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Highlights

Anisotropic damage state modeling based on harmonic decomposition and discrete simulation of fracture

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- This study proposes an anisotropic damage state modeling for quasi-brittle materials.
- It aims at representing around 76 000 (discrete) beam-particle computations of bi-dimensional effective (damaged) elasticity tensors.
- It proposes a methodology to formulate an anisotropic damage model based on a covariant reconstruction formula of bi-dimensional orthotropic elasticity tensors.

Anisotropic damage state modeling based on harmonic decomposition and discrete simulation of fracture

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ABSTRACT

This study proposes an anisotropic damage state modeling based on (i) a discrete element model for quasi-brittle material and (ii) a decomposition of the elasticity tensor in covariants. A procedure is proposed to measure the evolutions of effective (damaged) elasticity tensors computed by a beam-particle model. Various multiaxial damaging loadings allow us to constitute a dataset of around 76 000 effective elasticity tensors. We then identify, in a tensorial manner, the anisotropic damage state for the whole dataset. A detailed analysis of the dataset, using the distance to orthotropy as a guideline, justifies representing the induced micro-cracking by a single second-order damage variable, even in the final stages with strong micro-cracks interaction. To formulate the damage state coupling, we use a reconstruction formula of orthotropic elasticity tensors in terms of invariants and (tensor) covariants. Thanks to this formula, some parts of the effective elasticity tensors $\tilde{\mathbf{E}}$ (such as the dilatation part) are modeled exactly from the single damage variable. Constitutive equations are proposed for the remaining parts of $\tilde{\mathbf{E}}$ (such as its generalized shear modulus and fourth-order harmonic part) using physical assumptions from micro-mechanics and a sparse data driven approach. The proposed anisotropic damage state coupling accurately models the damaged elasticity tensors in multiaxial loading, proportional or non-proportional, up to high damages. The present study firstly highlights the need for an anisotropic damage model for quasi-brittle materials and, secondly, offers a methodology to formulate the damage state coupling by explicit formulas introducing at most two dedicated parameters: the (optional) nonlinear shear-damage coupling parameter m and the harmonic prefactor h .

1 Introduction

2 Predicting the behavior of quasi-brittle materials – such as concrete or mortar – is essential to guarantee the
3 integrity of civil engineering structures. When undamaged, these quasi-brittle materials often exhibit an isotropic
4 elastic behavior. Severe mechanical loading leads to the nucleation and growth of micro-cracks and the loss of load-
5 bearing capabilities (Bažant and Gambarova, 1984; Bažant and Oh, 1985; Landis, 1999). The orientation of the micro-
6 cracks due to loading produces induced mechanical anisotropy (Mazars, 1984; Bažant and Prat, 1988a,b; Mazars
7 et al., 1990; Ramtani et al., 1992; Lubarda and Krajcinovic, 1993; Fichant et al., 1999). Further increase of the
8 loading gradually leads to the concentration and the coalescence of micro-cracks, which result in structural failure
9 by macroscopic cracking (Lemaitre, 1992).

10 Continuous damage models account for the material mechanical degradation during loading, including damage
11 initiation (Lemaitre, 1992; Krajcinovic, 1996; Lemaitre and Desmorat, 2005; Murakami, 2012). The modeling of
12 macroscopic damage usually starts with the choice of a thermodynamics variable, the damage variable, which
13 represents the micro-cracking state of the material. The tensorial nature of the damage variable has been discussed
14 in classical literature (Vakulenko and Kachanov, 1971; Chaboche, 1979; Leckie and Onat, 1981; Chaboche, 1984;
15 Lemaitre and Chaboche, 1985; Murakami, 1988) as well as in recent works (Cormery and Weleman, 2010; Desmorat
16 and Desmorat, 2016; Dormieux and Kondo, 2016; Fassin et al., 2019; Oliver-Leblond et al., 2021). The main question
17 was whether or not the damage state could be represented by a fourth-order tensor (Chaboche, 1978, 1979; Krajcinovic,
18 1985; Kachanov, 1993), by two second-order tensors (Ladevèze, 1983, 1995; Desmorat and Desmorat, 2016), or by
19 a single second-order tensor (Murakami and Ohno, 1978; Cordebois and Sidoroff, 1980, 1982; Murakami, 1988;

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Kachanov, 1993; Halm and Dragon, 1996; Papa and Taliercio, 1996; Lemaitre et al., 2000; Lemaitre and Desmorat, 2005; Desmorat et al., 2018) instead of a scalar variable.

The simplest modeling choice is the one of a scalar damage variable (Kachanov, 1958; Rabotnov, 1969; Lemaitre, 1984). Thanks to their simplicity, isotropic damage models are often used to compute the degradation of concrete structures (Mazars, 1984; Grassl and Jirásek, 2006; Richard and Ragueneau, 2013). These models assume that the material behavior remains isotropic when damaging. In accordance with damage measurements (Ramtani et al., 1992; Lemaitre et al., 2000), micro-mechanics studies of micro-cracked media, such as the ones of Chaboche (1984), Lubarda and Krajcinovic (1993) and Kachanov (1993), show indeed that damage is not isotropic and has to be represented by a damage tensor physically linked to the crack density:

- a fourth-order tensor in the 3D case,
- a second-order tensor in the simpler 2D case with lubricated non-interacting cracks.

We aim to generalize the latter 2D result to the case of strongly interacting micro-cracks, *i.e.*, up to their coalescence, to model the total failure of a specimen (an Area Element in the present work). A first possibility would be to use a nonlinear homogenization scheme (Kachanov, 1993; Ponte Castañeda and Willis, 1995; Dormieux and Kondo, 2016). But these schemes rely on Fracture Mechanics at the microscale. This theory that does not deal with crack initiation, nor does accurately represent multiple cracks interaction and coalescence. Following Rinaldi and Lai (2007) and Delaplace and Desmorat (2008), we prefer instead to rely on discrete simulations of multiple cracking by lattice models (Hrennikoff, 1941; Kawai, 1978; Herrmann and Roux, 1990; Schlangen and van Mier, 1992; Bolander et al., 1996) — more precisely, on a beam-particle model (Delaplace, 2008; Vassaux et al., 2016). Indeed, these discrete models are based on the brittle failure of beams (at the micro-scale). They allow for both the modeling of micro-cracks initiation and the natural representation of micro-cracks coalescence. They represent well the material behavior of quasi-brittle materials such as concrete or mortar (Bažant et al., 1990; Delaplace et al., 1996; van Mier et al., 2002; Challamel et al., 2015; Oliver-Leblond, 2019).

We aim at formulating an accurate anisotropic damage state coupling for quasi-brittle materials as a twin modeling of discrete (beam-particle) bi-dimensional fracture. The present work is a continuation of the one of Oliver-Leblond et al. (2021), who did introduce a suitable macroscopic damage variable with such an approach. But, contrary to these authors, who did assess for the representativity of their damage variable in a few loading cases only, we here build a large dataset of around 76 000 bi-dimensional effective elasticity tensors. The dataset is constituted of tensors from 21 mechanical loadings, proportional or not, and 36 virtual specimens with different micro-structures. Repeated computations for different micro-structures allow us to obtain statistically representative results. Performing complex multiaxial loadings allow to obtain multiple fracture patterns representative of quasi-brittle specimens. The harmonic decomposition of bi-dimensional elasticity tensors (Blinowski et al., 1996; Vianello, 1997) is completed by an analysis their harmonic part (Desmorat and Desmorat, 2015) and by computations of their distance to orthotropy. It is used to derive a meaningful macroscopic second-order damage variable, as well as its full coupling with the scalar (invariant) and tensorial (covariant) components of the elasticity tensor harmonic decomposition.

Section 1 introduces the harmonic decomposition and the reconstruction of a bi-dimensional elasticity tensor by means of its covariants, which serves as the basis of the proposed modeling. It also defines the distance of an elasticity tensor to a symmetry class, which will be used to analyze our whole dataset. Section 2 begins with the presentation of the considered discrete model, then details a measurement method for the effective elasticity tensors computed by discrete virtual testing (of Area Element cracked by severe mechanical loading). This procedure is applied to multiple complex mechanical loadings, proportional or not, to constitute a dataset of 76 356 effective (*i.e.*, damaged) elasticity tensors. Based on this large dataset, sections 3 and 4 are dedicated to modeling the effect of micro-cracking, *i.e.*, of anisotropic damage, on the (invariant) shear modulus μ and the (covariant) fourth-order harmonic part \mathbf{H} of the elasticity tensors. Section 5 summarizes and combines the results from sections 1, 3, and 4 to propose an anisotropic damage state coupling by means of only two specific material parameters: the nonlinear shear-damage coupling parameter m and the harmonic prefactor h . Finally, the proposed coupling is assessed in section 6.

Notations and definitions

Let $d = 2$ be the dimension, and $O(2)$ be the orthogonal group. The (left) action of an orthogonal transformation $Q \in O(2)$ on a second-order tensor \mathbf{t} or a fourth-order tensor \mathbf{T} is

$$(Q \star \mathbf{t})_{ij} = Q_{ik} Q_{jl} t_{kl}, \quad (Q \star \mathbf{T})_{ijkl} = Q_{ip} Q_{jq} Q_{kr} Q_{ls} T_{pqrs}. \quad (1)$$

69 An elasticity tensor is a positive-definite fourth-order tensor \mathbf{E} having the index symmetries $E_{ijkl} = E_{jikl} = E_{ijlk} =$
 70 E_{klij} . The vector space

$$\text{Ela}(\mathbb{R}^2) = \{ \mathbf{E} \mid E_{ijkl} = E_{jikl} = E_{ijlk} = E_{klij} \}, \quad (2)$$

71 of bi-dimensional elasticity tensors, is of dimension 6. A covariant of a bi-dimensional elasticity tensor \mathbf{E} is a tensorial
 72 function $\mathbf{C}(\mathbf{E})$ such that

$$\mathbf{C}(Q \star \mathbf{E}) = Q \star \mathbf{C}(\mathbf{E}), \quad \forall Q \in O(2). \quad (3)$$

73 An invariant of a d -dimensional elasticity tensor \mathbf{E} is a covariant of order zero of \mathbf{E} , *i.e.*, a function $I(\mathbf{E})$ such that

$$I(Q \star \mathbf{E}) = I(\mathbf{E}), \quad \forall Q \in O(2). \quad (4)$$

74 A harmonic tensor is a traceless totally symmetric tensor. A second-order harmonic tensor is a so-called deviatoric
 75 tensor. We denote by $\mathbb{H}^n(\mathbb{R}^2)$ the vector space of harmonic bi-dimensional tensors of order n . Remark that $\mathbb{H}^0(\mathbb{R}^2)$ is
 76 isomorphic to \mathbb{R} .

77 **1. Reconstruction of a bi-dimensional orthotropic elasticity tensor by means of its** 78 **covariants**

79 **1.1. Harmonic decomposition**

80 The harmonic decomposition of a 2D elasticity tensor \mathbf{E} is its equivariant decomposition into harmonic tensors
 81 (Blinowski et al., 1996; Vianello, 1997)

$$\mathbf{E} = (\mu, \kappa, \mathbf{d}', \mathbf{H}), \quad (5)$$

82 such that

$$Q \star \mathbf{E} = (\mu, \kappa, Q \star \mathbf{d}', Q \star \mathbf{H}), \quad \forall Q \in O(2), \quad (6)$$

83 the harmonic components of \mathbf{E} being the invariants $\mu, \kappa \in \mathbb{H}^0(\mathbb{R}^2)$ (the generalized shear and bulk moduli,
 84 respectively), the second-order covariant $\mathbf{d}' = \mathbf{d}'(\mathbf{E}) \in \mathbb{H}^2(\mathbb{R}^2)$ and the fourth-order covariant $\mathbf{H} = \mathbf{H}(\mathbf{E}) \in \mathbb{H}^4(\mathbb{R}^2)$.
 85 The covariant $\mathbf{d}'(\mathbf{E})$ is the deviatoric part $\mathbf{d}' = \mathbf{d} - \frac{1}{2}(\text{tr } \mathbf{d}) \mathbf{1}$ of the dilatation tensor

$$\mathbf{d} = \text{tr}_{34} \mathbf{E} = \mathbf{E} : \mathbf{1}, \quad (7)$$

86 and the covariant $\mathbf{H}(\mathbf{E})$ is the fourth-order harmonic part of \mathbf{E} . We note $\mathbf{1}$ the second-order identity tensor. The scalar
 87 components of the harmonic decomposition of \mathbf{E} are

$$\mu = \frac{1}{8} (2 \text{tr } \mathbf{v} - \text{tr } \mathbf{d}), \quad \kappa = \frac{1}{4} \text{tr } \mathbf{d}, \quad (8)$$

88 where $\mathbf{v} = \mathbf{v}(\mathbf{E})$ is the second-order covariant

$$\mathbf{v} = \text{tr}_{13} \mathbf{E}. \quad (9)$$

89 It is such that $\mathbf{v}' = \mathbf{d}'$.

90 The scalars

$$I_2(\mathbf{E}) = I_2(\mathbf{d}') = \|\mathbf{d}'\|^2 = \mathbf{d}' : \mathbf{d}', \quad \|\mathbf{H}\|^2 = \mathbf{H} : : \mathbf{H}, \quad \text{and} \quad K_3(\mathbf{E}) = \mathbf{d} : \mathbf{H} : \mathbf{d}, \quad (10)$$

91 are three other invariants of the elasticity tensor (Vianello, 1997).

92 A first reconstruction formula of an elasticity tensor \mathbf{E} by means of its covariant is the explicit harmonic
 93 decomposition itself,

$$\mathbf{E} = 2\mu\mathbf{J} + \kappa\mathbf{1} \otimes \mathbf{1} + \frac{1}{2} (\mathbf{1} \otimes \mathbf{d}' + \mathbf{d}' \otimes \mathbf{1}) + \mathbf{H}, \quad \begin{cases} \mathbf{Iso} = 2\mu\mathbf{J} + \kappa\mathbf{1} \otimes \mathbf{1}, \\ \mathbf{Dil} = \frac{1}{2} (\mathbf{1} \otimes \mathbf{d}' + \mathbf{d}' \otimes \mathbf{1}), \end{cases} \quad (11)$$

94 which defines \mathbf{Iso} as the isotropic part of \mathbf{E} , \mathbf{Dil} as its dilatation part and $\mathbf{H} = \mathbf{E} - \mathbf{Iso} - \mathbf{Dil}$ as its fourth-order harmonic
 95 part. All three tensors \mathbf{Iso} , \mathbf{Dil} and \mathbf{H} are fourth-order covariants of \mathbf{E} . The reconstruction formula (11) applies to
 96 all 2D elasticity tensors, possibly fully anisotropic (*i.e.*, biclinic). In Eq. (11), \mathbf{I} is the fourth order identity tensor (of
 97 components $I_{ijkl} = \frac{1}{2}(\delta_{ik}\delta_{jl} + \delta_{il}\delta_{jk})$) and $\mathbf{J} = \mathbf{I} - \frac{1}{2}\mathbf{1} \otimes \mathbf{1}$ is the fourth-order deviatoric projector.

1.2. Harmonic square

To obtain a reconstruction formula dedicated to orthotropic elasticity tensors, we have to introduce the harmonic product $\mathbf{h}_1 * \mathbf{h}_2 \in \mathbb{H}^4(\mathbb{R}^2)$ of two second-orders harmonic tensors \mathbf{h}_1 , and \mathbf{h}_2 . In 2D, it is defined as the fourth-order harmonic tensor (see Olive et al. (2017))

$$\mathbf{h}_1 * \mathbf{h}_2 = \mathbf{h}_1 \otimes \mathbf{h}_2 - \frac{1}{2}(\mathbf{h}_1 : \mathbf{h}_2) \mathbf{J}, \quad \mathbf{J} = \mathbf{I} - \frac{1}{2} \mathbf{1} \otimes \mathbf{1}. \quad (12)$$

where \mathbf{J} is the so-called deviatoric projector. Recall then that any 2D fourth-order harmonic tensor $\mathbf{H} \in \mathbb{H}^4(\mathbb{R}^2)$ can be written as a harmonic square (Desmorat and Desmorat, 2015),

$$\mathbf{H} = 2\Lambda \mathbf{e} * \mathbf{e}, \quad \text{tr } \mathbf{e} = 0, \quad \|\mathbf{e}\| = 1, \quad (13)$$

where $\mathbf{e} \in \mathbb{H}^2(\mathbb{R}^2)$ is a unit second-order deviatoric eigentensor associated with a non-zero eigenvalue Λ or $-\Lambda$ of the harmonic tensor \mathbf{H} . This is not a so-called reconstruction formula for \mathbf{H} since \mathbf{e} is not a covariant of \mathbf{H} .

A more interesting formula is obtained when $\mathbf{H} = \mathbf{H}(\mathbf{E})$ is the fourth order harmonic part of an (exactly) orthotropic elasticity tensor. We have in that case, in 2D still (Oliver-Leblond et al., 2021),

$$\mathbf{H} = \frac{2K_3(\mathbf{E})}{I_2^2(\mathbf{E})} \mathbf{d}'(\mathbf{E}) * \mathbf{d}'(\mathbf{E}). \quad (14)$$

Remark that the covariants —including invariants— involved are covariants of the elasticity tensor, which is orthotropic, not of the harmonic tensor \mathbf{H} , which has the square symmetry (Verchery, 1982; Vianello, 1997; Vannucci, 2005). This means that we have the following reconstruction formula (by means of its covariants) for a 2D orthotropic elasticity tensor

$$\mathbf{E} = 2\mu \mathbf{J} + \kappa \mathbf{1} \otimes \mathbf{1} + \frac{1}{2} (\mathbf{1} \otimes \mathbf{d}' + \mathbf{d}' \otimes \mathbf{1}) + \frac{2K_3}{I_2^2} \mathbf{d}' * \mathbf{d}', \quad (15)$$

where μ , κ , I_2 and K_3 are invariants of the elasticity tensor (defined by Eq. (8) and Eq. (10)), and \mathbf{d} is a second-order covariant of \mathbf{E} (defined by Eq. (7)). Remark that for this formula to hold, since $I_2(\mathbf{d}' = 0) = 0$ it is necessary that $\mathbf{d}' \neq 0$. In other words, it is necessary that the dilatation tensor $\mathbf{d} = \mathbf{d}(\mathbf{E})$ —which inherits the symmetry of \mathbf{E} , Olive et al. (2022)— and therefore \mathbf{E} , are orthotropic.

1.3. Definition of a tensorial damage variable

We can furthermore assume that the elasticity tensor \mathbf{E} of a quasi-brittle material evolves during loading, for instance, due to damage, and that it has the initial isotropic value

$$\mathbf{E}_0 = 2\mu_0 \mathbf{J} + \kappa_0 \mathbf{1} \otimes \mathbf{1}. \quad (16)$$

The initial dilatation tensor is then isotropic (*i.e.*, spherical),

$$\mathbf{d}_0 = \mathbf{E}_0 : \mathbf{1} = 2\kappa_0 \mathbf{1}. \quad (17)$$

A damage variable, noted \mathbf{D} in the present work, represents the state of micro-cracking of a quasi-brittle material (Lemaitre and Chaboche, 1985). It is set as zero when the effective elasticity tensor \mathbf{E} is the initial elasticity tensor \mathbf{E}_0 . The eigenvalues of the damage tensor are usually bounded by 1. The present work aims to determine the general coupling with damage $\mathbf{E} = \mathbf{E}(\mathbf{D})$.

By Eq. (8), the bulk modulus κ is exactly reconstructed from the dilatation tensor \mathbf{d} . This has led Oliver-Leblond et al. (2021) to define the dimensionless damage variable \mathbf{D} as the second-order tensor

$$\mathbf{D} = \mathbf{1} - \frac{\mathbf{d}}{2\kappa_0}. \quad (18)$$

Remark that since the initial dilatation tensor is given by $\mathbf{d}_0 = \text{tr}_{12} \mathbf{E}_0 = 2\kappa_0 \mathbf{1}$, we have the equalities

$$\mathbf{D} = \frac{1}{2\kappa_0} \text{tr}_{12}(\mathbf{E}_0 - \mathbf{E}) = (\mathbf{d}_0 - \mathbf{d}) \cdot \mathbf{d}_0^{-1} = \mathbf{d}_0^{-1} \cdot (\mathbf{d}_0 - \mathbf{d}). \quad (19)$$

127 This mapping provides a bijection between the damage variable \mathbf{D} and the dilatation tensor \mathbf{d} . Indeed, the latter and
 128 the bulk modulus are related to \mathbf{D} as

$$\mathbf{d} = 2\kappa_0 (\mathbf{1} - \mathbf{D}), \quad \kappa = \frac{1}{4} \text{tr } \mathbf{d} = \kappa_0 \left(1 - \frac{1}{4} \text{tr } \mathbf{D}\right). \quad (20)$$

129 **1.4. Distance to isotropy – Distance to orthotropy**

130 A key question is then whether or not the damage of quasi-brittle materials can be represented in 2D by the single
 131 second-order damage tensor \mathbf{D} . An underlying question is whether or not the damaged elasticity tensor of an Area
 132 Element (AE) of a quasi-brittle material can be close to orthotropy (since \mathbf{D} is either isotropic or orthotropic). One will
 133 also have to check to what extent the initial (elastic) AE is isotropic.

134 The determination of the symmetry class of a measured elasticity tensor is a difficult problem (Gazis et al., 1963;
 135 François, 1995; François et al., 1998; Moakher and Norris, 2006; Diner et al., 2011). A cause is that the measurement
 136 orientation might not correspond to the principal direction of the expected symmetry class, which prevents direct
 137 identification by comparison to normal (Kelvin) forms. Furthermore, experimental measurements provide a noised
 138 approximation of the material's elastic properties (Roux et al., 1985; Migliori et al., 1993). The measured elasticity
 139 tensor will generically be biclinic in 2D (and triclinic in 3D).

140 Those issues can be mitigated by calculating the distance to the expected elasticity symmetry class, more precisely,
 141 the distance to the considered symmetry stratum (which is the set of all tensors which have the same symmetry class
 142 (Auffray et al., 2014; Abramian et al., 2020)). This usually consists, first, in finding elasticity tensor \mathbf{E}^* in the symmetry
 143 stratum $\bar{\Sigma}$ which is the closest to the measured elasticity tensor \mathbf{E} , and second, in calculating the distance between \mathbf{E}
 144 and \mathbf{E}^* . The relative distance to the symmetry stratum $\bar{\Sigma}$ is then

$$\Delta_{\bar{\Sigma}}(\mathbf{E}) = \min_{\mathbf{E}^* \in \bar{\Sigma}} \frac{\|\mathbf{E} - \mathbf{E}^*\|}{\|\mathbf{E}\|}. \quad (21)$$

145 In the case of isotropy, the harmonic decomposition provides, by orthogonal projection (Vianello, 1997), the closest
 146 isotropic tensor \mathbf{E}^* to \mathbf{E} as its isotropic part \mathbf{Iso} (defined by Eq. (11)),

$$\Delta_{\text{Iso}}(\mathbf{E}) = \min_{\mathbf{E}^* \text{ isotropic}} \frac{\|\mathbf{E} - \mathbf{E}^*\|}{\|\mathbf{E}\|} = \frac{\|\mathbf{E} - \mathbf{Iso}(\mathbf{E})\|}{\|\mathbf{E}\|}, \quad \mathbf{E}^* = \mathbf{Iso}(\mathbf{E}). \quad (22)$$

147 The calculation of the distance to 2D elastic orthotropy requires more mathematical development (Vianello, 1997;
 148 Antonelli et al., 2022). An upper bound of this distance is obtained thanks to the orthotropic reconstruction formula
 149 (15) (Oliver-Leblond et al., 2021).

$$\Delta_{\text{Ort}}(\mathbf{E}) = \min_{\mathbf{E}^* \text{ orthotropic}} \frac{\|\mathbf{E} - \mathbf{E}^*\|}{\|\mathbf{E}\|} \leq \frac{\|\mathbf{E} - \mathbf{E}^{\text{up}}\|}{\|\mathbf{E}\|}, \quad (23)$$

150 where

$$\mathbf{E}^{\text{up}} = 2\mu\mathbf{J} + \kappa\mathbf{1} \otimes \mathbf{1} + \frac{1}{2} (\mathbf{1} \otimes \mathbf{d}' + \mathbf{d}' \otimes \mathbf{1}) + \frac{2K_3}{I_2^2} \mathbf{d}' * \mathbf{d}'. \quad (24)$$

151 This upper bound, based on the covariants of the elasticity tensor, is easier to calculate than the exact distance (the
 152 corresponding formulas are recalled in Appendix A).

153 **2. Discrete virtual testing**

154 This part aims at presenting the discrete virtual testing procedure based on discrete simulations of the cracking
 155 of Area Elements. The discrete model used is a hybrid beam-particle model which combines two types of models
 156 (Meguro and Hakuno, 1989; Kun and Herrmann, 1996; D'Addetta et al., 2002; Bolander et al., 2021): the lattice
 157 models (Hrennikoff, 1941; Kawai, 1978; Herrmann and Roux, 1990) and the particular models (Cundall and Strack,
 158 1979; Bažant et al., 1990). The model, which directly originates from the work of (Delaplace et al., 1996; Delaplace,
 159 2008), is first presented, followed by the procedure for the systematic measurement of elasticity tensors. Then, the
 160 evolutions of effective elasticity tensors measured during various loadings allow us to generate a large dataset of
 161 elasticity tensors.

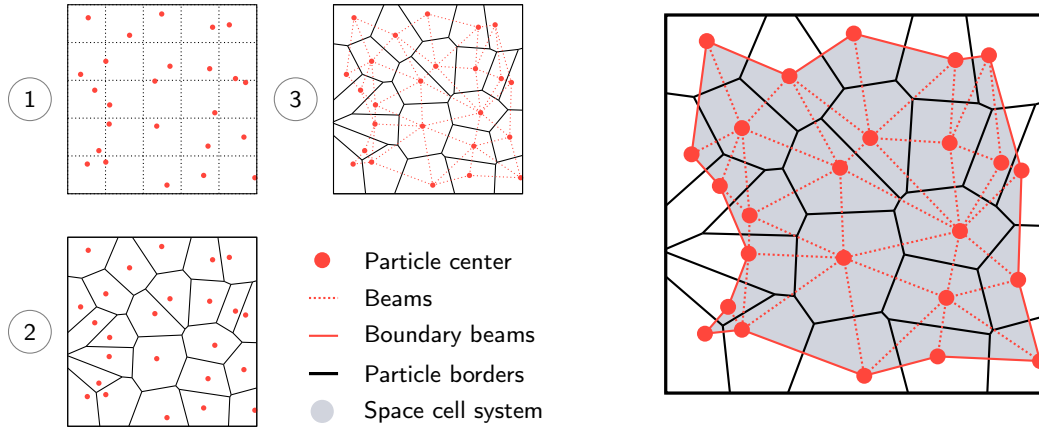


Figure 1: Representation of the mesh of the beam-particle model. (1) is the positioning of the particle centers in the grid. (2) is the generation of the particle border by the Voronoi tessellation of the particle centers. (3) adds the beam network based on the Delaunay triangulation of the particle centers.

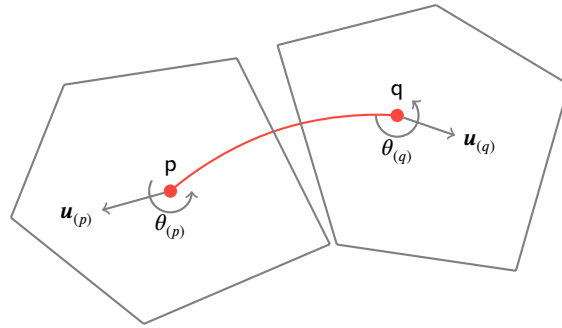


Figure 2: Representation of a beam and notations

2.1. Beam-particle model

The discrete hybrid model considered is the beam-particle one developed by (Vassaux, 2015; Vassaux et al., 2016). As shown by Oliver-Leblond (2019), it accurately represents the failure process encountered in quasi-brittle materials. For this study, a new linear solver (Davis, 2011) has been incorporated in the implementation. Here, the 2D version of the model is used.

An elementary area is modeled using a beam-particle model. The left part of Figure 1 illustrates the procedure to generate the mesh of the model. The beam-particle specimen is composed of a set of rigid particles. Particle centers are randomly placed in each cell of a grid with a cell size \bar{l}_b which corresponds to the average beam length. Particle boundaries are obtained from the Voronoi tessellation of the particle centers. The dual graph of the Voronoi tessellation is the Delaunay triangulation. It associates a segment to each pair of neighboring particles. Those segments are used as the geometric support for a beam network. This beam network models the cohesion of the material. Each beam (p, q) , linking particles p and q , has an Euler-Bernoulli behavior and is parametrized by:

- its length $l_{(p,q)}$,
- its section $A_{(p,q)}$,
- its Young modulus $E_{(p,q)}$, and
- its coefficient of inertia $\alpha_{(p,q)} = 64I_{(p,q)}\pi/A_{(p,q)}^2$.

Name	Symbol	Value	Unit
Average beam length	\bar{l}_b	0.002	m
Young's modulus	E_b	60	GPa
Coefficient of inertia	α_b	0.85	-
Scale factor (extension)	$\lambda_{\varepsilon_{cr}}$	5.0×10^{-4}	-
Scale factor (rotation)	$\lambda_{\theta_{cr}}$	2.8×10^{-3}	-
Shape factor	k	1.0	-

Table 1

Parameters of beam-particle model

178 The geometric parameters $l_{(p,q)}$ and $A_{(p,q)}$ are obtained from the mesh's geometry; they thus depend on the beam. Note
 179 that the cell size of the grid \bar{l}_b corresponds to the average beam length. The mechanical parameters $E_{(p,q)}$ and $\alpha_{(p,q)}$ are
 180 chosen equal to E_b and α_b for all beams, which are identified to match a cement mortar macroscopic elastic behavior.

181 Fracture properties are introduced by adding a brittle failure criterion $P_{(p,q)}$ to each beam, so beam rupture occurs
 182 when

$$P_{(p,q)} = \frac{\varepsilon_{(p,q)}}{\varepsilon_{(p,q)}^{cr}} + \frac{|\theta_{(p)} - \theta_{(q)}|}{\theta_{(p,q)}^{cr}} > 1. \quad (25)$$

183 where:

- 184 • $\varepsilon_{(p,q)} = \frac{\|\mathbf{u}_{(p)} - \mathbf{u}_{(q)}\|}{l_{(p,q)}}$ is the extension of the beam,
- 185 • $\mathbf{u}_{(p)}$ is the displacement of particle p ,
- 186 • $\theta_{(p)}$ is the rotation of particle p ,
- 187 • $\varepsilon_{(p,q)}^{cr}$ is the breaking threshold in extension of beam (p, q) , and
- 188 • $\theta_{(p,q)}^{cr}$ is the breaking threshold in rotation.

189 Those quantities are illustrated in Figure 2.

190 Delaplace and Desmorat (2008) took the same failure thresholds for all beams. Following (Rossi and Richer, 1987;
 191 de Arcangelis and Herrmann, 1989; Herrmann et al., 1989; Herrmann and Roux, 1990; D'Addetta et al., 2002; Vassaux,
 192 2015), random distributions for the failure thresholds are here considered, as they are more suitable for the modeling
 193 of cement (Schlangen and van Mier, 1992; van Mier et al., 2002).

194 Here, both breaking thresholds $\varepsilon_{(p,q)}^{cr}$ and $\theta_{(p,q)}^{cr}$ are randomly drawn from a Weibull distribution,

$$f(x) = \frac{k}{\lambda} \left(\frac{x}{\lambda}\right)^{k-1} e^{-\left(\frac{x}{\lambda}\right)^k} \quad (26)$$

195 where λ is the scale factor and k is the shape factor. The spatial variability of the breaking thresholds is supposed to be
 196 identical for both thresholds: $k_{\varepsilon_{cr}} = k_{\theta_{cr}} = k$. This means that the fracture is controlled by three parameters: the shape
 197 factor k , the scale factor in extension $\lambda_{\varepsilon_{cr}}$, and the scale factor in rotation $\lambda_{\theta_{cr}}$. Those three parameters are identified
 198 by fitting the non-linear macroscopic behavior.

199 **Remark 1.** The beam-particle model considered can also represent the microcrack closure effects by adding contact
 200 and friction between the particles when a beam is broken. Contact and friction are not accounted for in this work.

201 The parameters of the beam-particle model, given in Table 1, correspond to a quasi-brittle material such as cement
 202 with the following properties: a Young modulus $E_0 = 36.35$ GPa, a Poisson ratio $\nu_0 = 0.22$, a tensile strength $f_t = 5$
 203 MPa. Note that the elastic properties are equivalent to a bulk modulus $\kappa_0 = 30.0$ GPa and a shear modulus $\mu_0 = 19.4$
 204 GPa.

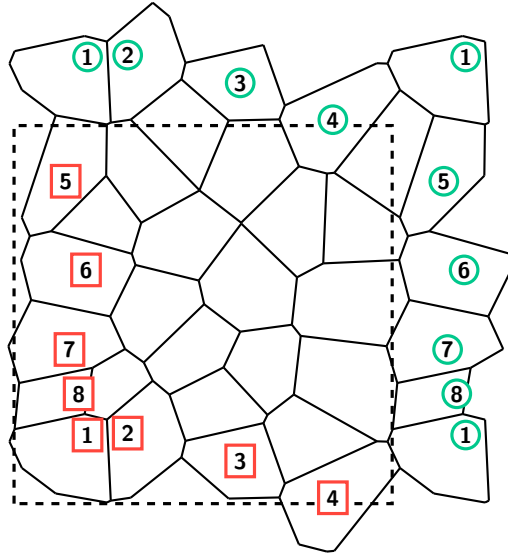


Figure 3: Periodic beam-particle mesh where the red boxed particles are guiding particles and green circled ones are guided particles. Guided particles have the same number as their guiding particle.

2.2. Periodic Boundary Conditions (PBC)

Periodic Boundary Conditions are used to compute the effective elasticity tensor of a square specimen. The PBC are imposed by adding a layer of guided particles on the top and right part of the square mesh, as shown in Figure 3. Each guided particle has the same geometry as the associated guiding particle on the bottom and left part of the mesh. The movement of a guided particle q is constrained to follow its guiding particle p through,

$$\mathbf{u}_{(q)} = \mathbf{u}_{(p)} + \varepsilon_{\text{imp}} (\mathbf{x}_{(q)} - \mathbf{x}_{(p)}) \quad (27)$$

where ε_{imp} is the imposed strain. This relation is enforced in the linear system via Lagrange multipliers.

Remark 2. The linear solver used in the previous versions of the beam-particle model was based on the Cholesky decomposition (Chen et al., 2008). When using Lagrange multipliers, the matrix of the linear system is no longer definite positive; thus, the Cholesky decomposition is no longer applicable. We use a linear solver based on the QR decomposition (Davis, 2011) to circumvent this issue.

2.3. Measurement of an effective elasticity tensor

To obtain the effective —*i.e.*, damaged— elasticity tensor of a discrete specimen, the average strain and stress must be defined from the particle displacements and forces. Numerous definitions of the average strain tensor in discrete media are discussed by Bagi (2006). For the present study, the average strain tensor is defined as

$$\bar{\varepsilon} = \frac{1}{S} \sum_{p=1}^N \left(\frac{\mathbf{u}_{(p)} + \mathbf{u}_{(p+1)}}{2} \odot \mathbf{n}_{(p,p+1)} \right) l_{(p,p+1)} \quad (28)$$

where S is the surface of the space cell system¹ proposed by Bagi (1996) (see Figure 1), $\mathbf{u}_{(p)}$ is the displacement of the particle p , $\mathbf{n}_{(p,p+1)}$ is the outward-pointing normal to the beam linking particles p and $p+1$, and $l_{(p,p+1)}$ is the length of the same beam, and where \odot is the symmetrized tensorial product. For two vectors \mathbf{a} and \mathbf{b} it is such that $\mathbf{a} \odot \mathbf{b} = \frac{1}{2} (\mathbf{a} \otimes \mathbf{b} + \mathbf{b} \otimes \mathbf{a})$. The sum is carried over the N particles on the boundary of the specimen.

The definition of the average stress tensor is a symmetrization of the definition proposed by (Bagi, 1996),

$$\bar{\sigma} = \frac{1}{S} \sum_{p=1}^N \mathbf{f}_{(p)} \odot \mathbf{x}_{(p)} \quad (29)$$

¹The surface of the space cell system is the surface of the specimen that can be deformed; thus, the surface bounded by the lattice network. It is illustrated on Figure 1.

224 where $\mathbf{f}_{(p)}$ is the force applied to particle p and $\mathbf{x}_{(p)}$ is the position of particle p .

225 **Remark 3.** The assumption that the strain and stress are symmetric tensors is necessary for the present small strain
 226 framework. Due to the rotation of the particles, the beam-particle model shall be modeled by a generalized continuum.
 227 Indeed, some studies use higher-order continuum models to represent discrete media (Pradel and Sab, 1998; Ehlers
 228 et al., 2003; Dos Reis and Ganghoffer, 2012; Rezakhani and Cusatis, 2016).

229 Knowing three linearly independent strain tensors $\boldsymbol{\varepsilon}^{(i)}$ and the associated stress tensors $\boldsymbol{\sigma}^{(i)}$, in Kelvin notation,

$$[\boldsymbol{\varepsilon}^{(i)}] = \begin{bmatrix} \boldsymbol{\varepsilon}_{xx}^{(i)} \\ \boldsymbol{\varepsilon}_{yy}^{(i)} \\ \sqrt{2}\boldsymbol{\varepsilon}_{xy}^{(i)} \end{bmatrix}, \quad [\boldsymbol{\sigma}^{(i)}] = \begin{bmatrix} \boldsymbol{\sigma}_{xx}^{(i)} \\ \boldsymbol{\sigma}_{yy}^{(i)} \\ \sqrt{2}\boldsymbol{\sigma}_{xy}^{(i)} \end{bmatrix} \quad (30)$$

230 the elasticity tensor in Kelvin notation can be obtained as the symmetrized 3×3 matrix product

$$[\mathbf{E}] = \left\{ \left[[\boldsymbol{\sigma}^{(1)}], [\boldsymbol{\sigma}^{(2)}], [\boldsymbol{\sigma}^{(3)}] \right] \cdot \left[[\boldsymbol{\varepsilon}^{(1)}], [\boldsymbol{\varepsilon}^{(2)}], [\boldsymbol{\varepsilon}^{(3)}] \right]^{-1} \right\}^S. \quad (31)$$

231 To obtain three linearly independent strain tensors, elastic periodic strain loadings are applied to the virtual specimen

$$[\boldsymbol{\varepsilon}_{\text{imp}}^{(1)}] = \begin{bmatrix} \varepsilon \\ 0 \\ 0 \end{bmatrix}, \quad [\boldsymbol{\varepsilon}_{\text{imp}}^{(2)}] = \begin{bmatrix} 0 \\ \varepsilon \\ 0 \end{bmatrix}, \quad [\boldsymbol{\varepsilon}_{\text{imp}}^{(3)}] = \begin{bmatrix} 0 \\ 0 \\ \sqrt{2}\varepsilon \end{bmatrix}, \quad (32)$$

232 where ε is sufficiently small (chosen such that the loading remains elastic). Algorithm 1 details the procedure to measure
 the evolution of the elasticity tensor during a mechanical loading.

Algorithm 1: Measurement of the evolution of effective elasticity tensor

```

Generate a virtual specimen (micro-structure);
Apply a damaging loading;
Create an empty list of effective elasticity tensor;
foreach load step do
    Extract the cracks;
    Add the cracks to uncracked virtual specimen;
    foreach measurement loading i do
        Apply measurement loading  $[\boldsymbol{\varepsilon}_{\text{imp}}^i]$ ;
        Compute average strain  $[\bar{\boldsymbol{\varepsilon}}^{(i)}]$  Eq. (28);
        Compute average stress  $[\bar{\boldsymbol{\sigma}}^{(i)}]$  Eq. (29);
    end
    Compute effective elasticity tensor Eq. (31);
    Store effective elasticity tensor in the list;
end
  
```

233

234 2.4. Dataset of 76 356 effective elasticity tensors

235 This part is dedicated to generating a large dataset of effective elasticity tensors. To constitute the dataset, 36 virtual
 236 specimens with different micro-structures (but with the same macroscopic properties) are submitted to 21 mechanical
 237 loadings, uniaxial or multiaxial. Each specimen (also called Area Element) is a square of $0.2\text{m} \times 0.2\text{m}$, with an average
 238 beam length $\bar{l}_b = 0.002\text{m}$. Thus, the specimens are composed of 100×100 particles. Each mechanical loading is
 239 discretized into 100 loading steps. The database contains $36 \times 21 = 756$ evolutions of elasticity tensors, each containing
 240 101 elasticity tensors, leading to a total of 76 356 elasticity tensors. Note that some elasticity tensors appear multiple
 241 times in the dataset (when the specimen is not yet damaged).

242 Different types of boundary conditions have been applied to generate this dataset:

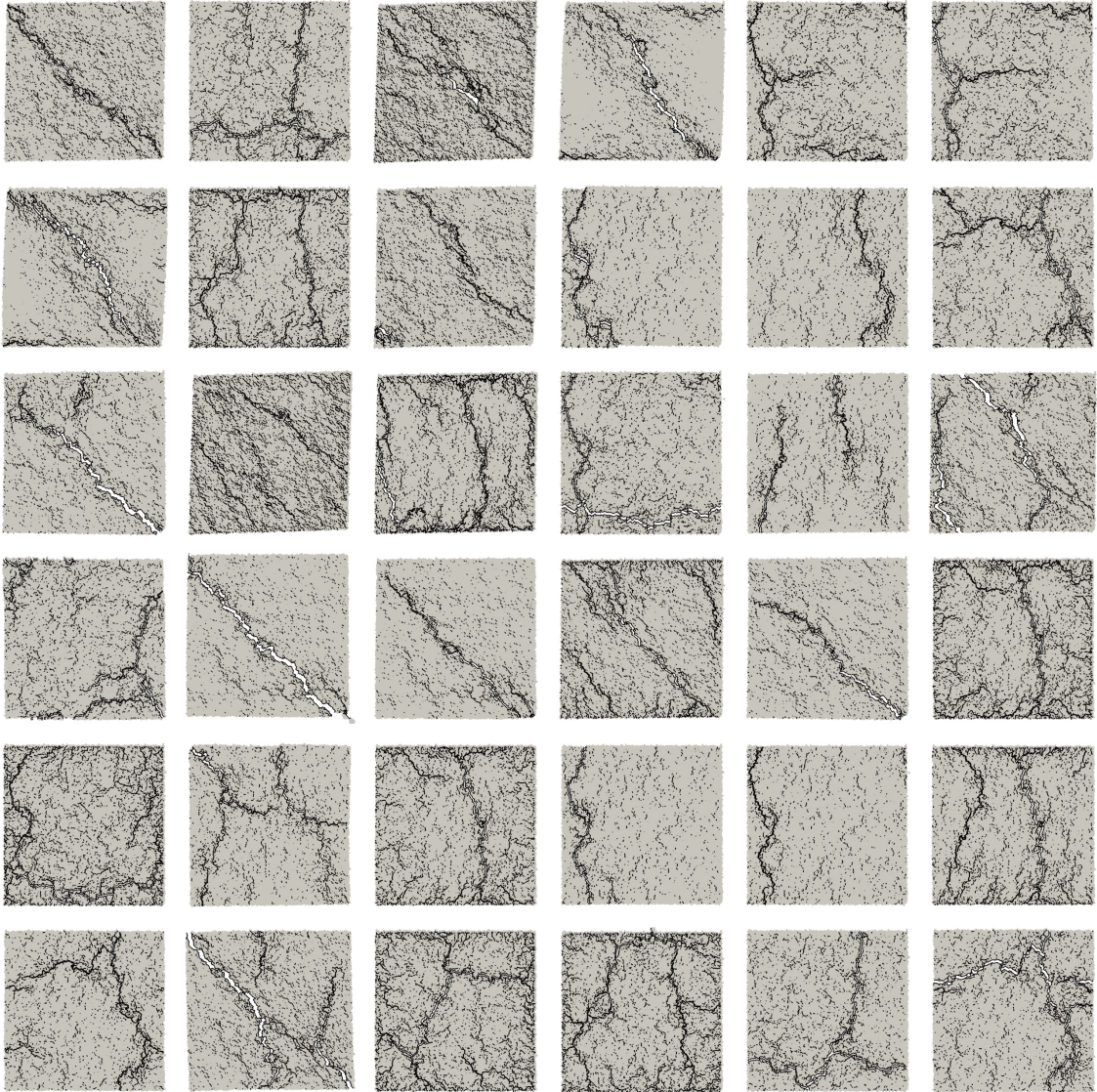


Figure 4: Illustration of localized cracking patterns in the dataset.

- 243 • Kinematic Uniform Boundary Conditions (KUBC), where strain is imposed on the whole boundary of the
244 specimen,
- 245 • Periodic Boundary Conditions (PBC) as described in subsection 2.2, and
- 246 • Experimental Boundary Conditions (EXPE), where displacement is imposed on parts of the boundary.

247 Loadings are also separated into proportional and non-proportional loadings. The latter lead to a rotation of the principal
248 strain/stress directions during the loading. It leads to a misalignment of the loading direction with first-stage micro-
249 cracks, and a change of the damaging direction. The names, descriptions and parameters of the applied loadings
250 are detailed in Appendix B. Examples of final micro-cracking patterns are provided in Figure 4. The measurement
251 procedure is applied for an EXPE bi-tension loading in Figure 5 for illustration purposes.

252 **Remark 4.** Instead of using physical loadings to generate micro-cracks, one could try to create random cracking
253 patterns by randomly breaking beams. This method does not account for the interactions of cracks during the loading.

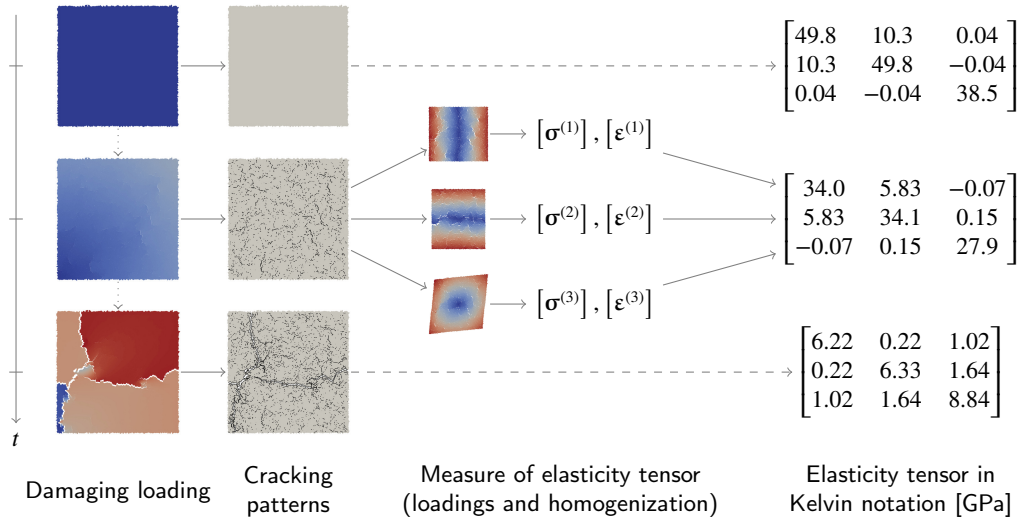


Figure 5: Illustration of the method to measure the evolution of the effective elasticity tensor in the EXPE bi-tension loading.

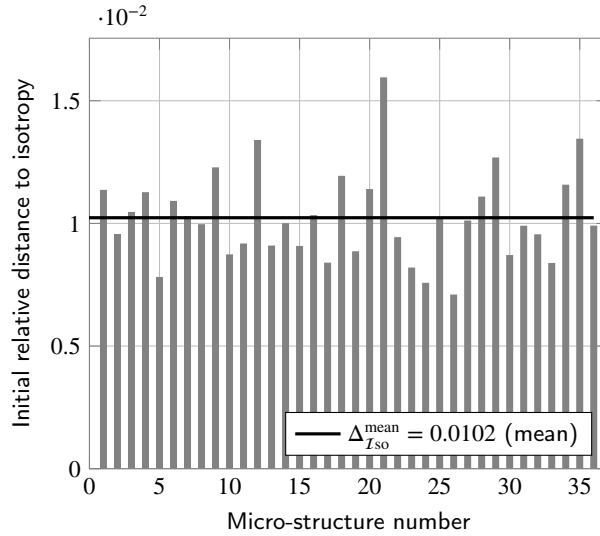


Figure 6: Initial distance to isotropy for each micro-structure in the dataset.

254 We have preferred to apply true mechanical loadings, as those constrain the micro-cracking patterns to "physically-
 255 reachable" ones.

256 **2.5. Isotropy of the initial elasticity tensor E_0**

257 For the present modeling, we suppose that the undamaged elasticity tensor is isotropic. To check that this is also
 258 the case for the undamaged (uncracked) elasticity tensors in the dataset, we compute the distance to isotropy, by
 259 Equation 22, for the 36 micro-structures in the dataset. The results are provided in Figure 6. The mean value of the
 260 initial relative distance to isotropy is $\Delta_{Iso}^{mean} = 0.0102$, whereas the standard deviation is $\Delta_{Iso}^{mean} = 0.0018$. These relative
 261 distances are all between $\Delta_{Iso}^{min} = 0.007$ and $\Delta_{Iso}^{max} = 0.016$. This is sufficient to consider that the elasticity tensors are
 262 initially isotropic.

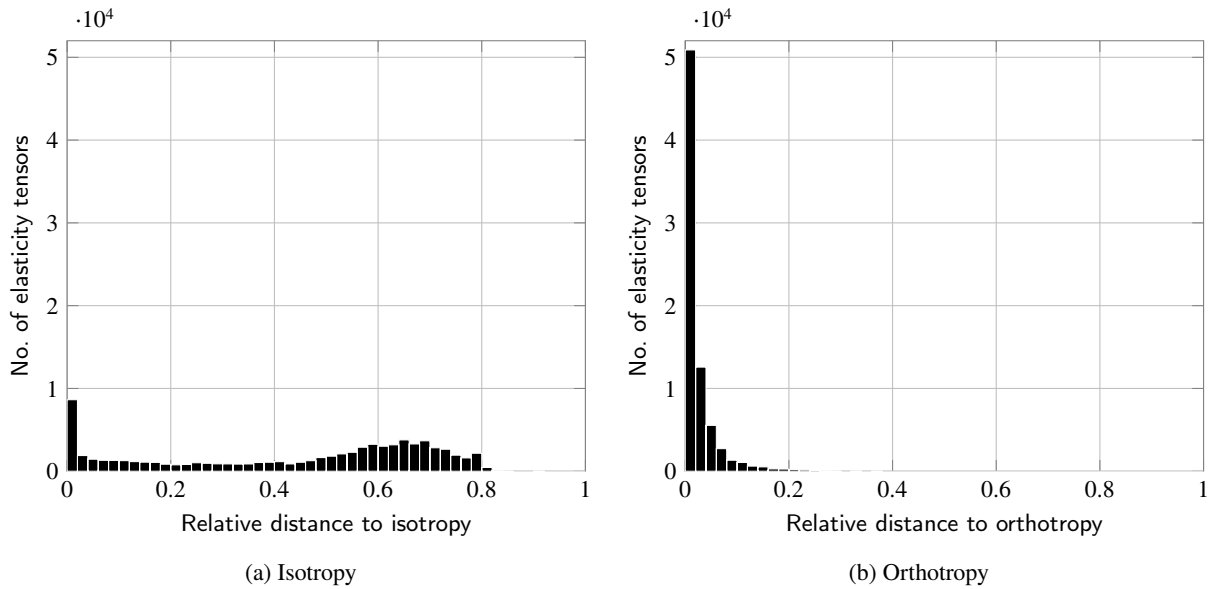


Figure 7: Histograms of relative distances to symmetry classes over the dataset

2.6. Distances to isotropy and to orthotropy of the effective elasticity tensors

The distances of the elasticity tensors to isotropy or to orthotropy can also be used to justify the tensorial nature of the damage variable (Oliver-Leblond et al., 2021). These distances have been computed for each elasticity tensor in the dataset. The corresponding histograms are plotted in Figure 7a and Figure 7b.

In Figure 7a, the distribution of the relative distance to isotropy (Equation 22) shows that a large part of effective elasticity tensors in the dataset is far from being isotropic. This means that a scalar (isotropic) damage variable is insufficient to represent the loss of stiffness (due to micro-cracking).

In the Figure 7b, the distribution of the relative distance to orthotropy (Equation 23) shows that most of the tensors in the dataset are close being orthotropic. This means that the effective elasticity tensor can be modeled as remaining orthotropic during the mechanical loadings of the whole dataset. From the reconstruction formula (15) and in accordance with (Desmorat and Desmorat, 2016), this implies that at most two second-order tensors are required to represent the impact of micro-cracking on the bi-dimensional elasticity tensor.

The question of whether the single second-order tensor \mathbf{D} within the reconstruction formulas of section 1 is sufficient to represent this coupling has to be addressed. By the damage definition in Eq. (18), the bulk modulus κ and the deviatoric part of the dilatation tensor are exactly modeled from the anisotropic damage variable \mathbf{D} . To fully determine the effective elasticity tensor $\mathbf{E} = \mathbf{E}(\mathbf{D})$, the shear modulus μ and the harmonic part \mathbf{H} of \mathbf{E} need to be modeled as functions of the damage \mathbf{D} . It proves essential to note that each term of the harmonic reconstruction formula (11) is orthogonal to each other (see (Blinowski et al., 1996; Vianello, 1997; Desmorat and Desmorat, 2015)). From a modeling point of view, this means that the modeling errors associated with each part \mathbf{Iso} , \mathbf{Dil} and \mathbf{H} of the harmonic decomposition are independent. They can be handled separately. Conversely, this also means that a modeling error on the harmonic part cannot be compensated for by the isotropic part \mathbf{Iso} or by the dilatation part \mathbf{Dil} .

3. Modeling of the shear modulus–damage state coupling

We recall first the expression of the generalized shear modulus μ of the elasticity tensor \mathbf{E} ,

$$\mu = \frac{1}{8} (2 \operatorname{tr} \mathbf{v} - \operatorname{tr} \mathbf{d}), \quad \mathbf{d} = \mathbf{E} : \mathbf{1}, \quad \mathbf{v} = \operatorname{tr}_{13} \mathbf{E}. \quad (33)$$

To express μ as a function of damage tensor \mathbf{D} , a relation between the trace $\operatorname{tr} \mathbf{v}$ of the Voigt tensor and the damage tensor \mathbf{D} has to be exhibited.

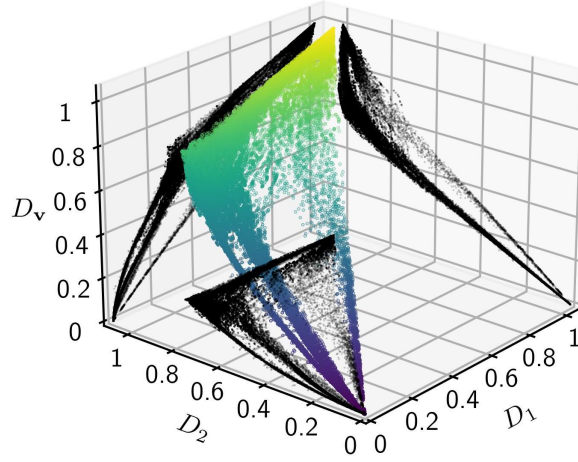


Figure 8: Damage D_v as a function of the eigenvalues D_1 and D_2 ($D_2 > D_1$) of the damage variable \mathbf{D} over the dataset. Each colored point is the value of D_v for an elasticity tensor of the dataset. The black dots are the projections of the data points onto the planes (D_1, D_v) , (D_2, D_v) and (D_1, D_2) .

288 To ease the modeling process, an intermediate scalar variable D_v such that $\text{tr } \mathbf{v} = \text{tr } \mathbf{v}_0(1 - D_v)$ is introduced,

$$D_v = \frac{\text{tr } \mathbf{v}_0 - \text{tr } \mathbf{v}}{\text{tr } \mathbf{v}_0}. \quad (34)$$

289 It can be interpreted as a damage variable based on $\text{tr}(\mathbf{v})$. However, since it represents the same micro-cracking pattern
 290 as \mathbf{D} , it is not assumed to be an additional thermodynamics (internal) variable. It will be modeled as a function of the
 291 damage variable \mathbf{D} .

292 Figure 8 contains a scatter plot of D_v as a function of the two eigenvalues D_1, D_2 of the damage tensor \mathbf{D} for each
 293 elasticity tensor of the dataset. It is observed that the points (D_1, D_2, D_v) of the dataset are grouped around a surface.
 294 Thus, D_v can be modeled as a function of damage by a constitutive equation $D_v = D_v^m(\mathbf{D})$. In practice, we approximate
 295 D_v by the linear combination of invariants of \mathbf{D} ,

$$D_v^m(\mathbf{D}) = c_1 I_1(\mathbf{D}) + c_2 I_2(\mathbf{D}), \quad I_k(\mathbf{D}) = \text{tr}(\mathbf{D}^k) = D_1^k + D_2^k, \quad (35)$$

296 where the upperscript m stands for model, $I_k(\mathbf{D})$ are invariants of \mathbf{D} , and c_k are the parameters of the model. A second
 297 expression

$$D_v^m(\mathbf{D}) = c_1 I_1(\mathbf{D}) + c_2 I_2(\mathbf{D}) + c_3 I_3(\mathbf{D}), \quad I_3(\mathbf{D}) = \frac{1}{2} (3I_1(\mathbf{D}) I_2(\mathbf{D}) - I_1(\mathbf{D})^3), \quad (36)$$

298 will also be studied (but the two-term expansion in Eq. (35) will prove sufficient).

299 The modeling process will be carried out in two steps. The first step consists in deriving and justifying some
 300 physical constraints on the material constants c_k . Those constraints will limit the number of independent parameters
 301 of the model. The second step consists in identifying the parameters c_k .

302 3.1. Physical constraints

303 *Constraint 1 – Undamaged state.* For an undamaged state, the trace of the Voigt tensor keeps its initial value,
 304 $\text{tr } \mathbf{v} = \text{tr } \mathbf{v}_0$,

$$D_v^m(\mathbf{D} = \mathbf{0}) = 0 \quad (37)$$

305 This constraint is satisfied by both Eq. (35) and (36) since the invariants of \mathbf{D} vanish ($I_k(\mathbf{D} = \mathbf{0}) = 0$).

306 *Constraint 2 – Fully damaged state.* For a fully damaged state, the effective elasticity tensor is a null fourth-order
 307 tensor. We have then $\text{tr } \mathbf{v} = 0$, which implies $D_v^m(\mathbf{D} = \mathbf{1}) = 1$ and,

$$2 \sum_{k=1}^n c_k = 1, \quad n = 2, 3. \quad (38)$$

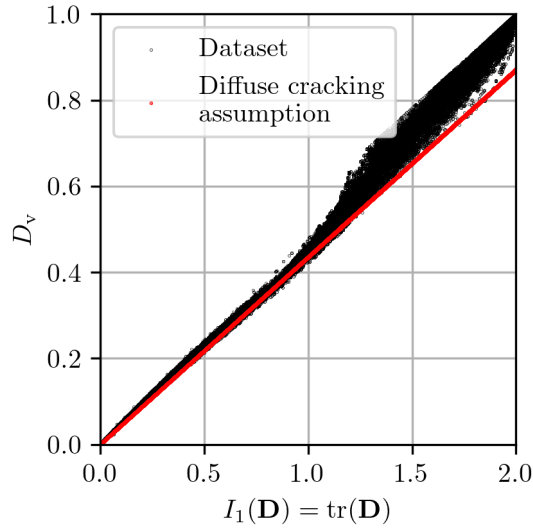


Figure 9: Check of the assumption of total symmetry of the stiffness loss tensor: the dots in black correspond to the value in the dataset and the red dots correspond to the D_v computed via Equation 41

308 *Constraints 3 – Diffuse micro-cracking.* In the early degradation stage, the micro-cracking is diffuse (in the sense
 309 that it is not localized within the RAE). In Figure 8, this stage corresponds to the region where the points (D_1, D_2, D_v)
 310 are close to a plane. It corresponds to the assumption of non-interacting cracks (as defined by *Kachanov (1992)*).

311 *Kachanov* has shown that in 2D and as long as the micro-cracks are not interacting, the gain in compliance is a
 312 totally symmetric fourth-order tensor. This property is not satisfied anymore when the micro-cracking is localized.
 313 This observation guided us to check if this property is satisfied by the weakly damaged elasticity tensors of the dataset.

314 Assuming in the early damage stage that the stiffness loss $\Delta \mathbf{E} = \mathbf{E} - \mathbf{E}_0$ is totally symmetric implies $\text{tr}_{12}(\mathbf{E} - \mathbf{E}_0) =$
 315 $\text{tr}_{13}(\mathbf{E} - \mathbf{E}_0)$, *i.e.*, $\text{tr } \mathbf{d} - \text{tr } \mathbf{d}_0 = \text{tr } \mathbf{v} - \text{tr } \mathbf{v}_0$. This means that we have, at low damage,

$$D_v = \frac{\text{tr } \mathbf{d}_0 - \text{tr } \mathbf{d}}{\text{tr } \mathbf{v}_0}. \quad (39)$$

316 Taking the trace of the definition (20), giving $\text{tr } \mathbf{d} = 2\kappa_0(2 - \text{tr } \mathbf{D})$, and using the relation between initial properties,
 317 $\text{tr } \mathbf{d}_0 = 4\kappa_0$ and $\text{tr } \mathbf{v}_0 = 4\mu_0 + 2\kappa_0$, we get, at low damage still,

$$D_v = \frac{\kappa_0}{2\mu_0 + \kappa_0} I_1(\mathbf{D}), \quad (40)$$

318 and

$$\left. \frac{\partial D_v}{\partial \mathbf{D}} \right|_{\mathbf{D}=\mathbf{0}} = \frac{\kappa_0}{2\mu_0 + \kappa_0} \mathbf{1} \quad (\text{diffuse micro-cracking assumption}). \quad (41)$$

319 Figure 9 provides a check of this assumption in the 76 356 elasticity tensors dataset. For small values of the damage
 320 ($\text{tr } \mathbf{D} < 1$), the values of D_v obtained by the diffuse micro-cracking assumption provide an accurate model for the
 321 values from the dataset.

322 For both constitutive equations (35) and (36), the diffuse micro-cracking constraint leads to

$$\left. \frac{\partial}{\partial \mathbf{D}} \right|_{\mathbf{D}=\mathbf{0}} \left(\sum_{k=1}^n c_k I_k(\mathbf{D}) \right) = \frac{\kappa_0}{2\mu_0 + \kappa_0} \mathbf{1}, \quad \text{i.e.,} \quad c_1 = \frac{\kappa_0}{2\mu_0 + \kappa_0}. \quad (42)$$

3.2. Parameters c_k

For the first two-term expression in Eq. (35), the physical constraints leads to

$$c_1 = \frac{\kappa_0}{2\mu_0 + \kappa_0}, \quad \text{and} \quad c_2 = \frac{1}{2} - c_1, \quad (43)$$

so that,

$$D_v^m(\mathbf{D}) = \frac{\kappa_0}{2\mu_0 + \kappa_0} (I_1(\mathbf{D}) - I_2(\mathbf{D})) + \frac{1}{2} I_2(\mathbf{D}). \quad (44)$$

Note that this first modeling does not introduce any material parameter.

Applying the physical constraints to the three-term expression in Eq. (36) leads to

$$c_1 = \frac{\kappa_0}{2\mu_0 + \kappa_0}, \quad c_2 = \frac{1}{2} - c_1 - c_3, \quad (45)$$

and

$$D_v^m(\mathbf{D}) = \frac{\kappa_0}{2\mu_0 + \kappa_0} (I_1(\mathbf{D}) - I_2(\mathbf{D})) + \frac{1}{2} I_2(\mathbf{D}) + c_3 (I_3(\mathbf{D}) - I_2(\mathbf{D})). \quad (46)$$

The parameter c_3 is determined via a regression over the whole dataset. We get the small value

$$c_3 = 0.0973, \quad (47)$$

to be compared to the particular case $c_3 = 0$ of the two-term expression in Eq. (44).

4. Modeling of the harmonic part–damage state coupling

The relative distance to orthotropy remains small for most elasticity tensors in our large dataset (as shown in Figure 7b). We thus make the simplifying assumption that the effective elasticity tensors \mathbf{E} are orthotropic. By Eq. (14), the harmonic part of a 2D orthotropic elasticity tensor can be written as the harmonic square

$$\mathbf{H} = \frac{2K_3}{I_2^2} \mathbf{d}' * \mathbf{d}' = \pm \|\mathbf{H}\| \frac{\mathbf{d}' * \mathbf{d}'}{\|\mathbf{d}' * \mathbf{d}'\|}, \quad \|\mathbf{d}' * \mathbf{d}'\| = \frac{1}{\sqrt{2}} \mathbf{d}' : \mathbf{d}' = \frac{1}{\sqrt{2}} I_2, \quad (48)$$

depending on the sign of the invariant of the elasticity tensor $K_3(\mathbf{E}) = \mathbf{d} : \mathbf{H} : \mathbf{d}$. Based on this parametrization, the modeling of the harmonic part of the elasticity tensors in the dataset can be carried out in two steps: (i) choosing an orientation (the sign) and (ii) modeling the harmonic part prefactor $\|\mathbf{H}\|$ as a function of the tensorial damage variable \mathbf{D} .

Remark 5. Note that orientation must be well-predicted when the relative norm of the harmonic part $\|\mathbf{H}\|/\|\mathbf{E}\|$ is large. When the harmonic part is small (when $\|\mathbf{H}\|/\|\mathbf{E}\| \ll 1$), a misprediction of the orientation has a small effect on the predicted elasticity tensor.

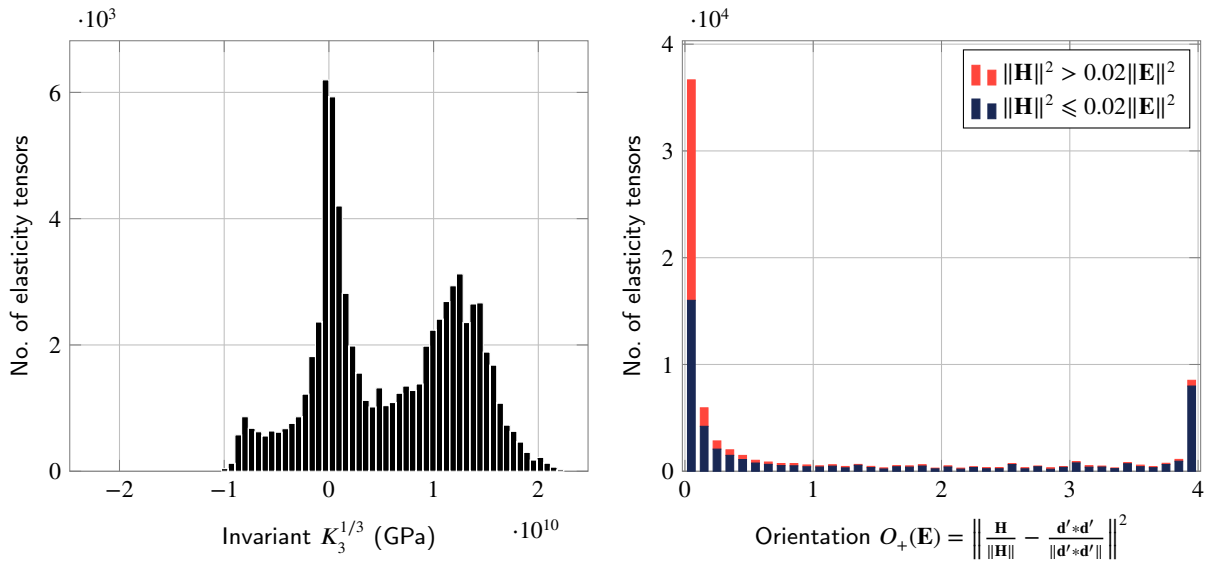
4.1. Orientation of the harmonic part

A first indicator of the orientation of the harmonic part \mathbf{H} is the sign of the invariant $K_3(\mathbf{E})$ or, in an equivalent manner, the sign of $K_3(\mathbf{E})^{1/3}$ (which is in GPa). Figure 10a shows the histogram of the invariant $K_3(\mathbf{E})^{1/3}$ over the dataset. It shows that the negative values of $K_3(\mathbf{E})^{1/3}$ are small in absolute, whereas the positive values of $K_3(\mathbf{E})^{1/3}$ are an order of magnitude higher. However, a large value of K_3 does not mean that the harmonic part is large, whereas a small value of K_3 does mean that the harmonic part is small (see Eq. (14) and remark 5).

Another orientation indicator is the norm of the difference between the normalized harmonic part and the normalized harmonic square

$$O_+(\mathbf{E}) = \left\| \frac{\mathbf{H}}{\|\mathbf{H}\|} - \frac{\mathbf{d}' * \mathbf{d}'}{\|\mathbf{d}' * \mathbf{d}'\|} \right\|^2. \quad (49)$$

The histogram of the orientation indicator $O_+(\mathbf{E})$ over the dataset is plotted in Figure 10b. It mainly exhibits two peaks, one at 0, corresponding to the plus sign in Eq. (48), and one at 4, corresponding to the minus sign. In order to decide which sign is the best for our modeling, the data set is split into two colored parts:



(a) Histogram of invariant $K_3^{1/3}$ (GPa) over the dataset.

(b) Stacked histogram of $O_+(\mathbf{E})$ over the data set.

Figure 10: Two indicators for the sign of the harmonic part.

- a blue part when the harmonic part is negligible ($\|\mathbf{H}\|^2/\|\mathbf{E}\|^2$ lower than 2%),
- and a red part when the harmonic part is significant ($\|\mathbf{H}\|^2/\|\mathbf{E}\|^2$ larger than 2%).

Figure 10b shows that a higher number of elasticity tensors have a significant harmonic part in the positive orientation ($O_+(\mathbf{E}) = 0$) than in the negative orientation ($O_+(\mathbf{E}) = 4$). This observation is consistent with the analysis based on the invariant K_3 . It also indicates that the preferred orientation is $+\frac{\mathbf{d}'*\mathbf{d}'}{\|\mathbf{d}'*\mathbf{d}'\|}$ (plus sign in Eq. (48)).

For the remaining of this section, we

- use the proportionality of the deviatoric part of the dilatation tensor with damage $\mathbf{d}' = -2\kappa_0 \mathbf{D}'$ (by Eq. (20)), and
- model the harmonic part of the effective elasticity tensors with a plus sign,

by setting (with a slight abuse of notation)

$$\mathbf{H} = \mathbf{H}(\mathbf{D}) = H^m(\mathbf{D}) \frac{\mathbf{D}'*\mathbf{D}'}{\mathbf{D}':\mathbf{D}'}, \quad (50)$$

where $H^m = \sqrt{2}\|\mathbf{H}\|$ is a positive function (to be determined) of the tensorial damage variable \mathbf{D} .

4.2. Modeling of the harmonic part

To identify the constitutive equation $H^m(\mathbf{D})$, the first step is to check if the norm $\|\mathbf{H}\|$ of the harmonic part can be represented by a function of the tensorial damage variable \mathbf{D} (through its invariants). Figure 11 shows the harmonic part norm $\|\mathbf{H}\|$ versus the damage invariants $I_1(\mathbf{D}) = \text{tr } \mathbf{D}$ and $I_2(\mathbf{D}') = \mathbf{D}':\mathbf{D}'$. Even if the discrepancy is large, especially in the region where $I_1(\mathbf{D}) > 1$, this figure indicates that it should be possible to approximate the norm $\|\mathbf{H}\|$ by a function of the two damage invariants $I_1(\mathbf{D})$ and $I_2(\mathbf{D}')$.

Remark 6. Figure 11 shows that the norm of the harmonic part does not vanish when the damage variable \mathbf{D} is equal to the second-order identity $\mathbf{1}$. Moreover, for the effective elasticity tensors in the dataset such that $I_1(\mathbf{D}) \approx 2$ and $I_2(\mathbf{D}') \approx 0$, different values of the norm $\|\mathbf{H}\|$ are associated with the same value of damage. This means that the definition (18) of the damage variable is insufficient in these few cases to fully represent the variations of the effective elasticity tensor due to highly interacting micro-cracks. To account for those variations, a second (internal) damage

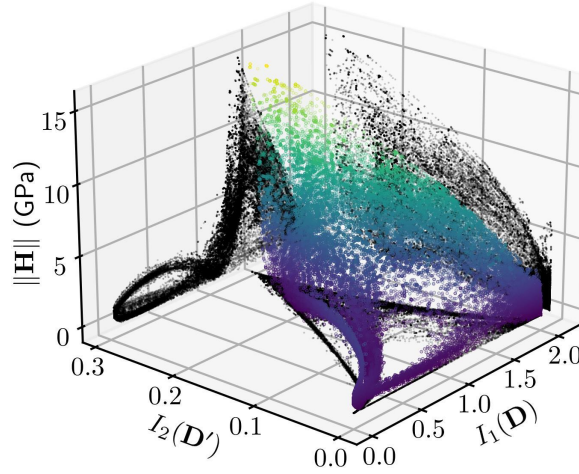


Figure 11: Norm of the harmonic part (in GPa) as a function of the damage invariants $I_1(\mathbf{D})$ and $I_2(\mathbf{D}') = \mathbf{D}' : \mathbf{D}'$.

375 variable, possibly of higher order, could be used (see (Cormery and Welemane, 2010; Desmorat and Desmorat, 2016)
 376 for instance). Yet, the gain of accuracy might not be worth the increased modeling complexity.

377 As in the previous section, let us frame the state modeling of the function $H^m(\mathbf{D})$ by physical assump-
 378 tions/constraints. The assumption of initial isotropy imposes that

$$H^m(\mathbf{D} = \mathbf{0}) = 0. \quad (51)$$

379 We also assume that the effective elasticity tensor \mathbf{E} vanishes when the material is fully damaged. This implies that the
 380 harmonic part \mathbf{H} must vanish when the damage grows to $\mathbf{D} = \mathbf{1}$,

$$H^m(\mathbf{D} = \mathbf{1}) = 0. \quad (52)$$

381 Figure 11 shows that the harmonic part norm $\|\mathbf{H}\|$ remains small when the damage invariant $I_2(\mathbf{D}')$ is small. We can
 382 assume that

$$H^m(I_1(\mathbf{D}), I_2(\mathbf{D}') = 0) = 0. \quad (53)$$

383 This new condition includes both previous assumptions.

384 **Remark 7.** The condition (53) is satisfied when the damage is purely hydrostatic (*i.e.*, when $\mathbf{D} = \frac{1}{2}(\text{tr } \mathbf{D})\mathbf{1}$). If the
 385 damage is hydrostatic, both the dilatation part $\mathbf{D}il$ and the harmonic part \mathbf{H} are obtained null (by the formula (11)).
 386 Thus, the modeled 2D effective elasticity tensor $\mathbf{E}(\mathbf{D})$ is isotropic during a hydrostatic damaging.

387 A sparse regression method (the LASSO regression, Tibshirani (1996)) has been applied to a (multivariate)
 388 polynomial in the damage invariants $I_1(\mathbf{D})$ and $I_2(\mathbf{D}')$. This optimization method aims at fitting a parametrized
 389 function with respect to data while penalizing the number of non-zero parameters. Note that, following Gaines et al.
 390 (2018), physical assumptions can be accounted for through additional minimization constraints. The constrained
 391 LASSO regression for the polynomial modeling of the function $H^m(\mathbf{D}) = \sqrt{2}\|\mathbf{H}(\mathbf{D})\|$ (introduced in Eq. (50)) recasts
 392 as the minimization problem

$$\min_{h_{n_1 n_2}} \sum_{i=1}^{N_{\text{ela}}} \left(\sqrt{2}\|\mathbf{H}_i\| - \sum_{n_1, n_2} h_{n_1 n_2} I_1(\mathbf{D}_i)^{n_1} I_2(\mathbf{D}'_i)^{n_2} \right)^2 + \alpha \sum_{n_1, n_2} |h_{n_1 n_2}|, \quad (54)$$

393 where $N_{\text{ela}} = 76\,356$ is the number of elasticity tensors in the dataset, $h_{n_1 n_2}$ are the coefficients of the sought
 394 polynomial, *i.e.*, the parameters, and α is an arbitrary hyper-parameter of the method. The first term corresponds to a

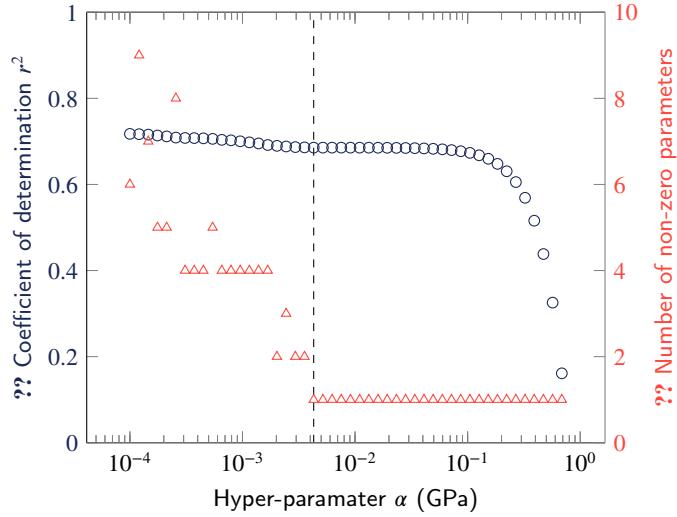


Figure 12: Illustration of the compromise between the precision and the number of non-zero parameters in the constrained LASSO regression. The dashed line shows the best compromise for us ($\alpha = 0.0043$ GPa).

395 classical regression with a least-square error. The second term (with α) penalizes the sum of the absolute values of the
 396 parameters $h_{n_1 n_2}$. In practice, the higher α , the fewer the non-zero parameters. The minimization has been carried out
 397 for different values of α . The coefficient of determination of the regression

$$r^2 = 1 - \frac{\sum_{i=1}^{N_{ela}} \left(\sqrt{2} \|\mathbf{H}_i\| - \sum_{n_1, n_2} h_{n_1 n_2} I_1(\mathbf{D}_i)^{n_1} I_2(\mathbf{D}'_i)^{n_2} \right)^2}{\sum_{i=1}^{N_{ela}} \left(\sqrt{2} \|\mathbf{H}_i\| - \text{mean} \left(\sum_{n_1, n_2} h_{n_1 n_2} I_1(\mathbf{D}_i)^{n_1} I_2(\mathbf{D}'_i)^{n_2} \right) \right)^2} \quad (55)$$

398 is introduced as an indicator of the accuracy of the regression.

399 As shown in Figure 12, the best compromise between the model's accuracy (evaluated via the coefficient of
 400 determination r^2 and the number of non-zero parameters) has been obtained for the one-parameter polynomial
 401 expression

$$\mathbf{H}^m(\mathbf{D}) = h I_1(\mathbf{D})^4 I_2(\mathbf{D}'), \quad h = h_{41} = 17 \text{ GPa}, \quad (56)$$

402 where h is the so-called harmonic prefactor. Combined with equations (50) and (12), the previous expression means
 403 that the harmonic part of the elasticity tensors of our large dataset is well modeled by the simple constitutive equation

$$\mathbf{H}(\mathbf{D}) = h (\text{tr } \mathbf{D})^4 \mathbf{D}' * \mathbf{D}', \quad \mathbf{D}' * \mathbf{D}' = \mathbf{D}' \otimes \mathbf{D}' - \frac{1}{2} (\mathbf{D}' : \mathbf{D}') \mathbf{J}, \quad (57)$$

404 which expresses the harmonic part of the 2D effective elasticity tensors as a function of the damage variable \mathbf{D} only.
 405 Recall that $\mathbf{J} = \mathbf{I} - \frac{1}{2} \mathbf{1} \otimes \mathbf{1}$ is the deviatoric projector.

406 4.3. Neglecting the harmonic part

407 As an alternative to the polynomial expression (57), it is also worth neglecting the harmonic part \mathbf{H} and simply
 408 setting $h = 0$, *i.e.*,

$$\mathbf{H}(\mathbf{D}) = 0. \quad (58)$$

409 Indeed, as shown in Figure 13, the harmonic part is a small proportion of the effective elasticity tensor in most cases.
 410 Due to these observations, the harmonic part can often be neglected.

411 **Remark 8.** The modeling assumption $h = 0$, $\mathbf{H}(\mathbf{D}) = 0$, makes the effective elasticity tensor r_0 -orthotropic in the
 412 sense of (Vannucci, 2002).

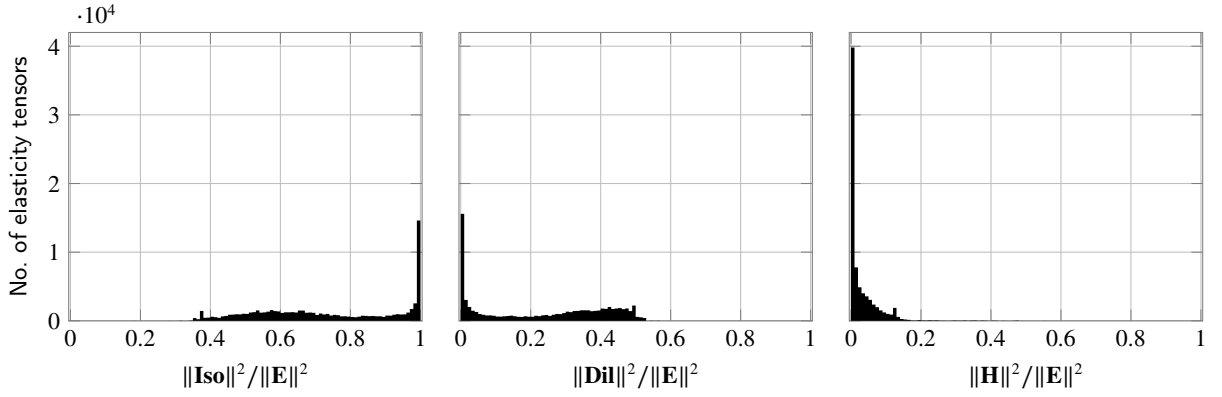


Figure 13: Proportion of each part of the elasticity tensor for each tensor of the dataset.

5. Summary of the proposed anisotropic damage state coupling

Let us summarize the constitutive equations obtained in sections 1, 3, and 4. These equations are obtained from both the elasticity tensors reconstruction formulas (11) and (15), the performed virtual beam-particle computations, and cross-identification over the large effective elasticity tensors dataset. Let us also switch to standard Continuum Mechanics notations and mark with a tilde the effective (damaged) quantities, such as the effective elasticity tensor $\tilde{\mathbf{E}} = \tilde{\mathbf{E}}(\mathbf{D})$, the effective generalized shear and bulk moduli $\tilde{\mu} = \tilde{\mu}(\mathbf{D})$, $\tilde{\kappa} = \tilde{\kappa}(\mathbf{D})$, the effective harmonic tensor $\tilde{\mathbf{H}} = \tilde{\mathbf{H}}(\mathbf{D})$. We recall and rewrite the state equations obtained by using the relation

$$\tilde{\mathbf{d}} = 2\kappa_0 (\mathbf{1} - \mathbf{D}), \quad (59)$$

between the effective dilatation tensor $\tilde{\mathbf{d}} = \tilde{\mathbf{E}} : \mathbf{1}$ and the second-order damage variable \mathbf{D} .

The proposed anisotropic damage coupling is based on the damage dependency of each component of the harmonic decomposition

$$\tilde{\mathbf{E}}(\mathbf{D}) = 2\tilde{\mu}(\mathbf{D}) \mathbf{J} + \tilde{\kappa}(\mathbf{D}) \mathbf{1} \otimes \mathbf{1} - \kappa_0 (\mathbf{1} \otimes \mathbf{D}' + \mathbf{D}' \otimes \mathbf{1}) + \tilde{\mathbf{H}}(\mathbf{D}), \quad (60)$$

of the effective bi-dimensional elasticity tensor. The effective shear modulus has been derived as

$$\tilde{\mu}(\mathbf{D}) = \frac{1}{8} (2 \operatorname{tr} \tilde{\mathbf{v}} - \operatorname{tr} \tilde{\mathbf{d}}), \quad \operatorname{tr} \tilde{\mathbf{v}} = \operatorname{tr}_{13} \operatorname{tr} \tilde{\mathbf{E}} = \operatorname{tr} \mathbf{v}_0 (1 - D_{\mathbf{v}}^m(\mathbf{D})) \quad (61)$$

with for $D_{\mathbf{v}}^m(\mathbf{D})$, function of the invariants $\operatorname{tr} \mathbf{D}$, $\mathbf{D} : \mathbf{D}$ and $I_3 = \operatorname{tr}(\mathbf{D}^3)$, either the no-additional parameter function in Eq. (44) or the one-additional parameter function in Eq. (46). Defining the nonlinear shear-damage coupling parameter

$$m = \frac{1}{2} (\kappa_0 + 2\mu_0) c_3, \quad (62)$$

these two expressions are unified as the first constitutive equation of Table 2, in which are also recalled the expressions obtained for $\tilde{\kappa}(\mathbf{D})$ and $\tilde{\mathbf{H}}(\mathbf{D})$.

The corresponding elasticity law coupled with anisotropic damage derives from a thermodynamics potential, the Helmholtz free energy density $\rho\psi$ function of the strain and the damage, as

$$\boldsymbol{\sigma} = \rho \frac{\partial \psi}{\partial \boldsymbol{\varepsilon}} = \tilde{\mathbf{E}}(\mathbf{D}) : \boldsymbol{\varepsilon}, \quad (63)$$

where

$$\rho\psi = \frac{1}{2} \boldsymbol{\varepsilon} : \tilde{\mathbf{E}}(\mathbf{D}) : \boldsymbol{\varepsilon} = \tilde{\mu}(\mathbf{D}) \boldsymbol{\varepsilon}' : \boldsymbol{\varepsilon}' + \frac{1}{2} \tilde{\kappa}(\mathbf{D}) (\operatorname{tr} \boldsymbol{\varepsilon})^2 - \kappa_0 \mathbf{D}' : \boldsymbol{\varepsilon}' \operatorname{tr} \boldsymbol{\varepsilon} + \frac{1}{2} h (\operatorname{tr} \mathbf{D})^4 \boldsymbol{\varepsilon}' : (\mathbf{D}' * \mathbf{D}') : \boldsymbol{\varepsilon}', \quad (64)$$

Quantity	Model
Shear modulus	$\tilde{\mu}(\mathbf{D}) = \mu_0 - \frac{1}{4}\kappa_0 \text{tr } \mathbf{D} + \frac{1}{4}(\kappa_0 - 2\mu_0) \mathbf{D} : \mathbf{D} + m (\mathbf{D} : \mathbf{D} - \text{tr}(\mathbf{D}^3))$
Bulk modulus	$\tilde{\kappa}(\mathbf{D}) = \kappa_0 (1 - \frac{1}{2} \text{tr } \mathbf{D})$
Dilatation tensor	$\tilde{\mathbf{d}} = 2\kappa_0 (\mathbf{1} - \mathbf{D})$
Harmonic part	$\tilde{\mathbf{H}}(\mathbf{D}) = h (\text{tr } \mathbf{D})^4 \mathbf{D}' * \mathbf{D}'$

Table 2

Summary of the constitutive equations.

Name	Symbol	Value in GPa
Initial shear modulus	μ_0	19.4
Initial bulk modulus	κ_0	30
Nonlinear shear-damage coupling parameter	m	3.35
Harmonic prefactor	h	17

Table 3

Summary of the constitutive parameters (and their value for the 76 356 elasticity tensors dataset).

431 is a polynomial of simple and joint invariants of the state variables, *i.e.*, of the strain and damage tensors. It details as

$$\begin{aligned} \rho\psi(\boldsymbol{\varepsilon}, \mathbf{D}) = & \left(\mu_0 - \frac{1}{4}\kappa_0 \text{tr } \mathbf{D} + \frac{1}{4}(\kappa_0 - 2\mu_0) \mathbf{D} : \mathbf{D} + m (\mathbf{D} : \mathbf{D} - \text{tr}(\mathbf{D}^3)) \right) \boldsymbol{\varepsilon}' : \boldsymbol{\varepsilon}' \\ & + \frac{1}{2}\kappa_0 \left(1 - \frac{1}{2} \text{tr } \mathbf{D} \right) (\text{tr } \boldsymbol{\varepsilon})^2 - \kappa_0 \mathbf{D}' : \boldsymbol{\varepsilon}' \text{tr } \boldsymbol{\varepsilon} + \frac{1}{2}h (\text{tr } \mathbf{D})^4 \boldsymbol{\varepsilon}' : (\mathbf{D}' * \mathbf{D}') : \boldsymbol{\varepsilon}'. \end{aligned} \quad (65)$$

432 Using definition (12), this state potential can be rewritten as

$$\begin{aligned} \rho\psi(\boldsymbol{\varepsilon}, \mathbf{D}) = & \left(\mu_0 - \frac{1}{4}\kappa_0 \text{tr } \mathbf{D} + \frac{1}{4}(\kappa_0 - 2\mu_0) \mathbf{D} : \mathbf{D} + m (\mathbf{D} : \mathbf{D} - \text{tr}(\mathbf{D}^3)) - \frac{1}{4}h (\text{tr } \mathbf{D})^4 \mathbf{D}' : \mathbf{D}' \right) \boldsymbol{\varepsilon}' : \boldsymbol{\varepsilon}' \\ & + \frac{1}{2}\kappa_0 \left(1 - \frac{1}{2} \text{tr } \mathbf{D} \right) (\text{tr } \boldsymbol{\varepsilon})^2 - \kappa_0 \mathbf{D}' : \boldsymbol{\varepsilon}' \text{tr } \boldsymbol{\varepsilon} + \frac{1}{2}h (\text{tr } \mathbf{D})^4 (\mathbf{D}' : \boldsymbol{\varepsilon}')^2. \end{aligned} \quad (66)$$

433 The thermodynamics force associated with the damage is then the symmetric second-order tensor

$$\begin{aligned} \mathbf{Y} = & -\rho \frac{\partial \psi}{\partial \mathbf{D}} \\ = & \left(\frac{1}{4}\kappa_0 \mathbf{1} + \frac{1}{2}(2\mu_0 - \kappa_0) \mathbf{D} + m (3\mathbf{D}^2 - 2\mathbf{D}) + h (\text{tr } \mathbf{D})^3 \left(\frac{1}{2}(\text{tr } \mathbf{D}) \mathbf{D}' + (\mathbf{D}' : \mathbf{D}') \mathbf{1} \right) \right) \boldsymbol{\varepsilon}' : \boldsymbol{\varepsilon}' \\ & + \frac{1}{4}\kappa_0 (\text{tr } \boldsymbol{\varepsilon})^2 \mathbf{1} + \kappa_0 (\text{tr } \boldsymbol{\varepsilon}) \mathbf{D}' - h (\text{tr } \mathbf{D})^4 (\mathbf{D}' : \boldsymbol{\varepsilon}') \boldsymbol{\varepsilon}'. \end{aligned} \quad (67)$$

434 The parameters of the final model are the initial shear modulus μ_0 , the initial bulk modulus κ_0 , the (optional)
435 shear-damage coupling parameter $m = \frac{1}{2}(\kappa_0 + 2\mu_0) c_3$ and the harmonic prefactor h . They are summarized, with
436 their value for our dataset, in Table 3.

437 It is worth pointing out that only one damage variable (the second-order tensor \mathbf{D}) and only two material parameters
438 (m and h) are introduced in this final state coupling for quasi-brittle materials between bi-dimensional elasticity and
439 anisotropic damage.

6. Representativity of the proposed anisotropic damage state coupling

440 This section provides assessments over the 76 356 tensors dataset of several modeling choices —summarized in
441 the previous section— for the coupling bi-dimensional elasticity-anisotropic damage:

- 443 • simplified modeling with vanishing parameters $m = 0$ and/or $h = 0$.

Percentile (error)	1 %	2 %	5 %	10 %
$m = 0$	43.8 %	60.7 %	92.4 %	99.9 %
$m = 3.35$ GPa	44.0 %	71.6 %	96.8 %	99.9 %

Table 4

Proportion of tensors with a relative error on the isotropic part below 1%, 2%, 5% and 10% for both value of m (results independent from the harmonic prefactor h).

- full modeling with non zero parameters $m = 3.35$ GPa and/or $h = 17$ GPa.

Each computed (micro-cracked) elasticity tensor \mathbf{E}_i from the dataset has an isotropic part \mathbf{Iso}_i , a dilatation part \mathbf{Dil}_i and a harmonic part \mathbf{H}_i (determined by harmonic decomposition (11)). For the assessments, the damage $\mathbf{D} = \mathbf{D}_i$ is taken as equal to the damage variable $\mathbf{D}_i = \mathbf{1} - \mathbf{d}_i/2\kappa_0 = \mathbf{1} - \mathbf{E}_i : \mathbf{1}/2\kappa_0$ measured for \mathbf{E}_i in the dataset.

To be quantitative, the error between a tensor \mathbf{E}_i of the dataset and the anisotropic damage modeling $\tilde{\mathbf{E}} = \tilde{\mathbf{E}}(\mathbf{D})$ is defined as

$$\|\mathbf{E}_i - \tilde{\mathbf{E}}(\mathbf{D}_i)\| = \sqrt{\|\mathbf{Iso}_i - \tilde{\mathbf{Iso}}(\mathbf{D}_i)\|^2 + \|\mathbf{Dil}_i - \tilde{\mathbf{Dil}}(\mathbf{D}_i)\|^2 + \|\mathbf{H}_i - \tilde{\mathbf{H}}(\mathbf{D}_i)\|^2}, \quad (68)$$

where, by the formulas of previous section,

$$\tilde{\mathbf{Iso}}(\mathbf{D}) = 2\tilde{\mu}(\mathbf{D})\mathbf{J} + \tilde{\kappa}(\mathbf{D})\mathbf{1} \otimes \mathbf{1}, \quad \tilde{\mathbf{Dil}}(\mathbf{D}) = -\kappa_0(\mathbf{1} \otimes \mathbf{D}' + \mathbf{D}' \otimes \mathbf{1}), \quad \tilde{\mathbf{H}}(\mathbf{D}) = h(\text{tr } \mathbf{D})^4 \mathbf{D}' * \mathbf{D}'. \quad (69)$$

Since the fourth-order isotropic (\mathbf{Iso}), dilatation (\mathbf{Dil}) and harmonic (\mathbf{H}) parts are orthogonal, the errors associated with each part are uncorrelated. This implies that the parameter m influences the isotropic part only (by shear modulus expression of Table 2), and that the parameter h influences the harmonic part only (by harmonic part expression of Table 2). We point out that the dilatation part has no modeling error (thanks to the equality $\tilde{\mathbf{Dil}}(\mathbf{D}_i) = -\kappa_0(\mathbf{1} \otimes \mathbf{D}'_i + \mathbf{D}'_i \otimes \mathbf{1}) = \mathbf{Dil}(\mathbf{E}_i)$).

6.1. Assessment of the isotropic part $\tilde{\mathbf{Iso}}(\mathbf{D})$

Let us first analyze the contribution of the isotropic part to the modeling error. A histogram of the relative error $\|\mathbf{Iso}_i - \tilde{\mathbf{Iso}}(\mathbf{D}_i)\|/\|\mathbf{E}_0\|$ on the isotropic part² is plotted in Figure 14a. The relative error range [0, 1] is discretized in 500 intervals for this histogram, and all the following ones. It shows that both modeling, with vanishing value $m = 0$ and with non-zero value $m = 3.35$ GPa, are able to represent well the isotropic part of all micro-cracked tensors in the dataset (with a relative error below 10%). Figure 14b provides the Cumulative Distribution Function associated with this histogram. The numbers of tensors in each interval are cumulated with the relative error going from 0 to 1. Afterward, the cumulated number is divided by the total number of tensors to define the Cumulative Distribution Function (such that it reaches 1 when the error is 1). This plot shows that most isotropic parts are modeled with an error below 10%.

More quantitative results are provided in Table 4, which focuses on different percentiles of the histogram. Each percentile corresponds to a percentage of elasticity tensors \mathbf{E}_i with a modeling error —on the isotropic part— below the given threshold. For instance, the 5-percentile gives the proportion of tensors that are modeled with an error below 5%. This table is obtained from the Cumulative Distribution of the error by fixing the error (in the x -axis) and reading the associated cumulative proportion of tensors (in the y -axis). The Table 4 shows that the case $m = 3.35$ GPa models 71.6% of the effective elasticity tensor with less than 2% of error, whereas the case $m = 0$ models only 60.7% of them. Thus, the case $m = 3.35$ GPa provides a slightly more accurate model of the isotropic part than the simplified case $m = 0$. However, it requires the introduction of the additional material parameter $m = \frac{1}{2}(\kappa_0 + 2\mu_0)c_3$. As the gain in accuracy is small compared to the increase of modeling/identification complexity by adding a parameter, we propose to retain $m = 0$ (*i.e.*, Eq. (44)) for the modeling of the coupling of the shear modulus with anisotropic damage.

6.2. Assessment of the harmonic part

Let us now analyze the contribution of the harmonic part to the modeling error. Figure 15a shows the histogram of the relative error $\|\mathbf{H}_i - \tilde{\mathbf{H}}(\mathbf{D}_i)\|/\|\mathbf{E}_0\|$ on the harmonic part. It indicates that the case $h = 17$ GPa substantially

²Duplicated tensors during a loading (two successive tensors with no crack growth) are filtered out in this plot. The total number of remaining tensors is 60 232.

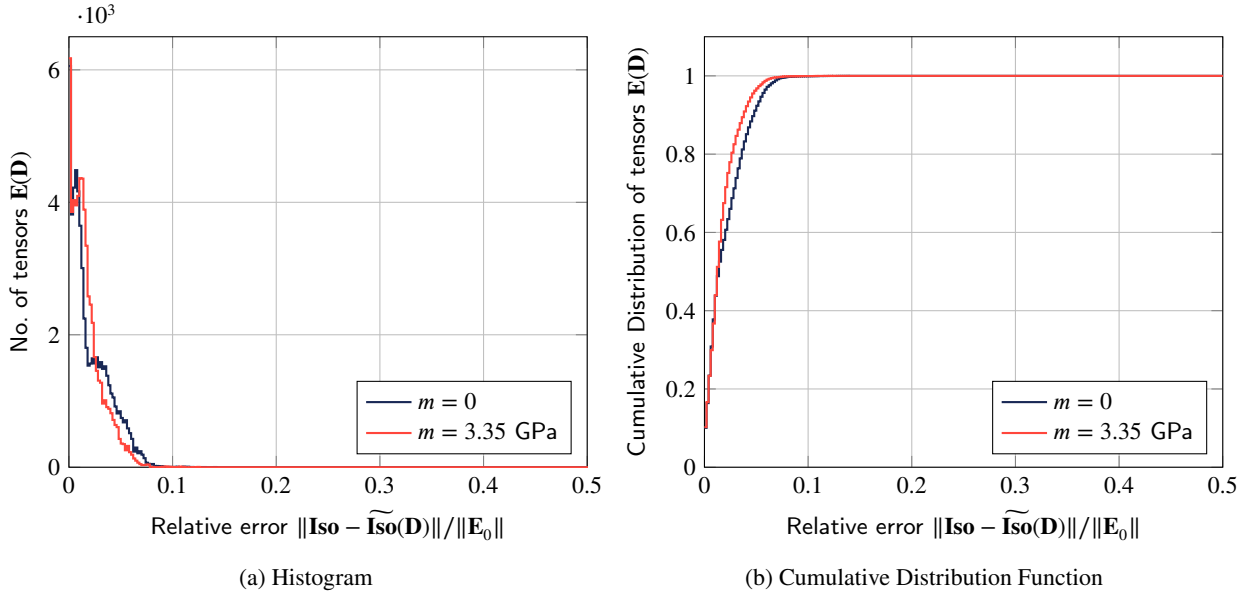


Figure 14: Histograms and Cumulative Distribution Functions of the relative error on the isotropic part over the dataset for both values of m (results independent from the harmonic prefactor h).

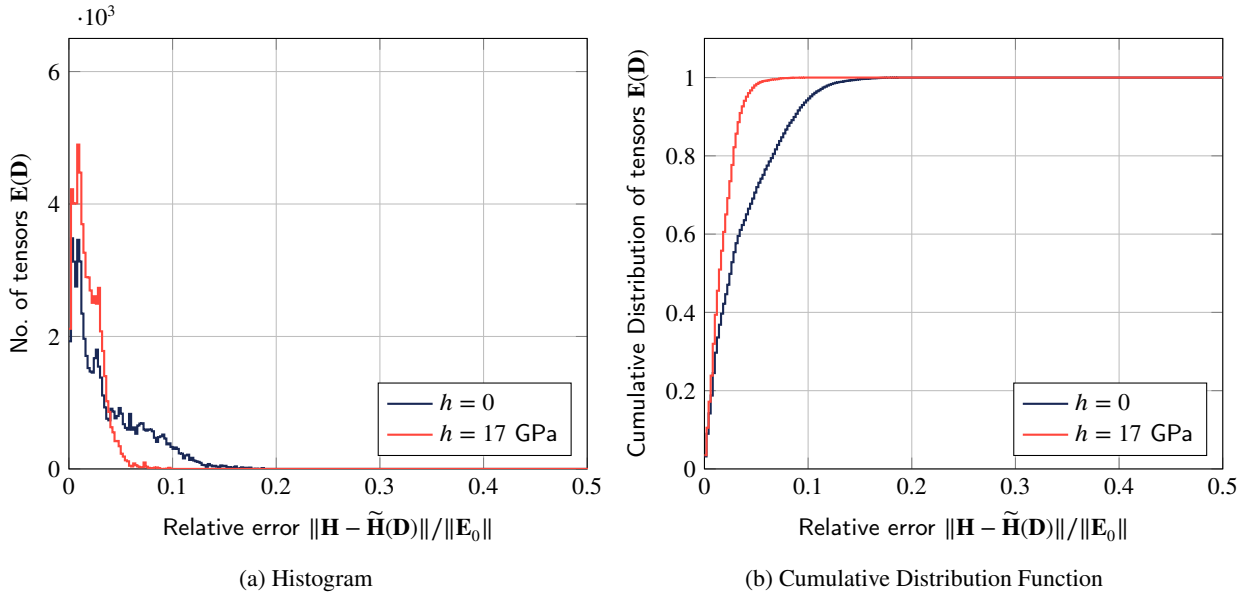


Figure 15: Histograms and Cumulative Distributions Functions of the relative error on the harmonic part over the dataset for both values of h (results independent from the parameter m).

479 improves the modeling in comparison to neglecting the harmonic part (case $h = 0$). Note that for $h = 17$ GPa, the
 480 contribution of the error on the harmonic part is at the same level as the contribution due to the isotropic part. Figure 15b
 481 provides the Cumulative Distribution Function of this histogram. It shows that setting $h = 17$ GPa enables to model
 482 most harmonic parts of the dataset with an error below 5% whereas it is not the case for $h = 0$.

483 More quantitative results are provided in Table 5, where different percentile of the histogram are given (as in
 484 Table 4). Once again, a percentile corresponds to percentage of elasticity tensors with a modeling error – on the
 485 harmonic part – below a given threshold. It shows that setting $h = 17$ GPa enables the modeling of most harmonic

Percentile (error)	1%	2%	5%	10%
$h = 0$	29.7%	44.7%	72.0%	94.7%
$h = 17$ GPa	39.3%	65.0%	98.4%	100%

Table 5

Proportion of tensors with an error on harmonic part below 1%, 2%, 5% and 10% for both values of the harmonic prefactor h .

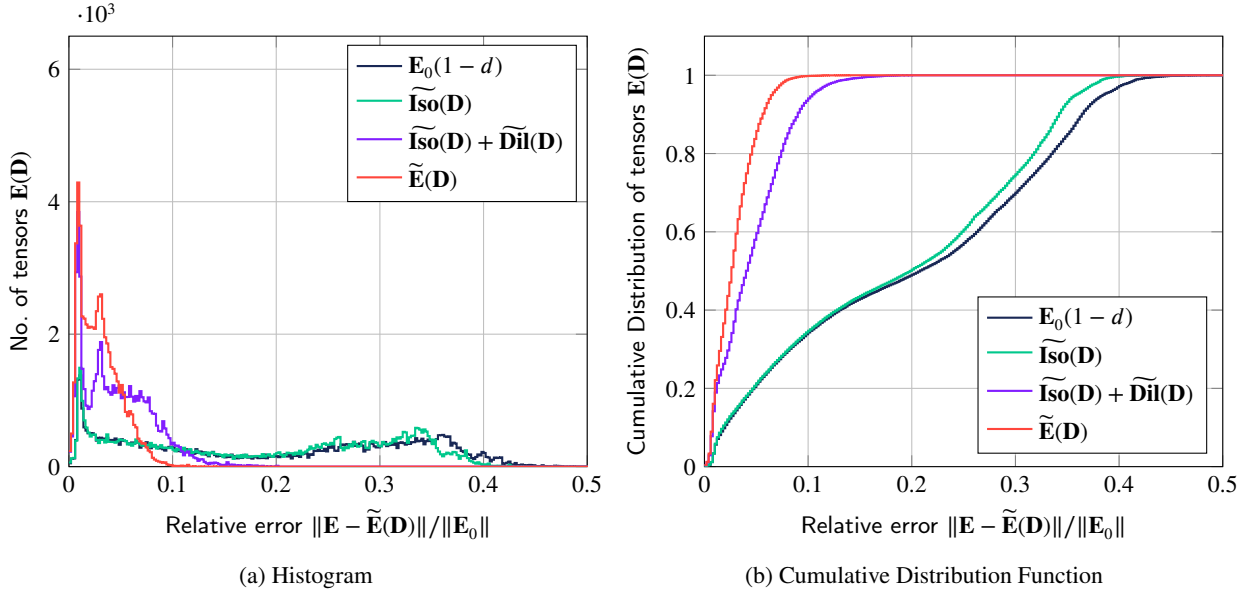


Figure 16: Histogram and Cumulative Distribution Functions of the total relative error on the effective elasticity tensors over the dataset for $m = 0$ and $h = 17$ GPa.

Percentile (error)	1%	2%	5%	10%	20%	30%	40%
$(1-d)\mathbf{E}_0$	5.63%	10.6%	21.0%	34.3%	49.0%	70.0%	97.3%
$\tilde{\mathbf{I}}\text{so}(\mathbf{D})$	5.87%	11.3%	21.3%	34.7%	50.3%	74.7%	99.7%
$\tilde{\mathbf{I}}\text{so}(\mathbf{D}) + \tilde{\mathbf{D}}\text{il}(\mathbf{D})$	18.9%	27.8%	59.7%	94.1%	100%	100%	100%
$\tilde{\mathbf{E}}(\mathbf{D})$	22.1%	40.1%	85.8%	99.8%	100%	100%	100%

Table 6

Proportion of tensors with a total error below 1%, 2%, 5%, 10%, 20%, 30% and 40%.

486 parts of the dataset (98.4%) with an error below 5%, which is far higher than in the case for $h = 0$ (72.0 %). Thus, the
487 case $h = 17$ GPa (using Eq. (56)) clearly improves the accuracy of the modeling.

6.3. Assessment of the complete elasticity tensor

488 Let us complete the previous independent results by analyzing the modeling error on the whole elasticity tensors.
489 Below, we gradually add each ingredient of the modeling (the dilatation part, then the harmonic part) up to the complete
490 modeling $\tilde{\mathbf{E}}(\mathbf{D})$. This allows quantifying the exact contribution of the different parts of the anisotropic damage model.
491

492 Figure 16 shows the histogram and Cumulative Distribution Function of the relative error on the effective elasticity
493 tensor for the different modelings. Different percentiles of the histogram are provided in Table 6. The first line of the
494 table,

$$\mathbf{E}_0(1-d), \quad d = \|\mathbf{E}\|/\|\mathbf{E}_0\|, \quad (70)$$

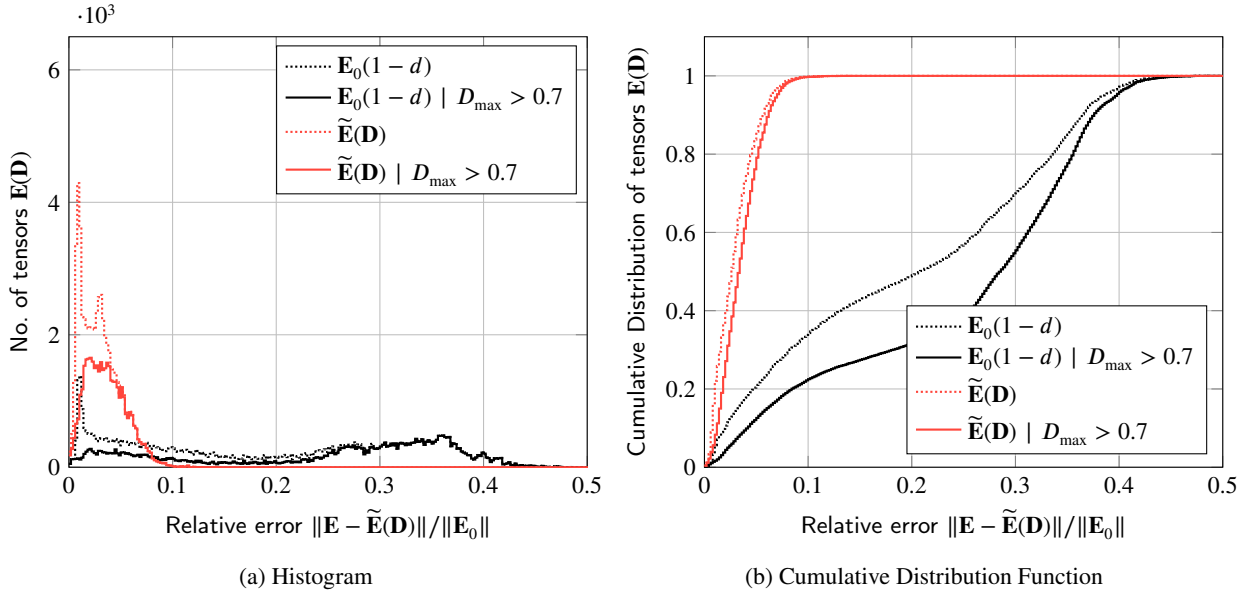


Figure 17: Histograms and Cumulative Distribution Functions of total error for large values of damage. The histogram and cumulative distribution of total error over the elasticity tensors in the dataset is also reproduced.

Percentile (error)	1%	2%	5%	10%	20%	30%	40%
$(1-d)\mathbf{E}_0$	1.66%	4.43%	12.6%	22.5%	31.7%	55.4%	95.9%
$\tilde{\mathbf{E}}(\mathbf{D})$	8.31%	27.1%	79.1%	99.7%	100%	100%	100%

Table 7

Proportion of highly damaged tensors ($D_{\max} > 0.7$) with a total error below 1%, 2%, 5%, 10%, 20%, 30% and 40%.

495 corresponds to an isotropic model (with scalar damage variable d) as it can be found in the literature (Mazars, 1984;
 496 Lemaitre and Chaboche, 1985; Lemaitre, 1992). The second line of the table $\tilde{\mathbf{Iso}}(\mathbf{D})$ corresponds to the isotropic
 497 part only of the proposed modeling ($\tilde{\mathbf{E}} = \tilde{\mathbf{Iso}}(\mathbf{D})$ with $m = 0$). The third line $\tilde{\mathbf{E}} = \tilde{\mathbf{Iso}}(\mathbf{D}) + \tilde{\mathbf{Dil}}(\mathbf{D})$ (with $m = 0$
 498 still, and $h = 0$) adds the modeling of the dilatation part, and the fourth line considers the whole damage model
 499 $\tilde{\mathbf{E}} = \tilde{\mathbf{Iso}}(\mathbf{D}) + \tilde{\mathbf{Dil}}(\mathbf{D}) + \tilde{\mathbf{H}}(\mathbf{D})$ with $m = 0$ and $h = 17$ GPa.

500 Both isotropic models provide a poor estimation of the elasticity tensors of the dataset: the effective elasticity
 501 tensors of a micro-cracked quasi-brittle material cannot be recovered satisfactorily with an isotropic damage model.
 502 Adding the dilatation part to the model, *i.e.*, modeling anisotropic damage, clearly improves its accuracy as it enables
 503 to account for anisotropy induced by micro-cracking. Accounting for the harmonic part (by the second-order damage
 504 tensor \mathbf{D} still) improves the modeling, bringing the proportion of the effective elasticity tensors with less than 5% of
 505 error from 59.7% (for the modeling with $h = 0$, $\tilde{\mathbf{H}}(\mathbf{D}) = 0$) to 85.8% (for $h = 17$ GPa).

506 Let us finally check whether it is possible or not to model the influence of micro-cracking on the elasticity tensor up
 507 to high levels of damage. This modeling feature is very complicated to gain from a micromechanics homogenization
 508 approach (Kachanov, 1993; Ponte Castañeda and Willis, 1995; Cormery and Welemane, 2010; Dormieux and Kondo,
 509 2016).

510 In Figure 17, we reproduce the histogram and Cumulative Distribution of relative errors with a filter to keep only
 511 the elasticity tensors associated with high damage value (*i.e.*, $D_{\max} = \max(D_1, D_2) > 0.7$). The differences between
 512 the filtered and the unfiltered distributions correspond to the relative errors for tensors with low damage (diffuse micro-
 513 cracking).

514 The histogram in Figure 17 shows that an isotropic modeling does not describe well effective elasticity tensors at
 515 high damage values. Table 6 shows that only 12.5% of highly damaged tensors at $D_{\max} > 0.7$ are reconstructed with

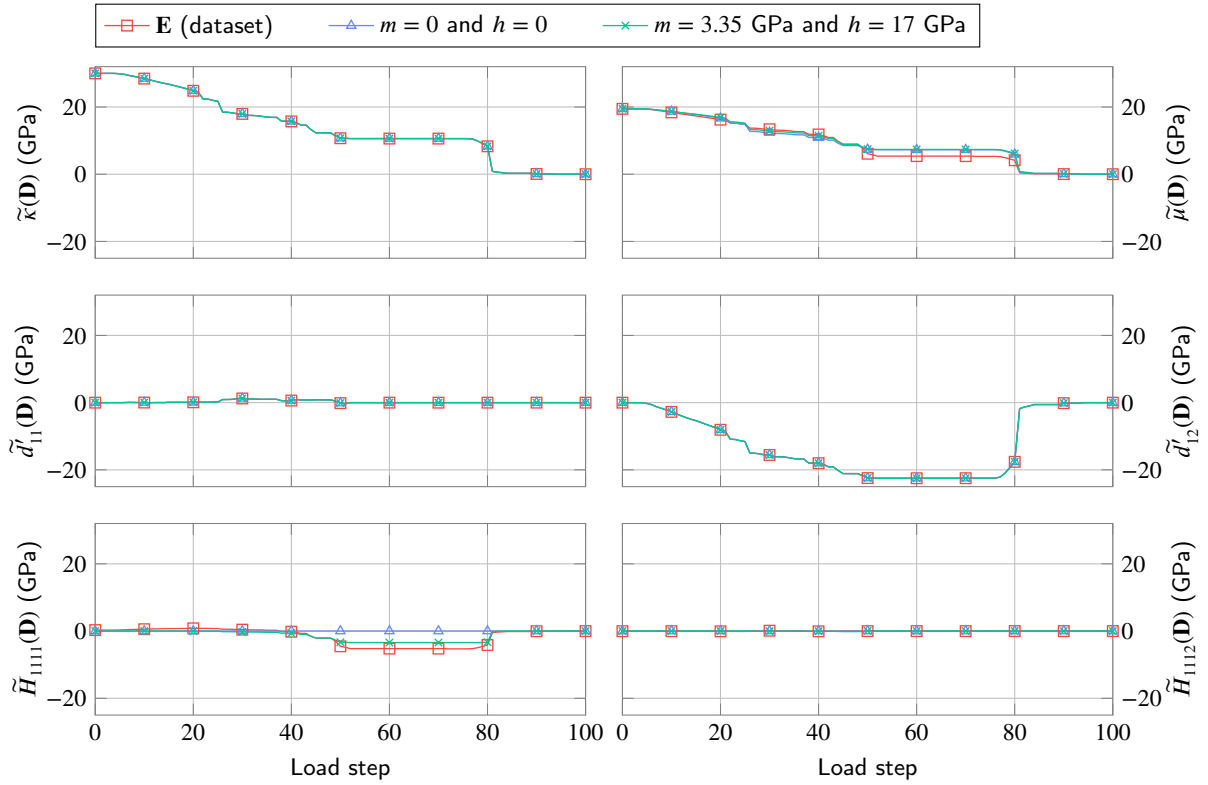


Figure 18: Comparison of the evolutions of elasticity tensors obtained via the two modelings ($m = h = 0$ in blue, and $m = 3.35$ GPa, $h = 17$ GPa in green) with the reference data (\mathbf{E} , in red) during a shear→tension loading.

516 an error below 5% (versus only 21% for the whole dataset). Isotropic damage does not provide an accurate modeling
 517 in the strong micro-cracks interactions stage.

518 The complete anisotropic damage modeling $\tilde{\mathbf{E}} = \tilde{\mathbf{Iso}}(\mathbf{D}) + \tilde{\mathbf{Dil}}(\mathbf{D}) + \tilde{\mathbf{H}}(\mathbf{D})$ (with $m = 0$ and $h = 17$ GPa) is able
 519 to model 79.1% of the tensors with an error below 5% (and 99.7% of the tensors with an error below 10%). It thus
 520 provides an accurate damage state coupling for the effective elasticity tensor, even for highly damaged specimens. This
 521 result emphasizes the strength of the proposed approach based on a beam-particle model of the anisotropic damage of
 522 quasi-brittle materials.

523 6.4. Illustration of the modeling on a multiaxial non-proportional loading

524 In order to illustrate the ability of the modeling to represent the anisotropic damage state coupling, let us detail
 525 both the beam-particle model response and the anisotropic damage $\tilde{\mathbf{E}} = \tilde{\mathbf{E}}(\mathbf{D})$ response for the PBC shear→tension
 526 loading of Table 8 of Appendix B. This loading is one of the non-proportional loadings with the largest harmonic part
 527 in our effective elasticity tensors dataset. Two modelings are compared to the reference data: a first one with $m = 0$
 528 and $h = 0$, and a second one with $m = 3.35$ GPa and $h = 17$ GPa.

529 The computed beam particle elasticity tensors \mathbf{E} and the results of the modeling $\tilde{\mathbf{E}}(\mathbf{D})$ are reported in Figure 18.
 530 As the damage $\mathbf{D} = \mathbf{1} - \mathbf{E} : \mathbf{1}/2\kappa_0$ is known, the bulk modulus κ and the deviatoric part of the dilatation tensor \mathbf{d}' are
 531 exactly modeled. The shear modulus is correctly predicted by both $m = 0$ and $m = 3.35$ GPa cases, close to each other.
 532 This loading leads to the significant growth of the harmonic part, which is neglected when $h = 0$. Setting $h = 17$ GPa
 533 provides a good modeling of the harmonic part.

534 Figure 19 displays the relative errors associated with the isotropic and harmonic parts during this loading. It
 535 confirms that the dilatation part is exactly modeled. For $h = 0$, the most significant part of the error is due to the
 536 modeling of the harmonic part. Note that for $h = 17$ GPa, the modeling of both the isotropic and the harmonic parts
 537 contribute at the same level of the total error on the effective elasticity tensor.

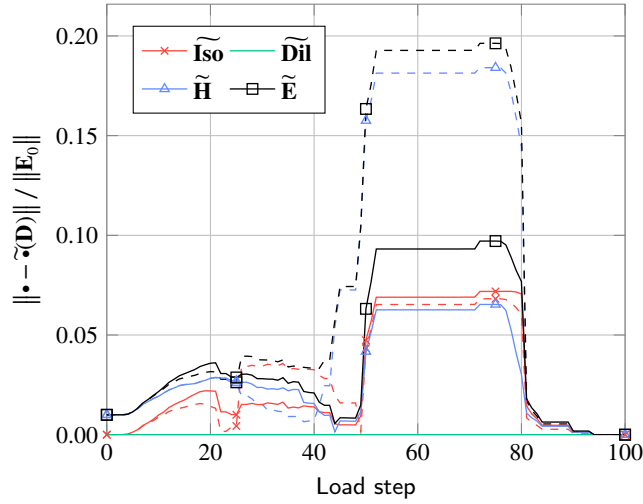


Figure 19: Evolution of relative errors during an EXPE tensile loading. Plain curves correspond to $m = 3.35$ GPa and $h = 17$ GPa, and dashed curves to $m = 0$ and $h = 0$.

7. Conclusion

We have performed 2D beam-particle simulations of Area Elements submitted to various complex loadings and have generated a dataset of 76 356 effective (damaged) elasticity tensors. High levels of anisotropic damage have been reached. Those correspond to discrete computations with strong micro-cracks interactions and multiple coalescences.

By analyzing the distance to orthotropy over the whole dataset, we have first shown that (at least) one second-order damage variable is necessary to represent the effect of micro-cracking on the effective elastic tensors in our dataset. Thanks to a reconstruction formula of the orthotropic elasticity tensor by means of its covariants, we have proposed an anisotropic damage state coupling by a single second-order damage tensor. By the proper definition (18) of the second-order damage variable \mathbf{D} , the isotropic part associated with the effective bulk modulus $\tilde{\kappa}$ and the effective dilatation part $\tilde{\mathbf{Dil}} = \frac{1}{2}(\mathbf{1} \otimes \tilde{\mathbf{d}}' + \tilde{\mathbf{d}}' \otimes \mathbf{1})$ are exactly reconstructed from the damage \mathbf{D} (Table 2). The orthogonality property of the isotropic/dilatation/harmonic parts of the harmonic decomposition has allowed us to build independent constitutive equations: a scalar one

$$\tilde{\mu}(\mathbf{D}) = \mu_0 - \frac{1}{4}\kappa_0 \text{tr } \mathbf{D} + \frac{1}{4}(\kappa_0 - 2\mu_0) \mathbf{D} : \mathbf{D} + m(\mathbf{D} : \mathbf{D} - \text{tr}(\mathbf{D}^3)),$$

for the effective shear modulus $\tilde{\mu}$, and a tensorial one, polynomial in the damage variable

$$\tilde{\mathbf{H}}(\mathbf{D}) = h(\text{tr } \mathbf{D})^4 \mathbf{D}' * \mathbf{D}', = h(\text{tr } \mathbf{D})^4 \left(\mathbf{D}' \otimes \mathbf{D}' - \frac{1}{2}(\mathbf{D}' : \mathbf{D}') \mathbf{J} \right), \quad (71)$$

for the fourth-order harmonic part of the effective elasticity tensor. In addition to the initial elasticity constants μ_0 , κ_0 , only two material parameters have been introduced: the nonlinear shear-damage coupling parameter m (which can furthermore be taken equal to zero) and the harmonic prefactor h (identified as $h = 17$ GPa). The proposed anisotropic damage state coupling models 85.8% of the effective elasticity tensors in the dataset with less than 5% of error, including those with strong micro-cracks interactions and multiple coalescences.

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References

- 561
562 Abramian, S., Desmorat, B., Desmorat, R., Kolev, B., and Olive, M. (2020). Recovering the Normal Form and Symmetry Class of an Elasticity
563 Tensor. *Journal of Elasticity*, 142(1):1–33.
- 564 Antonelli, A., Desmorat, B., Kolev, B., and Desmorat, R. (2022). Distance to plane elasticity orthotropy by Euler–Lagrange method. *Comptes*
565 *Rendus. Mécanique*, 350(G2):413–430.
- 566 Auffray, N., Kolev, B., and Petitot, M. (2014). On Anisotropic Polynomial Relations for the Elasticity Tensor. *Journal of Elasticity*, 115(1):77–103.
- 567 Bagi, K. (1996). Stress and strain in granular assemblies. *Mechanics of Materials*, 22(3):165–177.
- 568 Bagi, K. (2006). Analysis of microstructural strain tensors for granular assemblies. *International Journal of Solids and Structures*, 43(10):3166–
569 3184.
- 570 Bažant, Z. P. and Gambarova, P. G. (1984). Crack Shear in Concrete: Crack Band Microplane Model. *Journal of Structural Engineering*,
571 110(9):2015–2035. Publisher: American Society of Civil Engineers.
- 572 Bažant, Z. P. and Oh, B. H. (1985). Microplane Model for Progressive Fracture of Concrete and Rock. *Journal of Engineering Mechanics*,
573 111(4):559–582. Publisher: American Society of Civil Engineers.
- 574 Bažant, Z. P. and Prat, P. C. (1988a). Microplane Model for Brittle-Plastic Material: I. Theory. *Journal of Engineering Mechanics*, 114(10):1672–
575 1688. Publisher: American Society of Civil Engineers.
- 576 Bažant, Z. P. and Prat, P. C. (1988b). Microplane Model for Brittle-Plastic Material: II. Verification. *Journal of Engineering Mechanics*,
577 114(10):1689–1702. Publisher: American Society of Civil Engineers.
- 578 Bažant, Z. P., Tabbara, M. R., Kazemi, M. T., and Pijaudier-Cabot, G. (1990). Random Particle Model for Fracture of Aggregate or Fiber Composites.
579 *Journal of Engineering Mechanics*, 116(8):1686–1705. Publisher: American Society of Civil Engineers.
- 580 Blinowski, A., Ostrowska-Maciejewska, J., and Rychlewski, J. (1996). Two-dimensional Hooke’s tensors - isotropic decomposition, effective
581 symmetry criteria. *Archives of Mechanics*, 48(2):325–345. Number: 2.
- 582 Bolander, J. E., Eliáš, J., Cusatis, G., and Nagai, K. (2021). Discrete mechanical models of concrete fracture. *Engineering Fracture Mechanics*,
583 257:108030.
- 584 Bolander, J. E., Shiraishi, T., and Isogawa, Y. (1996). An adaptive procedure for fracture simulation in extensive lattice networks. *Engineering*
585 *Fracture Mechanics*, 54(3):325–334.
- 586 Chaboche, J.-L. (1978). Description thermodynamique et phénoménologique de la viscoélasticité cyclique avec endommagement. *Description*
587 *thermodynamique et phénoménologique de la viscoélasticité cyclique avec endommagement*.
- 588 Chaboche, J.-L. (1979). Le concept de contrainte effective appliqué à l’élasticité et à la viscoplasticité en présence d’un endommagement anisotrope.
589 *Col. Euromech*, 115:737–760.
- 590 Chaboche, J.-L. (1984). Anisotropic creep damage in the framework of continuum damage mechanics. *Nuclear Engineering and Design*, 79(3):309–
591 319.
- 592 Challamel, N., Picandet, V., and Pijaudier-Cabot, G. (2015). From discrete to nonlocal continuum damage mechanics: Analysis of a lattice system
593 in bending using a continualized approach. *International Journal of Damage Mechanics*, 24(7):983–1012. Publisher: SAGE Publications Ltd
594 STM.
- 595 Chen, Y., Davis, T. A., Hager, W. W., and Rajamanickam, S. (2008). Algorithm 887: CHOLMOD, Supernodal Sparse Cholesky Factorization and
596 Update/Downdate. *ACM Transactions on Mathematical Software*, 35(3):22:1–22:14.
- 597 Cordebois, J.-P. and Sidoroff, F. (1980). Anisotropic Damage in Elasticity and Plasticity. *Journal de mécanique théorique et appliquée*, pages
598 45–59.
- 599 Cordebois, J.-P. and Sidoroff, F. (1982). Damage Induced Elastic Anisotropy. pages 761–774, Dordrecht. Springer Netherlands. Book Title:
600 *Mechanical Behavior of Anisotropic Solids / Comportment Mécanique des Solides Anisotropes*.
- 601 Cormery, F. and Welemane, H. (2010). A stress-based macroscopic approach for microcracks unilateral effect. *Computational Materials Science*,
602 47(3):727–738.
- 603 Cundall, P. A. and Strack, O. D. L. (1979). A discrete numerical model for granular assemblies. *Géotechnique*, 29(1):47–65. Publisher: ICE
604 Publishing.
- 605 D’Addetta, G. A., Kun, F., and Ramm, E. (2002). On the application of a discrete model to the fracture process of cohesive granular materials.
606 *Granular Matter*, 4(2):77–90.
- 607 Davis, T. A. (2011). Algorithm 915, SuiteSparseQR: Multifrontal multithreaded rank-revealing sparse QR factorization. *ACM Transactions on*
608 *Mathematical Software*, 38(1):8:1–8:22.
- 609 de Arcangelis, L. and Herrmann, H. J. (1989). Scaling and multiscaling laws in random fuse networks. *Physical Review B*, 39(4):2678–2684.
610 Publisher: American Physical Society.
- 611 Delaplace, A. (2008). *Modélisation discrète appliquée au comportement des matériaux et des structures*. Mémoire d’habilitation à diriger des
612 recherches, Ecole Normale Supérieure de Cachan.
- 613 Delaplace, A. and Desmorat, R. (2008). Discrete 3D model as complimentary numerical testing for anisotropic damage. *International Journal of*
614 *Fracture*, 148(2):115–128.
- 615 Delaplace, A., Pijaudier-Cabot, G., and Roux, S. (1996). Progressive damage in discrete models and consequences on continuum modelling. *Journal*
616 *of the Mechanics and Physics of Solids*, 44(1):99–136.
- 617 Desmorat, B. and Desmorat, R. (2015). Tensorial Polar Decomposition of 2D fourth-order tensors. *Comptes Rendus Mécanique*, 343(9):471–475.
- 618 Desmorat, B. and Desmorat, R. (2016). Second order tensorial framework for 2D medium with open and closed cracks. *European Journal of*
619 *Mechanics - A/Solids*, 58:262–277.
- 620 Desmorat, R., Desmorat, B., Olive, M., and Kolev, B. (2018). Micromechanics based framework with second-order damage tensors. *European*
621 *Journal of Mechanics - A/Solids*, 69:88–98.
- 622 Diner, Ç., Kochetov, M., and Slawinski, M. A. (2011). Identifying Symmetry Classes of Elasticity Tensors Using Monoclinic Distance Function.
623 *Journal of Elasticity*, 102(2):175–190.

624 Dormieux, L. and Kondo, D. (2016). *Micromechanics of Fracture and Damage*. Wiley, 1 edition.

625 Dos Reis, F. and Ganghoffer, J. F. (2012). Construction of micropolar continua from the asymptotic homogenization of beam lattices. *Computers*
626 *& Structures*, 112-113:354–363.

627 Ehlers, W., Ramm, E., Diebels, S., and D’Addetta, G. A. (2003). From particle ensembles to Cosserat continua: homogenization of contact forces
628 towards stresses and couple stresses. *International Journal of Solids and Structures*, 40(24):6681–6702.

629 Fassin, M., Eggersmann, R., Wulfinghoff, S., and Reese, S. (2019). Gradient-extended anisotropic brittle damage modeling using a second order
630 damage tensor – Theory, implementation and numerical examples. *International Journal of Solids and Structures*, 167:93–126.

631 Fichant, S., La Borderie, C., and Pijaudier-Cabot, G. (1999). Isotropic and anisotropic descriptions of damage in concrete structures. *Mechanics of*
632 *Cohesive-frictional Materials*, 4(4):339–359. Publisher: Wiley.

633 François, M. (1995). *Identification des symétries matérielles de matériaux anisotropes*. phdthesis, Université Pierre et Marie Curie - Paris VI.

634 François, M., Geymonat, G., and Berthaud, Y. (1998). Determination of the symmetries of an experimentally determined stiffness tensor: Application
635 to acoustic measurements. *International Journal of Solids and Structures*, 35(31-32):4091–4106.

636 Gaines, B. R., Kim, J., and Zhou, H. (2018). Algorithms for Fitting the Constrained Lasso. *Journal of Computational and Graphical Statistics*,
637 27(4):861–871. Publisher: Taylor & Francis _eprint: <https://doi.org/10.1080/10618600.2018.1473777>.

638 Gazis, D. C., Tadjbakhsh, I., and Toupin, R. A. (1963). The elastic tensor of given symmetry nearest to an anisotropic elastic tensor. *Acta*
639 *Crystallographica*, 16(9):917–922.

640 Grassl, P. and Jirásek, M. (2006). Damage-plastic model for concrete failure. *International Journal of Solids and Structures*, 43(22):7166–7196.

641 Halm, D. and Dragon, A. (1996). A Model of Anisotropic Damage by Mesocrack Growth; Unilateral Effect. *International Journal of Damage*
642 *Mechanics*, 5(4):384–402. Publisher: SAGE Publications Ltd STM.

643 Herrmann, H. J., Hansen, A., and Roux, S. (1989). Fracture of disordered, elastic lattices in two dimensions. *Physical Review B*, 39(1):637–648.
644 Publisher: American Physical Society.

645 Herrmann, H. J. and Roux, S., editors (1990). *Statistical Models for the Fracture of Disordered Media*. Random Materials and Processes. North-
646 Holland, Amsterdam.

647 Hrennikoff, A. (1941). Solution of Problems of Elasticity by the Framework Method. *Journal of Applied Mechanics*, 8(4):A169–A175.

648 Kachanov, L. M. (1958). On Creep Rupture Time. *Izv. Acad. Nauk SSSR, Otd. Techn. Nauk*, 8:26–31.

649 Kachanov, M. (1992). Effective Elastic Properties of Cracked Solids: Critical Review of Some Basic Concepts. *Applied Mechanics Reviews*,
650 45(8):304–335. Publisher: American Society of Mechanical Engineers Digital Collection.

651 Kachanov, M. (1993). Elastic Solids with Many Cracks and Related Problems. In Hutchinson, J. W. and Wu, T. Y., editors, *Advances in Applied*
652 *Mechanics*, volume 30, pages 259–445. Elsevier.

653 Kawai, T. (1978). New discrete models and their application to seismic response analysis of structures. *Nuclear Engineering and Design*, 48(1):207–
654 229.

655 Krajcinovic, D. (1985). Continuous Damage Mechanics Revisited: Basic Concepts and Definitions. *Journal of Applied Mechanics*, 52(4):829–834.

656 Krajcinovic, D. (1996). *Damage Mechanics*. Elsevier.

657 Kun, F. and Herrmann, H. J. (1996). A study of fragmentation processes using a discrete element method. *Computer Methods in Applied Mechanics*
658 *and Engineering*, 138(1):3–18.

659 Ladevèze, P. (1983). Sur une théorie de l’endommagement anisotrope. Rapport Interne 34, LMT Cachan.

660 Ladevèze, P. (1995). Modelling and simulation of the mechanical behaviour of CMCs. *Ceram. Trans. Vol. 57*, pages 53–63.

661 Landis, E. N. (1999). Micro–macro fracture relationships and acoustic emissions in concrete. *Construction and Building Materials*, 13(1):65–72.

662 Leckie, F. A. and Onat, E. T. (1981). Tensorial Nature of Damage Measuring Internal Variables. In Hult, J. and Lemaitre, J., editors, *Physical*
663 *Non-Linearities in Structural Analysis*, International Union of Theoretical and Applied Mechanics, pages 140–155, Berlin, Heidelberg. Springer.

664 Lemaitre, J. (1984). How to use damage mechanics. *Nuclear Engineering and Design*, 80(2):233–245.

665 Lemaitre, J. (1992). *A Course on Damage Mechanics*. Springer-Verlag, Berlin Heidelberg.

666 Lemaitre, J. and Chaboche, J.-L. (1985). *Mécanique des matériaux solides*. Dunod, english translation 1990 ‘Mechanics of Solid Materials’
667 Cambridge University Press.

668 Lemaitre, J. and Desmorat, R. (2005). *Engineering Damage Mechanics: Ductile, Creep, Fatigue and Brittle Failures*. Springer-Verlag, Berlin
669 Heidelberg.

670 Lemaitre, J., Desmorat, R., and Sauzay, M. (2000). Anisotropic damage law of evolution. *European Journal of Mechanics - A/Solids*, 19(2):187–208.

671 Lubarda, V. A. and Krajcinovic, D. (1993). Damage tensors and the crack density distribution. *International Journal of Solids and Structures*,
672 30(20):2859–2877.

673 Mazars, J. (1984). *Application de la mécanique de l’endommagement au comportement non-linéaire et à la rupture du béton de structure*. THESE
674 DE DOCTEUR ES SCIENCES, Université Pierre et Marie Curie - Paris VI - Laboratoire de Mécanique et Technologie.

675 Mazars, J., Berthaud, Y., and Ramtani, S. (1990). The unilateral behaviour of damaged concrete. *Engineering Fracture Mechanics*, 35(4):629–635.

676 Meguro, K. and Hakuno, M. (1989). Fracture Analyses of Concrete Structures by the Modified Distinct Element Method. *Doboku Gakkai*
677 *Ronbunshu*, 1989(410):113–124.

678 Meurer, A., Smith, C. P., Paprocki, M., Čertík, O., Kirpichev, S. B., Rocklin, M., Kumar, A., Ivanov, S., Moore, J. K., Singh, S., Rathnayake, T., Vig,
679 S., Granger, B. E., Muller, R. P., Bonazzi, F., Gupta, H., Vats, S., Johansson, F., Pedregosa, F., Curry, M. J., Terrel, A. R., Roučka, Š., Saboo,
680 A., Fernando, I., Kulal, S., Cimrman, R., and Scopatz, A. (2017). SymPy: symbolic computing in Python. *PeerJ Computer Science*, 3:e103.
681 Publisher: PeerJ Inc.

682 Migliori, A., Sarrao, J. L., Visscher, W. M., Bell, T. M., Lei, M., Fisk, Z., and Leisure, R. G. (1993). Resonant ultrasound spectroscopic techniques
683 for measurement of the elastic moduli of solids. *Physica B: Condensed Matter*, 183(1):1–24.

684 Moakher, M. and Norris, A. N. (2006). The Closest Elastic Tensor of Arbitrary Symmetry to an Elasticity Tensor of Lower Symmetry. *Journal of*
685 *Elasticity*, 85(3):215–263.

686 Murakami, S. (1988). Mechanical Modeling of Material Damage. *Journal of Applied Mechanics*, 55(2):280–286.

- 687 Murakami, S. (2012). *Continuum Damage Mechanics*, volume 185 of *Solid Mechanics and Its Applications*. Springer Netherlands, Dordrecht.
- 688 Murakami, S. and Ohno, N. (1978). A constitutive equation of creep damage in polycrystalline metals. In *IUTAM Colloquium Euromech*, volume
689 111.
- 690 Olive, M., Kolev, B., Desmorat, B., and Desmorat, R. (2017). Harmonic Factorization and Reconstruction of the Elasticity Tensor. *Journal of*
691 *Elasticity*, 132(1):67–101.
- 692 Olive, M., Kolev, B., Desmorat, R., and Desmorat, B. (2022). Characterization of the symmetry class of an elasticity tensor using polynomial
693 covariants. *Mathematics and Mechanics of Solids*, 27(1):144–190. Publisher: SAGE Publications Ltd STM.
- 694 Oliver-Leblond, C. (2019). Discontinuous crack growth and toughening mechanisms in concrete: A numerical study based on the beam-particle
695 approach. *Engineering Fracture Mechanics*, 207:1–22.
- 696 Oliver-Leblond, C., Desmorat, R., and Kolev, B. (2021). Continuous anisotropic damage as a twin modelling of discrete bi-dimensional fracture.
697 *European Journal of Mechanics - A/Solids*, 89:104285.
- 698 Papa, E. and Taliercio, A. (1996). Anisotropic damage model for the multiaxial static and fatigue behaviour of plain concrete. *Engineering Fracture*
699 *Mechanics*, 55(2):163–179.
- 700 Ponte Castañeda, P. and Willis, J. R. (1995). The effect of spatial distribution on the effective behavior of composite materials and cracked media.
701 *Journal of the Mechanics and Physics of Solids*, 43(12):1919–1951.
- 702 Pradel, F. and Sab, K. (1998). Cosserat modelling of elastic periodic lattice structures. *Comptes Rendus de l'Académie des Sciences - Series IIB -*
703 *Mechanics-Physics-Astronomy*, 326(11):699–704. Publisher: Elsevier Masson.
- 704 Rabotnov, Y. N. (1969). Creep Problems in Structural Members. *North-Holland Publishing Company, Amsterdam*.
- 705 Ramtani, S., Berthaud, Y., and Mazars, J. (1992). Orthotropic behavior of concrete with directional aspects: modelling and experiments. *Nuclear*
706 *Engineering and Design*, 133(1):97–111.
- 707 Rezakhani, R. and Cusatis, G. (2016). Asymptotic expansion homogenization of discrete fine-scale models with rotational degrees of freedom for
708 the simulation of quasi-brittle materials. *Journal of the Mechanics and Physics of Solids*, 88:320–345.
- 709 Richard, B. and Ragueneau, F. (2013). Continuum damage mechanics based model for quasi brittle materials subjected to cyclic loadings:
710 Formulation, numerical implementation and applications. *Engineering Fracture Mechanics*, 98:383–406.
- 711 Rinaldi, A. and Lai, Y.-C. (2007). Statistical damage theory of 2D lattices: Energetics and physical foundations of damage parameter. *International*
712 *Journal of Plasticity*, 23(10):1796–1825.
- 713 Rossi, P. and Richer, S. (1987). Numerical modelling of concrete cracking based on a stochastic approach. *Materials and Structures*, 20(5):334–337.
- 714 Roux, J., Hosten, B., Castagnede, B., and Deschamps, M. (1985). Caractérisation mécanique des solides par spectro-interférométrie ultrasonore.
715 *Revue de Physique Appliquée*, 20(6):351–358. Publisher: Société Française de Physique.
- 716 Schlangen, E. and van Mier, J. G. M. (1992). Simple lattice model for numerical simulation of fracture of concrete materials and structures. *Materials*
717 *and Structures*, 25(9):534–542.
- 718 Tibshirani, R. (1996). Regression Shrinkage and Selection via the Lasso. *Journal of the Royal Statistical Society. Series B (Methodological)*,
719 58(1):267–288. Publisher: [Royal Statistical Society, Wiley].
- 720 Vakulenko, A. A. and Kachanov, M. (1971). Continuum theory of medium with cracks. *Mekhanika tverdogo tela*, 4:159–166.
- 721 van Mier, J. G. M., van Vliet, M. R. A., and Wang, T. K. (2002). Fracture mechanisms in particle composites: statistical aspects in lattice type
722 analysis. *Mechanics of Materials*, 34(11):705–724.
- 723 Vannucci, P. (2002). A Special Planar Orthotropic Material. *Journal of elasticity and the physical science of solids*, 67(2):81–96.
- 724 Vannucci, P. (2005). Plane Anisotropy by the Polar Method*. *Meccanica*, 40(4):437–454.
- 725 Vassaux, M. (2015). *Comportement mécanique des matériaux quasi-fragiles sous sollicitations cycliques : de l'expérimentation numérique au*
726 *calcul de structures*. phdthesis, École normale supérieure de Cachan - ENS Cachan.
- 727 Vassaux, M., Oliver-Leblond, C., Richard, B., and Ragueneau, F. (2016). Beam-particle approach to model cracking and energy dissipation in
728 concrete: Identification strategy and validation. *Cement and Concrete Composites*, 70:1–14.
- 729 Verchery, G. (1982). Les Invariants des Tenseurs d'Ordre 4 du Type de l'élasticité. In Boehler, J.-P., editor, *Mechanical Behavior of Anisotropic*
730 *Solids / Comportement Mécanique des Solides Anisotropes*, pages 93–104, Dordrecht. Springer Netherlands.
- 731 Vianello, M. (1997). An integrity basis for plane elasticity tensors. *Archives of Mechanics*, 49(1):197–208. Number: 1.
- 732 Willam, K., Pramono, E., and Sture, S. (1989). Fundamental Issues of Smearred Crack Models. In Shah, S. P. and Swartz, S. E., editors, *Fracture*
733 *of Concrete and Rock*, pages 142–157, New York, NY. Springer.

734 A. Distance to bi-dimensional elastic orthotropy

735 This appendix provides a summary of the calculation of the exact distance of a 2D elasticity tensor to orthotropy.
736 We refer to (Antonelli et al., 2022) for the details.

737 The first step is to parametrize the orthotropic tensors \mathbf{E}^* from Eq. (23), in Kelvin notation,

$$738 \mathbf{E}^* = \mathbf{Q} \star \mathbf{A}, \quad \mathbf{Q} = \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix}, \quad [\mathbf{A}] = \begin{bmatrix} A_{1111} & A_{1122} & 0 \\ A_{1122} & A_{2222} & 0 \\ 0 & 0 & 2A_{1212} \end{bmatrix}, \quad (72)$$

738 where \mathbf{Q} is a rotation matrix, \mathbf{A} is the normal form of orthotropic 2D elasticity tensors, and $[\mathbf{A}]$ stands for its Kelvin
739 notation. With this parametrization, the minimization problem becomes

$$d_{\mathcal{O}rt}(\mathbf{E}) = \min_{\theta, \mathbf{A}} \|\mathbf{E} - \mathbf{Q} \star \mathbf{A}\|, \quad \Delta_{\mathcal{O}rt}(\mathbf{E}) = \frac{d_{\mathcal{O}rt}(\mathbf{E})}{\|\mathbf{E}\|}, \quad (73)$$

740 where $\|\mathbf{E}\| = \sqrt{E_{ijkl}E_{ijkl}}$. By applying the harmonic decomposition to \mathbf{E} and \mathbf{A} , and using the orthogonality of its
741 isotropic/dilatation/harmonic parts, we have

$$d_{\mathcal{O}rt}(\mathbf{E})^2 = \min_{\theta, \mathbf{A}} (\|\mathbf{Iso}(\mathbf{E}) - \mathbf{Iso}(\mathbf{A})\|^2 + \|\mathbf{Dil}(\mathbf{E}) - \mathbf{Q} \star \mathbf{Dil}(\mathbf{A})\|^2 + \|\mathbf{H}(\mathbf{E}) - \mathbf{Q} \star \mathbf{H}(\mathbf{A})\|^2). \quad (74)$$

742 For the isotropic part, the closest isotropic tensor is the isotropic tensor itself, $\mathbf{Iso}(\mathbf{A}) = \mathbf{Iso}(\mathbf{E})$ (by Eq. (22)).
743 Furthermore:

744 • For the dilatation part term, we can introduce the deviatoric part of the dilatation tensor

$$\mathbf{d}'(\mathbf{E}) = \begin{bmatrix} d'_{11} & d'_{12} \\ d'_{11} & -d'_{12} \end{bmatrix}, \quad \mathbf{d}'(\mathbf{A}^*) = d^* \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix}, \quad \mathbf{Q} \star \mathbf{d}'(\mathbf{A}) = d^* \begin{bmatrix} \cos 2\theta & \sin 2\theta \\ \sin 2\theta & -\cos 2\theta \end{bmatrix}, \quad (75)$$

745 where

$$746 \quad d'_{11} = \frac{1}{2} (E_{1111} - E_{2222}), \quad d'_{12} = E_{1112} + E_{2212}.$$

747 • For the harmonic part term, we can introduce the harmonic parts (in Kelvin notation)

$$\begin{aligned} [\mathbf{H}(\mathbf{E})] &= \begin{bmatrix} H_{1111} & -H_{1111} & \sqrt{2}H_{1112} \\ -H_{1111} & H_{1111} & -\sqrt{2}H_{1112} \\ \sqrt{2}H_{1112} & -\sqrt{2}H_{1112} & -2H_{1111} \end{bmatrix}, & [\mathbf{H}(\mathbf{A})] &= H^* \begin{bmatrix} 1 & -1 & 0 \\ -1 & 1 & 0 \\ 0 & 0 & -2 \end{bmatrix}, \\ [\mathbf{Q} \star \mathbf{H}(\mathbf{A})] &= H^* \begin{bmatrix} \cos 4\theta & -\cos 4\theta & \sqrt{2} \sin 4\theta \\ -\cos 4\theta & \cos 4\theta & -\sqrt{2} \sin 4\theta \\ \sqrt{2} \sin 4\theta & -\sqrt{2} \sin 4\theta & -2 \cos 4\theta \end{bmatrix}, \end{aligned} \quad (76)$$

748 where

$$749 \quad H_{1111} = \frac{1}{8} (E_{1111} - 2E_{1122} - 4E_{1212} + E_{2222}), \quad H_{1112} = \frac{1}{2} (E_{1112} - E_{2212}).$$

750 We have then, by Eq. (11),

$$d_{\mathcal{O}rt}(\mathbf{E})^2 = \min_{\theta, d^*, H^*} (\|\mathbf{d}'(\mathbf{E}) - \mathbf{Q} \star \mathbf{d}'(\mathbf{A})\|^2 + \|\mathbf{H}(\mathbf{E}) - \mathbf{Q} \star \mathbf{H}(\mathbf{A})\|^2). \quad (77)$$

751 The minimizations with respect to d^* and to H^* give

$$752 \quad d^* = d'_{11} \cos 2\theta + d'_{12} \sin 2\theta, \quad H^* = H_{1111} \cos 4\theta + H_{1112} \sin 4\theta. \quad (78)$$

752 The minimization with respect to θ ends then up to the equation

$$A \cos 8\theta + B \sin 8\theta + C \cos 4\theta + D \sin 4\theta = 0, \quad (79)$$

753 where (Antonelli et al., 2022):

$$\begin{aligned} A &= 2(E_{1111} - 2E_{1122} - 4E_{1212} + E_{2222})(E_{1112} - E_{2212}) = 32H_{1111}H_{1112}, \\ B &= 4(E_{1112} - E_{2212})^2 - \frac{1}{4}(E_{1111} - 2E_{1122} - 4E_{1212} + E_{2222})^2 = 16(H_{1112}^2 - H_{1111}^2), \\ C &= 2(E_{1111} - E_{2222})(E_{1112} + E_{2212}) = 4d'_{11}d'_{12}, \\ D &= 2(E_{1112} + E_{2212})^2 - \frac{1}{2}(E_{1111} - E_{2222})^2 = 2(d'_{12}^2 - d'_{11}^2). \end{aligned} \quad (80)$$

754 Setting $\theta = \frac{1}{2} \arctan t$, we obtain the fourth-order polynomial in t ,

$$(A - C)t^4 + (2D - 4B)t^3 - 6At^2 + (2D + 4B)t + A + C = 0. \quad (81)$$

755 The roots t_k of the polynomial are obtained by symbolic resolution of the polynomial using (Meurer et al., 2017),
 756 and then evaluated numerically. The root retained corresponds to either to the solution $\theta = \frac{1}{2} \arctan(t_k)$ or to the
 757 solution $\theta = \frac{1}{2} \arctan(t_k) - \frac{\pi}{2}$ that minimizes $d_{\text{ort}}(\mathbf{E})^2$. Finally, the distance to orthotropy is obtained by injecting the
 758 minimizers $-d^*$ and H^* both from Eq. (78), and θ — and taking the square root of Eq. (77).

759 B. Damaging loadings

760 Table 8 and Table 9 provide a description of the damaging loadings. Each loading is discretized into load steps.
 761 During KUBC and PBC loadings, the strain is imposed on the whole boundary $\partial\Omega$ of the Area Element. During EXPE
 762 loading, a displacement is imposed on the sub-parts of the boundary $\partial\Omega$. Each load step adds an increment of strain
 763 $\Delta\boldsymbol{\varepsilon}(\mathbf{x})$, and displacement $\Delta\mathbf{u}(\mathbf{x})$, to the currently imposed strain, and displacement, respectively. The strain at load step
 764 i is

$$\begin{cases} \boldsymbol{\varepsilon}^0 = \mathbf{0}, \\ \boldsymbol{\varepsilon}^i = \boldsymbol{\varepsilon}^{i-1} + \Delta\boldsymbol{\varepsilon}^i. \end{cases} \quad (82)$$

765 The displacement at load step i , on a sub-part of the boundary $\partial\Omega_u$, is

$$\forall \mathbf{x} \in \partial\Omega_u, \quad \begin{cases} \mathbf{u}^0(\mathbf{x}) = \mathbf{0} \\ \mathbf{u}^i(\mathbf{x}) = \mathbf{u}^{i-1}(\mathbf{x}) + \Delta\mathbf{u}^i(\mathbf{x}). \end{cases} \quad (83)$$

766 In practice, the boundary $\partial\Omega_u = \{\mathbf{x} = (x, y) \mid x = 0\}$ corresponds to the the layer of particle having their center in the
 767 rectangle defined by $[0, \bar{l}_b] \times [0, L]$.

768 **Remark 9.** The rotation of particle is never imposed in those loadings.

Type	Name	Load steps (i)		Strain incs $\Delta \epsilon^i \times 10^6$		
		Start	End	ϵ_{xx}	ϵ_{yy}	ϵ_{xy}
KUBC	bi-tension	1	100	6	6	0
	shear	1	100	0	0	15
	tension	1	100	10	0	0
	shear \rightarrow tension	1	50	0	0	10
		50	100	20	0	0
	tension \rightarrow shear	1	50	10	0	0
		50	100	0	0	20
	tension \rightarrow tension	1	50	10	0	0
50		100	0	10	0	
(Willam et al., 1989)	1	100	4	0	0	
	100	200	2	1	3	
PBC	bi-tension	1	100	5	5	0
	shear	1	100	0	0	10
	tension	1	100	3	0	0
	shear \rightarrow tension	1	50	0	0	10
		50	100	40	0	0
	tension \rightarrow shear	1	50	10	0	0
		50	100	0	0	20
	tension \rightarrow tension	1	50	6	0	0
50		100	0	6	0	
(Willam et al., 1989)	1	100	8	0	0	
	100	200	4	6	2	

Table 8

KUBC and PBC damaging loadings. For PBC loadings, an particle is locked in displacement to prevent rigid body motions.

Name	Load steps		Displacement incs $\Delta u^i(x) \times 10^6$							
	Start	End	$x = 0$		$x = L$		$y = 0$		$y = L$	
			u_x	u_y	u_x	u_y	u_x	u_y	u_x	u_y
bitension	1	100	0	-	1.2	-	-	0	-	1.2
tension	1	100	0	-	1	-	-	-	-	-
shear	1	100	-	0	-	0.8	0	-	0.8	0
simple shear	1	100	-	-	-	-	0	0	0	4
shear \rightarrow tension	1	50	-	0	-	1.6	0	-	1.6	0
	50	100	0	-	2	-	-	-	-	-
tension \rightarrow shear	1	50	0	-	1	-	-	-	-	-
	50	100	-	0	-	1.6	0	-	1.6	-
tension \rightarrow tension	1	50	0	-	1.2	-	-	-	-	-
	50	100	-	-	-	-	-	0	-	1.2

Table 9

EXPE loadings. For most of those loadings, an additional constraint is applied to a particle to prevent rigid body motion.