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# Multi-pixel X-ray detection integrated at the end of a narrow multicore fiber

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We introduce and demonstrate the concept of a multi-pixel detector integrated at the tip of an individual multicore fiber. A pixel consists here of an aluminum-coated polymer microtip incorporating a scintillating powder. Upon irradiation, the luminescence released by the scintillators is efficiently transferred into the fiber cores owing to the specifically elongated metal-coated tips which ensure efficient luminescence matching to the fiber modes. Each pixel being selectively coupled to one of the cores of the multicore optical fiber, the resulting fiber-integrated X-ray detection process is totally free from inter-pixel cross-talk. Our approach holds promise for fiber-integrated probes and cameras for remote X- and Gamma-ray analysis and imaging in hard-to-reach environments. © 2023 Optica Publishing Group

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The need for novel tools able to detect ionizing radiations within tiny recesses and/or extreme environments (of high pressure, temperature or radioactivity) is seen to rapidly grow in many scientific, medical and industrial domains. Being compact, robust and flexible, optical fibers are widely considered as a promising optical tool for addressing this demand, as they allow a direct control on light encoded information collected from hard-to-reach locations.

Fiber probes based on the integration of a scintillating element onto the tip of the optical fiber have been widely explored for the local and real-time dosimetry of ionizing radiations. Given their inert, passive, and possibly biocompatible nature, such devices are particularly appealing in a variety of applications and techniques ranging from in-vivo dosimetry in cancer therapies to *in situ* dosimetry within harsh environments such as a nuclear reactor [1–5]. Reaching such a degree of miniaturization from a direct X-ray-to-electron conversion within microfabricated silicon[6], diamond[7] or perovskite [8] structures remains a challenge. Note however that perovskite materials provide a new generation of scintillators of unmatched properties, thus opening new prospects in the design of indirect

detection of X-rays [9].

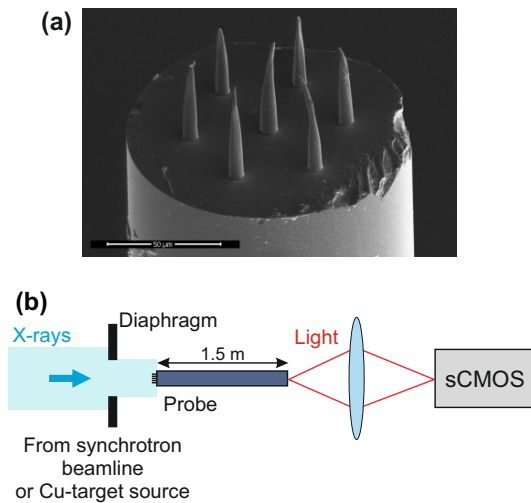
Most of fiber-integrated X-ray detector consist of single pixel systems obtained by coupling a scintillating micro-cell to an individual fiber. Bringing multi-pixel X-ray detectors within hard-to-reach environments would enable new opportunities in radiation analysis, opening the prospect of *in vivo* or *in situ* real-time imaging. However, integrating a pixel array in a compact fiber-integrated architecture remains a challenge. The parallel implementation of a single pixel fiber probe in a fiber bundle represents limits in terms of compactness and image sampling [10] since optical fibers are usually larger than 90  $\mu\text{m}$  (outer diameter including protective coating).

Compactness and resolution issues can be alleviated by implementing multiple pixels onto the same optical fiber. Linares et al. developed a three-pixel detector integrated at the end of an individual fiber that is sufficiently compact to be inserted within a catheter (for brachytherapy monitoring) [11]. However, since the luminescence spectra of the three different scintillators used as detection pixels noticeably overlap, the detector suffers from inter-pixel cross-talk. The development of an array of detection pixels at the tip of an individual optical fiber has so far never been reported.

In this paper, we demonstrate a seven-pixel X-ray detection platform engineered at the tip of an individual fiber. Our detector is achieved by coupling seven metal-coated scintillating micro-tips to a multicore fiber, each microtip being coupled to one of the fiber cores. The resulting seven parallel detection channels are shown to be totally independent from each other, thus holding promise for a high contrast real-time imaging in hard-to-reach environment. Multicore fibers have recently demonstrated new prospects for sensing applications [12, 13] and lab-on-fiber technology [14, 15] with recent important achievements in optical detection [16, 17]. We here extend the multicore-fiber-based technology to the analysis and imaging via ionizing radiations.

Our fiber-integrated multipixel detection system is fabricated using a photopolymerization process at one endface of a 1.5-meter multicore fiber from Fibercore (Model SM-7C1500). The optical fiber shows seven 6.3- $\mu\text{m}$ -diameter cores arranged in a hexagonal lattice, with a 35- $\mu\text{m}$  inter-core spacing. The photo-

64 polymerization process involves a scintillating photopolymer  
 65 locally exposed to a laser light travelling through the fiber. One  
 66 fiber endface is immersed within the polymer/scintillator mixture  
 67 while an expanded laser beam ( $\lambda=521$  nm, laser diode from  
 68 Thorlabs) is projected onto the other end to homogeneously il-  
 69 luminate all the seven cores of the fiber. The so-excited seven  
 70 parallel fiber modes carry almost the same power, thereby simi-  
 71 larly triggering polymer hardening at the core outputs. The total  
 72 laser power at the fiber output and exposure time are  $0.7 \mu\text{W}$  and  
 73 4 seconds, respectively. After fiber rinsing with ethanol, seven  
 74 scintillating microtips arranged in a hexagonal lattice appear  
 75 at the fiber output face. Being realized from the fiber modes  
 76 themselves at a wavelength closely approaching that of the scin-  
 77 tillator luminescence, the so-produced elongated scintillating  
 78 microtips are expected to reciprocally efficiently transfer their  
 79 X-ray excited luminescence into the fiber [18]. To increase probe  
 80 efficiency, the multipixel detection array can be metal coated to  
 81 limit the luminescence leaving the microtips outside the fiber.  
 82 Metal coating involves here the deposition of a few-nanometer-  
 83 thick titanium adhesion layer followed by a 125-nm thick alu-  
 84 minum layer. Aluminum is chosen for its high reflectivity at  
 85 visible wavelengths and high transparency to X-rays. Note that  
 86 polymer growth at the endface of a multicore fiber has been  
 87 reported by Dika et al. [19].

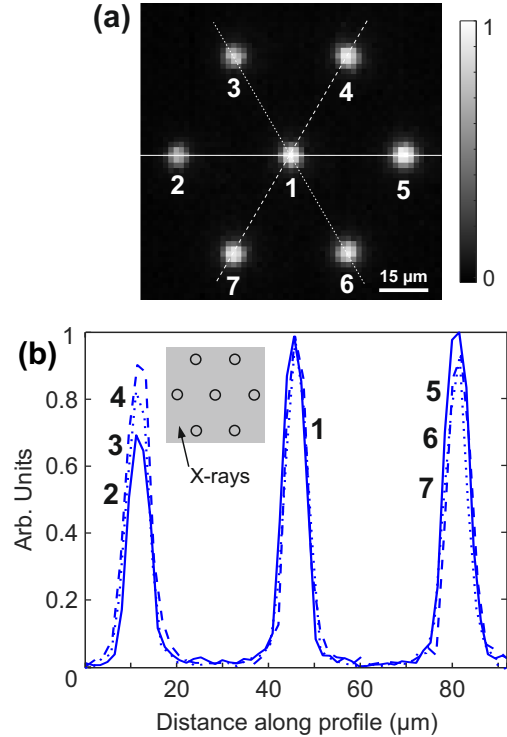


**Fig. 1.** (a) SEM image of a fiber-integrated multi-pixel detection array on top of a seven-core optical fiber. Each pixel is in direct optical coupling with one of the fiber core. (b) Scheme of the experimental set-up for the detector demonstration.

88 To produce the scintillating photopolymer, we first grind  
 89 a commercial  $\text{Gd}_2\text{O}_2\text{S:Eu}$  powder (Phosphor Technology,  
 90 Ref.UKL63/UF-R1) in a mortar with a pestle. The ground powder  
 91 is then mixed with ethanol to be filtered with a cellulose  
 92 acetate membrane whose pore diameter is of  $1.2 \mu\text{m}$ . Finally,  
 93 the filtrate is dried to form a superfine powder. Next, the scin-  
 94 tillating material is mixed with a photosensitive polymer, which  
 95 combines an eosin Y (tetrabromofluorescein) used as a sensi-  
 96 tizer dye, a co-initiator (MDEA: N-methyldiethanola-mine) and  
 97 a multifunctional acrylate monomer, pentaerytritoltriacrylate  
 98 (PETIA) [20]. This photosensitive formulation provides robust  
 99 microstructures at the endface of an optical fiber [18, 21]. A  
 100 weight ratio of 1:5.2 between the photopolymer and the scin-  
 101 tillating powder ensures a high concentration of scintillator within  
 102 the mixture.  $\text{Gd}_2\text{O}_2\text{S:Eu}$  shows excellent yield, linearity and

103 stability upon exposure [22, 23]. This scintillator also shows sub-  
 104 millisecond decay and low afterglow upon exposure at energies  
 105 of the order of a few keV, thereby leading to a response time that  
 106 is fast enough for numerous applications. Faster luminescence  
 107 may however be achieved for instance with  $\text{Gd}_2\text{O}_2\text{S:Tb}$  material  
 108 [5, 24, 25] or perovskites [9]. We verified that, upon excitation  
 109 with X-rays, the residual luminescence of the photosensitive  
 110 polymer is orders of magnitudes weaker than the emission from  
 111 scintillators (as already evidenced in Ref. [18]).

Figure 1(a) displays a scanning electron micrograph of a re-  
 sulting fiber-integrated multipixel detector. The pixel array takes  
 the form of seven aluminum-coated scintillating micro-tips of  
 similar geometries located on top of the seven fiber cores.

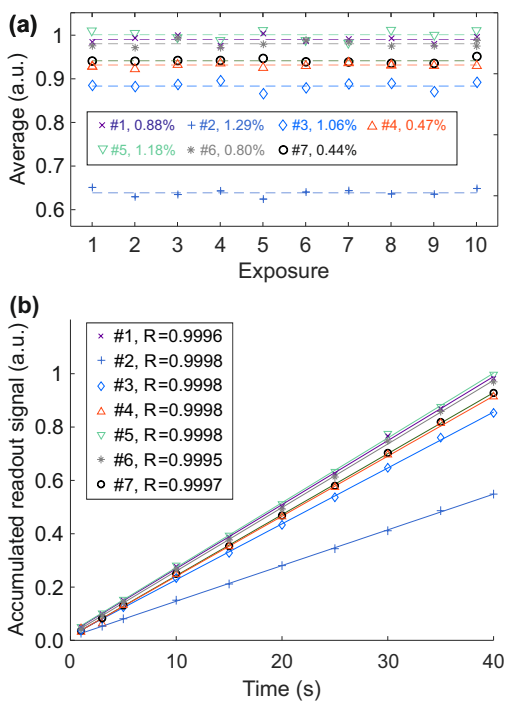


**Fig. 2.** (a) Optical image of the fiber output face when the pixel array is exposed to a  $1 \times 1 \text{ mm}^2$  radiation field (see inset of (b)). (b) Intensity plots along the three white lines of (a). Each pixel is identified with a number ranging from 1 to 7.

116 The microfabricated detector is demonstrated at the  
 117 METROLOGIE beamline of the synchrotron SOLEIL [26]. The  
 118 experimental set-up is depicted in Fig. 1(b). A monochromatic  
 119 12-keV radiation is projected onto the microstructured facet of  
 120 the fiber (the beam and fiber axes are aligned). At 12 keV, a flux  
 121 of  $2.1 \cdot 10^9 \text{ photons}\cdot\text{s}^{-1}$  is measured across a  $1 \times 1 \text{ mm}^2$  radiation  
 122 field. An adjustable diaphragm is positioned in front of the fiber,  
 123 to control the beam width. The diaphragm and fiber detector are  
 124 positioned on two independent 3D motorized stages. The bare  
 125 output face of the fiber is imaged with a standard sCMOS camera  
 126 (Zyla model from Andor Technology) equipped with a ( $\times 10$ ,  
 127 0.3) microscope objective (Olympus). The camera is positioned  
 128 outside the irradiation zone of the primary beam: although the  
 129 optical fiber is shown straight in Fig. 1(b), it follows a S-shaped  
 130 curvature in the set-up. We verified that negligible stem effect  
 131 (i.e., Cerenkov effect) [27, 28] is generated by the fiber itself upon  
 132 exposure: no signal is detected when a bare scintillator-free mul-  
 133 ticore fiber is placed within the above-described test-bed. The

camera is used as a photometer array to simultaneously read the seven instant optical signals delivered in parallel by the fiber-integrated multipixel platform. The readout signals are obtained by integrating image intensity over 64x64-pixel regions of interest (ROI) tightly enclosing the seven output light spots (one ROI per spot). Images are recorded at a rate of 3.3 Hz.

Figure 2(a) shows an image of the output endface of the multicore fiber. The observed seven light spots originate from the scintillation light generated upon irradiation by the fiber-integrated pixel array and guided through the fiber to the camera. These light spots are well separated in the image, thereby avoiding artifactual inter-pixel crosstalk in the optical readout process. Since a relatively homogeneous distribution of light spots is imaged by the camera (see Fig. 2(b)), we conclude that the concentration of scintillators across the microtip array is almost constant and the fabrication process satisfies pixel homogeneity. Only one pixel shows a noticeably weaker optical signal. The main reason is either a lower concentration of scintillators at the tip location during photopolymerization, or a tip shape that is less efficient to outcouple light into the fiber. Regularity of the tip shape could be improved with single-mode multicore fibers (not commercialized yet). Given the few-mode nature of the fiber at the photopolymerization wavelength, the guided light used for tip fabrication shows tight intensity inhomogeneities which may affect tip shape and pixel sensitivity. Note that correction factors can be applied to the pixel array to correct signal offsets.



**Fig. 3.** (a) Repeatability of the multipixel detection system over ten successive exposures of 10s. Each point corresponds to the accumulated readout signal for each exposure. In the inset are reported the relative standard deviation to the average accumulated signal from each pixel. Pixels are identified with a number ranging from 1 and 7 (cf. Fig. 2(a)). (b) Linearity of the detector versus exposure duration (i.e., accumulated dose).

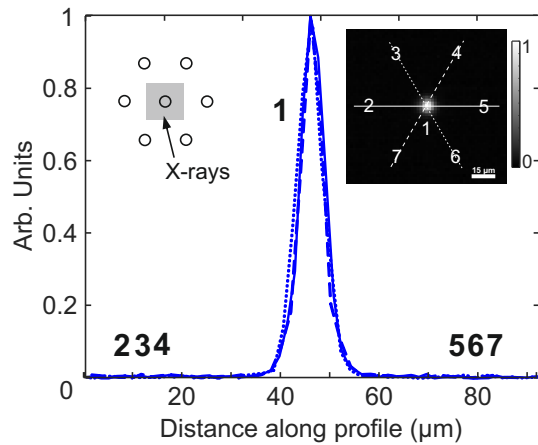
The response of our fiber-integrated multipixel detector in terms of dose linearity and repeatability is reported in Fig. 3. The measurement repeatability (Fig. 3(a)) is determined over

ten exposures of ten seconds each. For the ten exposures at a near-constant radiation flux, the light intensities accumulated by each detection pixel show standard deviation from signal average spanning from 0.4 % to 1.29 %. Note that these errors are mainly due to slight variations of the X-ray intensity at the synchrotron beamline. The X-ray flux in a synchrotron is known to be a decaying function of time due to lifetime limitations of the electrons within the storage ring. To overcome this problem, electrons are periodically injected into the storage ring to compensate beam losses and keep a constant photon flux at beamlines (cf. "top-up" operation). Since our measurements are realized between two successive "top-ups", we numerically compensated the X-ray intensity decay in our data acquisition from a linear regression calculation. A linear regression being a first approximation of the real time-varying decay of the X-ray beam, residual intensity fluctuations are preserved and explain the harmonic fluctuations of the data points visible in Fig. 3(a). Therefore the offsets to the perfect repeatability imputed to our detection system are smaller than the values given in the figure inset. The linearity of the detector with regards to the deposited dose is assessed by accumulating the signals detected by each of its fiber-integrated pixels over 1, 3, 5, 10, 15, 20, 25, 30, 35 and 40 seconds of irradiation at a near-constant flux (see Fig. 3(b)). The linearity factor  $R$  across the pixel array exceeds 0.999. Note that we did not observe noticeable performance degradation of our probe during our few-hour probe tests. We also verified detection stability with a single pixel fiber probe (implemented onto a multimode single mode fiber) during a 72h continuous exposure at the METROLOGY beamline.

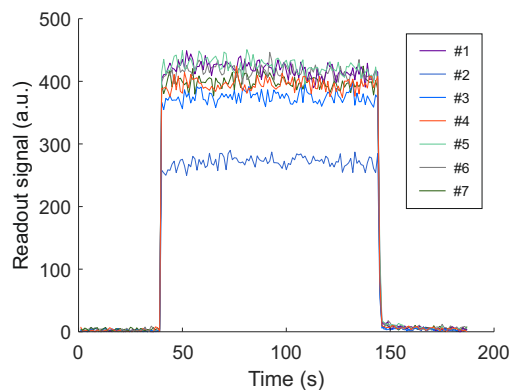
To evidence potential spurious inter-pixel cross-talk in the overall detection process, the X-ray radiation is narrowed until exposing a single pixel. To this end, the diaphragm diameter is decreased down to 35  $\mu\text{m}$  and the resulting pinhole is centered with respect to one of the seven pixels of the fiber probes. Fig. 4(a) reports an optical image of the output endface of the fiber when the tight X-ray pencil selectively irradiates the pixel at the center of the detection array. We see that only the exposed pixel delivers light to the camera via the multicore fiber, the neighboring detection channels remain unexcited. This is confirmed on the intensity plots of Fig. 4(b). Outside the fiber core coupled to the pixel under exposure, the detected intensity does not exceed the dark current of the camera: inter-pixel cross-talk is therefore negligible.

Our fiber detector has also been tested with the radiation from a Cu-target source (40 kV, 40 mA / Bruker D8 DISCOVER diffractometer). Figure 5 shows time traces simultaneously delivered by the seven pixels of the fiber probe upon exposure. At the beginning and at the end of the acquisition, the source shutter is closed to verify that no spurious residual light (such as in-fiber coupled room light or scintillator afterglow) is detected by the system. We see that without X-rays, the afterglow generally observed with Eu-doped gadolinium oxysulfide [22] is here negligible. When the shutter is open (during 110 seconds), seven signals are simultaneously detected with a signal-to-noise ratio ranging from 30 to 42. We measure a rise and fall times of our detection system limited by the detection rate of our camera. The shorter temporal response of the system is defined to the order of 1 ms by the decay time of the scintillators [29]. Note that the signal-to-noise ratio can be enhanced by finding an optimum combination between tip shape and scintillator concentration within the photopolymer. After metal deposition onto the tips, the pixel sensitivity is enhanced by a factor of about two.

To conclude, we introduce the concept of a multi-pixel X-ray



**Fig. 4.** Detector response when the pixel array is exposed to a  $35 \times 35 \mu\text{m}^2$  radiation field centered with respect to the center pixel (see inset, left part). Intensity profiles are plotted along the three white lines of the top right inset which shows the optical image of the fiber output face.



**Fig. 5.** Readout signal from the seven detection pixels upon a 110 s exposure to X-rays from a Cu-target source. The source shutter is closed during the first and last 40 s of the acquisition.

226 detector integrated at one endface of an individual multicore  
 227 fiber. A seven-pixel array is demonstrated onto a narrow  $125\text{-}\mu\text{m}$   
 228 diameter seven-core fiber, each pixel being engineered simul-  
 229 taneously on top of each fiber core by photolithography. The  
 230 resulting imaging system shows good repeatability and linear-  
 231 ity regarding the accumulated radiation dose and it is totally  
 232 free from inter-pixel crosstalk. Our fiber detector could be used  
 233 to perform multi-point analysis of X-ray microbeams [30]. This  
 234 multipoint detection unit could also be seen as the building block  
 235 of a future ultracompact camera engineered from a bundle of  
 236 multicore fibers. Note that our multipixel detection architecture  
 237 can be engineered with a wide variety of scintillators, including  
 238 halide perovskites of high potential for X-ray detection [9]. Being  
 239 compact and flexible, such fibered camera systems would enable  
 240 *in situ* or *in vivo* high resolution X-ray imaging in hard-to-reach  
 241 locations. By leveraging the ubiquity of fiber-optics technology,  
 242 this may represent new prospects in a broad range of scientific,  
 243 medical, and industrial applications.

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249 **Disclosures.** The authors declare no conflicts of interest.

250 **Data availability.** Data underlying the results presented in this  
 251 paper are not publicly available at this time but may be obtained from  
 252 the authors upon reasonable request.

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