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Mechanism of O₂ influence on the decomposition process of the eco-friendly gas insulating medium C₄F₇N/CO₂

Fanchao Ye, Yitian Chu, Pascal Brault, Dunpin Hong, Shuangshuang Tian, Yi Li, Song Xiao, Xiaoxing Zhang

Abstract—The C₄F₇N/CO₂/O₂ gas mixture is the most promising eco-friendly gas insulation medium available. However, there are few studies on the mechanism of the influence of the buffer gas O2 ratio and its role in the decomposition characteristics of C₄F₇N/CO₂. In this paper, based on the ReaxFF reaction molecular dynamics method and density functional theory, a simulation of the thermal decomposition process of the C₄F₇N/CO₂ mixture under different O₂ ratios was carried out at temperatures in the range 2000 - 3000 K. A constructed model of the C₄F₇N/CO₂/O₂ mixture reaction system was used that included the possible reaction paths, product distribution characteristics and their generation rates. The calculation results show that the thermal decomposition of C₄F₇N/CO₂/O₂ mainly generates species such as CF₃, CF₂, CF, F, C₂F₅, C₂F₄, C₂F₂, C₃F₇, C₂F₂N, C₃F₄N, CFN, CN, CO, O, and C. Among them, the two particles CF₂ and CN are the most abundant. The first decomposition time of C₄F₇N is advanced by the addition of O2, while the amount of C_4F_7N decomposed and the generation of major decomposed particles decreases. The addition of 0%-4% of O₂ decreases the reaction rate of the main decomposition reaction in the reaction system. Quantum chemical calculations show that the dissociation process occurring from the combination of C₄F₇N with O atom is more likely to occur compared to the direct dissociation process of C₄F₇N molecules. The conclusions of this study provide a theoretical basis for the optimization of the application ratio of C₄F₇N/CO₂/O₂ and the diagnosis of its equipment operation and maintenance.

Index Terms—C₄F₇N/CO₂/O₂; Decomposition mechani sm; DFT; MD simulation

I. INTRODUCTION

S ulphur hexafluoride (SF_6) is widely used in all kinds of gas-insulated electrical equipment thanks to its excellent insulation properties and arc extinguishing ability [1]. However, SF_6 gas is an extremely potent greenhouse gas, with a GWP (Global Warming Potential)

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23,500 times that of CO₂ and an atmospheric lifetime of up to 3,200 years [2][3]. As a possible SF₆ gas replacement, $C_4F_7N/CO_2/O_2$ gas mixture, the most promising eco-friendly gas insulating medium, has already demonstrated its ability in gas-insulated equipment in power systems around the world [4][5][6][7].

Some results have been obtained from experimental studies on the insulation, arc extinguishing and decomposition characteristics of C4F7N/CO2/O2 gas mixtures. Zhang et al. carried out short-circuit current breaking tests on a 40.5 kV ceramic column circuit breaker filled with a $C_4F_7N/CO_2/O_2$ gas mixture, and found that increasing the O_2 content improved the breaking performance of the gas mixture by 10% [8]. Earlier experimental studies on the insulating properties of $C_4F_7N/CO_2/O_2$ gas mixtures with different O_2 contents, air pressures and electric fields were carried out by Gao, Tu and Zhang et al., who analyzed the influence of different factors on the breakdown voltage and partial discharge inception voltage of the gas mixtures. They found that a certain content of O₂ could effectively improve the insulating properties of C_4F_7N/CO_2 gas mixtures [9][10][11][12]. Yang et al. the decomposition investigated characteristics of C₄F₇N/CO₂/O₂ gas mixture under suspension discharge and found that the inhibition effect on C₄F₇N decomposition was most obvious when the volume fraction of O_2 was 4% [13]. Ye et al. investigated the local superheated decomposition of a C₄F₇N/CO₂/O₂ gas mixture and found that the volume fraction of all products except C₃F₆ decreased to different degrees when 2% O2 was added to the C4F7N/CO2 gas mixture [14].

Macro-level experimental studies have shown that the addition of a certain amount of O_2 can effectively improve the insulation, arc extinguishing performance and chemical stability of C_4F_7N/CO_2 gas mixtures [4][5][8]. The effect of

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O₂ addition on the decomposition characteristics of $C_4F_7N/CO_2/O_2$ is essentially due to the large differences in the microchemical processes of the breakdown of $C_4F_7N/CO_2/O_2$ under the effect of changes in the O₂ content and other influencing factors, which could not be revealed by experimental studies. Fu et al. revealed the mechanism of the influence of O atoms on the decomposition process of C₄F₇N by calculating the thermodynamic parameters of different reaction paths [15]. However, they did not consider the influence of O2 molecules and their content variations on the decomposition process of the C₄F₇N/CO₂ reaction system. For larger reaction systems consisting of molecules with complex structures, molecular dynamics methods are suitable for calculating their chemical reaction processes. Zhang et al. and Liu et al. investigated the distribution pattern of decomposed particles of C₄F₇N/CO₂ gas mixtures based on the combination of molecular dynamics (MD) and quantum chemistry of the ReaxFF reaction [16][17]. They did not take into account, however, the effect of the addition of O₂ as a buffer gas on the decomposition process of the whole reaction system.

In this paper, the molecular dynamics simulation of the ReaxFF reaction was carried out through the constructed thermal decomposition model of the $C_4F_7N/CO_2/O_2$ gas mixture, and the composition, distribution and generation rate of particles of thermal decomposition of the gas mixture with different O_2 content and different temperatures were obtained. Based on density functional theory and transition state theory, the thermodynamic parameters of the decomposition process were obtained under the conditions of O_2 participation in the reaction. They revealed the decomposition process of C_4F_7N and the mechanism of the product generation with the addition of O_2 .

II . METHODS

A. ReaxFF calculation method

The ReaxFF reactive force field expresses the interactions between atoms in a reactive system as a function of bond level on the basis of the bond order (BO), i.e., the interaction energy of each part of the molecule is expressed in the form of bonding poles. The energy expression of the system is as follows [18]:

$$E_{system} = E_{bond} + E_{over} + E_{angle} + E_{torsion} + E_{vdWaals} + E_{coulomb} + E_{specific}$$
(1)

where E_{system} is the total system energy; E_{bond} is the bond energy term between the atoms; E_{angle} and $E_{torsion}$ represents the three-bond correction energy term and the four-body energy action term, respectively; E_{over} is an over-coordination energy correction term; $E_{vdwaals}$ and $E_{coulomb}$ are van der Waals and Coulomb terms, respectively, which describe the electrostatic and dispersive effects in the interaction, and are non-bonding terms; $E_{specific}$ is usually used for energy terms for specific systems, such as lone pair electrons, conjugated electrons, hydrogen bonding and C2 correction terms.

A 260Å*260Å*260Å periodic simulation box was first constructed. The whole reaction system contained 500 molecules including 75 C₄F₇N molecules (15%). The ReaxFF-MD simulations were carried out by varying the O₂ content (0%, 2%, 4%, 6%, 8%, and 10%, considering the stability of C₄F₇N, the oxygen content should not exceed 10%) at a temperature of 2600 K and varying the simulated temperatures (2000 K, 2200 K, 2400 K, 2600 K, 2800 K, and 3000 K) for a given O₂ content (6%) of the C₄F₇N/CO₂/O₂ mixture. The composition of reactant particles in the simulated system, the temperature settings and the system density are shown in Table I

	Number of		Number of		Number			
NO.	C ₄ F ₇ N	Percentage	CO_2	Percentage	of O_2	Percentage	Temperature	Density
	molecules		molecules		molecules			
1	75	15%	425	85%	0	0%	2600	0.003148
2	75	15%	415	83%	10	2%	2600	0.003137
3	75	15%	405	81%	20	4%	2600	0.003125
4	75	15%	395	79%	30	6%	2600	0.003114
5	75	15%	385	77%	40	8%	2600	0.003103
6	75	15%	375	75%	50	10%	2600	0.003091
7	75	15%	395	79%	30	6%	2000	0.003114
8	75	15%	395	79%	30	6%	2200	0.003114
9	75	15%	395	79%	30	6%	2400	0.003114
10	75	15%	395	79%	30	6%	2800	0.003114
11	75	15%	395	79%	30	6%	3000	0.003114

 Table I

 MODELLING SYSTEM REACTANT PARTICLE COMPOSITION

Firstly, based on the NVE system (i.e. the values of the number of atoms, the size of the reaction system and the energy are fixed), the geometry of the system was optimised at 20K for 10 ps (closed system, no heat exchange with the outside) to establish a more reasonable initial structure of the reaction. The optimized reaction systems of 15%C4F7N/85%CO2 and 15%C₄F₇N/79%CO₂/6%O₂ are shown in Fig 1. Subsequently, equilibrium calculations were carried out for the system at 1000 K for 10 ps based on the NVT system (with constant values for the number of atoms, the size of the reaction system and the temperature). Finally, ReaxFF-MD was carried out for the C₄F₇N/CO₂/O₂ gas mixture system at different O₂ contents (0%-10%) and temperature intervals of 2000K-3000K. Considering the computational resources as well as the simulation results, the total duration of the simulation is 500 ps with a sampling step of 0.25 fs. The NVT system was used for simulation and the Berendsen temperature control method was chosen for the temperature control procedure. All Reax FF-MD simulations in this paper are based on the ReaxFF module in the cross-scale computational chemistry platform AMS (Amsterdam Density Functional) [19]. The force-field files were optimised using Monte Carlo methods based on NiCH.ff developed by Mueller et al. in conjunction with the properties of the C₄F₇N molecule [20].



Fig. 1. Optimized reaction system model (a) $15\%C_4F_7N-85\%CO_2$ (b) $15\%C_4F_7N-79\%CO_2-6\%O_2$

B. Density functional theory

Density functional theory (DFT) and transition state (TS) theory based on quantum chemistry can provide theoretical support for calculating the microscopic parameters of the decomposition process of the decomposition process and revealing the decomposition of the C₄F₇N discharge and the product generation mechanism under the O₂ participation in the reaction. In this paper, the decomposition mechanism of C₄F₇N/CO₂/O₂ was calculated based on DFT and TS. The Dmol³ module of Materials Studio was used in order to obtain the energy and reaction enthalpies of the proposed reaction pathways. Geometry optimization and harmonic frequency calculation were based on the generalized gradient approximation and Perdew-Burke-Ernzerhof (GGA-PBE) methods [21]. Dual numerical plus polarization (DNP) was chosen as the basis group. The activation energy of the transition state reaction was obtained by searching the transition state of the proposed path using LST and QST methods [22].

III. RESULTS AND DISCUSSION

A. Kinetic analysis of the effect of O_2 on C_4F_7N /CO₂/O₂ thermal decomposition particles

As the simulation temperature selected in this paper was 2000K-3000K, the temperature will not affect the reaction sequence or the reaction mechanism. However, in order to ensure completion of the chemical reaction process, a median temperature of 2600K was selected to carry out the kinetic analysis of the effect of O2 on the thermal decomposition of C₄F₇N/CO₂/O₂ particles. The changes of C₄F₇N and various types of decomposed particles in the C₄F₇N/CO₂/O₂ reaction system with different ratios of O₂ at 2600 K with simulation times are given in Fig. 2, and the number of each particle at the end of the simulated reaction is also given. It can be seen that a total of 18 particles, namely CF₃, CF₂, CF, F, CF₃CF₂ (C₂F₅), CF_2CF_2 (C_2F_4), C_2F_2 , (CF_3)₂CF, C_2F , CF_2CN , CF_3CFCN (C₃F₄N), CFN, CNO, CN, CO, O, C and C₂, were generated in the 15% $C_4F_7N/85\%$ CO₂ system at the end of the reaction. The number of decomposed particle species in the reaction system after the addition of O₂ depended on its ratio and was 14 (2% O₂), 15 (4% O₂), 16 (6% O₂), 13 (8% O₂) and 11 (10% O₂), respectively. The number of particle species in the reaction system basically shows a decreasing trend with the increase in O₂ content, indicating that the addition of O₂ can inhibit the generation of some particles to a certain extent. The main decomposition particles under different O₂ ratios are CF₃, CF₂, CF, F, CN and C_2F_5 (the number of particles is greater than 5). The production of O-containing products is relatively small, and COF₂ (carbonyloxyfluoride) is generated only when 6% O₂ and 8% O₂ are added, the number of COF₂ particles is 1 after 500 ps





Fig. 2. Time evolution of $C_4F_7N/CO_2/O_2$ thermal decomposition particles with different O_2 contents at 2600k temperature. Numbers in brackets are the final values.

In the 15% C₄F₇N/85% CO₂ system, the decomposition of C₄F₇N begins at 1.4 ps to form CF₃ and CF₃CFCN, and at 4.7 ps to form C₃F₇ and CN. The decomposition of C₄F₇N to form CF_3CF_2 and CF_2CN at a reaction time of 5.8 ps is not a simple one-time dissociation reaction: there is a transition state during the reaction. This reaction is more difficult than the dissociation reactions that occur at 1.4 ps and 4.7 ps. As the simulation time increases, CF₃CFCN further decomposes to form CF₃, CF and CN, and CF₃ further decomposes to form CF₂ and F. Therefore, the maximum number of particles of CF_3CFCN (C_3F_4N) at the end of the reaction is only 3 and decreases after the addition of O₂, suggesting that the addition of O₂ may accelerate the decomposition of CF₃CFCN, resulting in the generation of the predominantly several particles were CF3, CF2, CF, F, CN and C_2F_5 . When 2% O_2 was added to the C_4F_7N/CO_2 system, the decomposition of C₄F₇N started to produce CF₃CF₂ and CF₂CN at 0.75 ps and CF3 and CF3CFCN at 1.1 ps, showing that the addition of O₂ can advance the initial dissociation time of C₄F₇N compared with that of the case without O₂. Since the decomposition of C₄F₇N to form CF₃CF₂ and CF₂CN involves a transition state, it indicates that the addition of O₂ makes the decomposition process of C₄F₇N more complicated from the early stage of the reaction.



Fig. 3. Changes in C_4F_7N particle number in reaction systems under different O_2 content (a) Trend with simulation time. (b) Trend with O_2 content at the end of the reaction

Fig 3(a) gives the variation of the number of C_4F_7N particles in the reaction system with reaction time for different

O₂ ratios. It can be seen that with the increase in simulation time, the decomposition of C_4F_7N with different O_2 ratios gradually increases, so the number of C₄F₇N particles in the reaction system decreases. It can be clearly seen that the decomposition rate (slope of the particle number versus time curve) accelerates at simulation times greater than 250 ps, especially in O₂-free conditions. Fig 3(b) gives the change in the decomposition amount of C₄F₇N in the system at the end of the reaction with the O₂ content. It can be seen that after the addition of O2, the decomposition amount of C4F7N was clearly reduced and showed an overall decreasing trend with the increase in O₂ ratio, reaching a minimum at 6% O₂. Only 30 C₄F₇N molecules were decomposed, which is 30.2% less compared with the decomposition of 43 C₄F₇N molecules before the addition of O₂, indicating that the addition of a certain content of O₂ can effectively inhibit the decomposition of C₄F₇N.

In order to further investigate the influence of O_2 on the reaction rate of the system, the reaction rate constants k for some of the reaction paths involved in several major decomposing particles were calculated by the chemical reaction analysis algorithm ChemTraYzer 2 in the Advanced Work Flow module of the AMS software. The results are shown in Table II. As an important physical quantity in kinetic analysis, the rate constant k It can be seen that the reaction rates of paths 1-3 in Table II exhibit a decreasing trend at 0%-4% O₂ in the reaction system, and the reaction rate starts to increase for an O_2 ratio greater than 6%. At 10% O_2 , there is an order of magnitude change in the reaction rate of path 3 compared to the other O₂ ratios. The reaction rate of path 4 decreases at 0%-8% O₂ in the reaction system and increases at 10% O₂. The addition of O₂ accelerates the reaction path 6. Overall, the addition of 0%-4% O₂ decreases the reaction rates of most of the decomposition reactions, but an O₂ ratio greater than 8% accelerates these reactions.

 Table II.

 DIFFERENT CONTENTS OF O2 RATE CONSTANT (2600K)

NO		Rate constant, k (cm ³ ·mol ⁻¹ ·s ⁻¹)						
NO.	The reaction path	0% O ₂	2% O ₂	4% O ₂	6% O ₂	8% O ₂	10% O ₂	
1	$C_4F_7N \rightarrow CF_2CN + CF_3CF_2$	2.75E+09	2.04E+09	1.83E+09	1.92E+09	2.02E+09	2.83E+09	
2	$C_4F_7N \rightarrow CF_3 + C F_3CFCN$	2.03E+09	1.48E+09	1.47E+09	1.73E+09	1.71E+09	2.21E+09	
3	CF ₂ CN→CF ₂ +CN	8.35E+11	7.63E+11	4.47E+11	4.66E+11	5.91E+11	6.15E+12	
4	$CF_2CF \rightarrow F + CFCF$	1.30E+12	1.03E+12	9.94E+11	5.76E+11	3.08E+11	1.33E+12	
5	$CF_3CF_2 \rightarrow CF_2 + CF_3$	4.84E+09	3.25E+09	4.47E+09	9.18E+09	8.40E+08	5.45E+09	
6	CO ₂ →CO+O	9.47E+06	9.69E+06	1.51E+07	1.53E+07	1.05E+07	-	

B. Kinetic analysis of the effect of temperature on $C_4F_7N/CO_2/O_2$ thermal decomposition particles

The variation in the number of C_4F_7N particles in the reaction system with simulation time at different temperatures is given in Fig. 4(a). It can be seen that the decomposition rate of C_4F_7N accelerates significantly with the increase in simulation temperature. Fig. 4(b) gives the variation in the amount of C_4F_7N decomposition in the system at the end of the reaction with the simulation temperature. The number of particle species generated by the decomposition of C_4F_7N at different

temperatures are 8 (2000K), 15 (2200K), 29 (2400K), 30 (2600K), 41 (2800K), and 48 (3000K), respectively, showing that at the simulation temperature in the range of 2200K-2400K, the decomposition rate of C_4F_7N is faster, with little change between 2400K and 2600K, and that it continues to increase when it is greater than 2600K. This indicates that the decomposition of C_4F_7N will reach a plateau when the simulated temperature increases to a certain interval, and that it is necessary to continue to increase the temperature in order to promote the decomposition of C_4F_7N .



Fig.4. Changes in C_4F_7N particle number under different temperature conditions (a) Trend with simulation time. (b) Trend with temperature at the end of the reaction

Table III shows the main thermal decomposition molecules of $C_4F_7N/CO_2/O_2$ containing 6% O_2 at different simulated temperatures. It can be seen that the two most abundant particles generated are CF_2 and CN, followed by CF_3 and F. The generation of C_2F_5 and CN shows a uniform increase with temperature and simulation time. It can be seen that the amount and rate of generation of CF_3 particles at the simulated temperature of 3000K is much larger than at other temperatures. CF_3 particles come from direct dissociation reactions of C_4F_7N , CF_3CFCN and C_2F_5 particles on the one hand, and recombination of CF_2 and F particles on the other hand, and these dissociation and recombination reactions are intensified by an increase in the energy of the reaction system when the simulated temperature reaches 3000 K. The production rate of CF_2 is slow at the simulated temperatures of 2000K and 2200K. Its production rate increases substantially only when the simulation time is greater than 450 ps, and is accelerated significantly when the temperature is greater than 2200 K. The CF and F particles follow the same trend with temperature, and their production starts to increase rapidly at temperatures above 2400K.

 Table III

 GENERATION OF THE MAIN THERMAL DECOMPOSITION

 PARTICLES AT DIFFERENT SIMULATED TEMPERATURES (6%O2)

Temperature	Particle species							
(K)	CF ₃	CF_2	CF	F	C_2F_5	CN	0	СО
2000	4	7	1	4	4	7	0	0
2200	1	13	3	2	14	14	0	0
2400	8	29	4	4	21	25	0	1
2600	14	32	6	6	16	26	4	3
2800	17	39	13	19	22	36	5	11
3000	29	44	16	27	17	45	1	4

Overall, the results of ReaxFF-MD simulations of the thermal decomposition process of the C₄F₇N/CO₂/O₂ mixture show that although the addition of O_2 to the C_4F_7N/CO_2 mixture decreases the initial decomposition time of C₄F₇N, it can effectively reduce the amount of decomposition and most of the particles generated, especially at an O₂ ratio of 6%, which results in the lowest amount of C₄F₇N decomposition. Moreover, the addition of 0%-4% O2 decreases the reaction rates of the major decomposition reactions in the reaction system, whereas O₂ levels greater than 8% accelerate these reactions. At simulated temperatures greater than 2600 K, the initial decomposition time of C₄F₇N is significantly reduced and the rate of decomposition particle generation is accelerated. From the simulation results at different O₂ ratios and at different temperatures, it can be seen that the two most abundant particles generated are CF₂ and CN, followed by CF₃ and F.

C. Decomposition mechanism based on quantum chemical calculation

From the above findings, it can be seen that the addition of O2 as a background gas to the C4F7N/CO2 mixture will have a significant effect on its decomposition particle distribution pattern and generation rate, so the dissociation of C₄F₇N under the conditions of O particles participating in the reaction and the recombination process of each particle after dissociation and its thermodynamic parameters are of important significance. Density functional theory and transition state theory based on quantum chemistry will provide energy barrier heights as well as the chemical pathways under the conditions of O₂ addition, and further reveal the decomposition and product generation mechanism of C₄F₇N with O₂ addition. To reveal the reaction mechanism of the C₄F₇N/CO₂ mixture with O₂ addition, 13 possible decomposition paths and 10 possible generation paths of O-containing products were constructed based on the structural characteristics of the C₄F₇N molecule. The C₄F₇N dissociation pathway with O addition is shown in Fig 5 (the molecules involved in the pathway are optimized configurations), and the enthalpies and activation energies under different pathways are shown in Table IV.



Fig. 5. C₄F₇N dissociation pathways under O-atom reactions

According to the results of the molecular dynamics simulation of the reaction above, the decomposition process of C₄F₇N becomes more complicated with the addition of O₂. In particular, the initial dissociation process is not a simple onetime dissociation process, but goes through a transition state. Firstly O₂ may react with C₄F₇N in the form of O particles. The formation process and enthalpy of O particles are given in Fig 5 and Table IV, respectively, which show that O particles originate from the dissociation of CO₂ and O₂ in the gas mixture. The dissociation of CO₂ to generate O particles requires the absorption of 153.07 kcal/mol of energy, which is more likely to occur compared to the dissociation of O₂ to generate O particles, which requires the absorption of 182.29 kcal/mol energy. As the difference is not large, both are the main source of O particle generation. However, the further generation of C and O particles from CO requires the absorption of 514.60 kcal/mol of energy and occurs only at higher temperatures.

N		$\Delta_r H$	ΔH
NO.	The reaction path	(kcal/mol)	(kcal/mol)
D 1	$C_4F_7N+O \rightarrow CF_3+CF_3COFCN$	-106.52	47.51
D 2	$CF_3COFCN \rightarrow CF_3COCN+F$	57.17	
D 3	$CF_3COFCN \rightarrow CF_3+COFCN$	7.97	-
D 4	CF ₃ COFCN→CF ₃ COF+CN	20.54	-
D 5	CF ₃ COCN →C F ₃ CO+CN	211.86	
D 6	$CF_3CO \rightarrow CF_3+CO$	-41.36	
D 7	$CF_3 \rightarrow CF_2 + F$	92.96	
D 8	$CF_2 \rightarrow CF + F$	131.27	
D 9	COFCN →COF+CN	134.38	-
D10	$CF_3COF \rightarrow CF_3 + COF$	85.28	-
D11	$CO_2 \rightarrow CO+O$	153.07	
D12	CO→C+O	514.60	
D13	$O_2 \rightarrow O+O$	182.29	

Path 1 in Table IV gives the initial dissociation process of C_4F_7N when O particles are involved in the reaction. The reaction produces CF_3 and CF_3COFCN particles. This reaction

needs to undergo the transition state structure of CF₃COFCNCF₃, with the enthalpy of the reaction of -106.52 kcal/mol, and the need to overcome the energy barrier of 47.51 kcal/mol for this reaction to proceed properly. It has been shown that the dissociation of C₄F₇N molecules to form CF₃ and CF₃CFCN particles requires the absorption of 73.14 kcal/mol of energy [23]. The activation energy of path 1 is much lower than 73.14 kcal/mol, indicating that the participation of O particles in the reaction makes the bond breaking process of C₄F₇N easier. Therefore, O₂ has a negative effect on the stability of C₄F₇N.

The CF₃ and CF₃COFCN particles dissociate further, and the three primary dissociation paths (D2, D3 and D4) and their enthalpies for CF₃COFCN are given in Table 4. The C=O bond breaking in CF₃COFCN in path D3 to form CF₃ and COFCN requires an energy absorption of 7.97 kcal/mol, which is the lowest among the three paths, indicating that the C=O bond formed between the O atom in the centre of the CF₃COFCN molecule and the CF₃ moiety has the lowest bonding energy. In path 2, dissociation of the CF₃COFCN molecule requires absorption of the highest amount of energy (57.17 kcal/mol) among the three primary dissociation paths in order to dissociate the CF₃COCN and F particles .

The particles such as CF₃COCN, CF₃COF and COFCN generated by the primary dissociation of the CF₃COFCN molecule are still macromolecules, which will be further dissociated under other molecules It can be seen that the energy required to further dissociate CF₃COCN molecules to generate CF₃CO and CN particles is higher (211.86 kcal/mol), indicating that the C-atoms of CF3COCN molecules indicating that the C-C bond connecting the CN group in the CF3COCN molecule is more stable. However, further dissociation of CF₃CO to form CF₃ and CO particles can occur spontaneously and releases 41.36 kcal/mol of energy. The breaking of C=O in the CF₃CO molecule to form CF₃C and O particles is more difficult and requires the absorption of 209.4741.36 kcal/mol of energy. Therefore, CF₃COFCN is more likely to decompose under sustained energy to form particles such as CF₃, CF and CN, which is in good agreement with the evolutionary pattern of the particles in the results of the molecular dynamics simulations above.

The possible formation pathways of the main O-containing products are given in Fig 6 (the molecules involved in the pathways are optimized configurations), and the enthalpies for the different pathways are shown in Table V. It can be seen that all O-containing products are generated by processes that can be spontaneous and exothermic (negative enthalpy), which may prevent the particles generated by the decomposition of C_4F_7N from recombining to form C_4F_7N or other stable by-products. The process of CO generation from C and O in pathway R10 releases the most energy (-236.4 kcal/mol), which explains why the addition of O₂ can inhibit the generation of carbon monomers from C_4F_7N mixtures during the discharge process, as reported in the literature [4].



Fig. 6. Generation path of O-containing products Table V

MAIN O-CONTAINING PRODUCT FORMATION PATHS AND THEIR ENTHALPY VALUES

No	The reaction path	$\Delta_r H$	ΔH	
10.	The reaction pair	(kcal/mol)	(kcal/mol)	
R1	$CF_3+O \rightarrow COF_3$	-104.05	-	
R2	$COF_3+CF \rightarrow C_2F_4O$	-72.59	-	
R3	$C_2F_4O+CF_3\rightarrow C_3F_7O$	-161.13	-	
R4	$CF_2+O \rightarrow COF_2$	-108.72	-	
R5	$COF+F \rightarrow COF_2$	-120.89	-	
R6	CF ₃ +CO→CF ₃ CO	-41.36	-	
R7	$CO+O\rightarrow CO_2$	-141.99	-	
R8	CO+F→COF	-85.33	-	
R9	CN+O→CNO	-177.12	-	
R10	C+O→CO	-236.4	-	

In summary, the energy released under superheated thermal failure conditions causes the simultaneous decomposition of C₄F₇N and O₂ in the gas mixture to produce particles such as CF₃, C₃F₇, CN, CF₂, CF, F, CF₃CF, and O, which interact with each other to produce gas by-products. The addition of O₂ complicates the dissociation process of C₄F₇N, and the dissociation process of the product generated by the combination of C₄F₇N and O occurs readily compared to the one-time dissociation process of the C₄F₇N molecule. This suggests that the addition of O_2 will have an effect on the formation process of the by-products of the decomposition of C₄F₇N, and that the spontaneous reaction of the O particles with the decomposed particles of C₄F₇N inhibits the generation of some of the by-products to a certain extent. Therefore, the addition of a certain amount of O₂ can reduce the generation of C₄F₇N decomposition by-products, but as the spontaneous reaction between O particles and decomposition particles (e.g., fluorocarbons) generates COF₂ (strong toxicity), the generation of some of the by-products shows a tendency to increase when the O₂ ratio is higher.

IV. CONCLUSION

In this paper, based on ReaxFF reaction molecular dynamics simulations and quantum chemical calculations, the mechanism of the influence of the buffer gas O_2 on the decomposition process of the environmentally friendly gas insulating medium C₄F₇N/CO₂ has been identified. The main conclusions are as follows:

(1) The ReaxFF-MD simulation results show that the thermal decomposition of the C₄F₇N/CO₂/O₂ gas mixture mainly generates particles such as CF₃, CF₂, CF, F, C₂F₅, C₂F₄, C₂F₂, C₃F₇, C₂F₂N, C₃F₄N, CFN, CN, CO, O, and C. The two particles generated in the highest amounts are CF₂ and CN. The addition of O₂ to the C₄F₇N/CO₂ gas mixture can effectively reduce the decomposition of C₄F₇N and the generation of most of the by-products. The decomposition of C₄F₇N is the least when the O₂ ratio is 6%. The addition of 0% -4% O₂ decreases the rate of the main decomposition reactions in the reaction system, and the rate of the reaction is increased when the O₂ ratio is greater than 8%. However, the initial decomposition time of C₄F₇N was significantly reduced and the generation rate of decomposed particles was accelerated when the simulated temperature was higher than 2600 K.

(2) The addition of O_2 complicates the dissociation process of C_4F_7N , and the dissociation process that occurs when C_4F_7N combines with O is more likely to occur compared to the direct dissociation process of the C_4F_7N molecule, which has a reaction enthalpy of -106.52 kcal/mol and an activation energy of 47.51 kcal/mol. The majority of the reactions between the O particles and the decomposed particles of C_4F_7N belong to the exothermic process that can occur spontaneously. This may prevent the particles generated by C_4F_7N decomposition from recombining to form C_4F_7N or other stable by-products, thus affecting the decomposition of the C_4F_7N gas mixture and the formation of byproducts.

(3) According to the simulation results, the addition of $2\%-6\%O_2$ can appropriately inhibit the decomposition of C_4F_7N and the generation of by-products, so the addition of $2\%-6\%O_2$ can improve the chemical stability of C_4F_7N/CO_2 gas mixture.

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