

Mass transfer assessment and kinetic investigation of biphasic catalytic systems

Carine Julcour-Lebigue, Jean-François Blanco, Laurie Barthe, Henri Delmas, Rinaldo Poli, Eric Manoury, Florence Gayet, Franck D'Agosto, Muriel Lansalot, Raj M. Deshpande, et al.

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Carine Julcour-Lebigue, Jean-François Blanco, Laurie Barthe, Henri Delmas, Rinaldo Poli, et al.. Mass transfer assessment and kinetic investigation of biphasic catalytic systems. Congrès national de la Société Chimique de France, Jul 2018, Montpellier, France. 2018. hal-04354189

HAL Id: hal-04354189 https://hal.science/hal-04354189v1

Submitted on 19 Dec 2023

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Context

Homogeneous catalysis:

- igh efficiency and selectivity towards desired product
- ☼ separation of the catalyst

Biphasic catalysis: confinement of the molecular catalyst in a solvent immiscible with the products (ex: water)

Industrial process: Ruhrchemie/Rhône Poulenc oxo process for the hydroformylation of propene into n-butanal, using aqueous phase and hydrosoluble ligand (TPPTS) – 800 000 tons aldehyde/year [Obrecht et al., 2013], Rh loss < 1 ppb

Pb: not applicable to higher olefins (> C4)!

Strategies for biphasic catalysis:

Water with additives

- * co-solvent in water
- * *ligand modification* → interfacial catalysis
- * phase transfer agents
- * thermomorphic systems
- * surfactants or amphiphilic polymers
- → micellar(-like) catalysis



New solvents

- * fluorous solvents
- * ionic liquids
- * scCO₂







Objectives & strategy

OBJECTIVES: to reach a kinetic formulation including phase equilibria, to characterize interfacial mass transfer effects

HOW: Thermodynamic study

Concentration of the substrates in the vicinity of the catalyst? Effect of products / µenvironment?



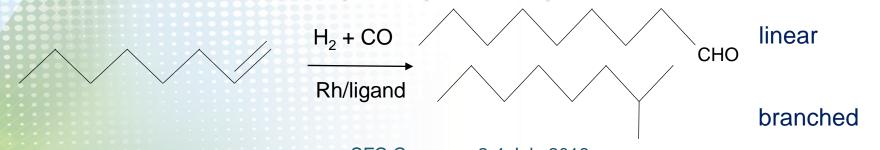
Mass transfer & kinetic study

Relevant intrinsic rate laws (derived from reaction mechanism)?



Mass transfer performance? Coupling of reaction & transfer?

APPLICATION: Rh-catalyzed hydroformylation of oct-1-ene





Ex.1: Ionic liquid biphasic catalysis

[Bmim][PF₆]/decane system

[BuPy][BF₄]/heptane system

PREVIOUS STUDIES (hydroformylation, ≤ 2004):

- High activity & selectivity: TOF > 1000 h^{-1} (100°C), I/b ratio > 40, rather low metal (Rh) loss (<0.1 %) [Chauvin et al. (1996), Bronger et al. (2004)]
- Most of the studies dedicated to screening of ILs & ligands

QUESTIONS:

- Thermodynamic vs. chemical effects?
- Relevant kinetic model?
- Viscosity effects on gas-liquid mass transfer?
- Coupling of reaction & transfer?



LGC

Thermodynamic study

Gas solubility in IL

Large discrepancies in the literature (by up to a factor 3)

 \triangleright Dynamic gas absorption measurements in the reactor ($\triangle P_{reac}$)

Solvent	T (°C)	He, bar.m ³ .kmol ⁻¹	
		H ₂	CO
[Bmim][PF ₆]	20	898	449
	50	816	558
	100	869	663
[BuPy][BF ₄]	60	470	419
	80	507	455
	100	724	487

Solubility of H₂ and CO in [Bmim][PF₆]:

data within the range of reported values (<20% dev. with Monte Carlo

calculations [Urukova et al. (2005)])

 $(\Delta H_{\text{solv,H2}} = [-0.6, 3] \text{ kJ.mol}^{-1}; \Delta H_{\text{solv,CO}} = -3.8 \text{ kJ.mol}^{-1})$

~ 3 times lower than in decane, but ~ 2 times higher than in water

Similar, but slightly higher gas solubility in [BuPy][BF4]





Thermodynamic study

Solubility & partition coef. of olefin (& aldehyde) in IL

Very few values available

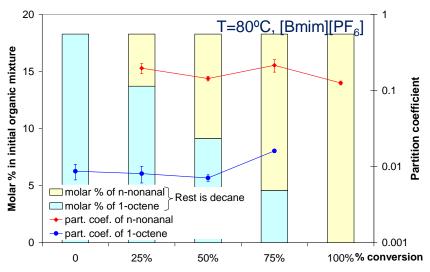
Routine chromatography or spectroscopy methods not suitable

- > L-L equilibria measured at reaction T
- with the help of Multiple HeadSpace Gas Chromatography (IL φ)
- validation of solubility data by thermogravimetry (IL φ)

System	T (°C)	TGA	MHS-GC/MS
oct-1-ene /[Bmim][PF ₆] /[BuPy][BF ₄]	25 80 80	0.6% ± 0.05% 0.85 ± 0.2 0.36%	0.64% 0.86 ± 0.15
n-nonanal /[Bmim][PF ₆] /[BuPy][BF ₄]	25 80 80	11.6% ± 0.5% 11.3 ± 0.3 4.2%	15.5% ± 0.2% 12.9 ± 0.3%

Solubility of octene in [Bmim][PF₆] (g/g): \times **2000 with respect to water** (25°C)

Much higher solubility of n-nonanal Lower values in [BuPy][BF₄]



Partition coef. almost unchanged



Injection head Hole for venting Glass vial



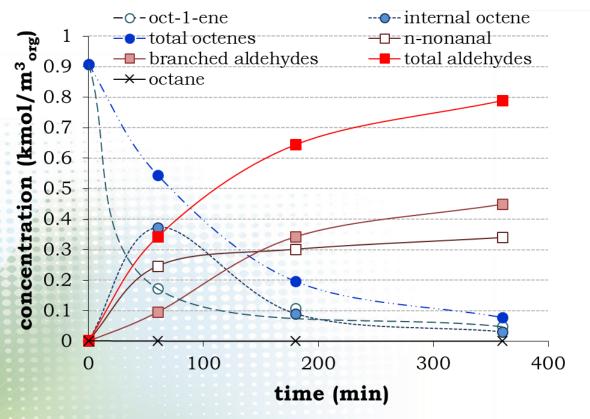
Kinetic study

Experimental study

- instantaneous syngas consumption from $P_{ballast}(R_0)$
- speciation in organic φ by GC/FID (M balance, I/b ratio)



Typical time-concentration profile in solution ([Bmim][PF₆]/decane with TPPTS)



High isomerization of oct-1-ene

 \rightarrow I/b ratio between 0.7 and 3

TOF: 15-75 h⁻¹ after 1h (60-80°C)







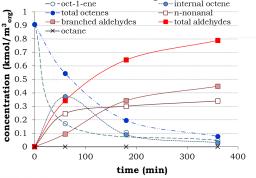
Kinetic study

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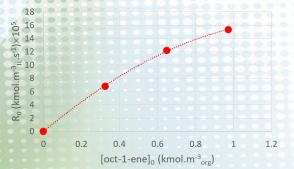


High isomerization of oct-1-ene \rightarrow I/b ratio between 0.7 and 3 TOF: 15-75 h⁻¹ after 1h (60-80°C)

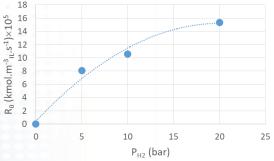
Parametric study

- Stirring speed & catalyst conc. (at given P/Rh) \rightarrow to check for **chemical regime**

Initial conc. of oct-1-ene

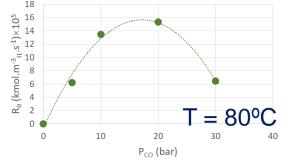


Partial pressure of H₂



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Partial pressure of CO





 $\omega = 1200 \text{ rpm}, V_{II}/V_{org}:40/60$

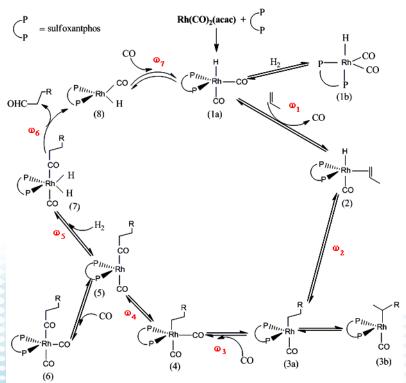






Kinetic modeling

> Empirical rate models or derived from elementary reaction steps



[BuPy][BF₄]/heptane with sulfoxantphos

« Christiansen matrix » approach

[Helfferich, 2004; Murzin and Salmi, 2005]

$$\begin{pmatrix} \omega_2 \omega_3 \omega_4 \omega_5 \omega_6 \omega_7 & \omega_{-1} \omega_2 \omega_4 \omega_5 \omega_6 \omega_7 & \omega_{-1} \omega_{-2} \omega_4 \omega_5 \omega_6 \omega_7 & \omega_{-1} \omega_{-2} \omega_{-3} \omega_5 \omega_6 \omega_7 & \omega_{-1} \omega_{-2} \omega_{-3} \omega_{-4} \omega_6 \omega_7 & \omega_{-1} \omega_{-2} \omega_{-3} \omega_{-4} \omega_{-5} \omega_{-6} & \omega_{-2} \omega_{-3} \omega_{-4} \omega_{-5} \omega_{-6} \omega_{-7} & \omega_{-2} \omega_{-3} \omega_{-4} \omega_{-5} \omega_{-6} & \omega_{-2} \omega_{-3} \omega_{-4} \omega_{-5} \omega_{-6} \omega_{-7} & \omega_{-2} \omega_{-4} \omega_{-5}$$

$$R = \frac{\omega_1 \omega_2 \omega_3 \omega_4 \omega_5 \omega_6 \omega_7}{D_{\text{Christiansen}} + T_{\text{inhibition}}} C_{\text{cat,II}}$$

Hypotheses on irreversibility of elementary steps & rate-determining steps

$$R = f([H_2]_{IL \varphi}, [CO]_{IL \varphi}, [cat]_{IL \varphi}, [octene]_{IL \varphi}, T)$$

Selection of best model(s) & optimization of rate parameters based on initial rates (after sensitivity study)



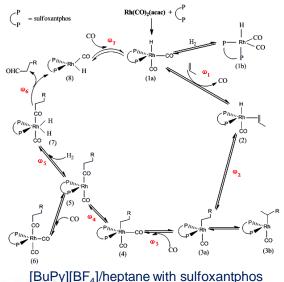
Ex:
$$R = \frac{kABCD}{(1 + K_aAB + K_bAD + K_cBD + K_dABD + K_eDB^2 + K_fA + K_gAB^2 + K_hB + K_iD)}$$



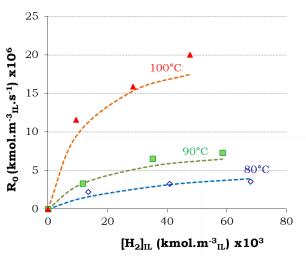
Kinetic study

IL biphasic catalysis

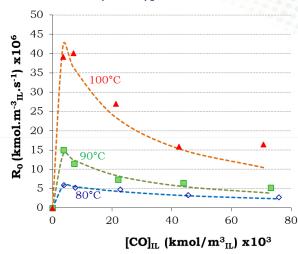
Kinetic modeling



Initial reaction rates



[Deshpande et al. (2011)]



Accounting for isomerization

oct-1-ene $\stackrel{R_1}{\rightarrow}$ n-nonanal oct-1-ene $\stackrel{R_2}{\rightarrow}$ iso-octenes iso-octenes $\xrightarrow{R_3}$ branched aldehydes

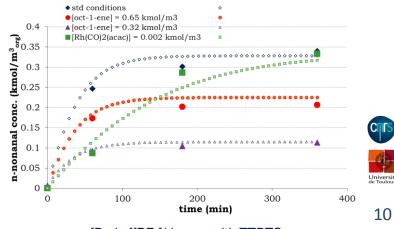
$$R_{1} = \frac{k_{1}C_{H2,IL}C_{CO,IL}C_{cat,IL}C_{1oct,IL}}{\left(1 + K_{d1}C_{1oct,IL}C_{CO,IL}^{3}\right)}$$
addition of H₂ as rate determining step

Time-concentration profiles

$$\begin{split} &\left(V_{org} + V_{IL}K_{wnon} \frac{\rho_{IL}}{\rho_{org}}\right) \frac{dC_{nnon,org}}{dt} = R_1V_{IL} \\ &\left(V_{org} + V_{IL}K_{woct} \frac{\rho_{IL}}{\rho_{org}}\right) \frac{dC_{loct,org}}{dt} = -(R_1 + R_2)V_{II} \\ &\left(V_{org} + V_{IL}K_{woct} \frac{\rho_{IL}}{\rho_{org}}\right) \frac{dC_{loct,org}}{dt} = (R_2 - R_3)V_{IL} \\ &\left(V_{org} + V_{IL}K_{wnon} \frac{\rho_{IL}}{\rho_{org}}\right) \frac{dC_{iald,org}}{dt} = R_3V_{IL} \end{split}$$

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[Sharma et al. (2010)]



[Bmim][PF₆]/decane with TTPTS



1500 rpm





G-L mass transfer evaluation without reaction (k, a)

 \triangleright Dynamic pressure step method: $P_{reac} = f(t)$

> In ionic liquids:

Correlation:
$$Sh_{GL} \propto Re_{st}^{\ b} \cdot (Fr_{st} - Fr_{st,cr})^c \cdot Sc_L^{0,5}$$

or $Sh_{GL} \propto (Re_{st} - Re_{st,cr})^{b'} \cdot Fr_{st}^{\ c'} \cdot Sc_L^{0,5}$
(RSD +/- 20%)



 $k_L a \uparrow$ (by up to factor 10) when $V_{IL}/V_{org} \downarrow$, marked variation around phase inversion

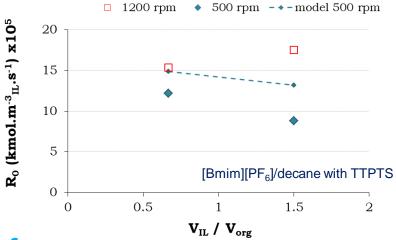
$$\frac{dC_{H2,IL}}{dt} - (k_L a)_{H2} \left(C_{H2,IL}^* - C_{H2,IL} \right) + \frac{kC_{H2,IL}C_{CO,IL}C_{cat,IL}C_{oct,IL}}{\left(1 + K_d C_{oct,IL} C_{CO,IL}^3 \right)} \frac{\varepsilon_{IL}}{\left(\varepsilon_{IL} + (1 - \varepsilon_{IL})m_{H2} \right)} = 0$$

$$\frac{dC_{CO,IL}}{dt} - (k_L a)_{CO} \left(C_{CO,IL}^* - C_{CO,IL} \right) + \frac{kC_{H2,IL}C_{CO,IL}C_{cat,IL}C_{oct,IL}}{\left(1 + K_d C_{oct,IL} C_{CO,IL}^3 \right)} \frac{\varepsilon_{IL}}{\left(\varepsilon_{IL} + (1 - \varepsilon_{IL}) m_{CO} \right)} = 0$$





[Sharma et al. (2009)]



Coupling of reaction and G-L mass transfer

- Chemical regime (≥1200 rpm): R₀ ~ independent of V_{IL}/V_{org}
- \blacktriangleright Mass transfer regime (500 rpm): $R_0 \downarrow$ by 30% when $V_{IL}/V_{org} \uparrow$ from 0.7 à 1.5
 - → overestimation of R₀ by the coupling model
 - → supplementary resistance from L-L mass transfer?





Improvements of IL system

[Bmim][PF₆]/decane with TPPTS

More selective ligand

sulfoxantphos

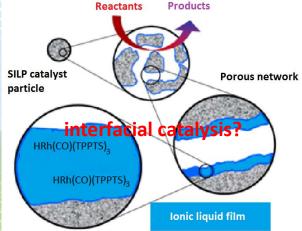
Conditions: $[Rh(CO)_2(acac)] \sim 7.0 \cdot 10^{-3} \text{ kmol.m}^{-3}_{IL}$, SX:Rh = 5:1, $[oct-1-ene]_0 \sim 0.9 \text{ kmol.m}^{-3}_{ora}$, $p_{H2} = p_{CO} \# 20 \text{ bar}$, IL:org = 40:60 v/v

- © No isomerization
- Only n-nonanal detected as product
- ⊗ But dramatic reduction of TOF (by a factor 20)

Solvent	T (°C)	R ₀ , kmol.m ⁻³ _{IL} .s ⁻¹
[Bmim][PF ₆]	80	13·10 ⁻⁶
0-	100	46·10 ⁻⁶
[BuPy][BF ₄]	80	12·10 ⁻⁶
	100	54·10 ⁻⁶

> similar R₀ in both solvents (lower octene solubility in [BuPy][BF₄], partly offset by higher gas solubility)

Supported ionic liquid phase catalysis (SILPC)



- Similar trend as biphasic catalysis
 - but © **lower amount of internal octenes** (with TPPTS) no CO inhibition observed (?)
- © **TOF increased by a factor 7** = up to 560 h⁻¹ at 80°C (conc. ratio of \sim 70 for olefin in between org. & IL ϕ)
- © Stable activity under recycling (Rh loss: 1-2 ppm)





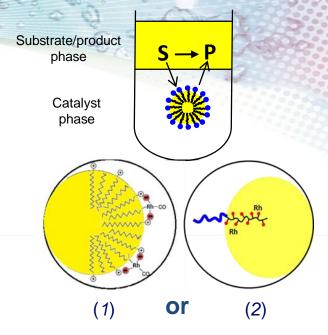
Ex.2: Biphasic catalysis with CCM

From micellar catalyst ...

using cationic surfactants (1) or amphiphilic ligands (2)

- © TOF up to 1000 h⁻¹ (1, 100°C) or 2500 h⁻¹ (2, 100°C)
- stable emulsions by excessive swelling of the micellar core
- ☼ Loss of catalytic objects at the interface

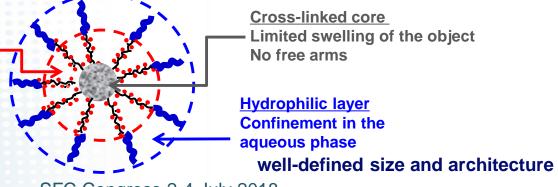
Loss of metal (Rh)



.. to polymeric core-shell catalyst

by cross-linking the hydrophobic segments of self-assembled amphiphilic block copolymers synthesized by "controlled" radical polymerization

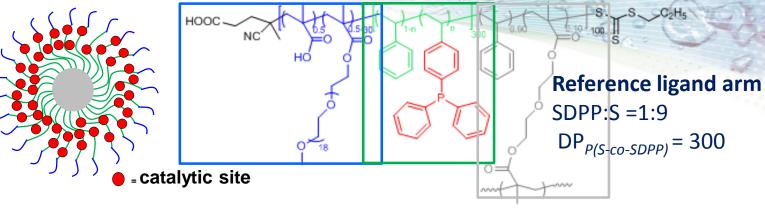
Hydrophobic
functionalized layer
Favorable environment
for the conversion of
hydrophobic substrates
Immobilization of the
catalyst





A closer look on CCM

biphasic catalysis with CCM



- made by convergent synthesis in water (shell → core)
 - reversible addition-fragmentation chain transfer (RAFT) as controlled polymerization method
 - self-assembly of amphiphilic block copolymers
 - addition of cross-linker together with additional styrene to form the core
 - in-situ preparation of Rh-catalyst during heating period under a few bar of syngas (Rh precursor introduced after pre-swelling CCM with n-decanal (reaction solvent))

QUESTIONS:

Latex "10%"

polymer

 $D_{7} \sim 80 \text{ nm}$

27.2% (w/w) of

0.128 mol.L⁻¹ of P

- Performance of CCM for aqueous biphasic catalysis?
- Driving mechanisms? Any limitation by mass transfer to/in the objects?
- How to optimize the objects?
- Content of the swelled CCM & phase separation dynamics?







Proof of concept (1/2)

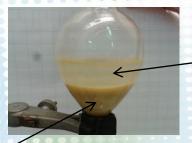
biphasic catalysis with CCM

Catalytic performance of CCM

Std conditions: Ref. TTP@CCM, [Rh] = 6.5·10⁻³ kmol·m⁻³_{aq}, [oct-1-ene] = 1.1 kmol·m⁻³_{org} (solvent: n-decanal), P/Rh = 4, V_{org} = 75 mL, $V_{ag(ns)}$ = 25 mL, T = 363 K, P = 20 bar (CO/H₂ = 1), ω = 1200 rpm



- \triangleright High catalytic activity (**TOF** \sim **500** h⁻¹ vs. 1000 h⁻¹ for homogeneous reaction with TPP functionalized star polymer), I/b ratio of ~ 5
- No hydrogenation and nearly no isomerization
- ➤ Low Rh leaching (~2 ppm measured by ICP/MS) and negligible activity of recovered organic phase
- > Excellent catalytic stability under recycling, when kept under syngas or without any caution

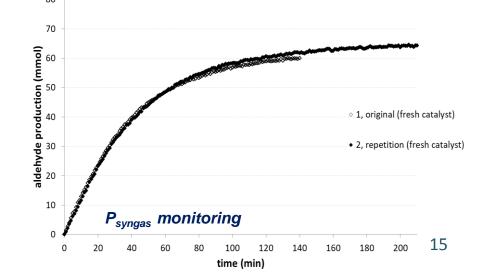


Organic phase (~90% aldehyde yield after 3 h)



Swelled TPP@CCM in

aqueous phase





Proof of concept (2/2)

biphasic catalysis with CCM

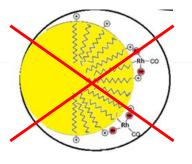
Driving mechanisms

> Interfacial catalysis?

Addition of a stronger water-soluble ligand (sulfoXantphos, sX/Rh = 5)

 \rightarrow inhibition of the reaction (TOF_{max} = 13 h⁻¹)

No "surfactant effect"



Phosphine-free CCM

→ very similar results as the homogeneous reaction without any ligand: aldehyde yield = 13% after 4 h (internal octenes = 35% of the substrate charge)

Rh coordination within the objects

Concept of « nano-reactors »



Catalysis within the hydrophobic microenvironment gathering catalyst and substrate



Mass transfer effects

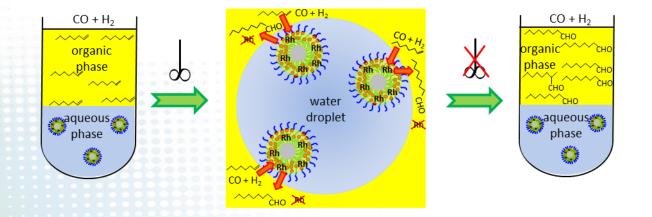
biphasic catalysis with CCM

External mass transfer limitation?

- **Variation of** ω [1200-1600 rpm] \rightarrow < 25% variation of R₀
- Increase of [Rh] by a factor 4

 - * at given [TPP@CCM] \rightarrow threefold increase in R₀
- Variation of [TPP@CCM] at given [Rh]
- → no significant effect of P/Rh [4-12] on TOF nor on regioselectivity

Weak external mass transfer resistance, probably at gas-emulsion interface







Mass transfer effects

biphasic catalysis with CCM

External mass transfer limitation?

- Variation of ω [1200-1600 rpm] \rightarrow < 25% variation of R₀
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Weak external mass transfer resistance, probably at gas-emulsion interface

Internal mass transfer limitation?

- chemical effect for SDPP/S Increase of SDPP:S: from 1:19 to 1:3 (Rh dimeric species?)
- \rightarrow reduction of R₀ by a factor > 3
- **Increase of DP**: from 300 to 500 $\rightarrow R_0$ & I/b ratio unchanged
- Variation of T [70-90°C] → E_A ~22 kcal.mol⁻¹
- → value close to those reported in chemical regime in homogeneous / biphasic system with TPP(TS)

Internal diffusion within the objects is not rate-limiting





Optimization of CCM architecture

biphasic catalysis with CCM

Length of hydrophobic segment /

→ no significant effect of increasing DP on R₀ or regioselectivity, slight reduction of Rh loss

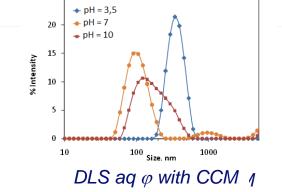
Functionalization degree (SDDP:S) -

→ Significant decrease of activity for higher SDPP:S, low effect on I/b ratio or metal

leaching (CCM or nanogel)







- \rightarrow Accessibility to the catalytic complexes not significantly reduced by cross-linking (R₀ \downarrow by 30%), but **dramatic reduction of Rh loss** from 7.2 to 0.6 ppm
- \rightarrow Rh loss sensible to ω for CCM, but no effect for nanogel

Shell properties

- \rightarrow stability \uparrow when pH \uparrow from 3.5 to 7 \rightarrow effect of methacrylic acid moieties
- \rightarrow [Rh]_{org} reduced to 0.1 ppm at 60°C \rightarrow effect of thermosensitive PEG



19



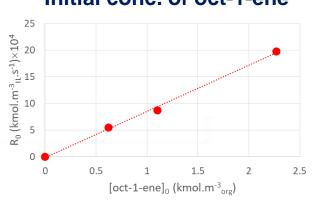
Towards a kinetic model

biphasic catalysis with CCM

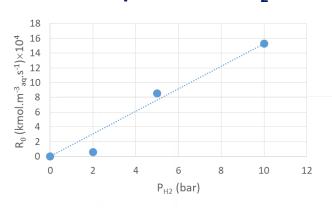
Selection of nanogel with 5% SDPP (pH=7)

Parametric study

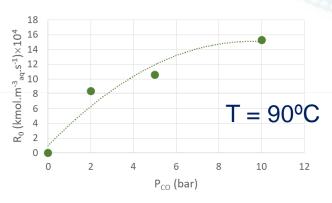
Initial conc. of oct-1-ene



Partial pressure of H₂



Partial pressure of CO



 $E_a = 20.2 \text{ kcal.mol}^{-1}$

Evaluation of the nanogel composition

- Concentration of the latex by centrifugal ultrafiltration
- Extraction of the object content by MHS & GC-MS analysis
- → up to now only qualitative information (difficulty in standardizing the method)



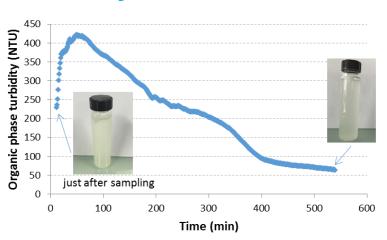




Dynamics of φ separation

biphasic catalysis with CCM

Turbidity evolution

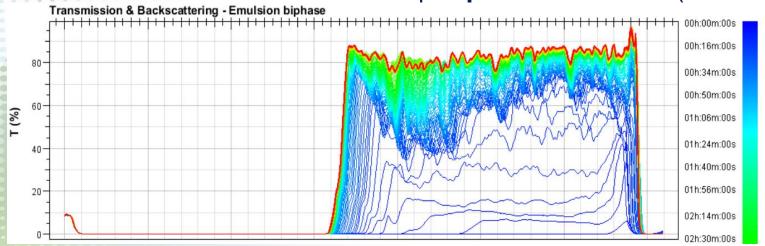


Sampling (30 mL) close to the W/O interface, 10 min after stopping the stirring

- → translucent organic phaseSeparation at ambient T
- → NTU obtained after 8h ~ value of samples analyzed by ICP / AES for Rh leaching

Stability evolution

Sampling of the whole emulsion (20 mL) & φ separation at 60°C (Turbiscan)

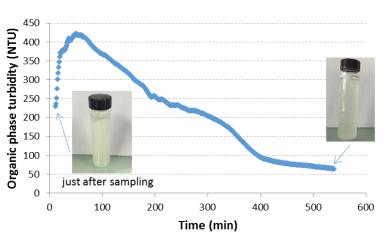






Dynamics of φ separation

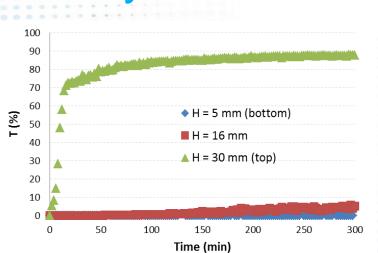
Turbidity evolution



Sampling (30 mL) close to the W/O interface, 10 min after stopping the stirring

- → translucent organic phase Separation at ambient T
- → NTU obtained after 8h ~ value of samples analyzed by ICP / AES for Rh leaching

Stability evolution



Sampling of the whole emulsion (20 mL) & φ separation at 60°C (Turbiscan)

showing 2 successive steps:

- a rapid disengagement (formation of two distinct φ) in 20 minutes
- \rightarrow a much slower ϕ evolution tending towards a plateau after 3 hours

$$T = 83\% \leftrightarrow 0.02\%$$
 of solid content
 \leftrightarrow [Rh] \sim 1 ppm (P/Rh = 4)



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Conclusions & perspectives

- High Turn Over Frequency was obtained for the Rh-catalyzed hydroformylation of oct-1ene in multiphase systems, using either ionic liquids or nanogel-based catalysts in water
- Successful collaboration between chemistry and chemical engineering teams allowed understanding several features of these complex systems, as well as providing clues for their optimization
- Kinetic, mass transfer & separation studies paved the way for the design & scale-up of continuous process with these systems, but still Rh leaching needs to be further reduced
- Further developments would be also required to better describe the coupling between mass transfer & catalytic reaction





Acknowledgements

Indo-French Center For the Promotion of Advanced Research for funding the project 3305-2 "Reaction Engineering in Ionic Liquids"

ANIX Agence Nationale de la Recherche for funding the Biphasnanocat Project (ANR-11-BS07-025-01),

Our PhD & post-doc students: A. Sharma, A. Cardozo, E. Lobry

Our technical staff: J.L. Labat, M. Morere I. Coghe, L. Farhi, M.L. Pern (LGC), for their support on the reactor pilot and the analyses

Our project partners at NCL, LCC & C2P2









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