

# Critical parameters for highly efficient and reproducible polyelectrolyte multilayer coatings for protein separation by capillary electrophoresis

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1	Critical parameters for highly efficient and reproducible SMIL
2	coatings for protein separation by capillary electrophoresis
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# 15 **HIGHLIGHTS**

- High repeatability and intra- and inter-capillary precision were achieved
- Cross-contamination between polyelectrolyte vials lowers repeatability and efficiency
- PDADMAC/PSS coatings are durable over 100 runs and can be regenerated
- Average retention factors of  $4 \times 10^{-2}$  quantify low residual adsorption
- Proteins must be stored separately in water to avoid degradation

## **ABSTRACT**

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Since the introduction of polyelectrolyte multilayers to protein separation in capillary electrophoresis (CE), some progress has been made to improve separation efficiency by varying different parameters, such as buffer ionic strength and pH, polyelectrolyte nature and number of deposited layers. However, CE is often overlooked as it lacks robustness compared to other separation techniques. In this work, critical parameters for the construction of efficient and reproducible Successive multiple ionic-polymer layers (SMIL) coatings were investigated, focusing on experimental conditions, such as vial preparation and sample conservation which were shown to have a significant impact on separation performances. In addition to repeatability, intra- and inter-capillary precision were assessed, demonstrating the improved capability of poly(diallyldimethylammonium chloride) / poly(sodium styrene sulfonate) (PDADMAC / PSS) coated capillaries to separate model proteins in a 2 M acetic acid background electrolyte when all the correct precautions are put in place (with run to run  $\Re RSD(t_m) < 1.8\%$ , day to day  $\Re RSD(t_m) < 3.2\%$  and cap to cap  $\Re RSD(t_m) < 4.6\%$ ). The approach recently introduced to calculate retention factors was used to quantify residual protein adsorption onto the capillary wall and to assess capillary coating performances. 5-layer PDADAMAC / PSS coatings led to average retention factors for the five model proteins of ~4×10<sup>-2</sup>. These values suggest a relatively low residual protein adsorption leading to reasonably flat plate height vs linear velocity curves, obtained by performing electrophoretic separations at different electrical voltages (-10 to -25kV).

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- **Keywords:** SMIL coatings, protein separation, separation efficiency, intermediate precision,
- 45 residual adsorption

## 1. Introduction

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As a highly efficient separation technique, capillary electrophoresis (CE) finds applications notably in the pharmaceutical field, where it can be used to separate molecules according to their size and charge [1]. Indeed, therapeutic compounds such as monoclonal antibodies (mAbs) and fusion proteins attract particular interest for the treatment of specific diseases and therefore require adequate analysis. Among different separations techniques, CE-based methods are pertinent to separate protein size and charge variants, and include capillary gel electrophoresis (CGE), capillary isoelectric focusing (CIEF) and free solution capillary zone electrophoresis (CZE) [2-3]. CZE offers the advantages of simplicity and good compatibility with mass spectrometry (MS), which enables the identification of separated variants. However, it has received less attention for the analysis of therapeutic drugs since positively charged proteins tend to adsorb onto the capillary wall which presents negatively charged silanol groups [4]. Indeed, in the ideal case, close to one million theoretical plates should be reached for a typical globular protein (~3 nm hydrodynamic radius) analyzed by CE. Experimentally, this number rarely exceeds 100 000 [5]. This may be explained by additional dispersion sources, such as capillary coiling, electromigration dispersion, temperature gradients, or residual protein adsorption [6]. Various methods of reducing protein adsorption onto the capillary wall have been investigated, including the use of extreme pH and ionic strengths [7] [8], zwitterionic additives [9], and capillary coatings. The latter are particularly interesting, as they are easy to put in place and can be finetuned to fit specific needs. Capillary coatings can be divided into three types, namely permanent, semi-permanent, and dynamic coatings [10]. Among these, semi-permanent coatings, which are physically adsorbed onto the capillary wall, are the simplest to achieve, as they do not require chemical reactions like covalently bonded permanent coatings, and remain compatible with MS, unlike dynamic coatings where the coating reagent present in the background electrolyte (BGE) can interfere with the detection. These semi-permanent coatings can be made up of a single neutral or charged layer, or successive multiple ionic-polymer layers (SMIL) which provide a more stable base [11].

Since their introduction in CE by Katayama [11], SMIL coatings have been widely studied as a tool to limit protein adsorption onto the capillary wall. The polyelectrolyte multilayers

are generated by flushing the capillary with alternating polycation and polyanion solutions until the desired number of layers is reached. Various polymers have been used as coating agents, the most common polycations being polyethylene imine (PEI) [12, 13], polybrene (PB) [5, 11, 14-16], poly(allylamine hydrochloride) (PAH) [12, 17], poly(diallyldimethylammonium chloride) (PDADMAC) [12, 18, 19], and the most common polyanions being dextran sulfate (DS) [5, 11, 13, 16], poly(methacrylic acid) (PMA) [5, 12, 17, 20], and poly(sodium styrene sulfonate) (PSS) [5, 12, 17-19]. Coatings with a final polycationic layer are well-suited to separate positively charged compounds, while those ending with a polyanion are preferred for negatively charged analytes. Polyelectrolyte nature has been shown to have a significant impact on separation efficiency as well as stability of the electroosmotic flow (EOF), with plate numbers ranging from 4000 plates/m with a PEI-DS-PEI coating [13] to over 800 000 plates/m with a 13-layer PDADMAC/PSS coating in a 20mM phosphate buffer (pH 4) [18] for the separation of model proteins. Other elements, such as the coating buffer, the BGE, the number of deposited layers, and the physicochemical characteristics of the polyelectrolytes, may have a great impact on coating performances, as was described in a recent review [20].

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Despite the abundance of studies on the subject, comparing different SMIL coatings and separation conditions remains challenging, as different proteins migrate at different speeds and the electroosmotic mobility changes the migration times on different coatings. To this end, the recently developed approach based on calculating protein retention factors *k* from separation efficiencies, enables a quantitative measurement of residual adsorption, and therefore a simple way of ranking capillary coatings [19]. Determining retention factors in CE is atypical, since they are calculated from separation efficiencies rather than migration times like in chromatography. Whereas repeatability is often evaluated for SMIL coatings, reproducibility and intermediate precision are less studied, though they are crucial for the comparison of different conditions and coatings. Bekri et al. performed such a study for a 5-layer PDADMAC/PLC coating, obtaining a 1.2% RSD on migration times for three capillaries [12]. Similarly, Qu et al. found run-to-run, day-to-day, and column-to-column reproducibilities all below 2% for a PDADMAC/graphene oxide coating [21]. Reproducibility of the EOF may also be considered, Liu et al. finding that a PB/DS coated capillary stored in water overnight had a day-to-day RSD of 9.2% (*n*=3), which was greatly improved by rinsing the capillary with

a buffer solution containing 0.01% w/v DS, reaching 0.8% (*n*=3) [22]. Likewise, Graul et al. tested several 13-layer PDADMAC/PSS coatings which had RSDs on the EOF below 2% [18]. Capillary-to-capillary intermediate precision or reproducibility in CE has been more investigated for silica capillaries compared to SMIL coatings. Intermediate precision and reproducibility problems in CE may be linked to unequal levels in the buffer vials, high current, insufficient rinsing between runs, or low injection pressures [24, 25]. Thus, it is clear that reproducibility studies for SMIL coatings in CE need to be further developed.

In this work, critical parameters for the construction of SMIL coatings used for protein separations by CE are examined with the aim of improving the experimental protocol and maximizing SMIL coating performance and reproducibility. Among these, sample preparation and conservation, contamination between polyelectrolyte vials, endurance and durability of the capillary coatings are investigated. Repeatability and intermediate precision are evaluated through run-to-run, day-to-day and cap-to-cap analyses, focusing on 5-layer PDADMAC/PSS coatings used to separate five model intact proteins in a 2 M acetic acid BGE. Separation performances are assessed by calculating retention factors for each protein, which enables an evaluation of the residual adsorption of proteins onto the capillary coating and provide a quantitative basis for the ranking of capillary coatings in 2 M acetic acid conditions. Overall, this work may serve as a guide to the obtention of efficient and performant SMIL coatings.

# 2. Materials and Methods

#### 2.1. Chemicals & Vial Preparation

2-[4-(2-hydroxyethyl)piperazin-1-yl]ethane sulfonic acid (HEPES) and acetic acid were purchased from Sigma-Aldrich (Saint-Quentin Fallavier, France). The model proteins, Carbonic Anhydrase I from human erythrocytes (CA, purity not indicated by the supplier), Trypsin Inhibitor from Flycine max (soybean) (TI, purity not indicated by the supplier), Myoglobin from equine skeletal muscle (Myo, purity  $\geq$  95%), Ribonuclease A from bovine pancreas (RNAse A, purity  $\geq$  60%), and Lysozyme from chicken egg white (Lys, purity  $\geq$  90%) were purchased from Sigma-Aldrich (Saint-Quentin Fallavier, France). Ultrapure water was obtained using a MilliQ system from Millipore (Molsheim, France). Poly(diallyldimethylammonium chloride) (PDADMAC, high molecular weight:  $M_W 4 \times 10^5 - 5 \times 10^5$  Da) 20% w/w in water was purchased

from Aldrich (Lyon, France). Poly(styrene sulfonate) (PSS,  $M_W$  7× 10<sup>5</sup> Da) was purchased from Acros Organics (Geel, Belgium).

2 M acetic acid was used as the background electrolyte (BGE), adding 64 mL of pure acetic acid to a 500 mL volumetric flask and completing with pure water. The measured pH was 2.2 and the solution was kept in the fridge. The vials were prepared by adding 1 mL of BGE into glass vials. The level should be the same for the inlet and outlet vials to ensure stable current. HEPES solution was used as the construction buffer. For a 1 L solution of HEPES at 20 mM, with 10 mM NaOH, add 4.8 g of HEPES and 10 mL of a 1 M NaOH solution to a 1 L volumetric flask and complete with water. The measured pH was 7.4 and the solution was kept in the fridge. The vials were prepared by adding 1 mL of HEPES buffer into glass vials.

Polyelectrolyte solutions (3 g/L PDADMAC and PSS) were prepared by weighing the desired amount of polymer in a 5 mL Eppendorf®, adding the corresponding amount of HEPES buffer for a 3 g/L solution. Both must be prepared one night before the first use. PDADMAC solution must be kept in the freezer. Indeed, PDADMAC solution freshness was shown to have an impact on the quality of the separations. To prepare the vials, 200 µL of the polyelectrolyte solution were added into a 1 mL polypropylene vial, making sure that the level of the liquid was below the electrode (in the case of Agilent CE equipment with long electrodes). The dangers of cross-contamination between polyelectrolyte vials will be detailed later in the paper.

The protein sample was prepared from individual solutions of proteins stored in water. To prepare these, proteins were weighed in 5 mL Eppendorfs® and the corresponding amount of water was added for 2 g/L solutions, which were stored in the freezer. Right before conducting the analyses, the stock solutions of proteins were thawed and 10  $\mu$ L of each one were added into a 1 mL Eppendorf®, adding another 50  $\mu$ L of BGE at double the concentration (4 M acetic acid) for a 100  $\mu$ L total solution, with each protein at 0.2 g/L in BGE. After heat treatment at 37°C for 30 min, the vial was prepared by adding 25  $\mu$ L of this aliquot to a polypropylene conical vial, an amount which is enough for 25 injections. The rest of the aliquot may be kept in the freezer over a short period (no degradation was observed over one week).

DMF was used as the EOF marker and injected before the proteins in BGE. A first solution was prepared by diluting 10  $\mu$ L of DMF in 5 mL of water (in a 5 mL Eppendorf®) to create a 0.2% solution. A second solution was made by diluting 50  $\mu$ L of the first solution in 5 mL of water (in a 5 mL Eppendorf®) for the 0.002% solution in water. Finally, 1 mL of the second solution was mixed with 1 mL of BGE for a 0.001% DMF solution in BGE (1 M acetic acid). To prepare the vial, 25 to 100  $\mu$ L of the final solution was added into a polypropylene conical vial.

#### 2.2. Coating Procedure

The SMIL coatings were prepared by preconditioning the silica capillary with 1 M NaOH for 10 min, then flushing with water for 5 min and HEPES for 10 min. Next, the polyelectrolyte solutions were flushed for 7 min each, followed by 3 min of HEPES, starting with the polycation and alternating with the polyanion, for a total of 5 layers. After the last HEPES flush, wait 5 min and flush with water for 3 min, with BGE for 10 min and wait for another 5 min before starting analyses. All flushes were performed at 930 mbar. Different HEPES vials were used after the polycation and the polyanion in order to limit cross-contamination.

#### 2.3. Capillary Electrophoresis

Analyses were performed on an Agilent 7100 CE in a 2 M acetic acid BGE at pH 2.2. Fused silica capillaries of 50  $\mu$ m in diameter and 40 cm total length (31.5 cm to the detector) were used. Applied voltages were typically between -25kV and -10kV. The capillary was flushed for 5 min with BGE before each run. A 0.001% solution of DMF in BGE was injected first as the EOF marker (30 mbar, 3 s), and the protein mixture next (30 mbar, 4 s), with CA, TI, Myo, RNAse A and Lys each at 0.2 g/L in BGE. The temperature was set at 25°C and detection wavelength was 214 nm.

Calculations of separation efficiencies were done with CEval software [25] available at [https://echmet.natur.cuni.cz/] as will be detailed in the results and discussion section. The capillary total ( $L_t$ ) and effective (I) lengths must be entered in the software, as well as the half ramp time ( $t_{1/2}$  = 0.6 s on Agilent instruments). The linear migration velocity u of each protein is given by Eq. 1:

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$$u = \frac{l}{t_{apex} - t_{1/2}} \tag{1}$$

where  $t_{apex}$  corresponds to the migration time at the peak apex written peak max at x in CEval.

#### 3. Results and discussion

# 3.1. Experimental determination of protein separation efficiency and retention factors on SMIL coated capillaries

Before studying the critical experimental parameters that are controlling the separation performances of SMIL coatings, it was important to set the experimental methodology for calculating the retention factors of the proteins which represent a quantitative estimation of the residual adsorption of the protein onto the capillary coating (and thus an estimation of coating performance). Traditionally, separation efficiency in CE, as well as chromatography, is determined from the total variance of the peak, which is related to the full width at half height  $\delta$  in the case of gaussian peak [26]. The plate number can therefore be expressed with the following equation (method 1):

$$N = 5.54 \left(\frac{t_{apex}}{\delta}\right)^2 \tag{2}$$

However, perfectly Gaussian peaks are rarely observed because of extra-column processes [27], which raises the question of how to best calculate separation efficiency. To this end, other methods were investigated and compared, starting with the formal expression of the plate number which relies on the moments of the peak, shown in Eq. 3, where  $m_1$  is the first moment which is equal to the average migration time, and  $m_2$  is the peak variance, or second moment of the peak (method 2):

$$N = \left(\frac{m_1^2}{m_2}\right) \tag{3}$$

This value of N corresponds to the  $N_{asym}$  value given by the CEval software. This approach has already been used to determine plate numbers in HPLC and compared to other methods (based on peak area, peak tangents and peak half-width) on tailing peaks [28]. For moderately tailing peaks, all methods gave good approximations of the plate number, with

errors compared to the true value below 4%. However, only the method with the moments gave satisfying results when peak tailing was more important.

In addition, a third method using the Haarhoff-van der Linde (HVL) function, a nonlinear regression engine included in the CEval software (see Eq. 4), was considered. This method is useful to fit asymmetrical peaks that can be observed in CE in the case of electromigration dispersion, as it takes the form of a distorted Gaussian peak (see Eq. 5). The parameters  $x_{mean,HVL}$  and  $\sigma_{mean,HVL}$  are given by CEval and are numerically calculated from  $a_0$ ,  $a_1$ ,  $a_2$ ,  $a_{3\delta}$ , which correspond to the peak area, the correct migration time of the analyte, the diffusional broadening of the peak, and the peak distortion, respectively [29].

$$N_{asym} = \left(\frac{x_{mean}}{\sigma_{mean}}\right)_{HVL}^{34} \tag{4}$$

 $HVL_{\delta}(t; a_0, a_1, a_2, a_{3\delta}) = \frac{\frac{a_0}{a_2 a_{3\delta} \sqrt{2\pi}} exp\left[\frac{-1}{2} \left(\frac{t - a_1}{a_2}\right)_{236}^2\right]}{\frac{1}{\exp(a_{3\delta}) - 1} + \frac{1}{2} \left[1 + erf\left(\frac{t - a_1}{\sqrt{2a_2}}\right)\right]}$ (5)

Then, plate heights may be obtained from plate numbers using Eq. 6:

$$H = \frac{l}{N} \tag{6}$$

As was shown by Schure et al. [30], the different sources of peak broadening may be summed, leading to the expression of plate height as a function of the linear velocity u, diffusion coefficient D, capillary internal diameter  $d_c$ , film thickness  $d_f$ , diffusion coefficient in the stationary phase  $D_s$ , and retention factor k:

$$H = \frac{2D}{u(1+k)} + \frac{d_c^2 u}{D} \frac{k^2}{16(1+k)} + \frac{2}{3} \frac{d_f^2 u}{D_s} \frac{k}{1+K} + con \Re \Omega t$$
(7)

The first term corresponds to axial diffusion, the second one to the resistance to mass transfer in the mobile phase and the third one to the resistance to mass transfer in stationary phase. The latter may be ignored as the film thickness is small compared to the capillary internal diameter (~10 nm vs 50  $\mu$ m). The addition of a constant allows a better fit of the experimental data and includes additional, extra-column dispersion sources, such as the Joule effect and electromigration dispersion. This equation may then be solved for k and the constant with the Excel solver using the experimental data and the known parameters. The

diffusion coefficients *D* were experimentally obtained by Taylor Dispersion Analysis for each protein in the BGE (see Table SI1 and Fig. SI1).

The three methods described previously for the determination of *N* were compared for the separation of five model proteins using a 5-layer PDADMAC/PSS coated capillary in Fig. 1. It can be seen that methods 1 and 3 give quite similar results with plate heights below 10 µm and small error bars, indicating good precision. Method 2, however, leads to much higher plate numbers and slopes and the points are not as well aligned on the theoretical curve, showing that the formal method with the moments is not well adapted to these experiments. This may be due to some protein impurities appearing at the basis of the peak which make difficult the determination of the first two moments by peak integration. The HVL method does not seem to bring much improvement, as the analyzed peaks are already quite symmetrical. Finally, the first method using the width at half height will be used for the rest of the calculations (see Fig. SI3 and Table SI3).

It should be noted that the range of electric fields was chosen as to obtain points that were in the linear part of the H=f(u) curve since that corresponds to the contribution of adsorption to the plate height. At lower velocities, plate heights were shown to increase as predicted by the theoretic curve due to axial diffusion, but were not included in the current study (see Fig. SI4).

#### 3.2. Protein sample preparation and conservation

Protein analysis requires proper preparation of the samples and conservation techniques in order to obtain consistent and efficient separations. Indeed, CE is generally performed in mild conditions, avoiding organic solvents and high salt concentrations in order to prevent protein degradation [31]. Moreover, it has been shown that acetic acid may partially denature protein structure, RNAse A in particular being folded in aqueous solutions and becoming unfolded in 40% acetic acid [32]. These considerations are relevant in view of the experimental results obtained for a protein sample analysed over time. Initial experiments were conducted by mixing four model proteins (TI, Myo, RNAse A, Lys) in the BGE, 2 M acetic acid, leading to the separations shown in Fig. 2A on a 5-layer PDADMAC/PSS coated capillary. The superposition of the five electropherograms at -10kV shows very repeatable results and thin peaks that indicate good separation efficiency (see Fig. SI2 and Table SI2 for the data on

all proteins). The protein mix was then stored in the freezer and used for analyses over several months. Five months later, the analysis was repeated in the same conditions using the aged protein mix, returning much larger peaks and poor return to the baseline between proteins (see Fig. 2B). This indicates the proteins have degraded over time, which is confirmed by the preparation of a fresh protein mix in BGE which yields thin, repeatable peaks very comparable to the initial test (see Fig. 2C and Fig. SI5).

Several options were considered to address this issue of protein conservation. The protein solutions in water were mixed and then frozen or lyophilized to test storage of the protein mix in water and dry storage, both of which still led to peak deformation over time, most likely due to protein interactions. Then, proteins were prepared in individual solutions in water at higher concentrations (2 g/L) and kept in the freezer, the mix being done right before the analysis by mixing equal parts of each protein solution and acetic acid at a higher concentration so as to keep the final concentration of each protein in BGE constant (see section 2.1). This method was successful in properly conserving the proteins without any evolution of peak shape or width over time and was used for the rest of the experiments. In addition to protein conservation, the polycation used for the SMIL coating was also seen to deteriorate over time if not kept in the freezer (data not shown).

Another important point to consider is the medium of the injected samples. Generally, protein separation in CE is conducted with the proteins in an aqueous solution, yet this may not be the most favourable option, therefore, two sample mediums were tested and compared.

Initially, the injected samples (protein mix and DMF) were in an aqueous medium, leading to the curves shown in Fig. 3 A and an average retention factor of  $k(10^{-2}) = 5.59 \pm 1.31$  ( $\pm$  one standard deviation for the 5 proteins). In contrast, injecting the samples in BGE resulted in the slopes shown in Fig. 3 B, with much flatter slopes in the linear part of the curve, which is reflected by a lower average retention factor:  $k(10^{-2}) = 3.33 \pm 0.93$ . Therefore, using BGE as the injection sample medium is advantageous, since the separation efficiency has less dependence on the electric field. It is important to note that both the protein and the DMF medium must be modified. This difference may be due to a stacking effect: to preserve the continuity of the current, the less conductive water leads to a higher electric field and therefore higher temperature, causing more diffusion [33]. At low electric field, the stacking

effect prevails, leading to lower plate heights, as can be seen in Fig. 3, and at high electric field, the thermal heating prevails, leading to higher plate heights, which explains the higher slope for the separations in water (see Table SI4 and Fig. SI6).

#### 3.3 Influence of polyelectrolyte cross-contamination during SMIL construction

Another aspect to take into account while building SMIL coatings is vial preparation and potential contamination. During capillary conditioning and injection, successive rinsing steps cause solutions to be deposited on the outer capillary surface and electrodes, which may lead to carryover between vials [34]. For this reason, it was ensured that the level of the polyelectrolytes in the vials stayed below the electrodes on Agilent machines (see section 2.1). Other steps such as burning the ends of the capillary so as to reduce adherence to the capillary surface and rinsing with fresh buffer between injections may be put in place. In the case of SMIL coatings, the presence of polyanion and polycation vials which are deposited one after the other, with a construction buffer rinsing step in between, constitutes an additional risk of contamination. Indeed, the stability of SMIL coatings is based on electrostatic interactions between polyanionic and polycationic layers [35], which may be disrupted if one of the polyelectrolyte solutions contains traces of the other.

In order to confirm the importance of this effect, polyelectrolyte vials were voluntarily contaminated with 10% v/v of the oppositely charged polyelectrolyte. Fig. 4 shows a comparison between the two contamination cases and the normal one, with both contaminated PSS (Fig. 4 A) and contaminated PDADMAC (Fig. 4 B) vials causing a loss in repeatability as well as separation efficiency: on average for all proteins,  $k(10^{-2}) = 6.21 \pm 1.51$  for contaminated PDADMAC and  $k(10^{-2}) = 8.20 \pm 1.78$  for contaminated PSS (see Table SI5, Fig. SI7 and Fig. SI8 in Supporting Information), whereas without contamination, the average retention factor was  $k(10^{-2}) = 3.33 \pm 0.93$  in the best case (Cap 2 in Table SI6). The contaminated PDADMAC seems to be especially detrimental to the repeatability of the separations, with %RSD( $t_m$ ) at -10kV averaging at 8.5% for all proteins, compared to 5.6% for the contaminated PSS, and 0.13% for normal, unpolluted polyelectrolytes. To limit this outcome, sufficient amounts of polyelectrolyte were added to the vials and different buffer vials were used to flush the capillary after each oppositely charged layer (see section 2.1).

#### 3.4. Intra- and inter-capillary reproducibility

In addition to repeatability, which was tested by repeating each separation 5 times leading to run-to-run RSDs, it is important to confirm the reproducibility and intermediate precision of the analyses. Strictly speaking, reproducibility refers to inter-laboratory comparisons, which are relatively rarely investigated either on silica capillaries [34] or for neutral coatings [36], since they are time consuming. Such investigations are also lacking for SMIL coatings in CE. Intra- and inter-capillary Intermediate precisions can be more easily evaluated, and are useful to evaluate method robustness. Figure 5 depicts the concepts of inter-capillary precision, which was measured by repeating the coating procedure on three different capillaries and comparing the separations obtained on each one (giving cap-to-cap RSDs), and intra-capillary precision, which was evaluated by repeating five series of measures on the same capillary coating. One series was made up of five runs at five different electric fields, for a total of 25 runs. This is equivalent to calculating day-to-day RSDs, while also testing the coating's durability.

Overall, the 5 series performed on the same 5-layer PDADMAC/PSS coating each showed very good repeatability, with RSDs on migration times all below 0.9% at -10kV and below 1.8% at -25kV (see Table 1). Moreover, intra-capillary precision was also satisfying, with a maximum RSD of 2.0% at -10kV and 3.2% at -25kV. Regarding the plate height, which even more sensitive compared to migration times, the first four series lead to quite similar plate heights for Myo, and only start to deviate for the fifth series, as can be seen in Fig. 6. This proves satisfying precision and durability over 100 runs. Similar results were found for the other proteins in the mix (see Fig. SI9). In terms of inter-capillary precision, RSDs on migration times were all below 4.6% with an average value of 4.2% at -10kV and 4.5% at -25kV, which is very satisfactory (see Table 1). RSDs on the retention factors and on the constant term in Eq. (7) were much higher, with an average value for all proteins of 12% and 16% respectively, which is understandable knowing the sensitivity of separation efficiency in general (see Table 2). Still, the retention factors obtained on the different capillaries are similar (within 10-20%) and validate the protocol for the determination of the retention factor as an estimation of residual protein adsorption. Plate numbers for the separations at -10kV vary between 51 000 and 82 000 on average (see Table SI7).

#### 3.5. Capillary coating regeneration

Regeneration possibilities were also investigated, as this simplifies the experimental procedure and increases the lifetime of each capillary. First, a used capillary stored in BGE vials over one month was tested, showing slightly lower separation efficiency with an average  $k(10^{-2}) = 7.48 \pm 1.68$  and a modified profile of the H versus u curves (see Fig. 7 A). Next, this same capillary was flushed with a 2 M NaCl, 0.1 M NaOH aqueous solution for 10 min, followed by the usual coating procedure, and tested once more for the separation of the model proteins. This led to lower retention factors,  $k(10^{-2}) = 5.55 \pm 1.69$  on average, and the same profile of plate heights as the initial experiments on new capillaries, showing that regeneration can be an option to revive old capillaries which have been properly stored (see Fig. 7). Rinsing with other solvents, such as a 2% v/v Hellmanex solution followed by a 2 M NaCl, 1 M NaOH solution, or 1 M HCl followed by 1 M NaOH, before regeneration of the PDADMAC/PSS coating also gave satisfying results, with average retention factors of  $k(10^{-2}) = 4.31 \pm 1.05$  and  $k(10^{-2}) = 3.94 \pm 0.98$  respectively (see Fig. SI10 and Fig. SI11).

# **Conclusions**

In this work, 5-layer PDADMAC/PSS coatings were used to separate a mix of model proteins in 2 M acetic acid BGE. The parameters having the most impact on separation performances were determined, paying particular attention to experimental conditions, such as vial preparation, and evaluating reproducibility and intermediate precision on migration times. First, different calculation methods for plate heights were compared, using the width at half heights, the moments, and CEval's HVL function, leading to the conclusion that the classic method with the width and half height is adapted to these experiments as the peaks are quite symmetrical. Next, protein sample conservation was shown to be a crucial aspect, as the proteins tend to alter over time if stored in BGE and/or in a mix prior to analysis, which leads to broader peaks and lower separation efficiency. The injection vial medium was also significant, as injecting samples in water rather than BGE led to a stacking effect, which increased plate height dependence on electric field and may lead to wrong evaluation of residual adsorption via the determination of the retention factor. Moreover, polyelectrolyte vial contamination must be avoided, as it was shown to be detrimental to the repeatability and efficiency of the analyses. Throughout these experiments, protein retention factors were

determined as a measure of residual adsorption onto the capillary wall, enabling a quantitative evaluation of the most important points to look out for. They varied between  $3.1\times10^{-2}$  and  $5.6\times10^{-2}$  for different proteins on a fresh PDAMDAC/PSS coating. Repeatability and intermediate precision of the separations were also assessed looking at run-to-run, day-to-day and cap-to-cap RSDs on migration times, which reached 1.3%, 3.2% and 4.6%, respectively. Overall, the aspects investigated in this paper have greatly improved protein separation efficiency and reproducibility through the identification of several critical parameters, which are highly relevant to control for the successful implementation of performant SMIL coatings in CE.

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# **Declaration of competing interest**

The authors declare no conflict of interest.

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## **Supporting Information**

422 Please find supplementary material provided with this file.

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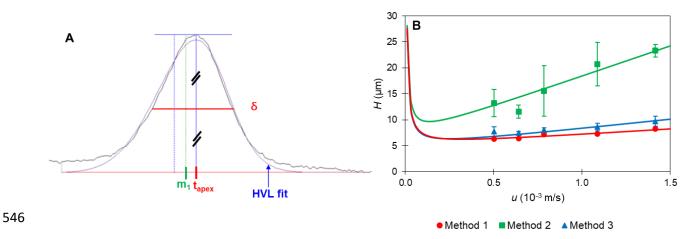
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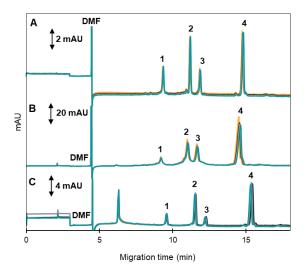
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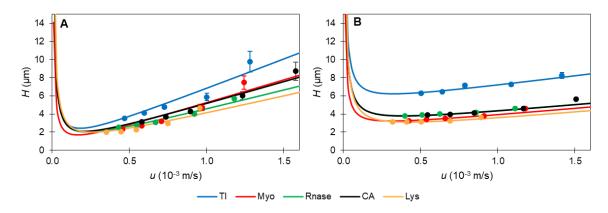
**FIGURES** 



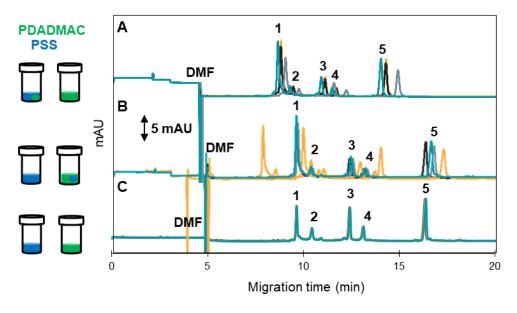
**Figure 1.** Different methods of calculating plate heights shown on a TI peak analyzed on a 5-layer PDADMAC/PSS coating (A) and corresponding representations of H as a function of u. Method 1 in red (eq. 2), method 2 in green (eq. 3) and method 3 (eq. 4) in blue (B). Experimental conditions: 5-layer SMIL coated capillary terminating with the polycation PDADMAC. Capillary: 40 cm (31.5 cm to the detector) x 50  $\mu$ m I.D. BGE: 2 M acetic acid, pH 2.2. Flush before each run: BGE 1 bar, 5 min. Hydrodynamic injection: 30 mbar, 4 s. Sample mixture: 0.2 g/L of each protein in BGE. Hydrodynamic co-injection of 0.02% DMF in BGE: 30 mbar, 3 s. Temperature: 25°C. For the coating procedure, see section 2.2.



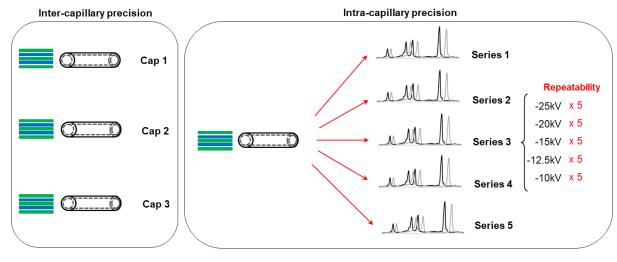
**Figure 2.** Superposition of five repetitions of electropherograms of 4 model protein mix at -10kV on 5-layer PDADMAC/PSS SMIL coatings for initial fresh protein mix in BGE (A), the same mix after 5 months storage in the freezer (B), and freshly prepared sample (C). Experimental conditions: 5-layer SMIL coated capillary terminating with the polycation PDADMAC. Capillary: 40 cm (31.5 cm to the detector) x 50 μm I.D. Electrolyte: 2 M acetic acid, pH 2.2. Flush before each run: BGE 1 bar, 5 min. Peak identification: TI (1), Myo (2), RNAse A (3), Lys (4). Hydrodynamic injection: 30 mbar, 4 s. Sample mixture: 0.2 g/L of each protein in BGE. Hydrodynamic co-injection of 0.02% DMF in BGE: 30 mbar, 3 s. Temperature: 25°C. For the coating procedure, see section 2.2.



**Figure 3**. Influence of the sample matrix (water (A) and BGE (B)) on the *H vs u* representations for the separation of five model proteins on a 5-layer PDADMAC/PSS SMIL coating. Sample mixture: 0.2 g/L of each protein in water (A) or BGE (B). Hydrodynamic co-injection of 0.01% DMF in water (A) or BGE (B). Error bars are ± one SD on *n*=5 repetitions. Other experimental conditions as in Fig. 1. (**A**) CA:  $k(10^{-2}) = 3.77 \pm 0.06$ ,  $cst(\mu m) = 0$ ; TI:  $k(10^{-2}) = 7.34 \pm 0.23$ ,  $cst(\mu m) = 0.01 \pm 0.03$ ; Myo:  $k(10^{-2}) = 5.04 \pm 0.20$ ,  $cst(\mu m) = 0$ ; RNAse A:  $k(10^{-2}) = 5.79 \pm 0.27$ ,  $cst(\mu m) = 0.08 \pm 0.18$ , Lys:  $k(10^{-2}) = 5.99 \pm 0.23$ ,  $cst(\mu m) = 0$ . (**B**) CA:  $k(10^{-2}) = 1.88 \pm 0.66$ ,  $cst(\mu m) = 4.71 \pm 0.12$ ; TI:  $k(10^{-2}) = 4.29 \pm 0.12$ ,  $cst(\mu m) = 4.71 \pm 0.12$ ; Myo:  $k(10^{-2}) = 3.08 \pm 0.23$ ,  $cst(\mu m) = 2.03 \pm 0.16$ ; RNAse A:  $k(10^{-2}) = 3.50 \pm 0.08$ ,  $cst(\mu m) = 2.61 \pm 0.04$ , Lys:  $k(10^{-2}) = 3.90 \pm 0.16$ ,  $cst(\mu m) = 1.78 \pm 0.06$ .

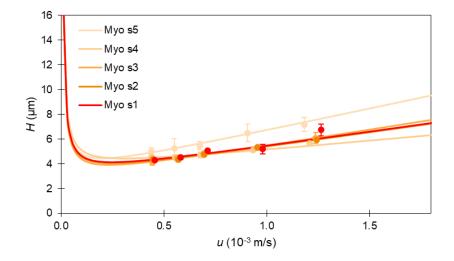


**Figure 4.** Superposition of five repetitions of electropherograms of five model proteins at -10kV on 5-layer PDADMAC/PSS SMIL coatings for PSS-contaminated PDADMAC coating solution (A), PDADMAC-contaminated PSS coating solution (B), and non-contaminated polyelectrolyte solutions (C). Peak identification: CA (1), TI (2), Myo (3), RNAse A (4), Lys (5). Other experimental conditions as in Fig. 1.



**Figure 5.** Principles of inter-capillary and intra-capillary intermediate precision.



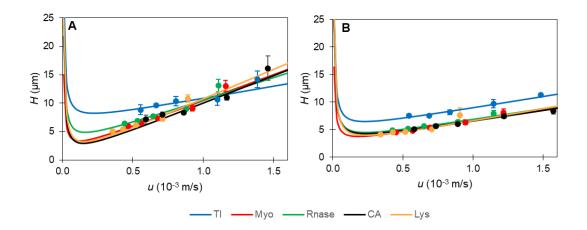


**Figure 6.** Superposition of five successive series of separations of five model proteins on a single 5-layer PDADMAC/PSS SMIL coating, showing the H vs u curves for Myo. Error bars are  $\pm$  one SD on n=5 repetitions. Experimental conditions as in Fig. 1.

		%RSD(t <sub>m</sub> ) at -10kV			%RSD( <i>t<sub>m</sub></i> ) at -25kV		
		run to run	day to day	cap to cap	run to run	day to day	cap to cap
	s1	0.12	1.3	4.3	1.0	2.2	4.5
	s2	0.19			0.04		
CA	s3	0.57			0.11		
	s4	0.12			0.95		
	s5	0.74			0.90		
	s1	0.18	1.4	4.1	1.07	2.2	4.3
	s2	0.19			0.05		
TI	s3	0.58			0.12		
	s4	0.11			1.01		
	s5	0.77			0.96		
	s1	0.13	1.6	4.4	1.3	2.6	4.6
	s2	0.23			0.06		
Myo	s3	0.55			0.15		
	s4	0.13			0.98		
	s5	0.82			1.02		
	s1	0.14	1.7	3.9	1.4	2.7	4.5
	s2	0.24			0.06		
RNAse A	s3	0.57			0.17		
	s4	0.14			0.98		
	s5	0.84			1.04		
	s1	0.11	2.0	4.3	1.8	3.2	4.4
	s2	0.30			0.09		
Lys	s3	0.57			0.19		
	s4	0.16			0.98		
	s5	0.90			1.3		

**Table 2.** Values and RSDs of calculated retention factors and constants. k and cst are given by the average of the values calculated by the Jackknife method  $\pm$  one standard deviation (n=5). Day-to-day RSDs are calculated on the five series and cap-to-cap RSDs on three capillaries. Experimental conditions as in Fig. 1.

		1 (40-2)	Average k in 10 <sup>-2</sup> (RSD)		( ( )	Average cst in µm (RSD)	
		k (10 <sup>-2</sup> )	day to day	cap to cap	cst (µm)	day to day	cap to cap
CA	s1	3.1 ± 0.2	3.1 (11%)	2.7 (27%)	2.9 ± 0.2	3.0 (10%)	2.7 (18%)
	s2	$3.0 \pm 0.2$			2.8 ± 0.4		
	s3	$3.0 \pm 0.2$			3.2 ± 0.4		
	s4	$3.2 \pm 0.3$			2.8 ± 0.5		
	s5	3.8 ± 0.2			3.5 ± 0.5		
	s1	$4.9 \pm 0.4$		4.7 (8.1%)	$6.0 \pm 0.3$	6.3 (14%)	5.4 (12%)
	s2	$4.7 \pm 0.04$	5.1 (7.4%)		6.1 ± 0.1		
TI	s3	$5.6 \pm 0.3$			5.9 ± 0.4		
	s4	$5.3 \pm 0.4$			$5.8 \pm 0.6$		
	s5	$5.3 \pm 0.6$			$7.8 \pm 0.5$		
	s1	$3.8 \pm 0.3$	3.5 (12%)	3.6 (14%)	2.7 ± 0.2	3.0 (10%)	2.3 (14%)
	s2	$3.4 \pm 0.1$			2.9 ± 0.1		
Myo	s3	3.6 ± 0.1			2.7 ± 0.1		
	s4	2.9 ± 0.2			$3.4 \pm 0.2$		
	s5	4.1 ± 0.1			$3.2 \pm 0.1$		
	s1	4.1 ± 0.3	4.2 (5.4%)	3.9 (10%)	3.5 ± 0.2	3.7 (6%)	3.0 (15%)
	s2	4.2 ± 0.3			$3.7 \pm 0.2$		
RNAse A	s3	4.3 ± 0.4			$3.4 \pm 0.3$		
,,	s4	$3.9 \pm 0.4$			$3.8 \pm 0.2$		
	s5	4.5 ± 0.3			3.9 ± 0.2		
	s1	$4.9 \pm 0.3$	4.9 (10%)	4.6 (13%)	2.5 ± 0.1	2.5 (13%)	2.2 (17%)
	s2	4.9 ± 0.2			2.4 ± 0.1		
Lys	s3	5.7 ± 0.3			2.0 ± 0.3		
	s4	4.3 ± 0.2			2.8 ± 0.2		
	s5	4.7 ± 0.1			2.7 ± 0.1		



**Figure 7.** Representations of plate heights H as a function of u on a 5-layer PDADMAC/PSS SMIL coating after storage for one month in BGE (A) and after regeneration (rinsed with a 2 M NaCl, 0.1 M NaOH solution for 10 min and then the normal coating procedure) (B). Other experimental conditions as in Fig. 1.

#### **LIST OF CAPTIONS**

**Figure 1.** Different methods of calculating plate heights shown on a TI peak analyzed on a 5-layer PDADMAC/PSS coating (A) and corresponding representations of H as a function of u. Method 1 in red (eq. 2), method 2 in green (eq. 3) and method 3 (eq. 4) in blue (B). Experimental conditions: 5-layer SMIL coated capillary terminating with the polycation PDADMAC. Capillary: 40 cm (31.5 cm to the detector) x 50  $\mu$ m I.D. BGE: 2 M acetic acid, pH 2.2. Flush before each run: BGE 1 bar, 5 min. Hydrodynamic injection: 30 mbar, 4 s. Sample mixture: 0.2 g/L of each protein in BGE. Hydrodynamic co-injection of 0.02% DMF in BGE: 30 mbar, 3 s. Temperature: 25°C. For the coating procedure, see section 2.2.

**Figure 2.** Superposition of five repetitions of electropherograms of 4 model protein mix at - 10kV on 5-layer PDADMAC/PSS SMIL coatings for initial fresh protein mix in BGE (A), the same mix after 5 months storage in the freezer (B), and freshly prepared sample (C). Experimental conditions: 5-layer SMIL coated capillary terminating with the polycation PDADMAC. Capillary: 40 cm (31.5 cm to the detector)  $\times 50 \text{ }\mu\text{m}$  I.D. Electrolyte: 2 M acetic acid, pH 2.2. Flush before each run: BGE 1 bar, 5 min. Peak identification: TI (1), Myo (2), RNAse A (3), Lys (4). Hydrodynamic injection: 30 mbar, 4 s. Sample mixture: 0.2 g/L of each protein in BGE. Hydrodynamic co-injection of 0.02% DMF in BGE: 30 mbar, 3 s. Temperature:  $25^{\circ}\text{C}$ . For the coating procedure, see section 2.2.

**Figure 3.** Influence of the sample matrix (water (A) and BGE (B)) on the H vs u representations for the separation of five model proteins on a 5-layer PDADMAC/PSS SMIL coating. Sample mixture: 0.2 g/L of each protein in water (A) or BGE (B). Hydrodynamic co-injection of 0.01% DMF in water (A) or BGE (B). Error bars are  $\pm$  one SD on n=5 repetitions. Other experimental conditions as in Fig. 1. (A) CA:  $k(10-2) = 6.32 \pm 0.12$ ,  $cst(\mu m) = 0$ ; TI:  $k(10-2) = 7.34 \pm 0.23$ ,

- cst( $\mu$ m) = 0.01 ± 0.03; Myo: k(10-2) = 5.04 ± 0.20, cst( $\mu$ m) = 0; RNAse A: k(10-2) = 5.79 ± 0.27,
- cst( $\mu$ m) = 0.08 ± 0.18, Lys: k(10-2) = 5.99 ± 0.23, cst( $\mu$ m) = 0. (B) CA: k(10-2) = 3.98 ± 0.31,
- cst( $\mu$ m) = 2.23  $\pm$  0.23; TI: k(10-2) = 4.29  $\pm$  0.12, cst( $\mu$ m) = 4.71  $\pm$  0.12; Myo: k(10-2) = 3.08  $\pm$
- 652 0.23,  $cst(\mu m) = 2.03 \pm 0.16$ ; RNAse A:  $k(10-2) = 3.50 \pm 0.08$ ,  $cst(\mu m) = 2.61 \pm 0.04$ , Lys: k(10-2)
- 653 =  $3.90 \pm 0.16$ , cst( $\mu$ m) =  $1.78 \pm 0.06$ .
- 654 Figure 4. Superposition of five repetitions of electropherograms of five model proteins at -
- 10kV on 5-layer PDADMAC/PSS SMIL coatings for PSS-contaminated PDADMAC coating
- 656 solution (A), PDADMAC-contaminated PSS coating solution (B), and non-contaminated
- polyelectrolyte solutions (C). Peak identification: CA (1), TI (2), Myo (3), RNAse A (4), Lys (5).
- Other experimental conditions as in Fig. 1.
- 659 **Figure 5**. Principles of repeatability and intermediate precision.
- 660 **Figure 6**. Superposition of five successive series of separations of five model proteins on a
- single 5-layer PDADMAC/PSS SMIL coating, showing the H vs u curves for Myo. Error bars are
- ± one SD on n=5 repetitions. Experimental conditions as in Fig. 1.
- Figure 7. Representations of plate heights H as a function of u on a 5-layer PDADMAC/PSS
- 664 SMIL coating after storage for one month in BGE (A) and after regeneration (rinsed with a 2
- M NaCl, 0.1 M NaOH solution for 10 min and then the normal coating procedure) (B). Other
- 666 experimental conditions as in Fig. 1.