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# Dispersion engineering in Brillouin fiber laser cavity for Kerr frequency comb formation

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We conduct numerical and experimental investigations on Kerr comb generation in a nonlinear and nonreciprocal fiber cavity by leveraging both stimulated Brillouin backscattering and cascaded four-wave mixing. By engineering the net cavity dispersion to be either normal or anomalous, we enable the formation of diverse patterns and localized structures in the cavity field. The comb's properties depend crucially on the mismatch between the frequency spacing of the bichromatic pump and the free spectral range of the Brillouin laser cavity in both cases. Particularly, in the anomalous regime, adjusting this parameter yields coherent, stable frequency combs in the modulation instability regime. This allows control and expansion of the spectral bandwidth up to 2 THz in normal dispersion and to 6 THz under anomalous net dispersion. This versatile and easily reconfigurable method holds potential for applications in high-speed communications and microwave synthesis. © 2023 Optica Publishing Group

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### **1. INTRODUCTION**

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Optical frequency combs (OFCs), comprising a series of equally 5 spaced coherent lines in the frequency domain, have found 6 widespread use in a wide panel of applications encompass-7 ing optical frequency metrology, spectrograph calibration, mi-8 crowave generation, and beyond [1]. OFCs originate from var-9 ious sources, including mode-locked lasers [2], electro-optic 10 modulation [3, 4], and passive nonlinear resonators [5]. The 11 latter, using the formation of dissipative temporal cavity solitons 12 in microresonators [6], generates smooth OFCs at high repetition 13 rates, ideal for optical communications and LIDAR systems. 14

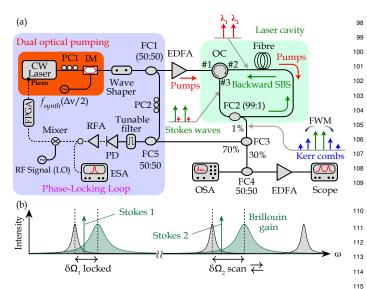
The pursuit of Kerr combs has not been confined to these tra-15 ditional optical platforms. While early work on microresonators 16 showed a competition between Kerr and Raman or Brillouin 17 scattering [7], a novel approach has recently emerged, demon-18 strating the generation of soliton-based combs leveraging Bril-19 louin lasing [8, 9]. In this paradigm, the Brillouin gain in the 20 21 cavity gives rise to counterpropagating Brillouin lasing [10] that serves as the coherent driving force behind Kerr comb genera-22 tion. This paradigm has been extended to fiber cavity Brillouin 23

lasers under bichromatic pumping, to trigger Kerr comb formation at a high repetition rate while using a long cavity [11–13]. Intriguingly, this dual-pumping configuration bestows an additional degree of freedom for manipulating cavity dynamics, specifically the frequency mismatch between the comb repetition rate and the cavity's free spectral range (FSR) [14, 15], which had not been investigated so far in these systems.

In this letter, we investigate the intricate interplay between stimulated Brillouin scattering (SBS) and cascaded four-wave mixing (FWM) in the nonlinear fiber cavity, to achieve coherent and stabilized frequency combs. We experimentally study and numerically validate the impact of the frequency mismatch parameter on the comb dynamics, and specifically its spectral shape and bandwidth. In addition, we perform this analysis in both normal and anomalous group velocity dispersion regimes, since the net fiber cavity dispersion can be easily adjusted by inserting a short fiber segment in the cavity. In each case, the generation of switching waves or localized structures through modulation instability (MI), from the initial bichromatic sinusoidal modulation pattern, is investigated and characterized in the spectral and temporal domains.

#### 2. EXPERIMENTAL SETUP AND RESULTS

Our experimental setup, depicted in fig. 1a, involves a cavity configuration that utilizes a highly nonlinear fiber (HNLF) with a length of 10 m, and standard single-mode fiber (SMF-28) components with a total length of 1.15 m, resulting in a normal net dispersion of -0.94 ps km<sup>-1</sup> nm<sup>-1</sup>. The dispersion and nonlinear parameters of the HNLF and SMF fibers used in our cavity at 1551.7 nm wavelength are D = -2.95 and  $18 \text{ ps km}^{-1} \text{ nm}^{-1}$ ,  $\beta_2 = 3.77$  and  $-21.7 \text{ ps}^2 \text{ km}^{-1}$ ,  $\gamma = 12$  and  $1.2 \text{ W}^{-1} \text{ km}^{-1}$ . Introducing a 1 m long segment of SMF-28 shifts the cavity into the anomalous net dispersion regime ( $\sim 0.5 \,\mathrm{ps} \,\mathrm{km}^{-1} \,\mathrm{nm}^{-1}$ ). For both cases, the cavity finesse was determined to be approximately  $f \sim 26$ . The total roundtrip losses, primarily attributed to the circulator, amounted to 1.2 dB. Considering the overall length of the fiber cavity, the FSR of the cavity are 18.39 MHz and 16.9 MHz in the normal and anomalous net dispersion regimes, respectively. To generate two pump lines of equal power, we use an electro-optic method. A tunable narrowlinewidth continuous-wave laser centered at 1551.7 nm is intensity modulated at the null transmission point of an intensity modulator (IM) to create two controllable sidebands while suppressing the optical carrier wave. The frequency spacing of the



**Fig. 1.** (a) Experimental setup for Kerr combs generation in 116 a dual-frequency Brillouin fiber laser cavity (green rectangle) 117 benefiting from the phase-locked stabilization loop diagram 118 (purple rectangle). CW: Continuous wave, PC: Polarization 119 controller, IM: Intensity modulator, FC: Fiber coupler, EDFA: 120 Erbium-doped fiber amplifier, OC: Optical circulator, SBS: Stimulated Brillouin scattering, FWM: Four wave mixing, OSA: Optical spectrum analyzer, PD: Photodiode, RFA: Radio frequency 123 amplifier, ESA: Electrical spectrum analyzer, LO: Local oscillator, 124 FPGA: Field-programmable gate array. (b) Principle of the offset 125 sideband-locking for the Brillouin gain spectrum detuning scan. 126

pumps is set by the modulation frequency around  $\Delta \nu \sim 40\,{
m GHz}_{-129}$ 67 and can be precisely tuned. A programmable optical filter is em-68 ployed to further reject the residual carrier and any higher-order 131 69 sidebands. The dual pump is then divided into two segments. 132 70 The first segment is amplified using an erbium-doped fiber am-71 plifier (EDFA) and introduced into the fiber cavity through an 134 72 optical circulator (OC). These pumps undergo a single pass 135 73 through the HNLF in the forward direction before being isolated 136 74 by the OC. Simultaneously, two backscattered Stokes waves are 75 137 76 generated, with a frequency down-shift of  $\sim$ 9.1 GHz from the 138 pump frequencies [16], corresponding to the acoustic phonon 77 139 energy. Within the cavity, a 99:1 fiber tap coupler is inserted 78 140 to extract and analyze the counterpropagating Brillouin laser 141 79 signals. The remaining 99% of the Stokes waves are recirculated 142 80 back into the passive fiber ring cavity, resulting in the dual lasing 81 143 effect that initiates a cascade of FWM and leads to the formation 144 82 of Kerr combs. The second part of the bichromatic laser is recom- 145 83 bined with a portion of the cavity's output, to create a beatnote 146 84 between one of the Stokes laser and its pump. This beatnote is 147 85 stabilized to a local oscillator via a digital phase-locking loop 148 86 (PLL) which feeds back on the laser wavelength [17, 18], and 149 87 compensates for the relative thermal drift between the fiber cav- 150 88 ity and the pump laser. This PLL scheme locks the detuning 151 89 of one of the Brillouin gain lobes relative to the cavity ( $\delta \Omega_1$  in 152 90 fig. 1b). Changing  $f_{\text{synth}} = \Delta \nu / 2$  hence controls  $\delta \Omega_2$  and thereby <sup>153</sup> 91 the Stokes lasing frequency via the mode pulling effect [9]. An 154 92 electrical spectrum analyzer (ESA) is used to monitor the pump 155 93 beatnote, to ensure single-frequency operation of the Stokes 156 94 laser. Note that the input polarization states were controlled 157 95 via polarization controllers to maximize the extracted Brillouin 158 96 lasing signal. Finally, spectral and temporal characterizations 159 97

of the cavity output field are performed using a high-resolution optical spectrum analyzer (APEX Technologies AP2243B) and an optical sampling oscilloscope (EXFO PSO-101). To simulate the cavity system, we employ a specific model based on coupled equations derived from the Ikeda map and use a two-step approach for each roundtrip in the fiber cavity [19]. First, we compute the SBS steady state by solving the Brillouin master equations [20] numerically, and then we solve the modified Nonlinear Schrödinger Equation using the split-step Fourier method, accounting for Brillouin gain in the pumped Stokes modes, cavity recirculation and losses. Our model is benchmarked against the measurements and provides excellent agreement.

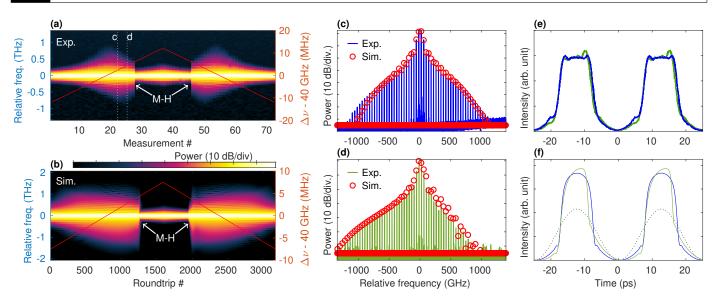
#### A. Normal dispersion regime

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We first characterized the comb dynamics under net normal dispersion. Figures 2a,b report both measured and numerically simulated Kerr comb spectra, while tuning  $\Delta v$  by changing the frequency modulation of the IM. Since one pump is effectively locked to a cavity mode via the PLL, its detuning is fixed, while that of the other pump is swept as a result. The total pump power is fixed at 430 mW. Spectral and temporal measurements are performed simultaneously during the frequency scan. Our results show that a mismatch between  $\Delta v$  and the FSR-multiple of the laser cavity has a significant impact on both the spectral broadening and shape of the Kerr comb in such dispersion regime. Our numerical predictions show good agreement with the experimental data. As predicted in [19], the optimal pump frequency spacing, where the stable Kerr comb spectrum is the broadest, occurs when  $\Delta v$  is commensurate with a multiple of the cavity FSR. This situation corresponds to an equal detuning for both pump lasers. We observed mode-hopping effects, as highlighted in fig. 2a depending on the detuning of the pumps. At these points, the lasing from a longitudinal mode switches to the adjacent one and the detuning of the tuned pump abruptly changes sign. Hence, mode hopping limits the achievable pumps detuning range. We could replicate this effect in simulations by wrapping the pump's detuning in the range  $\pm$ FSR/2 (see fig. 2b). Note that the FSR of the fiber cavity must be greater than the spontaneous Brillouin gain bandwidth (typically around 55 MHz [16] in our case) in order to avoid multimode Brillouin lasing [19]. The dual-frequency pump spacing and pump power were chosen to preserve a coherent single Brillouin frequency lasing emission while maximizing the Kerr comb spectral bandwidth. Figures 2c,d shows two distinct Kerr comb spectra from the previous maps. In both cases, our numerical predictions match the experimental data remarkably well. The first corresponds to the commensurate  $\Delta v$  spacing case, and exhibits a symmetric shape of the comb with a maximum bandwidth around 2 THz at -60 dB. The other comb has an asymmetrical shape, which is caused by the unequal detuning of the pumps, which leads to a shift of the Kerr comb center frequency. In addition, we characterized these two combs in the time domain, as illustrated in fig. 2e which shows the temporal intensity profiles of the picosecond pulses corresponding to the combs in figs. 2c,d. They correspond to the formation of a switching wave [21] onto the sinusoidal modulation pattern induced by the interference between the two Stokes fields in the cavity. Our numerical prediction (fig. 2f) of the intracavity temporal intensity profile shows good agreement with the experimental data. In both cases, the measured temporal profiles follow the expected switching wavefront formation, i.e. a pulse train with a  $\sim$ 25 ps period with flat-top pulses in the case of the symmetric Kerr comb (fig. 2e, blue curve). The pulse shape changes slightly





**Fig. 2.** Normal net dispersion regime. (a) Experimental recording of the comb evolution with  $\Delta v$ , at fixed injected optical power of 430 mW. M-H : Mode Hopping. (b) Simulated evolution of the comb spectrum when scanning the detuning of one pump. (c) Examples of symmetric comb in the scan in (a). The red circles show the numerical simulation. (d) Examples of asymmetric comb in the scan in (a) and comparison with simulations. (e) Experimental temporal intensity profiles of the generated pulse train corresponding to both cases reported in (c) and (d). (f) Numerical simulation of intra-cavity temporal intensity profile corresponding to the cases in (c) and (d). The dashed lines corresponds to the interference between the 2 Stokes lines.

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when the comb shape is asymmetric (fig. 2e, green curve).

#### 161 B. Anomalous dispersion regime

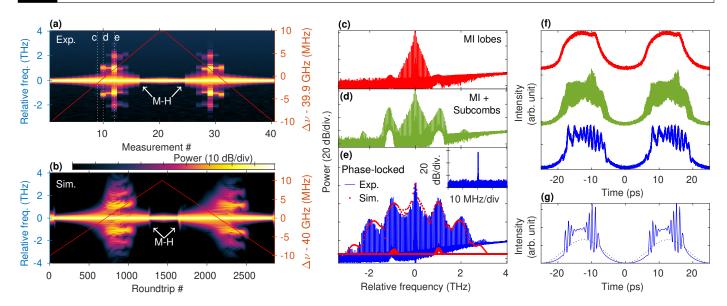
197 Next, we analyzed the cavity with net anomalous dispersion. 162 198 The same previous set of measurements were performed, and 163 199 the numerical simulations have been adapted to the new laser 164 200 cavity parameters. Figure 3a shows the experimental evolution 165 201 Kerr comb spectra when changing the detuning of one pump, 166 when varying  $\Delta v$ , at fixed injected pump power of 535 mW. As 167 in the net normal dispersion case, tuning this parameter sig-168 204 nificantly impacts the Kerr comb spectral shape and stability. 169 205 A striking distinct feature of the anomalous dispersion regime 170 206 is the formation of MI gain lobes [14], spaced by  $\sim$ 1 THz from 17 207 172 the pumps. Our numerical simulations of the scan, shown in fig. 3b, provide good agreement with the experiment and help 173 to shed some light on the comb formation mechanism. The 174 210 initial multiple FWM creates a narrow coherent comb around 175 the pump lines. Changing the pump frequency detuning leads 176 212 to the emergence of spontaneous MI gain lobes, under which 177 multiple cavity modes are oscillating [22], which degrades the 178 coherence. In addition, the MI induces sub-combs (fig. 3d.), 179 whose line spacing matches that of the initial Kerr comb, with a 214 180 frequency offset [23]. These sub-combs can be still synchronized, 215 18 under appropriate detuning conditions, to form one globally 216 182 coherent comb [24], which is shown in fig. 3e. This optimal 217 183 Brillouin pumps spacing is commensurate with the cavity's FSR, 218 184 which provides a wider stable Kerr comb spectrum and allows a 219 185 spectral broadening of around 6 THz. Interestingly, the desyn- 220 186 chronization does not significantly affect the comb symmetry, 221 187 as in the normal dispersion case, but rather the strength of the 222 188 MI lobes and the offset mismatch of the subcombs. When the 223 189 pump detuning is strongly mismatched, the cascaded FWM be- 224 190 comes less efficient and creates a narrow Kerr comb spectrum, 225 191 as shown in fig. 3a, with a bandwidth less than 1 THz. The ex- 226 192 cellent coherence of the synchronized Kerr comb was confirmed 227 193

by beating a selected comb line (-10) and an auxiliary tunable narrow-linewidth laser (see inset in fig. 3e). Indeed, the intrinsic properties of SBS induce a linewidth-narrowing of the Stokes laser [25, 26]. The combs have also been characterized in the time domain. Figure 3f shows the temporal intensity profiles of the pulse trains corresponding to the combs in figs. 3c,e. Our numerical prediction (fig. 3g) of the intracavity temporal intensity profile corresponding to the wider comb shows good agreement with the experimental data. The broad synchronized Kerr comb spectrum corresponds to stable MI patterns emerging on top of a flat-top modulation pattern (blue curve). The fact that these patterns can be captured with a sampling oscilloscope further validates the coherence and stability of the comb. When the MI sub-combs are mismatched and incoherent, these additional patterns are smeared (green curve). In the strongly mismatched driving case, the pulse train shows little deviation from a sinusoidal pattern (red curve). Note that the soliton state could not be reached in our experiments, due to the inherent detuning limitation imposed by mode-hopping [19].

#### 3. CONCLUSION

In conclusion, we have experimentally and numerically explored the dynamics of Brillouin – Kerr comb formation in nonlinear fiber cavities. The dual-pumping configuration provides an easy way to harness Kerr combs in fiber laser cavities and is an interesting alternative to traditional methods. The key feature of this scheme is the ability to easily change and reconfigure the dispersion as well as the comb spacing, which is determined by the spacing between the two Brillouin pumps. We demonstrate the key importance of these two quantities in the emergence, shape, and dynamics of the Kerr comb states. The comb repetition rate can also be varied across a wide range, which is desirable in applications such as microwaves generation or telecommunications. Finally, this architecture opens perspectives for operation in new spectral windows using higher confinement waveguides





**Fig. 3.** Anomalous net dispersion regime. (a) Experimental recording of the comb spectrum evolution with  $\Delta v$ , at a fixed injected optical power of 535 mW. M-H : Mode Hopping. (b) Numerical modeling of the Kerr combs evolution depending on  $\Delta v$ . (c) Kerr comb spectrum showing the growth of spontaneous MI around the initial comb. (d) Illustration of the sub-comb formation on the MI gain lobes. These comb are offset from the center comb. (e) Broadest phase-locked comb with minimized spontaneous modulationinstability, when matching the pump spacing with a FSR-multiple. The sub-combs are synchronized, to form a single coherent comb. Inset: Beatnote signal between the comb and an auxiliary narrow-linewidth laser around 1555 nm (resolution bandwidth 30 kHz). (f) Experimental temporal intensity profiles of the generated pulse train corresponding to the cases reported in (c) to (e). (g) Numerical simulation of intra-cavity temporal intensity profile corresponding to the comb reported in (e).

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and new specialty fiber materials with strong nonlinearity. 228

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