



Antenna Design for Spin Wave Caustic Beams

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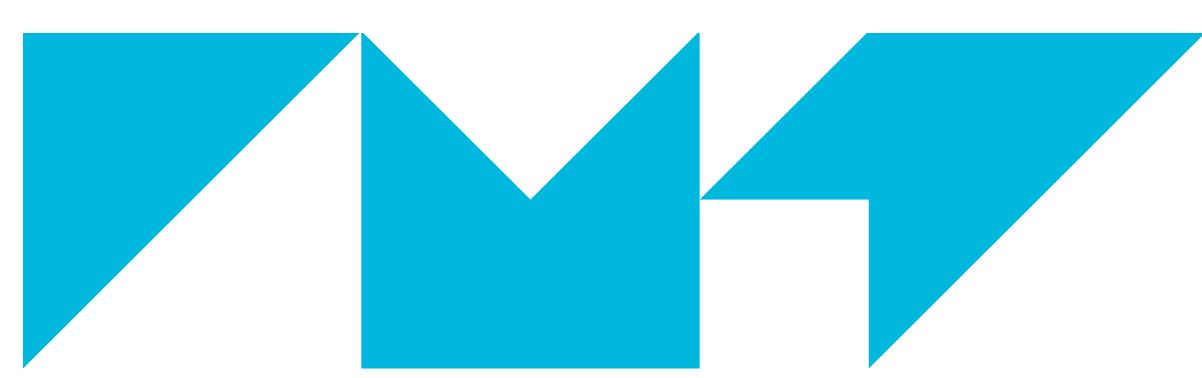
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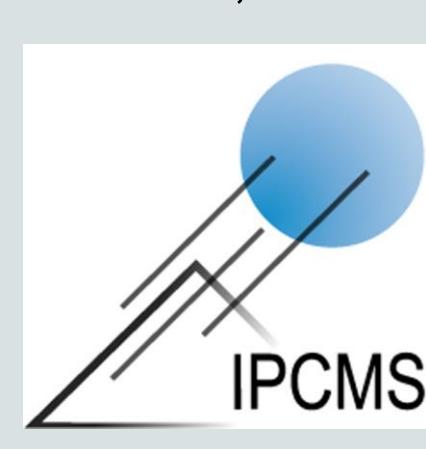


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Fundings



Thomas Jefferson
Magnon
Interferometry



SOS MAG

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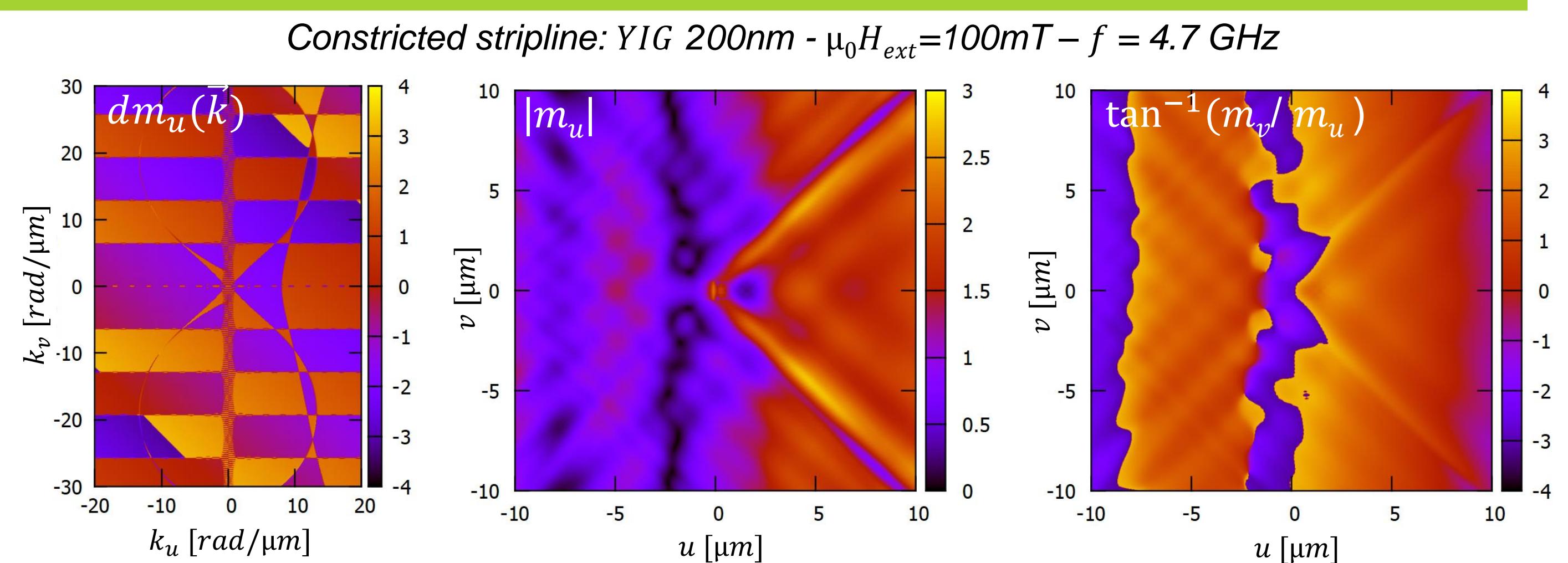
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Motivations

- **Non-reciprocal magnonic devices**
Miniaturizing isolator, circulator, delay lines

- **Shaping spin-wave beams in extended layer**
Development of magnon interferometric devices [1-3]

- **Diffraction model for in-plane spin-wave modes**
Efficient tool to map the Near-Field Diffraction (NFD) patterns of any shape of spin-wave antennas [4]



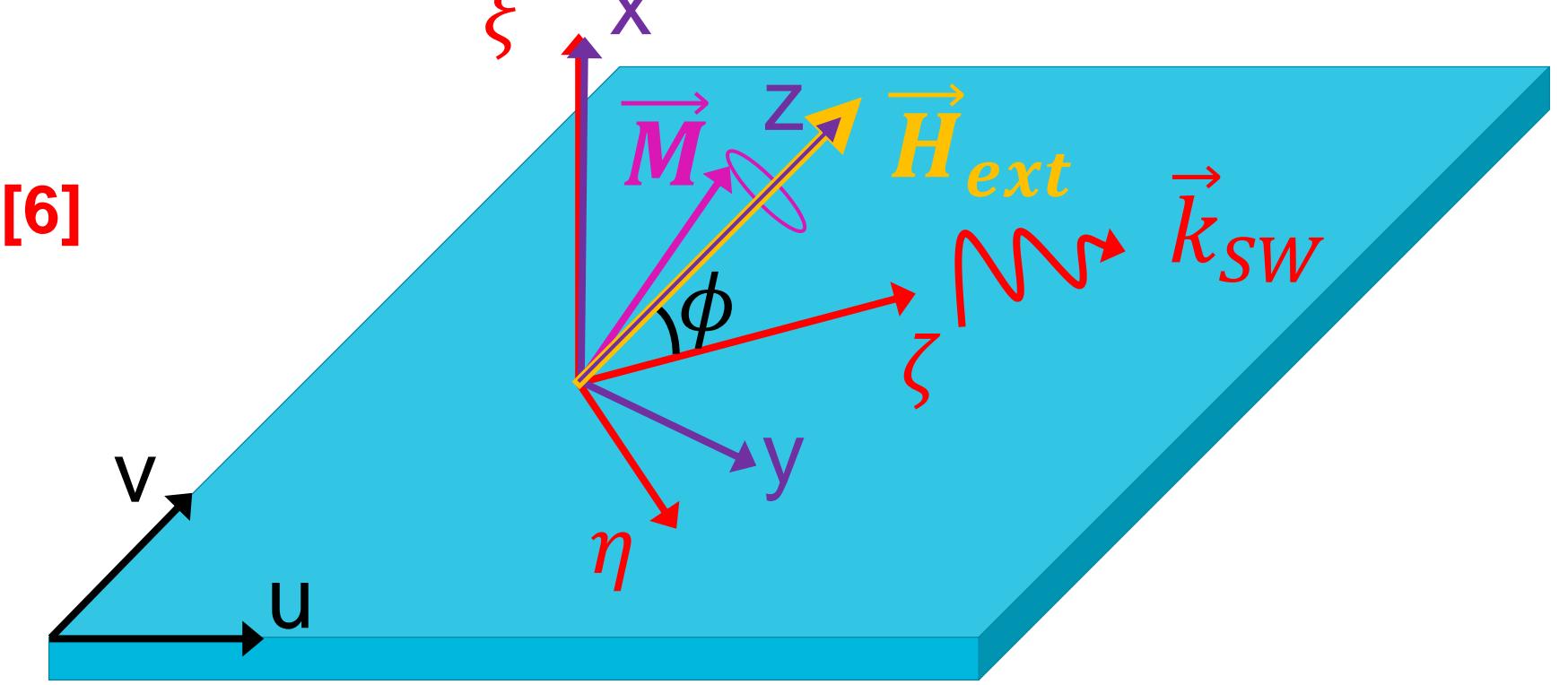
Near-Field diffraction model for in-plane magnetized films

- ❖ **Kalinikos's approach to express $\vec{m}(u, v, t)$ [5]**

- **(ξ, η, ζ) SW Propagation frame \Rightarrow dynamic dipolar field $\vec{h}_d(\xi)$ from Green functions [6]**

$$\vec{h}_d(\xi) = \int_{-\frac{l}{2}}^{\frac{l}{2}} \bar{G}_{xy}(\xi - \xi') \vec{m}(\xi') d\xi' = -\bar{N}_{dip} \vec{m}$$

$$\bar{G}_{\xi\eta\zeta}(\xi - \xi') = \begin{pmatrix} G_p - \delta(\xi - \xi') & 0 & iG_Q \\ 0 & 0 & 0 \\ iG_Q & 0 & -G_p \end{pmatrix} \quad \text{change of frame } (\xi, \eta, \zeta) \Rightarrow (x, y, z) \quad (P = 1 - \frac{1 - e^{-kt}}{kt})$$

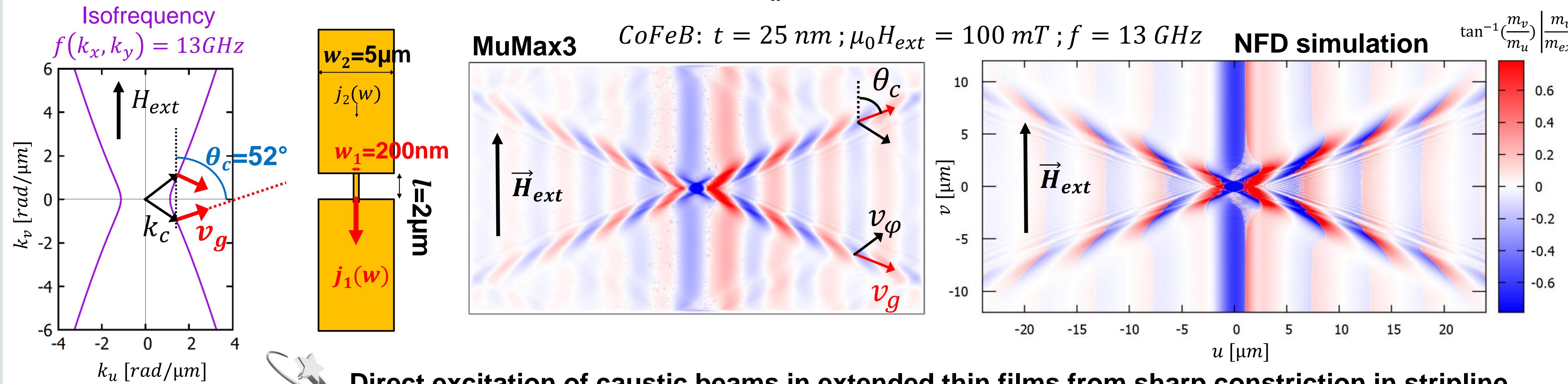


- **(x, y, z) $\vec{M}(\vec{r}, t)$ frame \Rightarrow Linearizing LLG**

$$i\omega \vec{m} = -\gamma \mu_0 H_{equ} \vec{m} \times \vec{u}_z + \gamma \mu_0 M_{equ} \vec{h} \times \vec{u}_z - \alpha i\omega \vec{m} \times \vec{u}_z \quad \Rightarrow \quad \bar{\chi}^{-1} \vec{m} = \vec{h}_{exc} \quad \Rightarrow \quad \frac{1}{\omega_M} \begin{pmatrix} \Omega_k + i\alpha\omega + \omega_M \bar{N}_{d,xx}^{00} & -i\omega + \omega_M \bar{N}_{d,xy}^{00} \\ i\omega + \omega_M \bar{N}_{d,yx}^{00} & \Omega_k + i\alpha\omega + \omega_M \bar{N}_{d,yy}^{00} \end{pmatrix} \begin{pmatrix} m_x \\ m_y \end{pmatrix} = \begin{pmatrix} h_x \\ h_y \end{pmatrix}$$

- **(u, v, ξ) Lab frame - antenna orientation $\Rightarrow FFT^{-1}\{\vec{m}(\vec{k})\}$** $\Rightarrow \vec{m}(u, v, t) = e^{i\omega t} \iint_{-\infty}^{+\infty} dk_u dk_v \bar{\chi}(k_u, k_v) \cdot \vec{h}_{exc}(k_u, k_v) e^{-i(k_u u + k_v v)}$

- ❖ **Anisotropic dispersion \Rightarrow Caustic beam when $\frac{d^2 k_v}{dk_u^2} = 0$**



Direct excitation of caustic beams in extended thin films from sharp constriction in stripline

Caustic beam definition

- ❖ **Thickness dependence $t_{YIG} = 200 nm$**

$w_1 = 200 nm$

$w_2 = 10 \mu m ; l = 2 \mu m$

$\mu_0 H_{ext} = 50 mT ; f = 3.2 GHz$

bottom surface $\xi = 0$

\vec{H}_{ext}

\vec{m}_{exc}

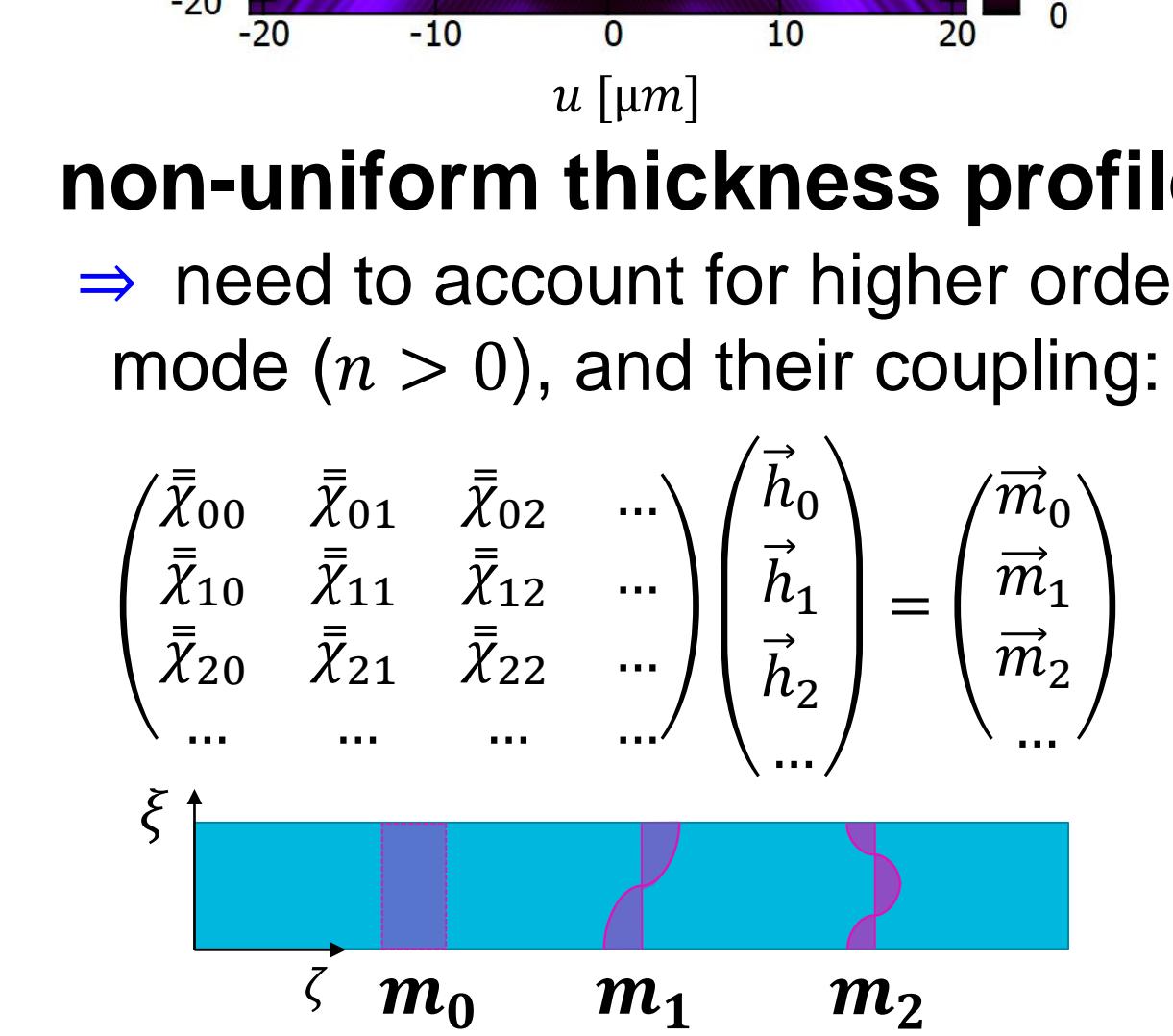
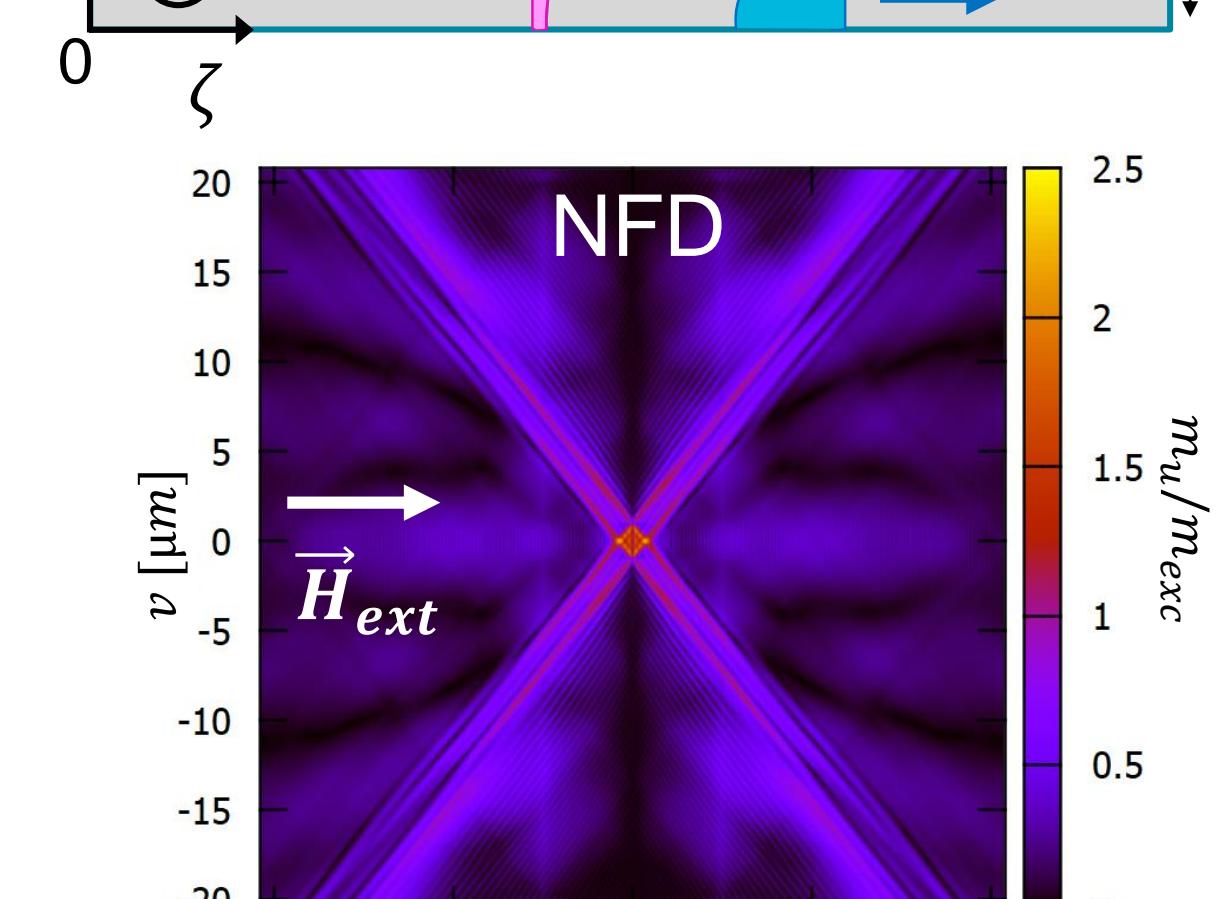
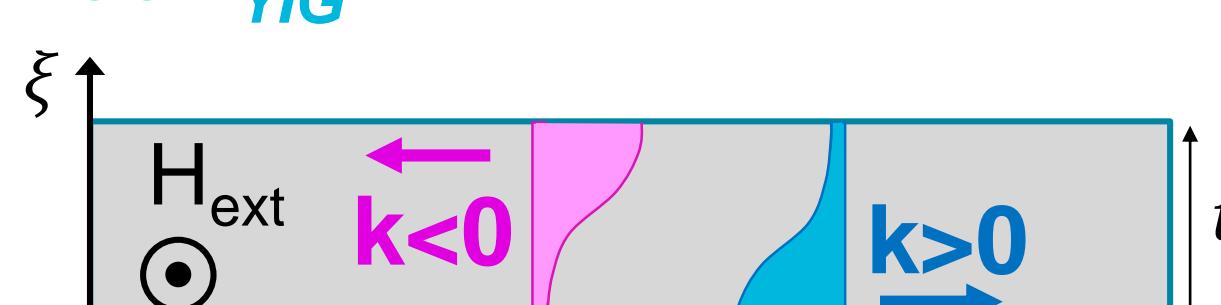
MuMax3

top surface $\xi = t$

\vec{H}_{ext}

\vec{m}_{exc}

MuMax3



non-uniform thickness profile
need to account for higher order mode ($n > 0$), and their coupling:

$$\begin{pmatrix} \bar{x}_{00} & \bar{x}_{01} & \bar{x}_{02} & \dots \\ \bar{x}_{10} & \bar{x}_{11} & \bar{x}_{12} & \dots \\ \bar{x}_{20} & \bar{x}_{21} & \bar{x}_{22} & \dots \\ \dots & \dots & \dots & \dots \end{pmatrix} \begin{pmatrix} \vec{h}_0 \\ \vec{h}_1 \\ \vec{h}_2 \\ \dots \end{pmatrix} = \begin{pmatrix} \vec{m}_0 \\ \vec{m}_1 \\ \vec{m}_2 \\ \dots \end{pmatrix}$$

- ❖ **Frequency and constriction size dependence**

$w_1 = 200 nm ; w_2 = 40 \mu m ; l = 500 nm$

$\mu_0 H_{ext} = 100 mT ; t_{YIG} = 200 nm$

4.4 GHz

\vec{H}_{ext}

\vec{m}_{exc}

MuMax3

4.8 GHz

\vec{H}_{ext}

\vec{m}_{exc}

MuMax3

5.2 GHz

\vec{H}_{ext}

\vec{m}_{exc}

MuMax3

4.4 GHz

\vec{H}_{ext}

\vec{m}_{exc}

MuMax3

4.8 GHz

\vec{H}_{ext}

\vec{m}_{exc}

MuMax3

5.2 GHz

\vec{H}_{ext}

\vec{m}_{exc}

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