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## **Hydrologic similarity: dimensionless runoff indices across scales in a semi-arid catchment**

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1 **Abstract**

2 In this study, an assessment of similarity relationships in runoff measurements at different  
3 spatial scales was carried in a typical Sahelian landscape, under semi-arid climate in northern  
4 Burkina Faso (west African Sahel). The scales of observations considered are the plot scale (1  
5 m<sup>2</sup>, 50 m<sup>2</sup>, 150 m<sup>2</sup>) and the sub-catchment scale (6.1 ha, 33.8 ha), under various soil surface  
6 conditions and slopes. These scales were monitored during six years (2010 to 2015) under  
7 natural rainfall. Based on monitoring data, a runoff potential index  $I_1$  and an effective runoff  
8 index  $I_2$  were developed, encapsulating the observation scale physical characteristics into  
9 dimensionless forms, hence reducing their sensitivity to the scale effects. These indices  
10 helped in assessing hydrological similarity across measurement scales. Results showed that  
11 runoff decreased with the increase of the observation scale size. Besides, dimensionless  
12 indices vary following a logarithmic decay relationship with the scale size ( $R^2 > 0.98$ ). Such  
13 results highlight the non-linear nature of runoff processes and also promotes similarity  
14 analysis as a means to model hydrological processes using soil surface and landscape  
15 descriptors.

16 **Keywords:** Dimensional analysis; Hydrologic similarity; Runoff; Scale effect; Scaling law.

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## 17 **1. Introduction**

18 The hydrologic similarity concept relates to the similarity in how catchments or surface units  
19 respond to rainfall. As a basis for catchment classification, this concept is helpful in  
20 transferring and generalizing knowledge in hydrology, but also in assessing the potential  
21 impacts of environmental change (Sawicz et al., 2011). Yet, hydrologists do not agree upon a  
22 consensus on catchment classification systems: in essence, the challenge lies in setting a  
23 classification framework integrating the spatial and temporal variability of hydrodynamic  
24 conditions which explicitly defines a catchment response, while accounting for uncertainty  
25 (Wagener et al., 2007).

26 A wide range of previous studies helped in gaining foundational insights at how hydrological  
27 processes are generated (Sivapalan and Kalma, 1995; Mayor et al., 2011; Mounirou et al.,  
28 2012; Mayerhofer et al., 2017). These studies contributed to a better characterization of runoff  
29 at the local scale. In most cases, the plots were installed on homogeneous units (in terms of  
30 soil surface conditions) in order to assess the typical runoff response of such soil surface  
31 conditions. Further research efforts built upon this knowledge and addressed the effect of  
32 scale on runoff. The dominant and consensual result often reported is that runoff decreases as  
33 the observation scale (or contributing area) increases (Kirkby et al., 2002; Gomi et al., 2008).  
34 Several root causes have been identified to support this observation. On agricultural areas, the  
35 scale effect on runoff has been related to a re-infiltration process (occurring at the  
36 downstream of the flow path), fostered by the spatial variation in soil permeability, during  
37 short duration and low-intensity rainfall events (Corradini et al., 1998; Jetten et al., 1999;  
38 Cerdan et al., 2004). Some studies also showed that the scale effect was mainly attributable to  
39 the rainfall intensity pattern (during an event), whereas the length and inclination of the soil  
40 surface slope amplify its effect (Stomph et al., 2002; Van de Giesen et al., 2005).

41 In arid and semi-arid areas, it was reported that the rainfall intensity and duration are the  
42 major factors explaining the scale effect (Reaney et al., 2007; Van de Giesen et al., 2011;  
43 Mohamadi and Kavian, 2015). However, in these environments, a significant link was  
44 identified between the runoff and the preponding rainfall (that is the minimal amount of  
45 rainfall depth after which the runoff process is triggered), hence contributing to the scale  
46 effect (Cammeraat, 2002, 2004; Boix-Fayos et al., 2007; Antoine et al., 2011; Cantón et al.,  
47 2011; Mayor et al., 2011; Miyata et al., 2019). In the recent years, the scale problem has been

48 the subject of much research, often prompted by the need to explain hydrologic behaviour at  
49 the catchment scale and therefore formulate answers to key challenges arising in water  
50 resource management. At the catchment level, the scale effect is mostly due to the emergence  
51 of specific elements such as ponds and infiltration wells, which are not perceptible at the plot  
52 scale because of the relative homogeneity at smaller scales (Lesschen et al., 2009; Mayor et  
53 al., 2011; Yonaba et al., 2021; Gbohoui et al., 2021). Another reported cause of the scale  
54 effect on runoff lies in the inherent non-linearity nature of the runoff process as it stems from  
55 complex relationships and transformations interacting altogether in the hydrological cycle  
56 (Sivapalan et al., 2002; Puech et al., 2003; Cerdan et al., 2004; Cantón et al., 2011). Overall, it  
57 appears that even though several identified causes can affect runoff, some factors are  
58 emergent given a specific scale but become overshadowed by others as the scale changes.

59 Thanks to the large collection of studies carried at the plot scale to understand and assess  
60 runoff mechanisms on different types of soil surface conditions and under various rainfall  
61 patterns, the dominant factors governing surface runoff processes have been well  
62 documented. However, the use of plots highlights the problem of representativeness as the  
63 investigated surface is limited. Moreover, the location of the plot is likely to influence the  
64 observations (Cammeraat, 2004; Mathys et al., 2005). It is therefore critical to assess the  
65 extent to which runoff observations across scales can be effectively linked together. An  
66 effective approach to this problem is the use of similarity parameters. This study aims to  
67 determine whether the mechanisms of surface runoff generation at different scales obey the  
68 same dimensionless relationships through the use of dimensionless variables. Such  
69 dimensionless numbers would then provide a basis to compare the respective contribution of  
70 different factors of runoff production across different spatial scales. Dimensional analysis  
71 helps define similarity relationships between different scales. It consists in reducing the  
72 number of dimensional variables describing a system to a smaller subset of dimensionless  
73 quantities, hence summarizes information from a given scale in the form of dimensionless  
74 numbers, related by a logical or an empirical relationship (Tillotson and Nielsen, 1984;  
75 Wagener et al., 2007; Peters-Lidard et al., 2017). Our focus on *scaling* and *similarity* directs  
76 attention to a challenging problem, yet unresolved, in the hydrologic sciences (Blöschl et al.,  
77 2019). We define *scale* as a “*characteristic length (or time) of process, observation, model*”  
78 whereas *scaling* is termed as the “*transfer of information across scales*”. Also, we consider  
79 *similarity* to be present when the characteristics of a system can relate to those of another  
80 system through a scale factor (Peters-Lidard et al., 2017). Dimensional analysis offers an

81 interesting framework to shed some light in studying how runoff scales in space, as it offers to  
82 possibility to encapsulate and account for multiple characteristics of the observation scale  
83 (size, slope inclination, surface roughness, infiltration capacity, soil moisture) and as well as  
84 those of the rainfall (intensity, amount). Yet, to date, only a few developments and  
85 applications of this approach have been investigated in hydrology. Sivapalan et al. (1987),  
86 among the first, used similarity analysis to characterise surface runoff processes. Julien and  
87 Moglen (1990) analysed runoff through a dimensionless index based on the relationship  
88 between the rainfall duration and the equilibrium time. Likewise, Larsen et al. (1994)  
89 explained the variability of the runoff coefficient through a dimensionless index based on the  
90 rainfall intensity and the soil characteristics. Yet, further investigations are needed to expand  
91 the actual knowledge and possibly, to account for more factors affecting runoff generation.

92 The catchment of Tougou (37 km<sup>2</sup>), located in the Sahelian zone of Burkina Faso, in the West  
93 African Sahel, was chosen for this research. As a physical unit, the catchment of Tougou has  
94 been a field support site for a large number of studies targeting Sahelian landscapes and semi-  
95 arid climate and for more than 5 decades. The soil surface conditions found in the catchment  
96 landscape were found to be representative of the Sahelian strip, hence suitable to provide  
97 interesting insights regarding the runoff generation processes. Moreover, previous research  
98 work showed that surface runoff generation mechanisms in Tougou catchment exhibit similar  
99 characteristics as those observed in typical Sahelian hydrosystems (Albergel, 1987),  
100 especially regarding the dependence on soil surface conditions (Karambiri et al., 2003;  
101 Mounirou et al., 2012; Zouré et al., 2019; Mounirou et al., 2020; Yonaba et al., 2021). The  
102 objectives of this study are: (i) to analyse the hydrologic similarity of runoff in a catchment  
103 under a semiarid climate at different small spatial scales, ranging from the plot scale (1 m<sup>2</sup>) to  
104 sub-catchment scale (tens of hectares); (ii) to develop analytical relationships between  
105 dimensionless variables defining the hydrological functioning across different scales of  
106 observations.

## 107 **2. Material and methods**

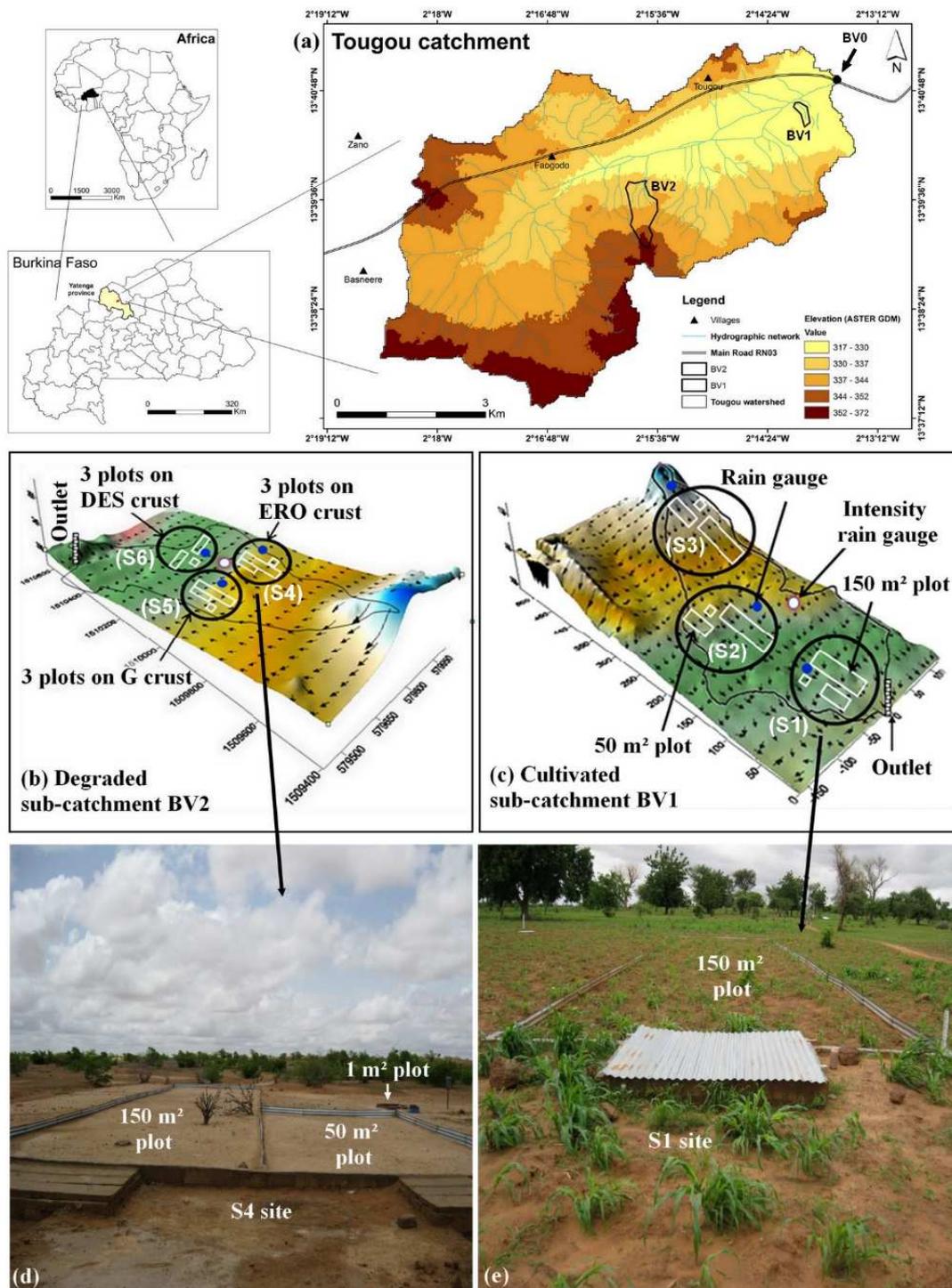
### 108 **2.1. Study area**

109 The catchment of Tougou (37 km<sup>2</sup>) is located in the northern part of Burkina Faso, in the  
110 West African Sahel (**Fig. 1a**). The catchment is located within the Northern region of the  
111 country, more precisely in the Yatenga province. Its outlet is located at 13° 40' 56" N and 2°  
112 13' 39" E geographical coordinates. The landscape features two dominants units of land use,  
113 which are cultivated soils estimated at 65% of the catchment area and degraded and

114 uncultivated soils covering 35% of the catchment area (Yonaba et al., 2021). Vegetation on  
115 the catchment is sparse and mostly made of savannah shrubs. According to the national soil  
116 survey database (IGB, 2002), three types of soil can be found within the area: (i) slightly  
117 evolved soils (covering 25% of the catchment), developing a sandy or sandy-gravel texture at  
118 the surface; (ii) mineral soils (covering 35% of the catchment) which tend to physical  
119 degradation, called ‘*zipelle*’ by the local populations (Sawadogo et al., 2008); (iii)  
120 hydromorphic soils (covering 40% of the catchment) located in alluvial terraces and are  
121 mostly clayey, often highly silted (IGB, 2002).

122 The climate is characterized by a unimodal rainfall regime with a rainy season from June to  
123 October and a dry season from November to May. The rainfall in the Tougou catchment, as in  
124 the Sahelian region, is produced by the so-called “*Mesoscale Convective systems*” (MCSs),  
125 which are of large spatial extension and propagates from East to West. In the region, MCSs  
126 produce 80% of the annual rainfall, whereas the remaining 20% result from more localized  
127 storm systems (Mathon et al., 2002). The annual rainfall varies between 400 and 750 mm,  
128 with an annual average of 650 mm, whereas annual evapotranspiration is 2090 mm on  
129 average (Zouré et al., 2019).

130 As in most Sahelian landscapes, runoff processes are Hortonian due to the development of  
131 crusts at the soil surface, sealing the soil surface, limiting infiltration and favouring runoff  
132 (Casenave and Valentin, 1992). Also, rainfall intensities in the context are high, as their  
133 values range from 130 to 180 mm/h in 5 minutes and 70 to 90 mm/h in 30 minutes (Mounirou  
134 et al., 2012, 2020).



135

136 **Fig. 1.** Study area location and experimental design. (a) Localization of the catchment of Tougou. The sub-  
 137 catchments locations BV<sub>1</sub> (cultivated) and BV<sub>2</sub> (degraded) are shown with black contour lines. Elevation on the  
 138 entire catchment is derived from ASTER GDEM Digital Elevation Model, 30m resolution, tile N13W003,  
 139 acquired from USGS EarthExplorer ([https://gdemdl.aster.jspacesystems.or.jp/index\\_en.html](https://gdemdl.aster.jspacesystems.or.jp/index_en.html)). (b) Detailed view  
 140 of the experimental layout in BV<sub>2</sub> (degraded sub-catchment). (c) Detailed view of the experimental layout in  
 141 BV<sub>1</sub> (cultivated sub-catchment). (d) Field photograph of the experimental design at S4 site in the degraded  
 142 sub-catchment (BV<sub>2</sub>). (e) Field photograph of the experimental design at S1 site in the cultivated  
 143 sub-catchment (BV<sub>1</sub>).

## 144 2.2. Experimental setup

145 Two hydrologic units (sub-catchments) were selected in the catchment. These units are  
146 homogeneous in terms of land use and soil surface conditions and are respectively identified  
147 as cultivated (BV<sub>1</sub>, 6.1 ha, **Fig. 1a, c**) and degraded/uncultivated (BV<sub>2</sub>, 33.8 ha, **Fig. 1a, b**)  
148 sub-catchments. Degraded and uncultivated refers to naturally occurring and undisturbed  
149 soils, corresponding to barren and degraded land use/land cover (Anderson et al., 1976) and  
150 developing a very low vegetation cover, mostly consisting of shrubs and herbaceous  
151 (Mounirou, 2012). In each sub-catchment, three sites were selected for their homogeneity in  
152 terms of soil type, land use and cropping systems. At each site, three plots with different sizes  
153 (1, 50 and 150 m<sup>2</sup>) were installed (**Fig. 1d, e**). The plots locations were chosen on the field  
154 where soil surface conditions could be assumed homogeneous, with identical agricultural  
155 practices. However, the microrelief (in terms of roughness and surface storage capacity)  
156 varied from one plot to another. Topographic surveys were conducted using a Trimble S6  
157 total station, at various square mesh sizes: 50 cm on the plots of 50 m<sup>2</sup> and 150 m<sup>2</sup>, 20 cm at  
158 plot scale of 1 m<sup>2</sup>; 25 m<sup>2</sup> at the scale of the two sub-catchments (BV<sub>1</sub> and BV<sub>2</sub>). These  
159 topographic surveys helped in evaluating the average longitudinal slope of each plot and of  
160 the sub-catchments: 6 measurements were made on 1 m<sup>2</sup> plots, 11 measurements on 50 m<sup>2</sup>  
161 plots and 13 measurements on 150 m<sup>2</sup> plots. The detailed description of the soil surface  
162 conditions on all plots is given in **Table 1**.

163 The soil types and their measured physical properties are further described in **Table 2**. The  
164 soil texture was determined through soil sieving and sedimentation protocol  
165 (AFNOR/NFISO11277) applied to 9 soil samples per site. Saturated hydraulic conductivity  
166  $K_S$  was measured with the double-ring infiltrometer (Reynolds and Topp, 2008). Bulk density  
167  $\rho_b$  was estimated from undisturbed soil samples through the core method after oven drying at  
168 105°C for 48h (Jawuoro et al., 2017) and calculated according to **Equation 1**:

$$\rho_b = m_s/V \quad (1)$$

169 where  $m_s$  (g) is the mass of the dry weight of soil (g) and  $V$  (cm<sup>3</sup>) is the soil volume. Porosity  
170  $p$  was then derived from the bulk density values  $\rho_b$ , according to **Equation 2** (Jawuoro et al.,  
171 2017):

$$p = 1 - \rho_b/\rho_s \quad (2)$$

172 where  $\rho_b$  is the bulk density,  $\rho_s$  is the particle density taken as  $2.65 \text{ g.cm}^{-3}$  (Mounirou, 2012;  
173 Jawuoro et al., 2017). The Manning roughness ( $n$ ) values were determined according to the  
174 median grain diameter  $d_{50}$  of the soil at each site, based on Strickler's formula, as given by  
175 **Equation 3** (Chanson, 2004):

$$\frac{1}{n} = 21.1 d_{50}^{-1/6} \quad (3)$$

176 where  $n$  ( $s.m^{-1/3}$ ) is the Manning roughness coefficient and  $d_{50}$  ( $m$ ) is the median grain  
177 diameter size in a soil sample distribution.

**Table 1.**  
Detailed description of soil surface conditions on all the plots in the experimental setup.

Site name	Unit name	Hydrological unit type	Size	Average slope (%)	Soil surface condition	Land use
Site S <sub>1</sub>	S <sub>1</sub> -1	Plot	1 m <sup>2</sup> (1x1)	1.60 ± 0.43		
	S <sub>1</sub> -50	Plot	50 m <sup>2</sup> (5x10)	1.80 ± 0.14		
	S <sub>1</sub> -150	Plot	150 m <sup>2</sup> (6x25)	1.35 ± 0.15		
Site S <sub>2</sub>	S <sub>2</sub> -1	Plot	1 m <sup>2</sup> (1x1)	1.70 ± 0.50		
	S <sub>2</sub> -50	Plot	50 m <sup>2</sup> (5x10)	1.40 ± 0.19	C	Cultivated
	S <sub>2</sub> -150	Plot	150 m <sup>2</sup> (6x25)	1.60 ± 0.10		
Site S <sub>3</sub>	S <sub>3</sub> -1	Plot	1 m <sup>2</sup> (1x1)	4.00 ± 0.52		
	S <sub>3</sub> -50	Plot	50 m <sup>2</sup> (5x10)	4.20 ± 0.59		
	S <sub>3</sub> -150	Plot	150 m <sup>2</sup> (6x25)	2.85 ± 0.15		
Site S <sub>4</sub>	S <sub>4</sub> -1	Plot	1 m <sup>2</sup> (1x1)	0.75 ± 0.16		
	S <sub>4</sub> -50	Plot	50 m <sup>2</sup> (5x10)	1.25 ± 0.09	ERO	
	S <sub>4</sub> -150	Plot	150 m <sup>2</sup> (6x25)	0.93 ± 0.08		
Site S <sub>5</sub>	S <sub>5</sub> -1	Plot	1 m <sup>2</sup> (1x1)	0.90 ± 0.31		
	S <sub>5</sub> -50	Plot	50 m <sup>2</sup> (5x10)	0.96 ± 0.11	G	Degraded and uncultivated
	S <sub>5</sub> -150	Plot	150 m <sup>2</sup> (6x25)	0.80 ± 0.14		
Site S <sub>6</sub>	S <sub>6</sub> -1	Plot	1 m <sup>2</sup> (1x1)	2.30 ± 0.24		
	S <sub>6</sub> -50 <sub>1</sub>	Plot	50 m <sup>2</sup> (5x10)	2.10 ± 0.28	DES	
	S <sub>6</sub> -50 <sub>2</sub>	Plot	150 m <sup>2</sup> (5x10)	3.55 ± 0.32		
BV1	Sub-catchment	6.1 ha	1.91 ± 0.28	C	Cultivated	
BV2	Sub-catchment	33.8 ha	1.18 ± 0.16	ERO, G, DES	Degraded and uncultivated	
BV0	Catchment	37 km <sup>2</sup>	0.60 ± 0.11	C, ERO, G, DES	Heterogeneous	

180 In the size column, for each unit at each site, the plot dimensions are given in parenthesis, using the following  
181 convention: (*l x L*), where *l* and *L* stands respectively for the plot width and length, both in meters. The plot  
182 length *L* is also the runoff length. Soil surface condition uses the naming convention for surface feature crusts  
183 presented in Casenave and Valentin (1992): erosion crust (ERO), desiccation crust (DES), agricultural crust (C)  
184 and gravel pavement crust (G). Regarding slope determination, 6 measurements were made on 1 m<sup>2</sup> plots, 11  
185 measurements on 50 m<sup>2</sup> plots and 13 measurements on 150 m<sup>2</sup> plots. The term “*crust*” designates a thin and  
186 stratified layer developing at the soil surface, which has undergone changes under the effect of meteorological,  
187 faunal or anthropogenic factors. Type C crusts are made of one or two micro-horizons, generally forming on  
188 clayey or sandy soils. ERO crusts are made of a single and thin micro-horizon, harden, clayey, prone to crackling  
189 when drying up. DES crusts are made of a single sandy micro-horizon, very fragile. G crusts are made of a single  
190 micro-horizon containing coarse sediments (diameter > 2 mm).

191 **Table 2.**  
192 Soil type and physical properties at monitoring sites.

Site	Soil type	Tillage operations	Crop type	K <sub>s</sub> (mm.h <sup>-1</sup> )	K <sub>s</sub> (mm.h <sup>-1</sup> ) (Casenave and Valentin, 1992)	Bulk Density ρ <sub>b</sub> (g.cm <sup>-3</sup> )	Porosity p (%)	Manning n (s.m <sup>-1/3</sup> ) roughness
S1	Loam	Row sowing + ploughing + weeding + hoeing	Millet, sorghum and cowpea	21 – 25		1.40 – 1.46	45 – 47	0.050
S2	Sandy	Row sowing + ploughing + ridging	Millet, sorghum and cowpea	27 – 33	15 - 35	1.36 – 1.44	46 – 49	0.060
S3	Sandy gravelly	Row sowing + weeding + hoeing	Millet, sorghum and peanut	16 – 19		1.46 – 1.48	44 – 45	0.065
S4	Dry clay			2 – 2.5	2 – 4	1.58 – 1.61	39 – 40	0.015
S5	Gravelly	No tillage	No cropping	3 – 3.5	3 – 5	1.88 – 1.94	27 – 29	0.020
S6	Sand			12 – 15	10 – 20	1.66 – 1.70	36 – 37	0.025

193 K<sub>s</sub> refers to the soil saturated hydraulic conductivity. Number of infiltration measurements by site: 12. Number  
194 of porosity measurements by site: 9.

195 The values in **Table 2** are in line with the observations made on similar types of crust in the  
196 Sahelian region reported by (Casenave and Valentin, 1992) and they also reflect the range of  
197 variability for each parameter, especially for the soil hydrodynamic properties in cultivated  
198 areas. However, within the same site, this range of variability is lesser and therefore, the  
199 hydrodynamic properties of the soil at each site are assumed homogeneous, and cultivation  
200 practices identical. On each site, only the microrelief (slope, surface roughness and surface  
201 storage capacity) is considered to be varying from one plot to another. Furthermore, the  
202 analysis of bulk density and porosity values (**Table 2**) in the first 15 cm of the soils of the  
203 plots showed that the soil is more compact on bare and degraded areas than on cultivated  
204 areas.

205 In the Tougou catchment, the major tillage operations carried on cultivated soils are  
206 ploughing, followed by sowing or manual weeding (weeding associated to hoeing) or  
207 weeding with animal traction (Marchal, 1983; Barbier et al., 2009; Zouré, 2019). These  
208 operations break the crusts developing at the soil surface and therefore improves infiltration.  
209 Partitioned ridging is also practised in Tougou catchment and also helps in reducing runoff  
210 and promote infiltration (Nyamekye et al., 2018; Zouré, 2019). The sizing and description of  
211 the tillage operations carried in Tougou catchment is presented in **Table 3**. It is also

212 interesting to note that stone bunds are heavily used in association with these tillage  
 213 operations, mostly as a soil conservation measure (Nyamekye et al., 2018; Zouré, 2019).

214 **Table 3.**  
 215 Sizing and description of tillage operation carried on cultivated fields in Tougou catchment (Dugué et al., 1994).

Ridge spacing/density	Tillage operations
Millet : 80 cm x 80 cm	
Sorghum: 80 cm x 40 cm	ploughing (0 – 15 cm depth), weeding (0-5 cm depth), hoeing (0 - 5 cm depth), ridging (15 – 20 cm)
Groundnut: 40 cm x 20 cm	
Cowpea: 80 cm x 40 cm	

216 The tillage operations described in this table are often combined by farmers in Tougou catchment (Barbier et al., 2009).

### 217 **2.3. Surface runoff and rainfall monitoring**

218 Each plot of 1 m<sup>2</sup> was isolated by a metal sheet frame, buried into the ground at a depth of 10  
 219 cm. The plot was also equipped with an outlet connected to a PVC pipe leading runoff to a  
 220 buried tank for runoff collection and measurement. Plots of 50 and 150 m<sup>2</sup> were isolated from  
 221 outside overland flow run-on using metallic sheet frames also buried at 10 cm depth into the  
 222 ground; downstream, the plots were equipped with a collector composed of a concrete tank  
 223 (with 2 or 3 compartments respectively for plots of 50 and 150 m<sup>2</sup>). Level gauges were  
 224 installed in each tank to monitor runoff depths.

225 Rainfall events were monitored from 2010 to 2015 (6 years), during each rainy season, using  
 226 a network of 12 rain gauges, including 6 rain gauges installed on runoff monitoring sites (one  
 227 per each site), whereas the remaining 6 were spread throughout the catchment to assess the  
 228 spatial variability of rainfall. Also, 5 tipping bucket rain gauges (including 1 per sub-  
 229 catchment, and the remaining 3 spread throughout the catchment) were used for rainfall  
 230 intensity measurement at 5 minutes timesteps. Average rainfall amount per event was  
 231 evaluated using Thiessen averaging method.

232 At the outlets of the sub-catchments BV<sub>1</sub> and BV<sub>2</sub> and the entire catchment named BV<sub>0</sub>, a  
 233 control section equipped with an *OTT Thalimedes* water level logger. Further, recorded water  
 234 levels were converted to series of instantaneous discharges using rating curves for each  
 235 control section. These rating curves were developed through a simple power-law equation fit  
 236 to direct measurements at the outlet of each control section. Derived hydrographs were  
 237 converted to runoff volumes and further, runoff depths for all the recorded rainfall events.  
 238 Runoff monitoring was also carried out during six years, from 2010 to 2015.

239 **2.4. Runoff dimensionless indices**

240 In this study, dimensionless numbers were developed to reduce the effect of the size of the  
241 observation scale on runoff.

242 The dimensionless indices proposed in this study were developed considering the topography,  
243 surface roughness, saturated hydraulic conductivity, rainfall amount and intensity. The  
244 theoretical basis and mathematical development leading to the expression of these  
245 dimensionless indices is further detailed and discussed in **Appendix A**. The proposed indices  
246 are the following:

247 (i) the *runoff potential* dimensionless index ( $I_1$ ) expressed as the ratio of the plot runoff  
248 coefficient to the square root of its slope. As defined in **Equation 4**, it expresses the  
249 runoff potential of the plot and reduces the effect of the slope (explicitly slope) on  
250 runoff production. This formulation results from a physically-based modelling of  
251 runoff based on Manning flow formula (Manning, 1891; Chanson, 2004).

$$I_1 = \frac{K_r}{\sqrt{S_0}} \quad (4)$$

252 where  $K_r$  is the runoff coefficient of the plot and  $S_0$  is the slope of the plot. Runoff  
253 coefficients were evaluated on an event scale basis, as a ratio of the observed runoff to  
254 the rainfall.

255 (ii) the *effective runoff* dimensionless index ( $I_2$ ), expressed as the ratio of the runoff  
256 depth ( $R$ ) measured at a given observation scale, out of the term ( $P - K_s \times T_e$ ), as  
257 shown in **Equation 5**:

$$I_2 = \frac{R}{P - K_s \times T_e} \quad (5)$$

258 where  $R$  ( $mm$ ) is the runoff depth,  $P$  ( $mm$ ) is the rainfall amount,  $K_s$  ( $mm.h^{-1}$ ) is the  
259 saturated hydraulic conductivity and  $T_e$  ( $h$ ) the time to equilibrium state, i.e., the time  
260 to the establishment of a steady-state runoff.

261  $T_e$  is also referred to as the *kinematic time to equilibrium* (Julien and Moglen, 1990) and is  
262 given by **Equation 6**:

$$T_e = \beta \left( \frac{L}{\alpha \times i^{\beta-1}} \right)^{\frac{1}{\beta}} \quad (6)$$

263 where  $L$  ( $m$ ) is the plot length,  $i$  is the infiltration excess,  $\alpha$  and  $\beta$  are parameters. Combining  
 264 Manning resistance turbulent flow equation with a kinematic wave approximation yields  $\beta =$   
 265  $5/3$  (Julien and Moglen, 1990). Parameter  $\alpha$ , on the other hand, is given by **Equation 7**:

$$\alpha = \frac{1}{n} \times \sqrt{S_0} \quad (7)$$

266 where  $S_0$  is the plot slope and  $n$  [ $s.m^{-1/3}$ ] is the Manning roughness coefficient. The product  
 267 term ( $Ks \times Te$ ) in the dimensionless number  $I_2$  (**Equation 5**) expresses infiltration losses  
 268 occurring along the flow path on the plot. Removing this term from the rainfall input confers  
 269 to the dimensionless number  $I_2$  the ability to reduce the scale effect due to re-infiltration  
 270 downstream of the plot.

271 At the sub-catchment scale, the evaluation of  $T_e$  requires an estimation of surface runoff  
 272 velocities  $V_p$  ( $m.s^{-1}$ ) on the measurement plots and  $V_h$  ( $m.s^{-1}$ ) in the sub-catchment and  
 273 catchment drainage system. The geometry of the drainage system was assumed to be invariant  
 274 over time and velocities uniform at each observation scale. Besides, to reduce the number of  
 275 parameters, we relied on the previous research work of which estimated that runoff velocity in  
 276 drainage network ( $V_h$ ) is approximately ten (10) times higher than the runoff velocity at the  
 277 plot scale ( $V_p$ ) (Gresillon and Taha, 1998; Tatard et al., 2008). As such, a constant ratio  
 278 between these velocities was defined as given in **Equation 8**:

$$V_h = 10V_p, \quad V_p = \frac{L}{T_e} \quad (8)$$

### 279 **3. Results**

#### 280 **3.1. Rainfall characteristics**

281 **Table 4** shows the daily rainfall distributions statistics from 2010 to 2015. Maximum daily  
 282 rainfall amount ranges between 41.8 and 114 mm during the entire observation period,  
 283 whereas cumulative annual rainfall varied between 450 and 730 mm. The interquartile range  
 284 (IQR), median (Q2) and mean daily rainfall events are also presented and illustrates the  
 285 skewness of the distributions towards smaller daily rainfall values.

286 **Table 4.**  
287 Daily rainfall distribution statistics in Tougou catchment from 2010 to 2015.

<b>Annual rainfall events</b>	<b>2010</b>	<b>2011</b>	<b>2012</b>	<b>2013</b>	<b>2014</b>	<b>2015</b>
Annual rainfall (mm)	671.6	449.3	697.7	578.6	624.3	729.6
Number of events	39	30	35	38	30	34
Daily minimum rainfall (mm)	1.6	1.6	2.2	2.8	4.7	3.7
Q1 (first quartile) (mm)	7.0	5.8	7.4	8.4	12.2	7.8
Q2 (median) (mm)	18.1	10.7	13.8	13.7	19.4	14.0
Mean (mm)	17.2	15.0	19.9	15.2	20.8	21.5
Q3 (third quartile)	24.4	23.4	29.6	20.9	26.8	24.6
Daily maximum rainfall (mm)	53.5	53.9	81.6	41.8	47.4	114.0

288 The monthly rainfall amount and rainfall intensities statistics are presented in **Table 5**. No  
289 significant correlation was found between the rainfall amount and its duration, highlighting  
290 the high variability in the rainfall intensity across the rainfall events. Maximum rainfall  
291 intensities recorded peaked at 120 mm.h<sup>-1</sup> in 5 minutes (*Imax-5mn*) and 70 mm.h<sup>-1</sup> in 30  
292 minutes (*Imax-30mn*). In terms of rainfall amount, during the six years of monitoring, nine  
293 (09) daily events exceeded 50 mm in amount, the most important one being the event which  
294 occurred on 05/08/2015, which peaked at 114 mm.

295 **Table 5.**  
296 Monthly rainfall statistics in Tougou catchment from 2010 to 2015.

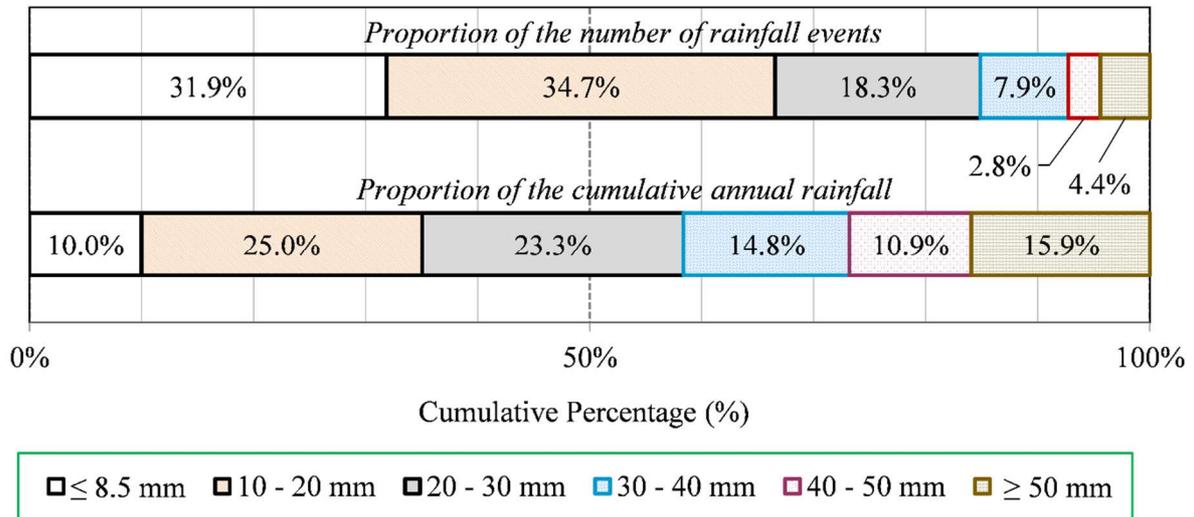
<b>Months</b>	<b>Rainfall amount</b>					<b>Rainfall intensity</b>			
	<b>Pd</b>		<b>Pm</b>		<b>Annual rainfall percent</b>	<b>Imax-5mn</b>		<b>Imax-30mn</b>	
	<b>(mm)</b>		<b>(mm)</b>			<b>(mm.h<sup>-1</sup>)</b>		<b>(mm.h<sup>-1</sup>)</b>	
	<b>Avg</b>	<b>σ</b>	<b>Avg</b>	<b>σ</b>		<b>Avg</b>	<b>σ</b>	<b>Avg</b>	<b>σ</b>
June	41.6	10.8	101.8	35.2	16%	81.6	7.5	42.2	6.2
July	43.3	12.1	146.5	42.7	23%	82.5	10.9	42.8	8.5
August	57.8	32.8	218.0	43.0	35%	95.9	16.7	58.8	9.4
September	35.9	16.6	119.6	41.8	19%	78.5	29.0	42.7	12.5
October	21.6	9.6	41.5	26.3	7%	37.6	14.9	26.7	11.5

297 Pd: average maximum daily rainfall. Pm: cumulative average monthly rainfall. Avg: average. σ: standard  
298 deviation. Imax-5mn: maximum rainfall rate in 5 minutes. Imax-30mn: maximum rainfall rate in 30 minutes.

299 It was also observed that in general, all rainfall events are homogeneous most of the time over  
300 the catchment, similarly to the findings reported in Mounirou (2012), Zouré (2019).

301 Examination of **Fig. 2** shows that, on average, nearly 32% of the rainfall events  
302 (corresponding to 10% of the annual rainfall volume) fall below 8.5 mm. The threshold of 8.5  
303 mm was found to be the preponding rainfall value of the entire catchment in Mounirou  
304 (2012). **Fig. 2** shows that nearly 35% of the events, the highest share, fall between 10 and 20

305 mm and contributes to 27% on average of the annual rainfall volume. Also, 31.9% of the  
 306 observed rainfall events are below 8.5 mm (the preponderant rainfall) and accounts for 10% of  
 307 the annual rainfall volume. Likewise, events above 40 mm account for 7.5% of the observed  
 308 events, yet they generate nearly 27% of the annual rainfall volume.

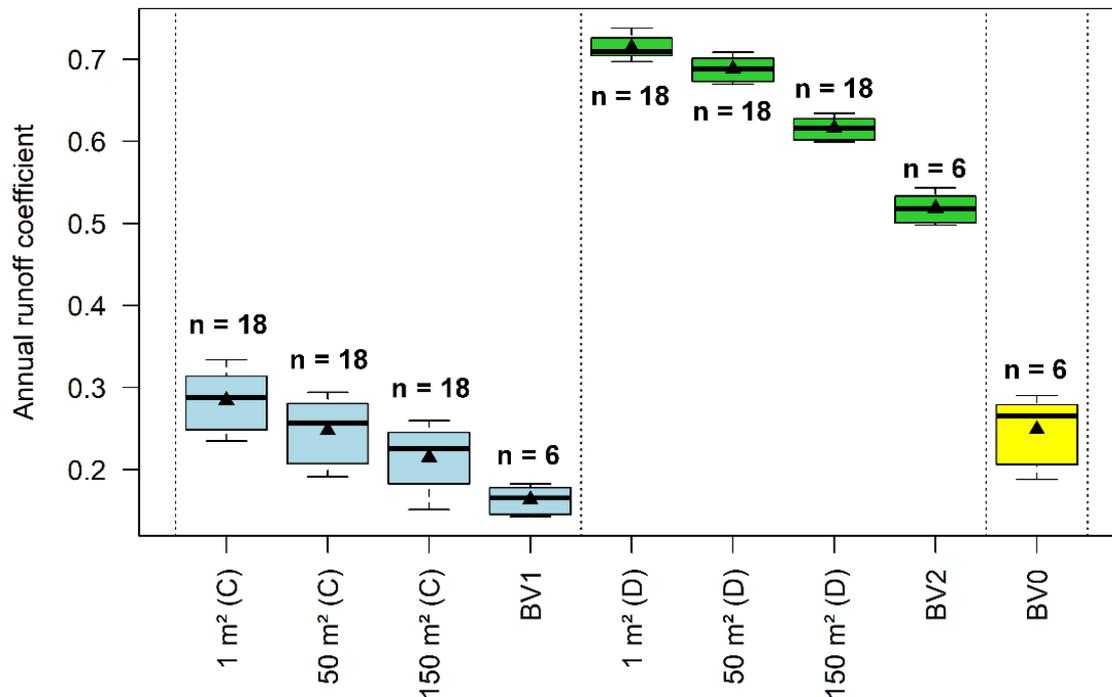


309

310 **Fig. 2.** Proportion of rainfall events per class. The upper bar chart shows the rainfall events distribution in terms  
 311 of number of events. The lower bar chart shows the proportion of rainfall events in terms of annual rainfall  
 312 volume. It can be seen that, for example, 31.9% of the rainfall events observed fall below 8.5 mm and account  
 313 for 10% of the annual rainfall volume on average. Similarly, rainfall events above 40 mm are observed 7.5% of  
 314 the time, but they generate nearly 27% of the annual rainfall volume.

315 **3.2. Variability of annual surface runoff coefficients**

316 Annual runoff coefficients values calculated on plots of 1, 50 and 150 m<sup>2</sup>, hydrologic units  
 317 (sub-catchments) of 6.1 ha and 33.8 ha and the catchment area of 37 km<sup>2</sup> are presented in **Fig.**  
 318 **3.**



319

320 **Fig. 3.** Annual runoff coefficient distribution across the monitoring sites during 2010-2015. The suffix (C) stands  
 321 for plots on the cultivated sub-catchment BV1, whereas (D) stands for the degraded sub-catchment. BV<sub>1</sub> and  
 322 BV<sub>2</sub> refer to the runoff coefficients for the cultivated and degraded sub-catchments respectively. BV0 refers to  
 323 runoff coefficients observed for the entire catchment. The middle bar in the boxplots shows the median (Q2) of  
 324 the distribution, whereas the black triangle dot inside the boxplots shows the mean. The size of the distribution is  
 325 indicated above (or below) each boxplot.

326 The median (Q2) values of annual runoff coefficients associated with the interquartile range  
 327 (IQR) are as follows: on agricultural soils, runoff coefficients varied between 0.29 (0.25 -  
 328 0.31) (plot of 1 m<sup>2</sup>) to 0.23 (IQR: 0.19 – 0.24) (plot of 150 m<sup>2</sup>), whereas the average runoff  
 329 coefficient for the agricultural sub-catchment BV<sub>1</sub> (6.1 ha) was 0.17 (IQR: 0.15 – 0.18).  
 330 These values were significantly lower (**Table 6**) than those measured on degraded plots,  
 331 which went from 0.71 (IQR: 0.70 – 0.72) (plot of 1 m<sup>2</sup>) to 0.62 (IQR: 0.60 – 0.63) (plot of  
 332 150 m<sup>2</sup>), with the degraded and uncultivated catchment BV<sub>2</sub> (33.8 ha) presenting a median  
 333 annual runoff coefficient of 0.52 (IQR: 0.50 – 0.53).

334 **Table 6.**  
 335 Statistical comparison of runoff coefficients at different scales.

Comparison	t-Student p-value
1 m <sup>2</sup> plots (cultivated) - 1 m <sup>2</sup> plots (degraded and uncultivated)	<b>0.31.10<sup>-6</sup></b>
50 m <sup>2</sup> plots (cultivated) - 50 m <sup>2</sup> plots (degraded and uncultivated)	<b>0.35.10<sup>-6</sup></b>
150 m <sup>2</sup> plots (cultivated) - 150 m <sup>2</sup> plots (degraded and uncultivated)	<b>0.56.10<sup>-6</sup></b>
BV <sub>1</sub> (cultivated sub-catchment) – BV <sub>2</sub> (degraded and uncultivated sub-catchment)	<b>0.10.10<sup>-9</sup></b>
BV <sub>0</sub> (catchment) – BV <sub>1</sub> (cultivated sub-catchment)	<b>0.004</b>
BV <sub>0</sub> (catchment) – BV <sub>2</sub> (degraded and uncultivated sub-catchment)	<b>7.50.10<sup>-6</sup></b>

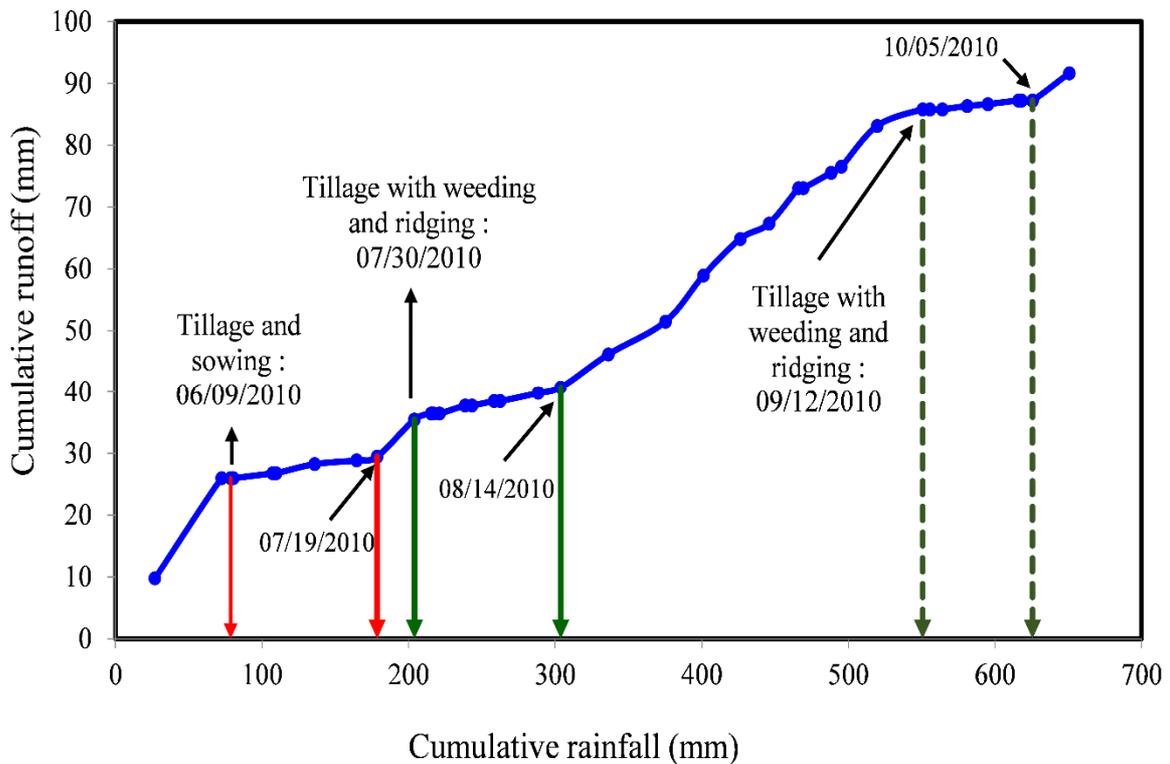
336 Significant values (at level  $\alpha = 5\%$ ) are shown in bold. The comparison is made on runoff coefficient values  
 337 calculated for all events observed during the monitoring period (2010-2015).

338 At all scales, degraded and uncultivated soils show a higher runoff production potential on  
 339 average than cultivated soils under similar rainfall conditions. This can be explained by their  
 340 higher compaction and crust development at the soil surface, which is limiting infiltration and  
 341 favouring runoff. The entire catchment (37 km<sup>2</sup>) showed a median runoff coefficient of 0.27  
 342 (IQR: 0.22 – 0.28), which was above the median for the cultivated sub-catchment BV<sub>1</sub> and  
 343 significantly smaller than the median for the degraded and uncultivated catchment BV<sub>2</sub>. Such  
 344 results can partly be explained by the heterogeneity and the hydrologic connectivity in terms  
 345 of soil surface conditions in the catchment. However, the dominance of agricultural areas  
 346 (65% of the catchment area) causes a global runoff coefficient on average which tends to the  
 347 one observed on the corresponding sub-catchment BV<sub>1</sub>.

348 It also appears that considering both cultivated or degraded and uncultivated soils, the runoff  
 349 coefficients decrease as the scale increases. This observed decrease in runoff can be explained  
 350 by several factors affecting runoff, such as the non-linearity nature of the runoff process  
 351 (Sivapalan et al., 2002; Cerdan et al., 2010; Cantón et al., 2011), the spatial variability of soil  
 352 infiltration (Cerdan et al., 2004; Mounirou et al., 2012; Miyata et al., 2019) but also the  
 353 temporal pattern of rainfall (Stomph et al., 2002; Van de Giesen et al., 2005; Cristiano et al.,  
 354 2019). On cultivated soils, coefficients of variation of runoff coefficient were respectively  
 355 14.17%, 16.87%, 19.46% and 10.25% at plots of 1 m<sup>2</sup>, 50 m<sup>2</sup>, 150 m<sup>2</sup> and the cultivated sub-  
 356 catchment BV<sub>1</sub> (6.1 ha). These values were higher than those of degraded and uncultivated  
 357 soils, which were respectively 2.12% (plot of 1 m<sup>2</sup>), 2.41% (plot of 50 m<sup>2</sup>), 2.41% (plot of 150  
 358 m<sup>2</sup>) and 3.54% (BV<sub>2</sub>, 33.8 ha).

359 To further assess the influence of agricultural practices on the observed runoff coefficients  
 360 through the change in soil surface conditions, the cumulative runoff evolution is plotted

361 against the cumulative rainfall. **Fig. 4** shows a typical example of such plot for the year 2010,  
362 on a cultivated plot of 150 m<sup>2</sup> at site S<sub>2</sub>.



363

364 **Fig. 4.** Impact of soil management operations on the rainfall-runoff relationship. Data of 2010 year were used for  
365 this example. Tillage operation is carried in general three times during a rainy season. At its beginning (early  
366 June), tillage and sowing are carried on cultivated fields. Two months later (in late July), tillage and ridging  
367 operations are carried, along with weeding for maintenance. The same operations are carried again, if necessary,  
368 in the late growing season at mid-September (Yonaba et al., 2021). It can be observed on the figure that from  
369 06/09/10 to 07/19/10, 07/30/10 to 08/14/10 and 09/12/10 to 10/05/10, the rate of increase in runoff is low  
370 because of the tillage operation, then increases after a cumulative rainfall of 80-100 mm is recorded (Mounirou,  
371 2012).

372 It appears that on cultivated soils, the observed runoff for each rainfall event is highly  
373 dependent on the soil surface conditions than rainfall amount or intensity. Immediately after  
374 tillage operation, observed runoff is significantly reduced. Yet, after a cumulative rainfall  
375 amount of 80-100 mm falling after the tillage operation has been carried, observed runoff  
376 increases significantly.

377 This significant increase in runoff after the threshold of 80-100 mm of cumulative rainfall can  
378 be explained by the regeneration of a structural crust at the soil surface, which further  
379 increases runoff (hence limiting infiltration). However, after any tillage operation, this crust is  
380 dismantled because of the ploughing. Similar findings have been reported in previous studies,  
381 however in the with slightly lower thresholds of 80 mm and 60 mm respectively in the Sahel  
382 region (Peugeot et al., 1997; Rockström and Valentin, 1997).

383 The higher variability observed in runoff coefficients on agricultural soils can be partly  
384 explained by the variability in runoff response induced by tillage management operations.  
385 Similar results have been reported in previous studies (Cammeraat, 2004; Mathys et al.,  
386 2005). These authors further emphasized that the location of runoff measurement strongly  
387 influences the observations since runoff, as a process, is largely influenced by the spatial  
388 variation of the soil infiltration capacity (texture, structural stability), the microtopography  
389 and agricultural practices.

### 390 **3.3. Analysis of runoff potential ( $I_1$ ) and effective runoff ( $I_2$ ) values**

391 **Table 7** presents the characteristic values of the kinematic time to equilibrium  $T_e$  and runoff  
392 velocity  $V_p$  distributions, which are key variables in the calculation of the dimensionless  
393 numbers  $I_1$  and  $I_2$ . Given a scale of observation,  $T_e$  is lower on bare and degraded soils and  
394 increases when the runoff length increases. Likewise, given a soil surface condition, the  
395 runoff velocity  $V_p$  increases when the runoff length increases as well. On a plot of 150 m<sup>2</sup>  
396 having a runoff length of 25 m, after the soil imbibition, an average time of 10.6 min on  
397 cultivated soils is required for the entire plot to produce surface runoff with an average  
398 velocity of 4 cm.s<sup>-1</sup>; Conversely, surface runoff arises on bare and degraded soil in an average  
399 time of 6.1 mn, with an average higher velocity of 7.2 cm.s<sup>-1</sup>. In the case of more intense  
400 rainfall events, these durations are respectively 6.2 mn (average velocity of 6.8 cm.s<sup>-1</sup>) and 3.4  
401 mn (average velocity of 12.1 cm.s<sup>-1</sup>) on cultivated and bare/degraded soils. At the sub-  
402 catchment scale, for which the runoff length is estimated at 541 and 1390 m respectively in  
403 BV<sub>1</sub> and BV<sub>2</sub>, it takes on average, 16.8 and 27.3 mn (respectively) for the entire area to  
404 contribute to runoff production. The average runoff velocities are 56.9 and 88.3 cm.s<sup>-1</sup>  
405 respectively. However, the time to ponding depends on the rainfall intensity and the  
406 antecedent soil moisture condition, as also observed by Mounirou, 2012 and Zouré et al.,  
407 2019. This time to ponding is lower on bare and degraded soils (which tend to produce runoff  
408 quickly) than on cultivated soils. Likewise, in the case of cultivated soils, this time to ponding  
409 increases as the area increases.

410 **Table 7.**

411 Characteristic values of  $T_e$  and  $V_p$  at different scales of observation in Tougou catchment.

<b><math>T_e</math></b> <b>(mn)</b>	<b>Cultivated</b>			<b>Bare and Degraded</b>			<b>Sub-catchment</b>	
	<b>1 m<sup>2</sup></b>	<b>50 m<sup>2</sup></b>	<b>150 m<sup>2</sup></b>	<b>1 m<sup>2</sup></b>	<b>50 m<sup>2</sup></b>	<b>150 m<sup>2</sup></b>	<b>BV1</b>	<b>BV2</b>
Minimum	0.6	2.3	6.2	0.5	1.9	3.4	8.0	16.1
Q1	1.4	5.5	9.7	0.8	2.9	5.2	14.7	24.3
Q2 (Median)	1.6	6.1	10.5	0.9	3.2	5.8	17.0	26.6
Mean	1.6	6.1	10.6	0.9	3.4	6.1	16.8	27.3
Q3	1.7	6.6	11.5	1.0	3.7	6.6	19.3	29.8
Maximum	2.7	10.6	18.6	1.7	6.2	12.6	31.9	43.6

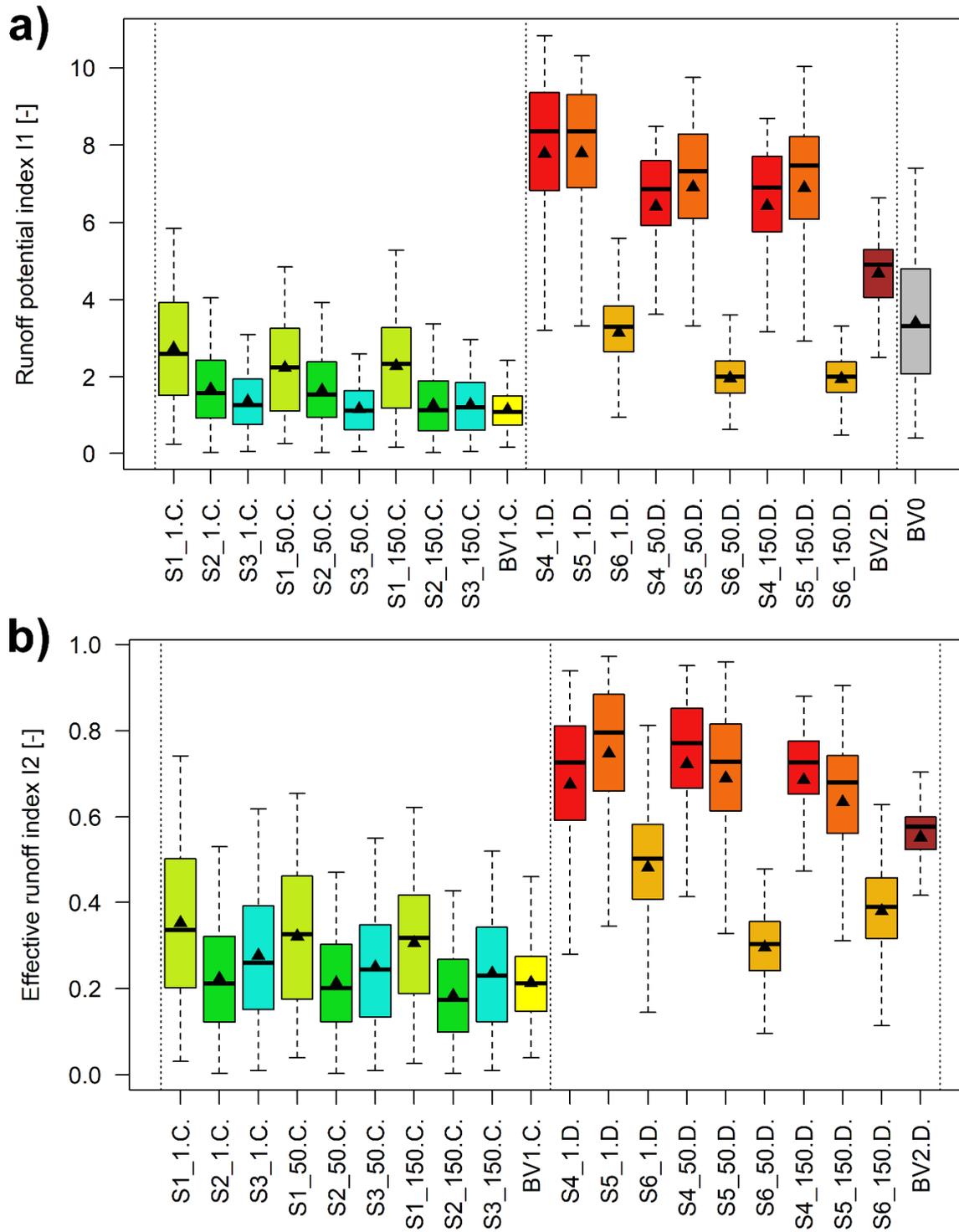
<b><math>V_p</math></b> <b>(cm.s<sup>-1</sup>)</b>	<b>Cultivated</b>			<b>Bare and Degraded</b>			<b>Sub-catchment</b>	
	<b>1 m<sup>2</sup></b>	<b>50 m<sup>2</sup></b>	<b>150 m<sup>2</sup></b>	<b>1 m<sup>2</sup></b>	<b>50 m<sup>2</sup></b>	<b>150 m<sup>2</sup></b>	<b>BV1</b>	<b>BV2</b>
Minimum	0.6	1.6	2.2	1.0	2.7	3.3	28.2	53.1
Q1	1.0	2.5	3.6	1.6	4.5	6.3	46.6	77.6
Q2 (Median)	1.1	2.7	4.0	1.9	5.2	7.2	53.0	87.1
Mean	1.1	2.8	4.0	1.9	5.2	7.2	56.9	88.3
Q3	1.2	3.0	4.3	2.1	5.8	8.0	61.5	95.3
Maximum	2.7	7.3	6.8	3.1	8.8	12.1	112.7	143.8

412  $T_e$ : kinematic time to equilibrium.  $V_p$ : surface runoff velocity. Q1: 1<sup>st</sup> quartile. Q2: Median. Q3: 3<sup>rd</sup> quartile.

413 The distribution of the runoff potential index  $I_1$  and the effective runoff index  $I_2$  values,  
 414 calculated for all the rainfall observations (from 2010 to 2015) is presented in **Fig. 5**. It  
 415 appears that for cultivated soils, the median (Q2) of the distribution is close to the mean and  
 416 centred in the boxplot, whereas the whiskers are almost symmetrical. On the other hand, on  
 417 bare and degraded soils, the median (Q2) is higher than the mean, whereas the distribution is  
 418 more elongated towards lower values of  $I_1$  and  $I_2$ . This is probably because, on bare and  
 419 degraded soils, even light rainfall events are likely to trigger surface runoff. Mounirou (2012)  
 420 showed that in Tougou catchment, the preponding rainfall, that is the minimal amount of  
 421 rainfall to trigger surface runoff is 3.5 mm on bare/degraded soils and 11-13 mm, significantly  
 422 higher, on cultivated soils, depending on the tillage operation management.

423 Given a spatial scale, the differences in boxplot distributions from one site to another can be  
 424 attributed to the differences in soil surface hydrodynamical properties and the associated  
 425 tillage operation management (on cultivated sites). Moreover, it is interesting to consider that  
 426 at the scale of BV<sub>1</sub> sub-catchment, the value of  $I_1$  and  $I_2$  ranges between 0.44 - 2.90 and 0.08 -  
 427 0.49 (respectively) in July and August, then between 0.20 - 1.52 and 0.04 - 0.26 (respectively)  
 428 in September and October. This decrease observed during the rainy season can be explained  
 429 by the development of vegetation and plant coverage at the soil surface.

430 Conversely, for bare and degraded soils, given a spatial scale, the values of  $I_1$  and  $I_2$  are  
431 relatively low on the DES crust (S6 site) in comparison to the ERO (S4 site) and G (S5 site)  
432 crusts whose distributions across sites seem to be almost identical. For the ERO (S4 site) and  
433 G (S5 site) crusts, the median is above mean and the distribution is skewed towards lower  
434 values. This might be explained with the fact that on bare and degraded soils, lighter rainfall  
435 events produce runoff (Mounirou, 2012). At the plot scale, the values of  $I_1$  and  $I_2$  vary  
436 between 0.58 - 10.80 and 0.06 - 0.97 (respectively) on ERO (S4 site) and G (S5 site) crusts.  
437 Moreover, at the scale of the  $BV_2$  (cultivated) sub-catchment, these values range between 0.70  
438 - 6.63 and 0.10 - 0.75 (respectively). The variation in monthly averages is not significant as  
439 the soil surface condition remain almost unchanged throughout the year on bare and degraded  
440 soils.

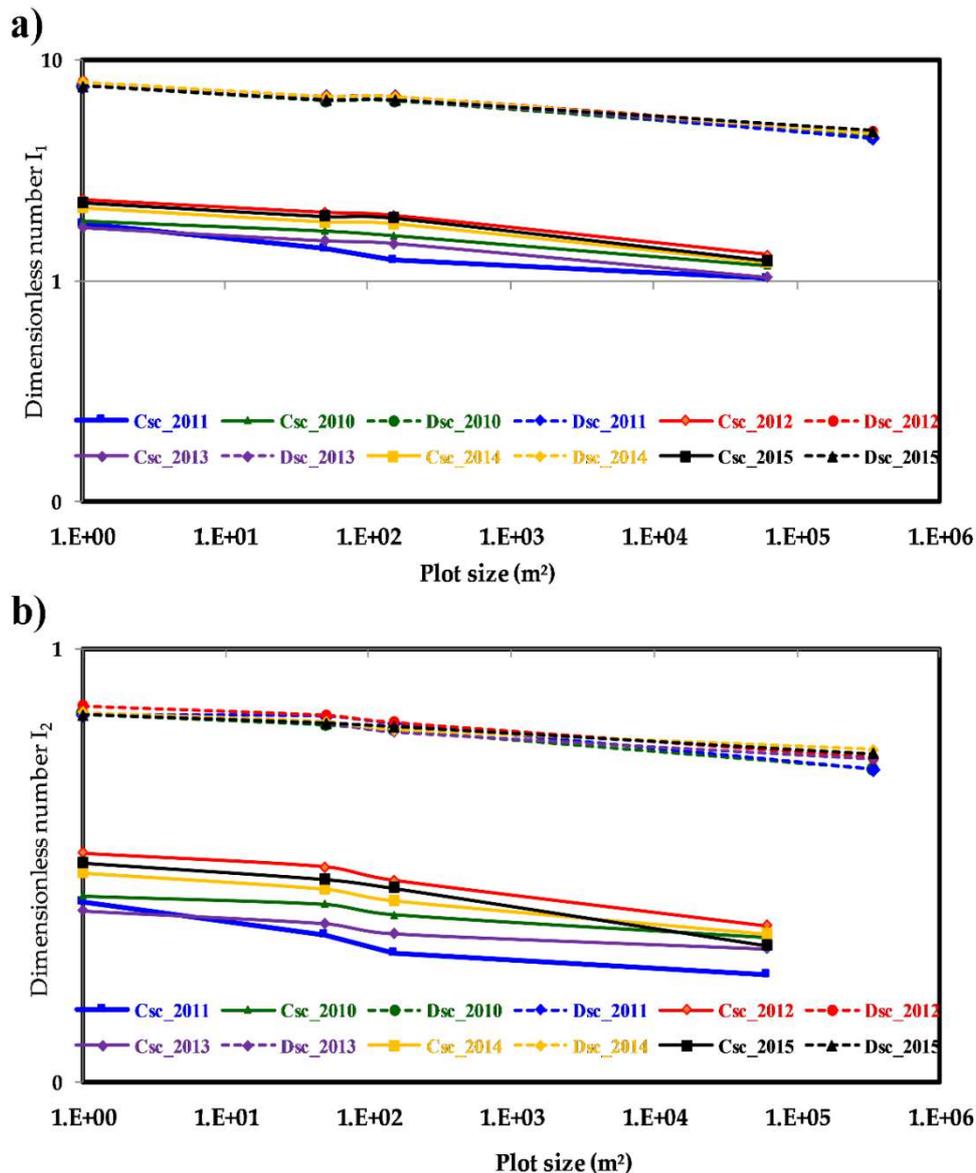


441

442 **Fig. 5.** Distribution of dimensionless indices  $I_1$  and  $I_2$  on measurement sites during the period 2010-2015 in  
 443 Tougou catchment. a) Values of the runoff potential index  $I_1$ . b) Values of the effective runoff index  $I_2$ . The  
 444 boxplots are names using the following convention: “SX” (the site names), followed by the plot size (1 m<sup>2</sup>, 50 m<sup>2</sup>  
 445 or 150 m<sup>2</sup>), followed by the letter C (cultivated) or D (bare or degraded). BV<sub>1</sub> refers to the cultivated sub-  
 446 catchment and BV<sub>2</sub> to the bare/degraded sub-catchment. BV<sub>0</sub> stands for the entire Tougou catchment. The  
 447 middle bar in the boxplots shows the median (Q2) of the distribution, whereas the black dot triangle shows the  
 448 mean. In panel b),  $I_2$  is not represented for the entire catchment as it cannot be evaluated as defined in this study due  
 449 to the heterogeneity of soil surface conditions on Tougou watershed.

450 **3.4. Scale size effect on runoff**

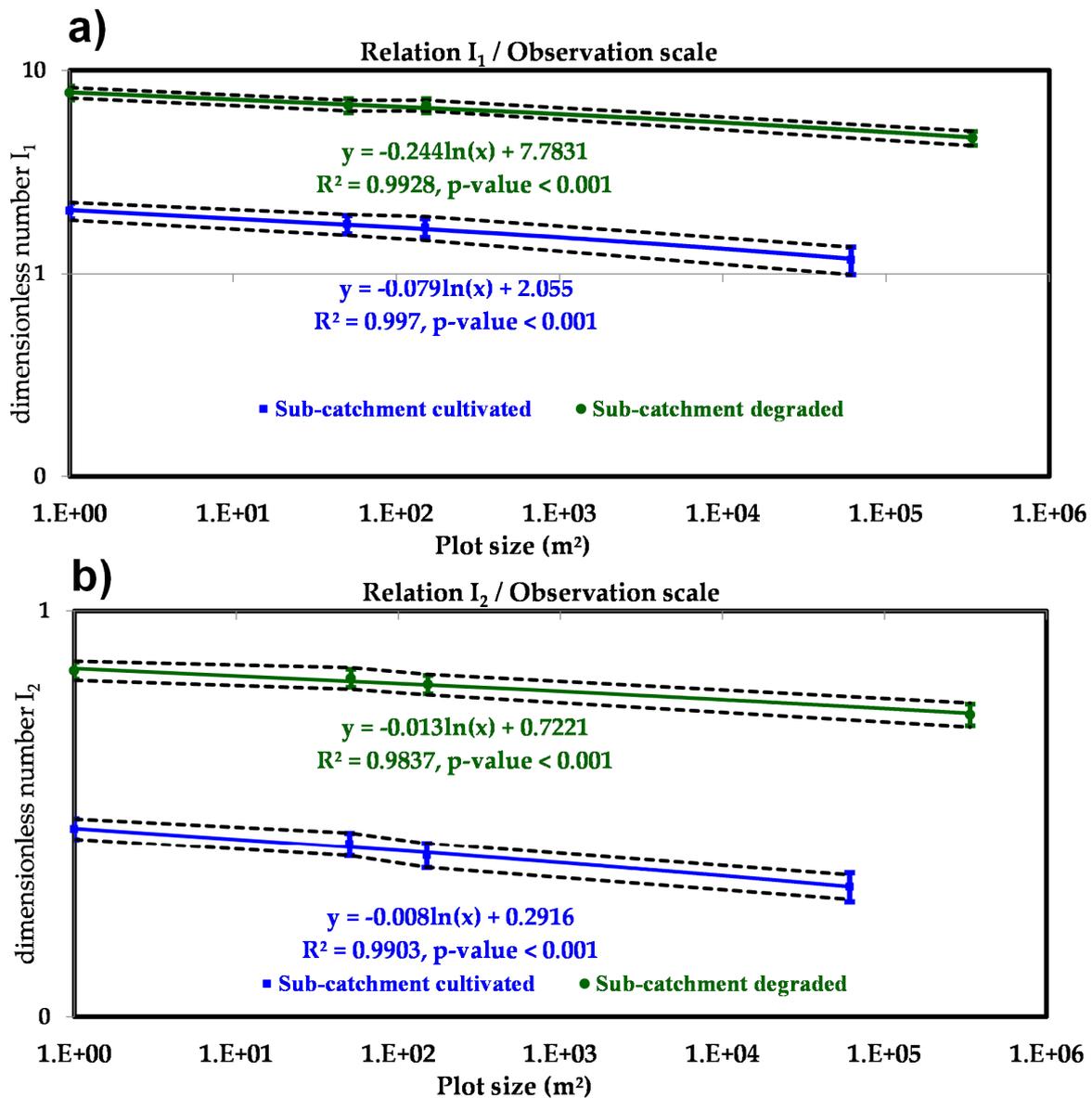
451 **Fig. 6** shows at different scales of observation (from the plot to the sub-catchment scale) the  
 452 evolution of the average annual values of the dimensionless indices for both cultivated and  
 453 degraded uncultivated soils. It appears that for each dimensionless index, there is a significant  
 454 correlation between the four scales of observation considered in this study ( $I_1$ :  $R^2 = 0.9928 -$   
 455  $0.9970$ ,  $p$ -value  $< 0.001$ ;  $I_2$ :  $R^2 = 0.9837 - 0.9903$ ,  $p$ -value  $< 0.001$ ). Also, it can be observed,  
 456 as already noted in **section 3.2**, that the spread in the values of the dimensionless indices  $I_1$   
 457 and  $I_2$  is lower for degraded and uncultivated soils than in cultivated soils.



458

459 **Fig. 6.** Evolution of dimensionless indices according to the observation scale size. (a) Relationship between the  
 460 runoff potential index  $I_1$  and the plot size. (b) Relationship between the effective runoff index  $I_2$  and the plot size.  
 461 In the two panels above, “Csc” refers to “Cultivated sub-catchment” whereas “Dsc” refers to “Degraded sub-  
 462 catchment”. Values of  $I_1$  and  $I_2$  shown in the figure are annual average for each observation scale.

463 The trend of evolution of each dimensionless index (shown in **Fig. 6**) in relation to the  
 464 observation scale size is non-linear. The logarithmic decay relationship was found to be  
 465 providing the best fit ( $R^2 > 0.98$  in all cases). **Fig. 7** shows the adjusted scaling law for both  
 466 dimensionless indices  $I_1$  and  $I_2$ .



467

468 **Fig. 7.** Logarithmic decay relationship between dimensionless indices and the scales of observation. (a)  
 469 Relationship between runoff potential index  $I_1$  and the observation scale. (b) Relationship between effective  
 470 runoff index  $I_2$  and the observation scale. The dotted lines on panels (a) and (b) indicate the width of the 95%  
 471 confidence interval around the relationships. p-values give the strength of the linear regression with the  
 472 Spearman non-parametric correlation test (at the 5% level).

#### 473 4. Discussion

474 In this study, surface runoff is analysed at various spatial scales (from the unit plot to the  
 475 catchment) and soil surface conditions to improve our understanding of the effect of the

476 observation scale on runoff production. First, our results show that surface runoff is  
477 significantly higher on bare and degraded soils than on cultivated soils. Also, on both  
478 cultivated and bare/degraded soils, surface runoff decreases when the contributing surface  
479 area increases, under similar rainfall and antecedent soil moisture conditions. At the plot  
480 scale, soil characteristics (microrelief, surface roughness, hydrodynamic parameters) are  
481 almost homogeneous and therefore, surface runoff is diffuse. At the sub-catchment and the  
482 catchment scales, due to re-infiltration into the hydrographic network and the increased  
483 heterogeneity of soil characteristics at such scales, surface runoff is anastomosed and/or  
484 concentrated. In this regard, Esteves and Lapetite (2003) showed that the runoff coefficient is  
485 significantly non-uniform in space, due to the higher variability of infiltration, surface storage  
486 capacity of the soil surface and vegetation development. Such variability occurs both in space  
487 and over time and significantly affects runoff. Moreover, these authors showed that at the  
488 local scale, infiltration and runoff are almost entirely dependent on the hydraulic properties of  
489 the crusts developing at the soil surface. Our results overall are in line with these runoff  
490 production mechanisms already reported in the Sahelian context.

491 To provide a better assessment of the scale effect, two dimensionless indices were defined in  
492 this study, based on the main factors of runoff. It is interesting to point out that various runoff  
493 indices have been proposed in the literature, mostly based on morphometric characteristics  
494 such as the shape, hydrographic network length, drainage density, slope, etc. Some notable  
495 examples include the compactness coefficient of Gravelius (1914), the Horton form index  
496 (Horton, 1932), the Schumm index (Schumm, 1956), the global slope index (Dubreuil, 1966),  
497 the topographic index (Beven, 1997). Such indices have been widely used by hydrologists to  
498 quantify the theoretical influence of the catchment morphology on their hydrological  
499 response. However, the dimensionless numbers proposed in this study allow us to account for  
500 both the catchment morphometric characteristics, but also the rainfall intensity and the soil  
501 surface hydrodynamic, which are typically known to be major factors in surface runoff  
502 formation especially for Sahelian hydrosystems (Casenave and Valentin, 1992; Karambiri et  
503 al., 2003; Zouré et al., 2019; Mounirou et al., 2020).

504 The runoff potential index  $I_l$  proposed in this study reduces the effect of the slope on the  
505 observed runoff. Indeed, it should be acknowledged that the role of slope on runoff is not  
506 clearly defined. In a handful of studies (Fox et al., 1997; Chaplot and Le Bissonnais, 2000;  
507 Mounirou et al., 2020), an increase in surface runoff with an increase in soil slope is reported.  
508 These authors attribute this effect to the decrease in soil surface storage and the decrease of

509 the ponds. As the slope increases, the running water head at the soil surface generally  
510 decreases whereas its velocity increases. However, on cultivated plots, due to the weeding  
511 operation management, the influence of the slope is moderate since the soil surface roughness  
512 and the microtopography is increased. Microtopography plays a key role in surface runoff  
513 production primarily through friction, surface storage and spatial distribution of runoff.  
514 Kamphorst et al. (2000) showed that an increase in the soil surface roughness causes an  
515 increase in friction, which will cause in turn the water head to increase and runoff velocity to  
516 decrease, as expressed in the Manning overland flow equation (Manning, 1891). On the other  
517 hand, on bare and degraded plots, the absence of ploughing leaves the soil surface roughness  
518 and the microtopography untouched. Therefore, the hydraulic slope increases with the  
519 topographic slope. On such soil surface conditions, the slope becomes a prominent factor in  
520 the surface runoff production as it affects straight the transfer time and therefore the runoff  
521 volume.

522 Conversely, some authors showed that there is a threshold above which the slope effect is  
523 shadowed by other processes. For example, Janeau et al. (2003) and Ribolzi et al. (2011)  
524 observed a decrease in runoff coefficient on tropical cultivated soils in Thailand and Laos,  
525 with slopes ranging from 16 to 63%, without rills, gullies or crust development. Moreover,  
526 these authors reported the greater compaction of the soil surface on less steep slopes, which  
527 was partly explained by the significant decrease in the rainfall kinetic energy on the sloping  
528 plot. They argue that the horizontal component of the rainfall kinetic energy, which is more  
529 important for steep slopes is transformed into shear, which would limit soil compaction for  
530 steep slopes and thereby sustain a stronger infiltration. Overall, it appears that the effect of the  
531 slope remains difficult to predict and seems to be strongly dependent on the soil surface  
532 conditions.

533 The effective runoff index  $I_2$  proposed in this study reduces the combined effect of rainfall  
534 intensity and soil surface hydrodynamic properties (saturated hydraulic conductivity, soil  
535 surface roughness, runoff length) on surface runoff observations. Several studies have  
536 demonstrated the influence of soil surface conditions on the spatial variability of surface  
537 runoff (Moreno et al., 2009; Anache et al., 2017; Langhans et al., 2019). It is also  
538 acknowledged that at the local scale, surface runoff is governed by physical laws involving  
539 surface roughness, slope and rainfall intensity (Karambiri et al., 2003; Mounirou et al., 2012,  
540 2020). Besides, Sivapalan and Wood (1986) showed that at the beginning of a rainfall event,  
541 surface runoff is majorly defined by the soil properties, which is typical of arid and semi-arid

542 Sahelian landscapes. More precisely, as a rainfall event begins, the rainfall intensity is  
543 generally lower than soil infiltration capacity, and surface runoff later appears when the  
544 infiltrated amount equals the precipitation amount. At this time, the rainfall intensity also  
545 equals the soil infiltration capacity. Hence, our effective runoff index  $I_2$  makes it possible to  
546 account for the initial losses due to infiltration and storage in micro-ponds at the soil surface.

547 The use of dimensionless numbers to assess hydrological similarity has already been  
548 investigated. Larsen et al. (1994) explained the variability of the runoff coefficient through a  
549 dimensionless index defined by the rainfall intensity and the soil characteristics. Similarly,  
550 Lyon and Troch (2010) developed a similarity parameter called the “*Péclet index*” to describe  
551 the groundwater response in small catchments. Compared to classical morphometric indices,  
552 our approach considers both the rainfall intensity, the hydrodynamic properties of soils  
553 (saturated hydraulic conductivity, surface roughness, slope, runoff length) which are known to  
554 be the main factors affecting surface runoff in typical Sahelian landscapes. It should be noted  
555 that the global scale, reflecting the combination of all local interactions, effective or not, very  
556 often hides effects of these smaller functional units. Hence, the use of such dimensionless  
557 numbers helps in reduce the differences observed at various measurement scales and therefore  
558 constitutes an attempt at normalizing such measurements across scales.

559 Also, it should be highlighted that our results highlight the non-linear nature of runoff as a  
560 result of separate contributions and interaction from factors such as spatial heterogeneity of  
561 soil hydrodynamic parameters. The scaling relationships proposed in this study are in line  
562 with previous research, which reported logarithmic decay relationship to be effective at fitting  
563 and describing physical processes such as surface runoff (Woods and Sivapalan, 1997; Labat  
564 et al., 2002; Mayor et al., 2011; Ayalew et al., 2014). Our results might also provide useful  
565 insight for parameterizing spatial variability of runoff coefficient in distributed hydrologic  
566 models (Gnouma, 2006). However, the dimensionless numbers proposed in this study requires  
567 first a physical characterization of the observation scale for which they are evaluated (area,  
568 runoff length, soil surface conditions, slope, soil surface roughness, saturated hydraulic  
569 conductivity). Also, the use of these numbers should be limited to mild slopes (0 to 3%).  
570 Moreover, the development of these dimensionless numbers on homogeneous hydrological  
571 units prevents their use on catchments with heterogeneous soil surface conditions. In such  
572 cases, additional processes such as water storage in ponds emerge as the observation scale  
573 increases (Cammeraat, 2004; Lesschen et al., 2009) and such effects are not well accounted in  
574 their actual formulations by the dimensionless indices proposed in this study. However, this

575 study shed light on the groundwork for the future development of surface runoff similarity  
576 indices which could later be improved in further research to account for spatial heterogeneity  
577 at larger scales.

## 578 **5. Conclusions**

579 The results in this study illustrate the complexity of hydrological processes and the number of  
580 factors involved in the production of runoff. Data collected from representative plots showed  
581 that infiltration is low on areas with permanent crusting (bare soil, degraded and uncultivated)  
582 and runoff amounts to more than 50% of the annual rainfall. On cultivated soil, however,  
583 runoff is less than 25% of the annual rainfall. These results also support that the location of  
584 plots on a slope strongly influences the observations. As such, the relative position of the  
585 investigated surface is of great importance in the typical Sahelian and semi-arid environment.

586 This study aimed at assessing how surface runoff evolves from the unit to the catchment scale  
587 in a typical Sahelian landscape, under semi-arid climate. Surface runoff was quantified at  
588 different spatial scales and on various soil surface conditions in the Tougou catchment.  
589 Through monitoring data collected from 2010 to 2015, hydrological similarity relationships at  
590 different observation scales were developed based on two dimensionless indices: a runoff  
591 potential index  $I_1$  and an effective runoff index  $I_2$ . These indices made it possible to reduce  
592 the scale effect and to identify functional relationships between the different scales of  
593 observation.

594 Beyond the results presented, the originality of this work lies first in the multi-scale analysis  
595 of hydrological processes, and second, in the search for similarity relations between different  
596 scales of observation through dimensional analysis. The dimensionless variables defined in  
597 this study are primarily designed to assess the hydrologic similarity in a homogeneous  
598 catchment at different spatial scales, albeit their use should be considered limited to small  
599 Sahelian catchments with mild slopes (0-3%). The dimensionless indices presented in this  
600 paper allowed characterization of runoff regardless of the spatial dimension at which it was  
601 observed. This is particularly useful in an attempt to extrapolate measurements carried at  
602 small scales to broader scales. Furthermore, a key challenge is to develop a methodology for  
603 the application of these dimensionless indices in heterogeneous landscapes.

## 604 **Data availability**

605 All the data used during the study are available upon request from the corresponding author.

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613 **Appendix A**

614 **Theoretical basis and development of dimensionless runoff indices  $I_1$  and  $I_2$**

615 In this appendix, the theoretical basis and assumptions which led to the development of the  
616 dimensionless indices proposed in this study is presented. These dimensionless numbers are  
617 developed to reduce the effect of the size of the observation scale on runoff observations,  
618 hence providing a basis to compare the respective contribution of different factors of runoff  
619 production across different scales.

620 The dimensionless indices proposed in this study are developed considering the topography,  
621 surface roughness, saturated hydraulic conductivity, rainfall amount and intensity and  
622 antecedent soil moisture (through the antecedent precipitation index and the runoff response  
623 time). Although the intensity and the rainfall amount may vary in space and time, simplifying  
624 assumptions are made in this study to consider only their average values. The theoretical basis  
625 and mathematical development leading to the expression of these dimensionless indexes  
626 detailed in this appendix. Relevant symbols and notations used in further equations are  
627 presented in **Table A.1**.

628 **Table A.1.**

629 Symbols and notations used in this appendix.

Symbol	Unit	Description
$K$	mm.h <sup>-1</sup>	Unsaturated soil hydraulic conductivity. As time increases, $K$ tends towards the saturated soil hydraulic conductivity.
$i$	mm.h <sup>-1</sup>	Instantaneous rainfall intensity at a given time $t$ .
$i_m$	mm.h <sup>-1</sup>	Average rainfall intensity.
$S_0$	-	Plot slope.
$x$	m	Distance downstream measured from the plot origin.
$L$	m	Total plot length, corresponding to the total flow length.
$n$	s.m <sup>-1/3</sup>	Manning roughness of the plot soil surface.
$h$	m	Overland runoff depth at abscissa $x$ .
$T$	s	Time.
$T_e$	s	Equilibrium time. It is the time at which all the plot surface is contributing to the observed runoff.
$v$	m.s <sup>-1</sup>	Instantaneous overland flow velocity at abscissa $x$ on the plot ( $v = dx/dt$ ).

630 Hydraulic engineers, in the late 1800s, were interested in developing rational formulations for  
 631 open channel flow. The most common formula, to date, is that of Manning-Strickler which  
 632 assumes that the flow is uniform, that is to say the pressure drop is due to the slope of the  
 633 channel  $S_0$  and the hydraulic radius  $R_h$ , as shown in **Equation A.1** (Chanson, 2004):

$$v = \frac{\sqrt{S_0} R_H^{2/3}}{n} \quad (\text{A.1})$$

634 where  $v$  (m.s<sup>-1</sup>) is the flow velocity,  $S_0$  is the channel slope,  $R_H$  (m) the hydraulic radius and  $n$   
 635 (s.m<sup>-1/3</sup>) the Manning roughness coefficient. This formula relates the flow velocity to the  
 636 square root of the channel slope  $S_0$ . As such, one can identify two runoff governing  
 637 parameters: the slope and the roughness or soil surface condition (in case of overland flow).

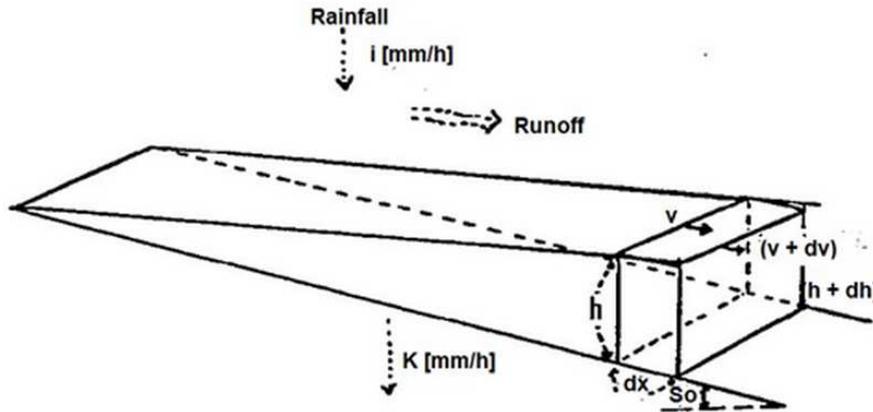
638 If we assume a very large cross-section flow and also assume this cross section is of  
 639 rectangular form shape, where the flow depth  $h$  is very small as compared to the flow width  $b$ ,  
 640 the hydraulic radius is further reduced to the flow height, as shown in **Equation A.2**:

$$R_H = \frac{b h}{b + 2 h} \cong h \quad (\text{A.2})$$

641 where  $b$  (m) is the flow width and  $h$  (m) is the flow depth. This hypothesis simplifies  
 642 **Equation A.1** which is now reduced to the form shown in **Equation A.3**:

$$v = \frac{\sqrt{S_0} h^{2/3}}{n} \quad (\text{A.3})$$

643 Let us consider an experimental plot case under a specific rainfall event illustrated in **Fig.**  
644 **A.1.**



645  
646 **Fig. A.1.** Conceptual representation of a rainfall event occurring on a plot and triggering surface runoff. Adapted  
647 from Guillobez (1990).

648 At a given time  $t$  after the onset of a rainfall event, at a distance  $x$  from the upstream plot  
649 origin, the instantaneous runoff height observed is  $h$ , flowing at velocity  $v$ . After a small  
650 amount of time increment  $dt$ , the cross-section of water has moved by a small increment in  
651 distance  $dx$ . The velocity has increased by  $dv$  and is now  $v + dv$ . The water height, because of  
652 the rainfall input received and the losses by infiltration along the flow path travelled  $dx$ , has  
653 now a height of  $h + dh$ . The continuity equation (mass conservation), yields **Equation A.4:**

$$(v + dv) (h + dh) = v h + (i - K) dx \quad (\text{A.4})$$

654 Neglecting second order product term ( $dh \times dv$ ), **Equation A.4** is further reduced to **Equation**  
655 **A.5:**

$$h dv + v dh = (i - K) dx \rightarrow d(h v) = (i - K) dx \quad (\text{A.5})$$

656 Based on **Equation A.3**, **Equation A.5** can be rewritten as follows (**Equations A.6-A.8**):

$$h = \left( \frac{n v}{\sqrt{S_0}} \right)^{3/2} \rightarrow d \left[ v \left( \frac{n v}{\sqrt{S_0}} \right)^{3/2} \right] = (i - K) dx \quad (\text{A.6})$$

$$\left( \frac{n}{\sqrt{S_0}} \right)^{3/2} d [v^{5/2}] = (i - K) dx \quad (\text{A.7})$$

$$\frac{5}{2} \left( \frac{n}{\sqrt{S_0}} \right)^{3/2} v^{3/2} dv = (i - K) dx \quad (\text{A.8})$$

657 Dividing both left-hand and right-hand terms by  $dt$  and replacing velocity  $v$  by  $dx/dt$ ,  
 658 **Equation A.8** is further rewritten as **Equation A.9**:

$$\frac{5}{2} \left( \frac{n}{\sqrt{S_0}} \right)^{3/2} \left( \frac{dx}{dt} \right)^{3/2} \frac{d^2x}{dt^2} = (i - K) \frac{dx}{dt} \quad (\text{A.9})$$

659 Simplifying **Equation A.9** by  $dx/dt$  brings the differential equation shown in **Equation A.10**:

$$\frac{5}{2} \left( \frac{n}{\sqrt{S_0}} \right)^{3/2} \left( \frac{dx}{dt} \right)^{1/2} \frac{d^2x}{dt^2} = (i - K) \quad (\text{A.10})$$

660 Further, by noticing the equivalence shown in **Equation A.11**:

$$\left( \frac{dx}{dt} \right)^{1/2} \frac{d^2x}{dt^2} = \frac{2}{3} \frac{d}{dt} \left( \frac{dx}{dt} \right)^{3/2} \quad (\text{A.11})$$

661 **Equation A.10** can now be rewritten into **Equation A.12**:

$$d \left( \frac{dx}{dt} \right)^{3/2} = \frac{3}{5} \left( \frac{\sqrt{S_0}}{n} \right)^{3/2} (i - K) dt \quad (\text{A.12})$$

662 In reality,  $i$  and  $K$  varies as a function of time  $t$ . However, when  $t$  is large,  $i$  and  $K$  tend  
 663 respectively to the average rainfall intensity ( $i_m$ ) and the saturated hydraulic conductivity ( $K_s$ ).  
 664 By integrating **Equation A.12** over time, **Equations A.13** and **A.14** are obtained.

$$\left( \frac{dx}{dt} \right)^{3/2} = \frac{3}{5} \left( \frac{\sqrt{S_0}}{n} \right)^{3/2} \int_0^t (i - K) dt = \frac{3}{5} \left( \frac{\sqrt{S_0}}{n} \right)^{3/2} (i_m - K_s) t \quad (\text{A.13})$$

$$v = \left(\frac{dx}{dt}\right) = \left(\frac{3}{5}\right)^{2/3} \frac{\sqrt{S_0}}{n} (i_m - K_s)^{2/3} t^{2/3} \quad (\text{A.14})$$

665 Integrating **Equation A.14** over time yields **Equation A.15**:

$$x = \left(\frac{3}{5}\right)^{5/3} \frac{\sqrt{S_0}}{n} (i_m - K_s)^{2/3} t^{5/3} \quad (\text{A.15})$$

666 **Equation A.14** relates the flow velocity  $v$  at distance  $x$  to the time  $t$ . This velocity is as high  
 667 as the slope of the plot is steep, or the rainfall duration is long, or the rainfall intensity is high  
 668 or the roughness is low. **Equation A.15** relates distance  $x$  to the time  $t$ . Knowing the dripping  
 669 length (or the plot length) helps in estimating the equilibrium time  $T_e$  whose value is at  
 670 minimum equal to the concentration time given by **Equation A.16**:

$$T_e = 5/3 \left( \frac{n L}{(i_m - K_s)^{2/3} \sqrt{S_0}} \right)^{3/5} \quad (\text{A.16})$$

671 The term  $T_e$  in **Equation A.16** can be rewritten as given by **Equation A.17** (also **Equation 6**  
 672 in this paper, Julien and Moglen, 1990):

$$T_e = \beta \left( \frac{L}{\alpha \times i^{\beta-1}} \right)^{1/\beta} \quad (\text{A.17})$$

673 where  $L$  ( $m$ ) is the plot length,  $i = i_m - K_s$  is the infiltration excess,  $\alpha$  and  $\beta$  are parameters.  
 674 Combining Manning resistance turbulent flow equation with a kinematic wave approximation  
 675 yields  $\beta = 5/3$  (Julien and Moglen, 1990). Parameter  $\alpha$ , on the other hand, is given by  
 676 **Equation A.18** (also **Equation 7** in this paper):

$$\alpha = \frac{1}{n} \times \sqrt{S_0} \quad (\text{A.18})$$

677 where  $S_0$  is the plot slope and  $n$  [ $s.m^{-1/3}$ ] is the Manning roughness coefficient.

678 Concentration time is therefore as high as the slope is mild, the rainfall intensity is low and  
 679 the soil surface is rough. It also increases as the plot length increases. It can therefore be

680 concluded that the overland flow velocity at distance  $x$ , also called *runoff intensity*, is a  
681 function of the four following parameters:

- 682 • the relative rainfall intensity, also called *excess precipitation*,
- 683 • the soil surface roughness,
- 684 • the slope of the plot,
- 685 • the rainfall event duration.

686 In this article, we sought to reduce these flow-related variables to two dimensionless numbers  
687 to reduce the effect of the size of the observation plot. Although the intensity and the rainfall  
688 amount vary in both space and time, simplifying assumptions have been made to consider  
689 only the average values. The two dimensionless indexes  $I_1$  and  $I_2$  are therefore defined as  
690 follows:

691 (i) the runoff potential index  $I_1$  which is the ratio of the runoff coefficient of the plot to  
692 the square root of its slope. It expresses the potential for runoff from the plot while  
693 reducing the effect of microrelief (explicitly the slope) on runoff production. Its  
694 formulation is given in **Equation 4** (in the paper).

$$I_1 = \frac{K_r}{\sqrt{S_0}} \quad (4)$$

695 (ii) the dimensionless number  $I_2$  which is the ratio of the depth of overland flow  $R$  ( $mm$ )  
696 measured at a given observation scale to the term  $(P - K_s \times T_e)$  where  $P$  ( $mm$ ) is the  
697 rainfall amount,  $K_s$  ( $mm.h^{-1}$ ) the saturated hydraulic conductivity and  $T_e$  ( $h$ ) the  
698 equilibrium time.  $I_2$  is given in **Equation 5** (in the paper).

$$I_2 = \frac{R}{P - K_s \times T_e} \quad (5)$$

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