has been highlighted as a key enabler for the growth of more circular practices in the battery field.

The experimental study evaluated the performance of a second-life battery. The capacity, resistance and efficiency of 12 cells were measured. The proposed experimental framework can be used as a reference test to evaluate a battery's suitability for a second life. The proposed framework is compliant with the 2023 Battery Regulation of the European Union, which is the only existing regulation to date describing the data requirements for second-life batteries. To the best of the authors' knowledge, this experimental work contributes to the existing literature on second-life batteries as it is the first to provide such a complete framework.

Based on the experimental results, the energy, power and efficiency of a second-life battery module were calculated. These performances were compared to the performance requirements of several mobile applications, and the suitability of second-life batteries for reuse was assessed. In terms of battery performance, the battery was tested four years after its production and after experiencing a first life in a vehicle. The experimental results show that it can still perform well. To the best of the authors' knowledge, this article is also one of the first to experimentally evaluate the suitability of a second-life battery for mobile second-life applications.

Finally, a definition of the health state based on application needs is provided. This can be used to track a battery's performance and suitability for second-life applications. Mobile charging stations and forklift trucks were shown to be suitable applications for the reuse of high-capacity prismatic cells. This SoH definition was also used to estimate the remaining useful life. This estimate showed that second-life batteries could be used for several thousands of cycles in a mobile application, resulting in an 11-year life extension at 25 °C. It also suggested that energy fade is the most limiting performance factor for lifetime, and that cell-to-cell variation should be considered as it may limit battery life.

This study has several limitations that can be the subject of further research efforts. Firstly, the described procedure should be tested on different battery technologies at the module and pack levels. The influence of cell-to-cell variations on the performance of a second-life battery is known to be important [94]. Evaluating this impact may be the subject of future articles. Lifetime predictions were made using linear extrapolation of the energy and power fade. Future work could improve the prediction by using an extrapolation based on the result of experimental ageing models. The thermal and safety characteristics

of the battery have been poorly considered in this article and there is limited research on these topics for second-life batteries to date. Fast characterisation techniques may also be considered to fill in the battery passport information in a reduced time.

The authors also invite researchers to address these research gaps as it may contribute to the development of reuse and circularity in the battery field.

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## Appendix A. Equations

### Appendix A.1. Performance Dispersion

$$k = \frac{\sigma}{\mu} \times 100 \quad (\text{A1})$$

with

- $k$  as the relative dispersion of performance in %;
- $\sigma_c$  as the standard deviation between performance measurements;
- $\mu_c$  as the average of performance measurements.

### Appendix A.2. Charge Power Capability

$$P_{ch}(SoC) = \frac{V_{max} - V_{oc}(SoC)}{R_{ch}(SoC)} \times V_{max} \quad (\text{A2})$$

with

- $P_{ch}(SoC)$  as the charge power capability in watts;
- $V_{oc}(SoC)$  as the battery open circuit voltage in volts;
- $V_{max}$  as the battery maximal voltage in volts;
- $R_{ch}(SoC)$  as the charge resistance of the battery in ohm.

### Appendix A.3. Discharge Power Capability

$$P_{dch}(SoC) = \frac{V_{oc}(SoC) - V_{min}}{R_{dch}(SoC)} \times V_{min} \quad (\text{A3})$$

with

- $P_{dch}(SoC)$  as the discharge power capability in watts;
- $V_{oc}(SoC)$  as the battery open circuit voltage in volts;
- $V_{min}$  as the battery minimal voltage in volts;
- $R_{dch}(SoC)$  as the discharge resistance of the battery in ohm.

#### Appendix A.4. Efficiency

$$\eta(\text{SoC}) = \frac{U_{dch}(\text{SoC})}{U_{ch}(\text{SoC})} \times 100 \quad (\text{A4})$$

with

- $\eta(\text{SoC})$  as the energy efficiency of a cell as a function of the state of charge in %;
- $U_{dch}(\text{SoC})$  as the cell voltage during discharge in volts;
- $U_{ch}(\text{SoC})$  as the cell voltage during charging in volts.

#### Appendix A.5. Module Efficiency

$$\eta_{module} = \frac{\sum_1^n U_{dch,celli}}{\sum_1^n U_{ch,celli}} \times 100 \quad (\text{A5})$$

with

- $\eta_{module}$  as the module efficiency in %;
- $\sum_1^n U_{dch,celli}$  as the sum of all cells' voltages during discharge in volts;
- $\sum_1^n U_{ch,celli}$  as the sum of all cells voltages during charge in volts.

#### Appendix A.6. Energy

$$E = \int_{t_{ini}}^{t_{fin}} U(t) \times I(t) dt \quad (\text{A6})$$

with

- $E(t)$  as the energy available in the cell in watt-hours;
- $t_{ini}$  as the time at start of discharge in hours;
- $t_{fin}$  as the time at end of discharge in hours;
- $U(t)$  as the voltage measured in volts;
- $I(t)$  as the current measured in amperes.

## Appendix B. Most Sold Electric Vehicles Worldwide Annually between 2012 and 2022

**Table A1.** Most sold electric vehicles worldwide annually since 2012. All information is for reference only. The actual specs are subject to change anytime. Empty cells indicate unknown data. The information was collected from the manufacturers' websites. Sales figures are from [95].

Year	OEM	Model	Pack Energy (kWh)	Module Energy (kWh)	Cell Energy (Wh)	Max AC Power (kW)	Max DC Power (kW)	Chemistry	Cell Format	Vehicles Sold (in Thousands)
2022	Tesla	Model Y	57	15	566	11	170	LFP	Prismatic	771
	Tesla	Model 3	51.9	12.9	17	11	170	NCA	Cylindrical	476
	Wuling	HongGuang Mini EV	9.3		424	1.6	-	LFP	Prismatic	424
	BYD	Song	59.1		271	6.6	50	LFP	Prismatic	410
	BYD	Qin	53.1		646	6.6	50	LFP	Prismatic	205
2021	Tesla	Model 3	51.9	12.9	17	11	170	NCA	Cylindrical	500
	Wuling	HongGuang Mini EV	9.3		424	1.6	-	LFP	Prismatic	424
	Tesla	Model Y	57	15	566	11	170	LFP	Prismatic	411
	VW	ID.4	52	5.8	271	7.2	110	NMC	Cylindrical	411
	BYD	Qin	53.1		646	6.6	50	LFP	Prismatic	65.1
2020	Tesla	Model 3	51.9	12.9	17.4	11	250	NCA	Cylindrical	365.2
	Wuling	HongGuang Mini EV	9.3		424	1.6	-	LFP	Prismatic	119.2
	Renault	ZOE	52	4.3	270.8	22	50	NMC	Pouch	100.4
	Tesla	Model Y	74.5	18.6	16.9	11	120	NCA	Cylindrical	79.7
	Hyundai	Kona	64	12.8	218	7.2	77	NMC	Pouch	65.1
2019	Tesla	Model 3	51.9	12.9	17.4	11	250	NCA	Cylindrical	300.1
	BAIC	EU-Series EB	54		7	7	60	NMC	Prismatic	111.0
	Nissan	Leaf	40	1.7	208	6.6	100	NMC	Pouch	69.9
	SAIC-GM	Baojun E100/E200 EV	24		2	2	-	LFP	Prismatic	60.1
	BYD	e5 450 EV S	60.5	4.6	360	7	60	LFP	Prismatic	58.0
2018	Tesla	Model 3	51.9	12.9	17.4	11	250	NCA	Cylindrical	145.9
	BAIC	EC180	20.3		7	7	-	LFP	Prismatic	90.6
	Nissan	Leaf	40	1.7	208	6.6	100	NMC	Pouch	87.1
	JAC	iEV	23		6	6	-	LFP	Cylindrical	55.6
	Tesla	Model S	74	4.6	10.4	11	200	NCA	Cylindrical	50.0
2017	BAIC	EC180	20.3		7	7	-	LFP	Prismatic	78.1
	Tesla	Model S	74	4.6	10.4	11	200	NCA	Cylindrical	54.7
	Toyota	Prius PHEV	4.4	4.4	79	2.3	-	Ni-MH	Prismatic	50.8
	Nissan	Leaf	40	1.7	208	7	50	NMC	Pouch	47.2
	Tesla	Model X	80.5	5	11.3	16.5	150	NCA	Cylindrical	46.5

Table A1. Cont.

Year	OEM	Model	Pack Energy (kWh)	Module Energy (kWh)	Cell Energy (Wh)	Max AC Power (kW)	Max DC Power (kW)	Chemistry	Cell Format	Vehicles Sold (in Thousands)
2016	Tesla	Model S	74	4.6	10.4	11	200	NCA	Cylindrical	50.9
	Nissan	Leaf	30	0.5	125	7	50	LMO-LNO	Pouch	43.5
	BYD	Tang PHEV	18.5		86		-	LFP	Prismatic	31.4
	Chevrolet	Volt	16	1.8	55	3.7	-	NMC-LMO	Pouch	28.3
	Mitsubishi	Outlander PHEV	12	2.4	150	3.7	-	NMC	Prismatic	27.8
2015	Tesla	Model S	74	4.6	10.4	11	200	NCA	Cylindrical	50.4
	Nissan	Leaf	30	0.5	125	7	50	LMO-LNO	Pouch	43.9
	Mitsubishi	Outlander PHEV	12	2.4	150	3.7	-	NMC	Prismatic	43.3
	BYD	Qin	13		1.3	7	-	LFP	Prismatic	31.9
	BMW	I3	21.6	2.7	225	3.7	50	NMC	Prismatic	24.1
2014	Nissan	Leaf	24.4	0.5	125	7	50	LMO-LNO	Pouch	60.6
	Mitsubishi	Outlander PHEV	12	2.4	150	3.7	-	NMC	Prismatic	31.2
	Tesla	Model S	74	4.6	10.4	11	200	NCA	Cylindrical	30.4
	Chevrolet	Volt	16	1.8	55	3.7	-	NMC-LMO	Pouch	20.0
	Toyota	Prius PHEV	4.4	4.4	79	2.3	-	Ni-MH	Prismatic	19.2
2013	Nissan	Leaf	24.4	0.5	125	7	50	LMO-LNO	Pouch	47.8
	Chevrolet	Volt	16	1.8	55	3.7	-	NMC-LMO	Pouch	28.2
	Toyota	Prius PHEV	4.4	4.4	79	2.3	-	Ni-MH	Prismatic	23.1
	Tesla	Model S	74	4.6	10.4	11	200	NCA	Cylindrical	22.2
	Mitsubishi	Outlander PHEV	12	2.4	150	3.7	-	NMC	Prismatic	18.4
2012	Chevrolet	Volt	16	1.8	55	3.7	-	NMC-LMO	Pouch	29.6
	Toyota	Prius PHEV	4.4	4.4	79	2.3	-	Ni-MH	Prismatic	27.1
	Nissan	Leaf	24.4	0.5	125	7	50	LMO-LNO	Pouch	26.9
	Renault	Twizy	7		125	3.7	-	LMO-NMC	Pouch	9.0
	Mitsubishi	I-Miev	16	1.6	182	3.7	50	NMC	Prismatic	7.9

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