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## Thermionic emission of a tungsten surface in high heat flux plasma: PIC simulations

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The surface temperature of a tungsten surface facing hot hydrogen plasma is evaluated thanks to 1d/3v particle-in-cell simulations in floating wall conditions. At each iteration, the plasma heat flux to the cathode is equalized with the outgoing one, which is due to thermionic emission, surface radiation and heat conduction through the wall. The thermal conductivity is chosen within the range 35-160 Wm<sup>-1</sup>K<sup>-1</sup> in the different simulations in order to take into account the surface condition. A transition from a cold temperature surface to a hot one arises for a critical thermal conductivity, whose value depends on the plasma parameters. This transition is very abrupt and leads to a space charge limited regime where the thermionic current penetrating the plasma has reached its maximal value and is about 3 times the Bohm current. Changing the initial conditions in the code, more particularly the timing of electron emission, can lead to a very different final surface temperature. This history effect and the associated hysteresis are evidenced by means of fluid calculations which are in a good agreement with the simulations results as well as with previous experimental measurements.

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## I. INTRODUCTION

The plasma-wall interaction is a fundamental issue in fusion devices, and specially for ITER, because high heat fluxes in the tens of  $\text{MWm}^{-2}$  range are expected to hit on parts of the first wall of this large size tokamak. High heat fluxes can lead to the formation of hot spots<sup>1</sup> on plasma-facing components, resulting for instance in erosion on the divertor plate material or antenna structures and in the subsequent pollution of the plasma core.

In the ITER scenario, the tungsten (W) mono-blocs are designed at the divertor to withstand a steady state  $10 \text{ MW/m}^2$  heat flux. In a numerical study, J.P. Gunn et al.<sup>2</sup> have showed that during this steady state phase, the W surface temperature  $T_s$  at the trailing edge of the mono-blocs can reach  $1300 - 1600 \text{ K}$  and even above the melting temperature during slow transient reattachment events with a heat flux of the order of  $20 \text{ MW/m}^2$ . In misaligned W mono-blocs with different shaping<sup>3</sup>, a temperature of the order of  $3400 \text{ K}$  is expected for a steady state perpendicular heat flux of  $31 \text{ MW/m}^2$ . An exposed leading edge receives actually 15 to 60 times more heat loads than a perfectly aligned surface<sup>4</sup>. Such misalignment of the W mono-blocs has been extensively studied in tokamak facilities under plasma conditions with parallel heat flux of the order of  $100 \text{ MW/m}^2$ . Melting of the mono-blocs edges and thermionic emission was evidenced in several reports<sup>5,6</sup>. These experimental observations have lead to further numerical works emphasizing the importance of sheaths at the vicinity hot tungsten surfaces in ELMs phases for modeling the melt motion induced by fast transients<sup>7</sup>.

In this context, thermionic emission of electrons from hot material surfaces is of a particular interest, because it deeply changes the energy transmission coefficient through the sheath<sup>8,9</sup>. On the one hand, thermionic emission can induce a reduction of the sheath voltage, which can prevent plasma species to overcome the sputtering threshold of the surface and suppress the impurity generation by physical sputtering<sup>10</sup>. On the other hand, the expected decrease of the potential drop in the sheath can lead to the enhancement of the heat flux to the wall because a larger amount of hot plasma electrons are allowed to reach the surface. The increased heat flux increases the surface temperature  $T_s$  as well as the thermionic current  $J_s$  according to the Richardson-Dushman's formula:

$$J_s = AT_s^2 \exp\left(-\frac{B_w}{k_b T_s}\right), \quad (1)$$

with  $A$  the Dushman's constant and  $B_w$  the electron work function which both depend on the surface material. For tungsten<sup>11</sup>,  $A = 60 \times 10^4 \text{ Am}^{-2}\text{K}^{-2}$  and  $B_w = 4.55 \text{ eV}$ . This enhancement of  $J_s$  in turn increases the plasma heat flux again; the instability finally ends up when an equilibrium surface temperature is reached<sup>12</sup>.

Surface heating induces at the same time the desorption of hydrogen atoms trapped at the material vacancies<sup>13</sup> but also the sublimation of the material itself<sup>14</sup>. The hydrogen atoms, if ionized near the surface, increase locally the density of the main plasma, and the ionized metallic vapor creates a secondary plasma in front of the spot. While the return of part of the material vapor to the surface contributes to its over-heating<sup>15</sup>, the presence of a denser secondary plasma allows for an enhancement of the thermionic current. Both phenomena are envisaged as the origin of unipolar arcs, which drain a very large amount of current circulating from the wall to the plasma<sup>16,17</sup>.

The emitted current is indeed strongly limited by space charge effects. The first model explaining this electrostatic phenomenon is due to Child<sup>18</sup> in 1911, which has been extended by Langmuir<sup>19</sup> two years later in order to explain the saturation of the thermionic current with the temperature of an emitting filament. Actually, when electrons are emitted without initial velocity from a cathode in vacuum, as soon as the electric field vanishes at the surface due to the accumulation of negative charges, the current is limited. This basic assumption allows the derivation of the well-known Child-Langmuir expression of the limited current:

$$J_s^* = \frac{4\epsilon_0}{9} \sqrt{\frac{2e}{m}} \frac{V^{3/2}}{L^2}, \quad (2)$$

where  $J_s^*$  is the maximum charge current,  $V$  the applied voltage,  $e$  and  $m$  the electron charge and mass respectively and  $L$  the distance between electrodes.

Although Eq. (2) is theoretically only applicable to vacuum, it is used in plasma physics in order to derive the variation of the sheath size with respect to a wall potential<sup>20,21</sup>, which is important for instance in Langmuir probe measurements and their interpretation. However, as sheaths are positive-space-charged regions built up in surfaces vicinity in order to balance particles flows, they modify substantially the assumptions used to derive Eq. (2). That is why several authors have extended the Child-Langmuir model by taking into account the presence of this thin positive charged layer extending over a few Debye lengths ( $\lambda_d$ ) and evaluating the effect of an emitted electron current  $J_s$ , which would tend to neutralize it. Models have been derived in floating<sup>8,22,23</sup> as well as under biased wall conditions<sup>24-26</sup>. Both

theoretical approaches lead to the same conclusion: above a maximum thermionic current  $J_s^*$ , the accumulation of negative charges at the wall vicinity induces a non monotonic variation of the plasma potential; the electric field cancels close to the surface. In this situation, the wall is covered up by a double layer, with a potential well (a virtual cathode), which regulates the electron current. In other words, if the space charge limited regime is not yet reached,  $J_s$  is given by the Richardson-Dushman formula (Eq. (1)), otherwise the current is limited and the current penetrating the plasma is  $J_s^*$  even if  $T_s$  is still increased. Then, the virtual cathode reflects the current  $J_s - J_s^*$ .

The effect of the thermionic emission onto the sheath structure has been also studied thanks to Particle In Cell (PIC) simulations, where  $J_s$  was varied by setting the surface temperature  $T_s$  according to the Richardson-Dushman's equation. Authors studied the variation of the sheath size<sup>27</sup>, the potential drop in the sheath and the saturation of the thermionic current penetrating the plasma with respect to  $T_s$ , the formation of the virtual cathode<sup>28</sup>, as well as the effect of electron redeposition in the presence of a tilted magnetic field<sup>29</sup>.

In this study, we propose to extend these previous numerical works by determining self-consistently the surface temperature of a cathode facing a hot hydrogen plasma by using PIC simulations corresponding to unmagnetized plasma cases. This can be achieved by balancing the heat fluxes at the wall coming from the plasma ie. the heat flux deposited by ions and electrons (kinetic and potential recombination or adsorption energy) and conducted away from the surface ie. the heat flux carried out by conduction, radiation and thermionic emission. Our goal is to be able to estimate the surface temperature of a tungsten wall, because this material is foreseen as a good candidate material for divertor target plates in future fusion reactors thanks to its low tritium retention and low sputtering yield<sup>30</sup>, with respect to different plasma conditions and surface properties. We focus in this study on thermionic emission only, where the amplitude of the emitted current relies on the surface temperature. Other effects can strengthen  $J_s$  though, such that the Schottky correction to the material work-function<sup>31</sup>, or secondary electron emission (see eg.<sup>7</sup> and references therein). If included in our numerical model, these effects would lead to an increase of the emitted current with respect to the one calculated with the Richardson formula and have an impact on the temperature at which the sheath limited regime appears. We also exclude the detached divertor regime from this study since it requires to introduce a large set

of additional mechanisms such as ionization processes, charge-exchange collisions, neutral particle recycling as mentioned in<sup>32,33</sup>, which is out of the scope of this paper.

In the first part of the paper, we present the simulated system and we detail the way the calculations are performed, especially how the surface temperature can be determined in the steady state. Then we focus on the numerical results, discussing the sheath formation during the first time iterations as well as the density and potential spatial variations in the presence of thermionic emission. We also analyze the variation of the surface temperature, the sheath potential and the emitted current with respect to an increasing surface thermal conductivity in two plasma conditions. We finally present a simple fluid model in order to explain qualitatively and quantitatively the numerical results and relate them to the bifurcation S curves obtained and already evidenced by other authors in fluid calculations.

## II. PIC SIMULATIONS

### A. Simulated system

In our 1d/3v PIC simulations, a semi-infinite plasma is bounded by a grounded conductive wall at  $x = 0$ , ie. with a surface potential  $\phi(0) = 0$ . The right boundary condition at  $x = L = 100\lambda_d$  is such that the electric field cancels,  $\phi'(L) = 0$ . Particles are moving along the  $x$  axis until they reach one of the simulated system boundary. At  $x = L$ , they are simply reflected and return back into the plasma with a velocity which is reset in the initial Maxwellian velocity distribution. As there is not net current at  $x = L$ , there should be a balance of the charges at the surface in order to preserve the plasma quasi-neutrality (floating wall conditions).

At  $x = 0$ , hydrogen ions recombine with electrons extracted from the wall material and are recycled as neutrals in the plasma. Though the wall material is at a lower potential than the plasma, an important electron flux can reach the wall, so that electrons arriving at  $x = 0$  are absorbed by the surface. There is no reflection of the plasma particles or energy at the wall in our simulations. The ion neutralization at  $x = 0$  or the electron absorption are sources of the cathode spot heating, which will be detailed in the next subsection. At each iteration, a number of thermo-emitted electrons is calculated thanks to the Richardson-Dushman formula (Eq. (1)).

Electrons are deposited at the surface at  $x = 0$  and are eventually accelerated toward the plasma due to a strong negative electric field in the sheath region. Their initial kinetic energy is set to be  $k_b T_s$  and their initial velocity vector is distributed over one hemisphere in order to provide an isotropic angular distribution as proposed in reference<sup>34</sup> for secondary electrons injection. The grid size is chosen as small as  $dX = 0.0125\lambda_d$  in order to describe accurately the wall vicinity and to track the motion of the emitted electrons with great precision. The time step is then picked up according to the grid size, due to the Courant condition, ie.  $v_{te} \times dt = 0.25 \times dX$ , where  $v_{te}$  is the electron thermal velocity. This procedure ensures that most electrons can not travel across an entire cell  $dX$  during a single  $dt$ .

We tagged during the simulations the emitted electrons vs the plasma ones in order to sort them. When a thermionic electron has traveled throughout the entire plasma and reached the right boundary, it is reflected back into the plasma (as the other particles) and its velocity reset in the initial Maxwell's distribution: then the electron is categorized as a plasma one. Tagging the emitted electrons is also very helpful for determining precisely the maximum emitted current  $J_s^*$  at the surface. For that purpose, it is indeed necessary to ascribe if one electron hitting the wall is from the plasma or a previous emitted one reflected by the virtual cathode.

Collisions between charged particles or with neutrals are not taken into account, nor ionization or recombination within the plasma. As in our previous studies based on PIC simulations<sup>35</sup>, the number of ions was kept constant during the calculations: once a single ion reaches the left boundary (the wall material), a couple ion + electron is injected randomly within the simulated plasma according to a uniform law in order to preserve quasi-neutrality. This injection method is known to distort the velocity distribution functions<sup>36-38</sup> and to induce a cooling of the plasma with respect to the nominal loaded one. As the different potential drops in the plasma, ie. in the sheath or the pre-sheath, depend on the electron temperature, as well as the amplitude of the ion acoustic velocity  $c_s$ , we determined the final temperatures of the plasma when the simulations are completed. For that purpose, the  $(x, v_x)$  phase space of the plasma species was saved at the end of the simulations. Then the plasma was arbitrary divided in 10 slabs, whose length was  $10 \lambda_d$ , and the temperature calculated on the first one, in a region encompassing the sheath by determining the average kinetic energy of the plasma slab.

The simulations are run for  $300 \times 2\pi/\omega_{pe}$  periods, with  $\omega_{pe}$  the electron plasma pulsation,

which is long enough for the sheath to be established ( $\omega_{pe}^{-1}$  is its characteristic time). For such a simulation window, hydrogen ions can travel across half of the plasma size at their thermal velocity, so that all the ion velocity distribution has passed through the sheath extending over a few  $\lambda_d$ , and contributed to the surface heating, during this time frame. We check at the end of the simulations that the steady state is reached for the heat flux to the surface or the space potential at its vicinity. The different quantities, such as the space potential or the particles density are averaged over the last  $50 \times 2\pi/\omega_{pe}$ . The emitted and plasma electrons as well as ion fluxes at the wall are recorded every hundred iterations and also averaged over the last 50 periods for further use and interpretation. Note that the time step according to our plasma properties and the grid size  $dX$  used can be as small as  $2.5 \times 10^{-14}$  s, for a total simulated time of 0.015  $\mu$ s.

## B. Heat flux balance at the surface

For each time iteration, the heat flux deposited by ions and electrons on the cathode surface is calculated during the PIC simulations; it consists of the kinetic energy of the particles added to the energy terms due to ion neutralization and electron absorption. The heat flux from the plasma to the wall writes:

$$Q_p = \Gamma_i (E_i - B_w) + \Gamma_e B_w + Q_i^k + Q_e^k, \quad (3)$$

where  $Q_i^k$  and  $Q_e^k$  are the ion and electron kinetic energy fluxes,  $\Gamma_i$  and  $\Gamma_e$  are the ion and electron fluxes at the surface and  $E_i = 13.6$  eV is the recombination energy for hydrogen. The hydrogen plasma density being chosen within the range  $1 - 10 \times 10^{18} \text{ m}^{-3}$  in the PIC simulations with  $k_b T_i = k_b T_e = 10$  eV, conditions met in the divertor plasmas of medium size tokamaks in attached mode such as JET or WEST<sup>39,40</sup>, and assuming  $\Gamma_e = \Gamma_i \simeq n_0 c_s$ , one can expect a particle flux of the order of  $10^{22}$  to  $10^{23} \text{ s}^{-1} \text{ m}^{-2}$  and a heat flux density which can reach  $1 \text{ MWm}^{-2}$  for the first two terms of Eq. (3).

The heat conducted away from the cathode surface is due to emission of electrons, surface radiation and heat conduction; all these terms depend on the surface temperature  $T_s$  which is to be determined. It can be calculated as:

$$Q_c = \frac{J_s(T_s)}{e} (B_w + k_b T_s) + \epsilon \sigma T_s^4 + \frac{\kappa}{t} (T_s - T_0), \quad (4)$$



where  $\epsilon$  is the emissivity of the surface,  $\sigma$  the Stefan-Boltzmann constant,  $\kappa$  the thermal conductivity and  $t$  the wall thickness (1 cm in the present study).

An average  $\epsilon = 0.25$  is chosen for all simulation runs<sup>41</sup>, while different values of  $\kappa$  are tested from 0 up to  $140 \text{ Wm}^{-1}\text{K}^{-1}$ . A typical value for the tungsten thermal conductivity<sup>42</sup> at room temperature ( $T_0 = 300 \text{ K}$ ) would be  $180 \text{ Wm}^{-1}\text{K}^{-1}$  and would decrease down to  $90 \text{ Wm}^{-2}\text{K}^{-1}$  within a temperature range of  $3000 - 4000 \text{ K}$ . However a conductivity as low as  $10 \text{ Wm}^{-1}\text{K}^{-1}$  is expected for an altered tungsten surface previously submitted to plasma irradiation<sup>43</sup>. It is known indeed that the presence of bubbles (empty or filled with He/D) in the tungsten lattice decreases its thermal conductivity<sup>44</sup>. Finally, micro-crackings in polycrystalline materials can also reduce the thermal conductivity by a factor 3 with respect to the expected value<sup>45</sup>. It is then worth testing in our plasma simulations a large range of the thermal conductivity to take into account the surface irradiation history corresponding to real divertors W mono-blocs or general targets having different surface conditions.

We neglect in the present study the heat flux due to the material wall evaporation. According to Langmuir<sup>46</sup>, the rate of evaporation of tungsten at  $3500 \text{ K}$  is of about  $J_{ev} = 2.52 \times 10^{22} \text{ m}^{-2}.\text{s}^{-1}$ , which induces a heat flux of the order of  $Q_{ev} = J_{ev} \times W_{ev}$ , with  $W_{ev} = 8 \text{ eV}$  the evaporation energy for W. It leads to  $Q_{ev} = 0.032 \text{ MW/m}^{-2}$ , which is two orders of magnitude smaller than the surface radiation contribution for the same temperature. Even at  $4000 \text{ K}$ , assuming the rate of evaporation of reference<sup>47</sup>, the heat flux due to the wall evaporation is still quite below the radiation one;  $Q_{ev}$  finally reaches the  $\text{MW/m}^{-2}$  mark for  $T_s = 4600 \text{ K}$  and liquid tungsten.

Assuming  $Q_p = Q_c$  enables straightforwardly the determination of  $T_s$  for the considered time iteration,  $Q_p$  being given by the PIC code and  $Q_c$  provided by an analytical expression (Eq. (4)) which only depends on the material properties and on  $T_s$ . Then the number of thermionic electrons to be released at the wall can be calculated for the deduced  $T_s$  thanks to Richardson-Dushman formula (Eq. (1)). Doing so, we suppose that the surface will converge to a final temperature in the steady state, where there is a balance between a stable heat flux coming from the plasma to the surface and conducted away from it, once the sheath and eventually the virtual cathode are established. The determination of the final temperature of the surface with respect to both the cathode and plasma properties is then achieved after the PIC simulations. The average heat flux  $\overline{Q_p}$  from the plasma species to the wall has been calculated from the recorded data points on the last  $50 \times 2\pi/\omega_{pe}$  periods. Then Eq. (4) is

used with  $\overline{Q_p}$  to determine the final  $T_s$ . We have implemented this method in order to avoid averaging the temperature deduced at each time iteration.

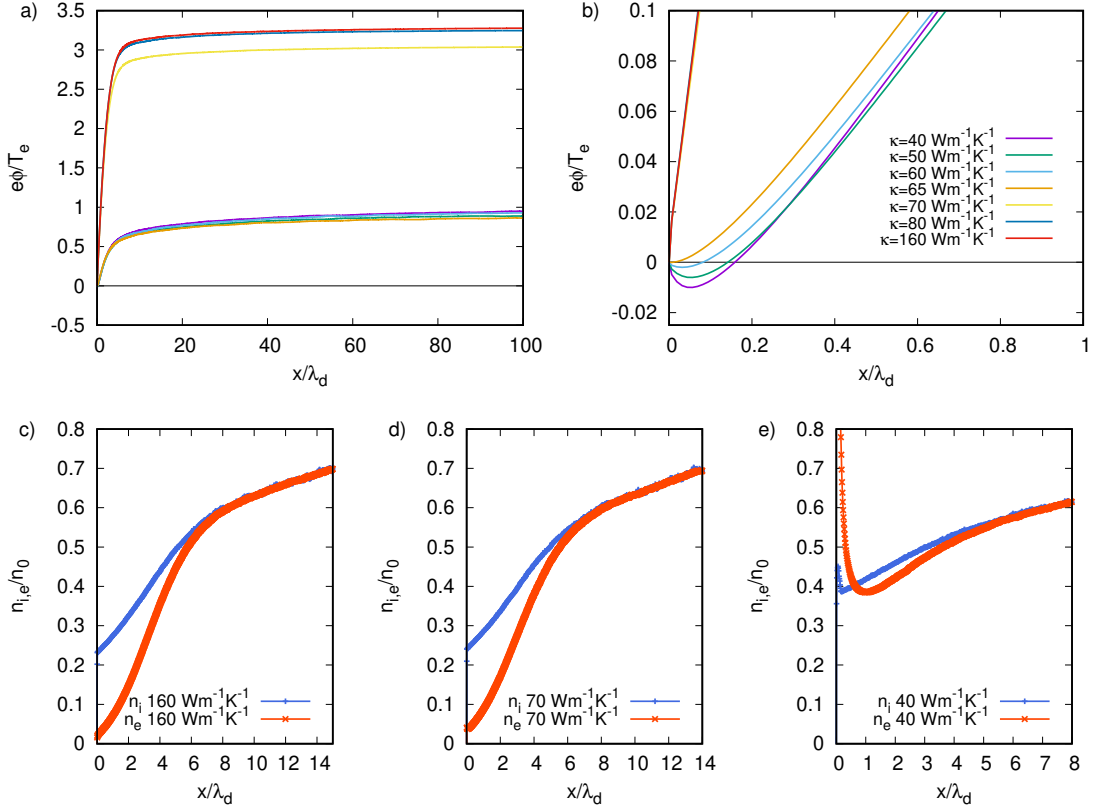


FIG. 1. a), b) Spatial variation of the plasma potential  $\phi$  for 7 values of the thermal conductivity  $\kappa$ . The simulation parameters are  $n_0 = 5 \times 10^{18} \text{ m}^{-3}$  and  $k_b T_i = k_b T_e = 35 \text{ eV}$ . The zoom in b) allows the visualization of the virtual cathode facing the wall for the lowest  $\kappa$  values. c), d) and e) Profiles of the ionic ( $n_i$ ) and electronic ( $n_e$ ) density in the surface vicinity for  $\kappa = 160, 70$  and  $40 \text{ Wm}^{-1}\text{K}^{-1}$  respectively.

### III. RESULTS

#### A. Plasma potential, density and sheath building

The simulated plasma potential profile for 7 values of  $\kappa$  in the case of a  $5 \times 10^{18} \text{ m}^{-3}$  hydrogen plasma with  $k_b T_i = k_b T_e = 35 \text{ eV}$ , values close to those found in the scrape-off layer of tokamaks, is shown in Fig. 1a. When  $\kappa$  decreases, less heat flows through the wall

thickness according to Eq. (4), so that the surface temperature is expected to increase as well as the thermionic current (both properties will be presented in Fig. 6). As a result, the electron density in the immediate surface vicinity exhibits a slight augmentation, Fig. 1d, as compared to the highest thermal conductivity, Fig. 1c. This phenomenon induces a small decrease of the space charge in the sheath as well as of the potential drop into it until  $\kappa = 65 \text{ Wm}^{-1}\text{K}^{-1}$ . At this threshold value of heat conductivity, the electron density facing the surface can not be increased further and the electric field at the target  $E_s$  vanishes for emitted current regulation purpose. It results in a drop of the plasma potential because the system abruptly bifurcates towards another energy minimum. If  $\kappa$  is decreased further,  $E_s$  becomes positive and a virtual cathode builds up close to the wall (Fig. 1b). In this case, the negative charge created by the thermionic emission counterbalances the positive one and a double layer occurs, Fig. 1e, which characterizes the space charge limited regime.

The building of the sheath and eventually of the double layer arises over the first plasma periods of the simulations. During the first ten or so time iterations, a large flux of electrons reaches the wall because of the absence of a sheath, which leads to a huge heat flux to the cathode, Fig. 2a. This loss of plasma electrons leads to a positive charge surplus in the near-surface environment. But because of the heat flux previously received by the wall, its temperature is raising (see Fig. 2c) resulting in strong thermionic emission: the positive charge surplus is then quickly neutralized by the emitted electrons, destroying the thin sheath. This process of high heat loads followed by strong emission, both large oscillating virtual cathode potential ( $\phi_{vc}$ ) and instantaneous surface temperature is repeated several times until  $\phi_{vc}$  and  $T_s$  stabilize and the sheath is completely deployed, Fig. 2b and c. As a consequence, the heat flux due to electrons decreases until the steady state is reached while the ion heat flux increases during the early stages of the simulations because of the building of the sheath potential. Finally, the total heat flux converges to a stable value which is higher (eg. for  $\kappa = 50 \text{ Wm}^{-1}\text{K}^{-1}$  in Fig. 2a) or lower (eg. for  $\kappa = 75 \text{ Wm}^{-1}\text{K}^{-1}$  in Fig. 2a) for higher and lower temperature (respectively  $\simeq 3000$  and  $\simeq 1100 \text{ K}$  in Fig. 2c). It is important to notice that even if the surface reaches a relatively cold temperature (without both strong emission and a virtual cathode close to it) in the steady state, during the transient one, it may have experienced high heat loads, as explained above. This history of the surface temperature surface may have a strong impact on the final results of the calculations, as will be emphasized later on in the paper.

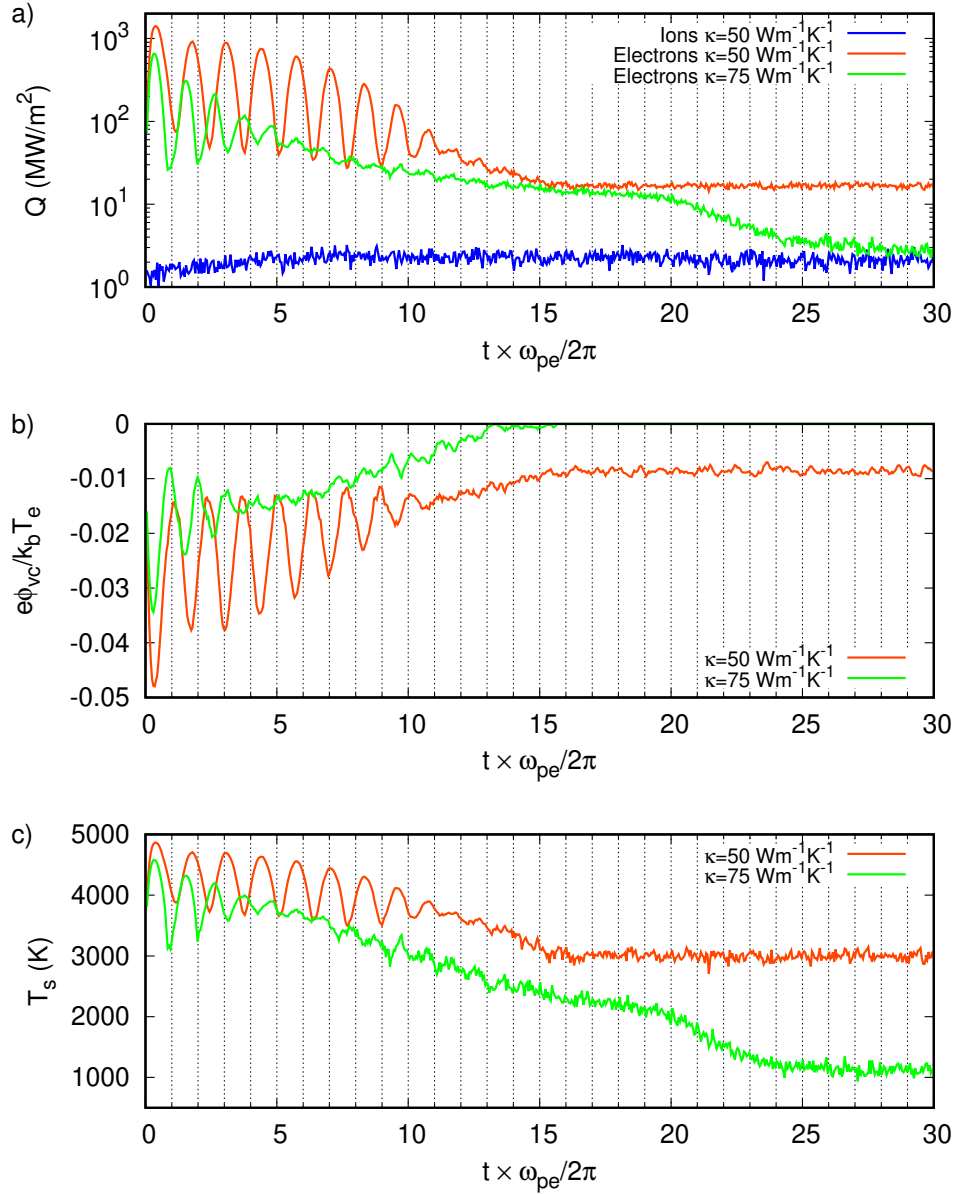


FIG. 2. a) Time variation of the heat flux from the plasma ion and electron to the wall for different thermal conductivity. b) Time variation of the virtual cathode potential  $\phi_{vc}$  for  $\kappa = 50$  and  $75 \text{ Wm}^{-1}\text{K}^{-1}$ . c) Corresponding time variation of the surface temperature.

In order to determine the sheath entrance location, several approaches are possible. Some authors base this determination onto the space-charge amplitude relative to the plasma density at the wall vicinity with a simple criterion such that  $n_i(s) - n_e(s) = 0.02 - 0.04 \times n_0$ , where  $s$  is the sheath size measured from the wall and  $n_i$  and  $n_e$  the ion and electron density<sup>48,49</sup>. As we have extracted the sheath entrance location when the simulations are

completed, we used, as in our previous studies, the Bohm criterion<sup>50</sup>, ie. the point where the ion fluid velocity perpendicular to the wall,  $v_{ix}$ , reaches the ion acoustic velocity,  $c_s$ , where quasi-neutrality breaks down. We also used this sonic point abscissa for estimating the potential drop in the sheath in our simulations.

The spatial variation of  $v_{ix}$  (the ion velocity averaged in each cell during the PIC simulations) for 5 values of the thermal conductivity is depicted in Fig. 3a. In the low temperature regime (the corresponding temperatures will be entirely displayed in Fig. 6 and discussed later), above the thermal conductivity threshold of  $65 \text{ Wm}^{-1}\text{K}^{-1}$ , ions are accelerated up to  $c_s$  thanks to the pre-sheath potential drop and enter the sheath at  $x/\lambda_d = 3.8$ , which is the sheath size in this regime. They then experience a large negative electric field in the sheath and reach the wall at a velocity close to  $-2 \times c_s$ . For smaller values of the thermal conductivity, the thermionic emission induced by the larger surface temperature neutralizes the positive space-charge close to the wall and the formation of a double layer occurs as depicted in Fig. 1e. The surface temperature in this case should be large enough for the emitted current to reach the order of the Bohm flux ( $0.1-1 n_0 c_s$ ) and to destabilize the Debye sheath. With the tungsten surface and plasma properties used in the simulations, it corresponds to  $T_s$  in the range  $2600 - 2900 \text{ K}$  thanks to Eq. (1). As a result, in the limited regime, ions experience a weaker negative electric field in the sheath region than above the thermal conductivity threshold. Therefore they impact the wall with a smaller velocity and the sheath size abruptly shrinks to  $x/\lambda_d = 1.6$ , sheath shrinking which has already been evidenced in reference<sup>27</sup>.

For  $\kappa = 40 \text{ Wm}^{-1}\text{K}^{-1}$ , the potential dip built close to the surface due to the double charged layer is large enough to trap ions as seen in the ion phase space (Fig. 4a), which induces a reduction of the averaged ion velocity at the wall direct vicinity. In return, their accumulation in this region leads to a small increase in the calculated ion density (see Fig. 1e). This slight ion accumulation has however no visible effect onto the potential well close to the surface because the large electron density increase due to thermionic emission is disproportionate. It was already mentioned that this trapping phenomenon could occur for instance in the presence of charge-exchange collisions between accelerated ions in the sheath and cold neutrals, or because of increased ionization processes<sup>51</sup>. It could flatten or eventually destroy the potential well, leading to an “inverse sheath”, because of the large ion accumulation possible in this case<sup>26,52</sup>. This inverse sheath regime due to electron emission

has been also investigated in the context of divertor plasmas<sup>53</sup> or radio-frequency sheaths<sup>49</sup>. In our case, there is no collision taken into account but there is a possibility due to the injection process (ions are deposited everywhere in the plasma according to an uniform distribution in the  $x$  direction) that ions with a small velocity compared to  $c_s$  appear in the potential dip neighborhood. As this region is quite narrow with respect to the plasma size (0.2 vs  $100 \lambda_d$ ), only a few of them are injected in this area during the simulations. If charge-exchange collisions or realistic ionization procedures taking into account the increased local electron density were used in the PIC simulations, the results may have been different and eventually exhibit an inverse sheath regime as evidenced by other authors.

Concerning the thermionic electrons, they are deposited at the wall with a small velocity with respect to plasma electrons and are eventually accelerated in the sheath, which can be seen in the electron velocity distributions of Fig. 3b recorded at different locations in the simulated plasma. For strong thermionic emission,  $\kappa = 40 \text{ Wm}^{-1}\text{K}^{-1}$ , a peak clearly visible around  $v_{ex}/v_{te} = 0.93$  at  $x/L = 0.2$  is due to this electron population. The velocity distribution is also truncated for large positive velocities compared to the one recorded for  $\kappa = 160 \text{ Wm}^{-1}\text{K}^{-1}$ , where the thermionic emission is negligible, and which is shown in the same figure for  $x/L = 0.2$  and  $x/L = 0.4$  (continuous lines). This missing part of the distribution in the strong emission regime is ascribed to the reduction of the potential drop between the plasma center and the wall exhibited in Fig. 1a by almost a factor 5 compared to the non emitting regime. More plasma electrons with smaller velocity can indeed reach the cathode in this case and disappear from the measured velocity distribution as they are absorbed by the surface. Finally, the effect of the potential well in the surface vicinity is also seen in the electron phase space, Fig. 4b: a significant part of the emitted electrons goes back to the cathode while another one corresponding to the space charge limited current is accelerated through the sheath.

## B. Heat flux and surface temperature

This increase of the plasma electron flux due to the reduction of the potential drop in the sheath comes along with an augmentation of their heat flux to the surface, Fig. 5a, when  $\kappa$  goes down from 160 to  $65 \text{ Wm}^{-1}\text{K}^{-1}$ . For smaller thermal conductivity, ie.  $\kappa \leq 65 \text{ Wm}^{-1}\text{K}^{-1}$  the system being in the space-charge limited regime, the sheath potential  $\phi_s$  does not vary

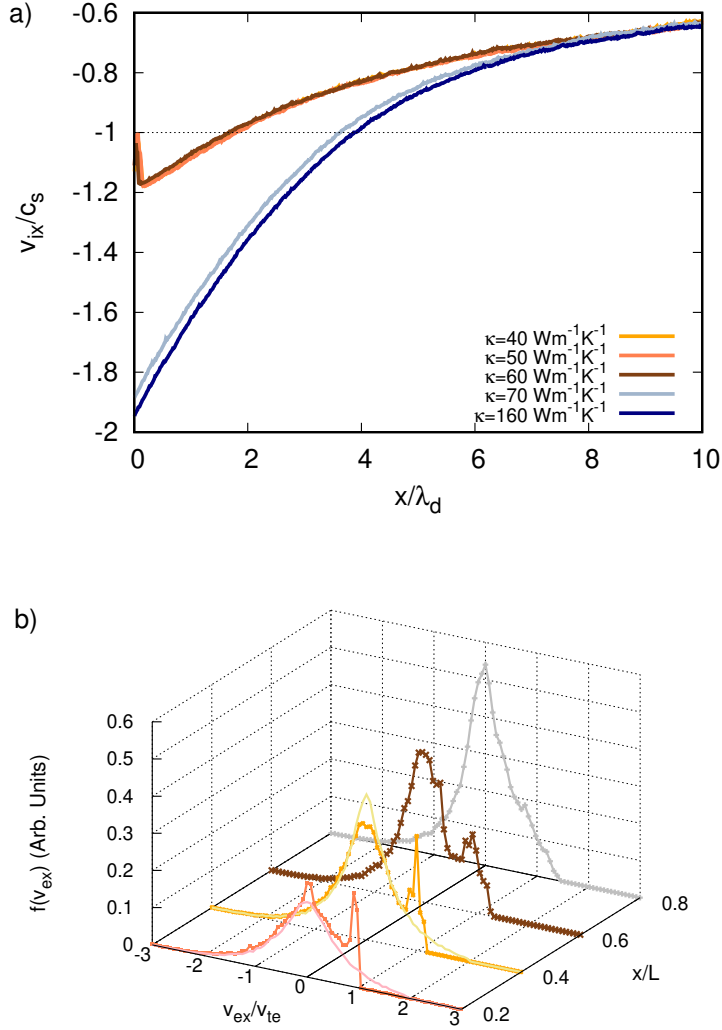


FIG. 3. a) Spatial variation of the averaged ion velocity  $v_{ix}$ . The sheath entrance location is determined at the sonic point  $v_{ix} = c_s$ . b) Electron velocity distribution recorded at different plasma locations for  $\kappa = 40 \text{ Wm}^{-1}\text{K}^{-1}$  (line+symbol). At  $x/L = 0.2$  and  $x/L = 0.4$ , the electron velocity distribution is also shown for  $\kappa = 160 \text{ Wm}^{-1}\text{K}^{-1}$  (continuous line).

any more and neither does the heat flux carried by plasma electrons at the cathode. However, as the surface temperature is expected to keep increasing for smaller  $\kappa$  below this threshold, the number of electrons emitted by the cathode according to the Richardson law  $J_s$  is also increasing. As the surplus of electrons above the space-charge limited current goes back to the surface, i.e.  $J_s - J_s^*$ , the total electron (plasma + emitted) heat flux still increases as depicted in the figure. The reduction of  $\phi_s$  with  $\kappa$  also implies that the energy gained in

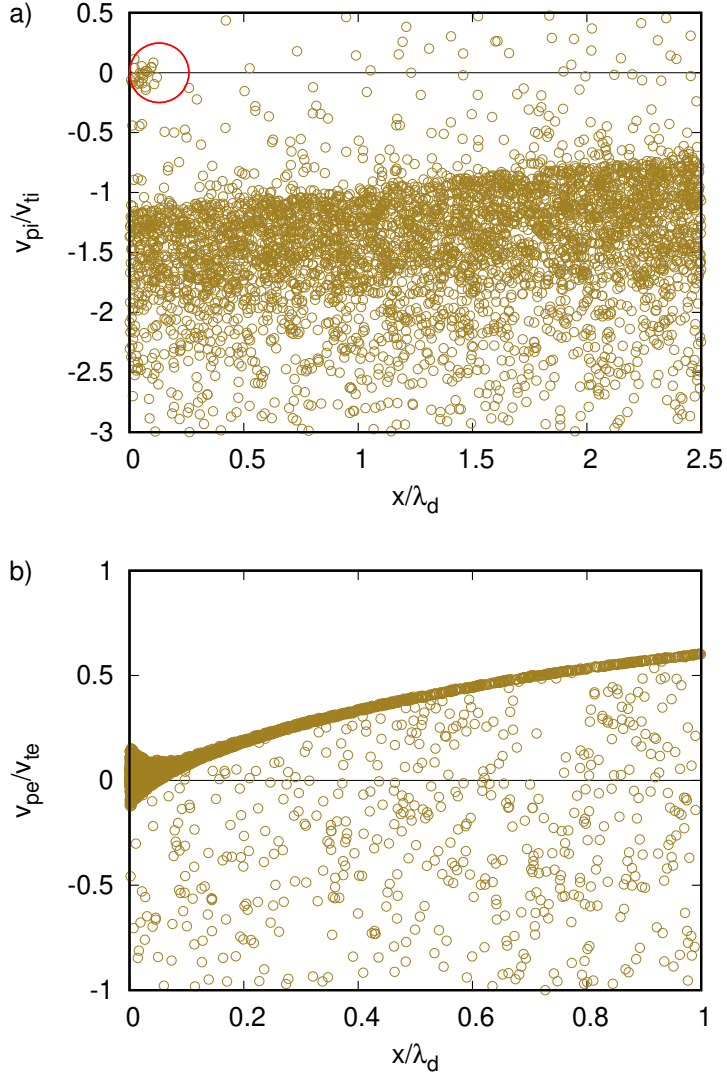


FIG. 4. a) Ions phase space for a  $5 \times 10^{18} \text{ m}^{-3}$  hydrogen plasma with  $k_b T_i = k_b T_e = 35 \text{ eV}$  and  $\kappa = 40 \text{ Wm}^{-1}\text{K}^{-1}$ . The particles circled in red are those trapped in the potential well evidenced in Fig. 1b. b) Electrons phase space for the same plasma conditions than in a).

the field by ions in the sheath region decreases as well as their heat flux to the wall, Fig. 5a. In this limited regime also, a large thermionic current  $J_s^*$  penetrates the plasma until the right boundary is reached. These emitted electrons are cold with respect to the plasma temperature in our simulations because they are injected at the surface one (less than 1 eV whereas the plasma is at tens of eV). If these electrons remained in the system, the overall temperature would decrease. However thanks to the reflection procedure at the right boundary explained before and the fact their velocities components are reset in the initial



Maxwell's distribution, the system can be refurnished in energy and the plasma temperature kept constant for the all set of simulations that we have run.

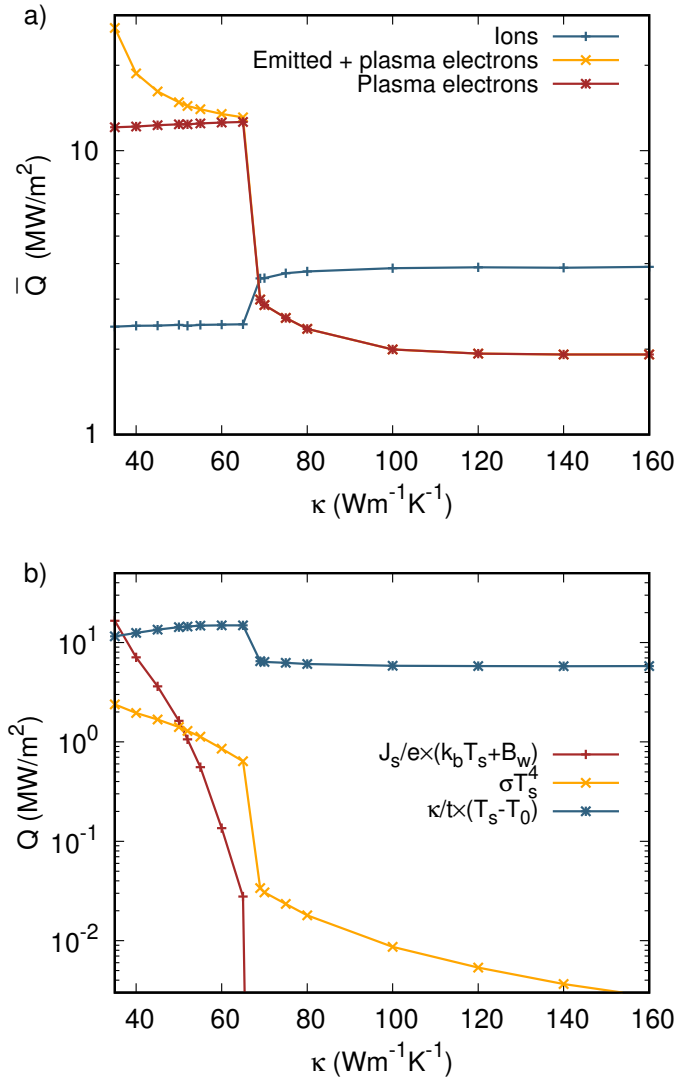


FIG. 5. a) Average heat flux to the surface due to ions, plasma electrons and emitted + plasma electrons in the case of a virtual cathode. b) Heat flux conducted away from the surface due to electrons emission, radiation and conduction.

As explained in the previous section, the determination of the surface temperature  $T_s$  is achieved by assuming that  $\bar{Q}_p$  (the average electron and ion total heat flux to the surface) balances the heat flux conducted away from the surface given by Eq. (4). The different terms of Eq. (4), ie. emission of electrons, surface radiation and heat conduction, are shown in Fig. 5b for the same plasma parameters and thermal conductivity than in Fig. 5a.

Most of the heat is evacuated through the wall thickness by conduction. In the space-charge limited regime ( $\kappa \leq 65 \text{ Wm}^{-1}\text{K}^{-1}$ ), a large part of emitted electrons return back to the cathode, which accentuates the heat flux from the plasma to the surface (as stated above) as well as the heat conducted away from it. In fact, each emitted electron carries an energy  $k_b T_s$  which will be redeposited entirely onto the surface thanks to the virtual cathode (if reflected) balancing both its heat fluxes to and from the cathode. Therefore in the space charge limited regime, the total heat flux conducted away from the surface due to thermionic emission actually keeps an almost constant value  $\equiv \frac{J_s^*}{e}(k_b T_s + B_w)$  (see Eq. (4)).

The variation of the sheath potential  $\phi_s$ , the surface temperature  $T_s$  and the thermionic current at the surface  $J_s$  with respect to  $\kappa$  is depicted in Fig. 6 for the same plasma parameters than previously (a  $5 \times 10^{18} \text{ m}^{-3}$  hydrogen plasma with  $k_b T_i = k_b T_e = 35 \text{ eV}$ ) as well as for a hotter one with the same density and  $k_b T_i = k_b T_e = 50 \text{ eV}$ . A similar trend is observed for both plasma: the sheath potential slowly decreases with  $\kappa$  and then abruptly drops down to its minimal value  $\simeq 0.4e\phi_s/T_e$ , corresponding to the space charge limited regime where the thermionic current saturates around  $3en_0c_s$ . The larger the plasma temperature, the larger is the thermal conductivity for which this saturation regime occurs. The surface temperature continuously increases when the thermal conductivity decreases and can reach 3500-3600 K for the lowest  $\kappa$  considered, ie. 35 and 60  $\text{Wm}^{-1}\text{K}^{-1}$  for the 35 eV and 50 eV plasma respectively. We did not investigate regimes of  $\kappa$  where the tungsten surface is expected to melt (around 3700 K).

The same general behavior has been evidenced in other simulations in which the electron plasma temperature was increased for a prescribed  $\kappa$  (15 and 100  $\text{Wm}^{-1}\text{K}^{-1}$ ) and for a plasma density and ion temperature of  $n_0 = 5 \times 10^{18} \text{ m}^{-3}$  and  $k_b T_i = 5 \text{ eV}$  respectively. The electron temperature  $T_e$  at which the abrupt transition between the non emitting regime to the space charge limited regime occurs increases with thermal conductivity, Fig. 7, with a steep augmentation of the thermionic current at the surface still saturating  $\simeq 3 - 3.2en_0c_s$ .

### C. Fluid model, bifurcation and evidence of hysteresis

In order to calculate the heat flux from the plasma to the wall, one needs the potential drop in the sheath  $\phi_s$  with respect to the thermionic current  $J_s$ . We based our analyses on the study by Hobbs and Wesson<sup>8</sup>, who derived the expression of  $\phi_s$  in the presence of

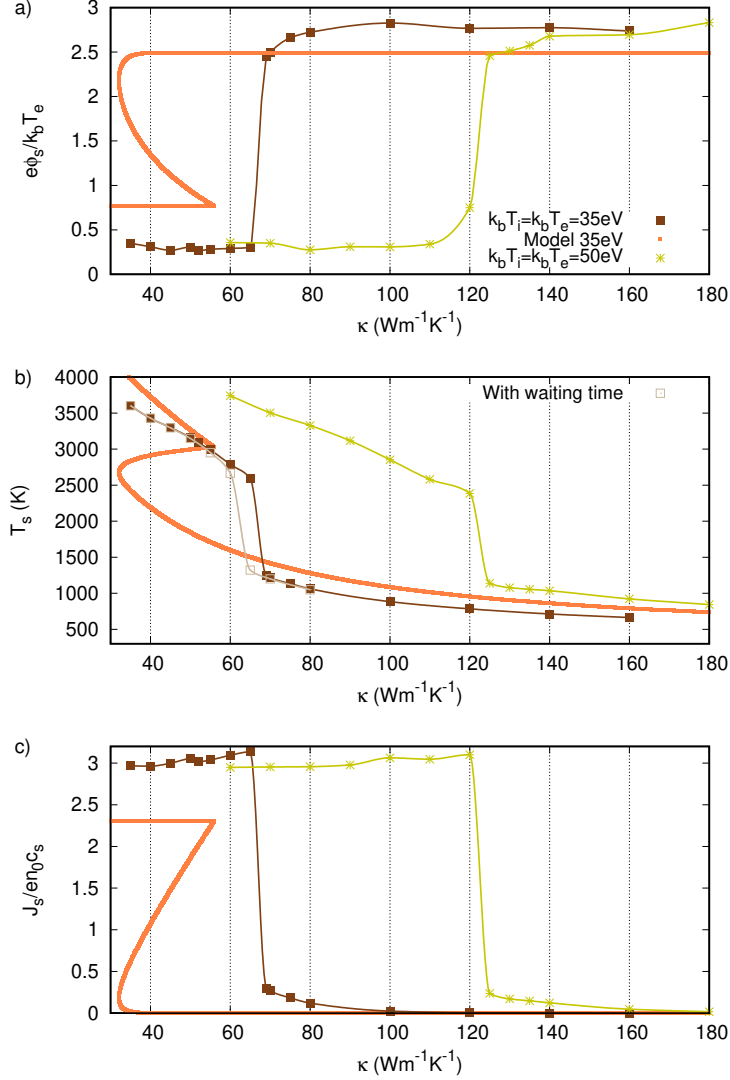


FIG. 6. a) Variation of the sheath potential  $\phi_s$ , b) the surface temperature  $T_s$ , c) the thermionic current at the surface  $J_s$  with respect to  $\kappa$  extracted from the PIC simulations and the fluid model of section III C for two plasma conditions. The opened symbols in b) corresponds to the case where a waiting time is used in the beginning of the simulations for  $k_b T_i = k_b T_e = 35$  eV.

electrons emitted at rest on the surface. The authors showed that, even in the presence of thermionic emission, ions keep entering the sheath at a velocity  $v_{ix} = v_s$  close to the acoustic velocity  $c_s$ , ie. the Bohm criterion is still valid<sup>50</sup>. Assuming floating wall conditions, the total current is zero at the wall, which writes according to reference<sup>8</sup>:

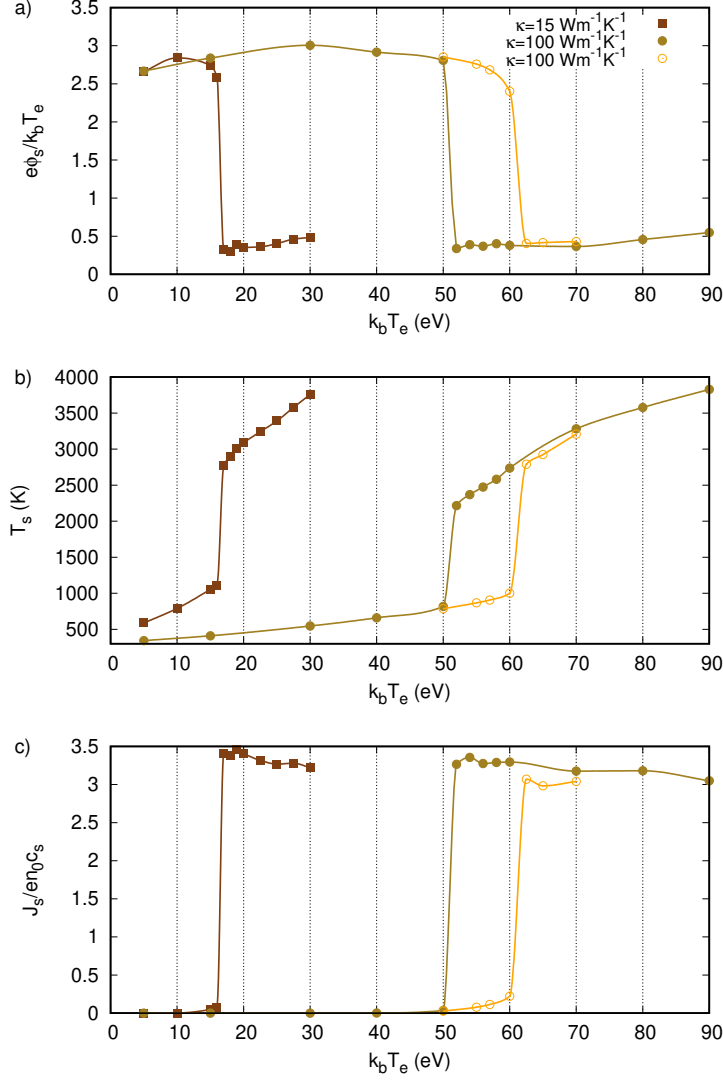


FIG. 7. a) Variation of the sheath potential  $\phi_s$ , b) the surface temperature  $T_s$ , c) the thermionic current at the surface  $J_s$  with respect to the electron temperature  $k_b T_e$  extracted from the PIC simulations for two values of the thermal conductivity. The hydrogen plasma parameters are  $n_0 = 5 \times 10^{18} \text{ m}^{-3}$  and  $k_b T_i = 5 \text{ eV}$ . The open symbols for the case  $\kappa = 100 \text{ Wm}^{-1}\text{K}^{-1}$  correspond to the case where a waiting time is used in the beginning of the simulations.

$$n_s v_s + \frac{J_s}{e} = \frac{n_s c_e}{4} \left( 1 - \frac{J_s}{en_s v_{te} \sqrt{\frac{2e\phi_s}{k_b T_e}}} \right) \exp\left(-\frac{e\phi_s}{k_b T_e}\right), \quad (5)$$

with  $c_e = \sqrt{\frac{8k_b T_e}{\pi m}}$  and  $n_s$  the plasma density at the sheath entrance.

If the thermionic current is small with respect to  $en_s v_{te}$ , substituting  $v_s = c_s$  into Eq. (5)

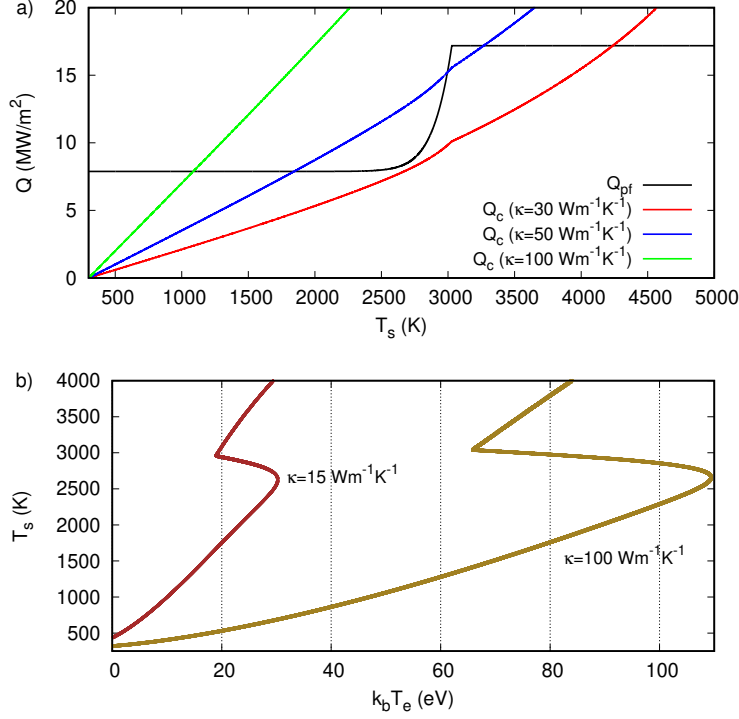


FIG. 8. a) Calculated heat flux from the plasma to the wall ( $Q_{pf}$ ) and conducted away from it ( $Q_c$ ) for 3 different values of the thermal conductivity. b) Surface temperature deduced from the fluid model with respect to the plasma electrons temperature.

leads straightforward to the determination of the sheath potential:

$$e\phi_s = e\phi_f - k_b T_e \log \left( 1 + \frac{J_s}{en_s c_s} \right), \quad (6)$$

with  $\phi_f$  the well-known floating wall potential<sup>54</sup> given by  $-\frac{k_b T_e}{2e} \log \left( 2\pi \frac{m}{M} \left( 1 + \frac{T_i}{T_e} \right) \right)$ . According to Eq. (6), an increase in the thermionic emission leads to a reduction of the sheath potential as evidenced in Fig. 6a or in Fig. 7a. However, this reduction can not go until the disappearance of the sheath, ie.  $\phi_s = 0$ , because the electric field at the surface  $E_s$  would cancel before for a critical thermionic current  $J_s^*$  marking off the space charge limited regime. As calculated by Hobbs and Wesson,  $E_s$  reads:

$$\begin{aligned} \frac{\epsilon_0}{2n_0k_bT_e}E_s^2 = \frac{Mc_s^2}{k_bT_e} \left[ \left( 1 + \frac{2e\phi_s}{Mc_s^2} \right)^{\frac{1}{2}} - 1 \right] \\ + \left( \exp \left( -\frac{e\phi_s}{k_bT_e} \right) - 1 \right) \left( 1 - \frac{J_s}{en_s v_{te} \sqrt{\frac{2e\phi_s}{k_bT_e}}} \right) - \frac{J_s}{en_s v_{te}} \sqrt{\frac{2e\phi_s}{k_bT_e}}. \end{aligned} \quad (7)$$

Thus, for an increasing thermionic current  $J_s$  due to an increase of  $T_s$ , the potential drop in the sheath  $\phi_s$  can be calculated according to Eq. (6) and then introduced in Eq. (7) until  $E_s^2$  becomes negative and the system enters the space charge limited regime with a minimum  $\phi_s^*$  and a maximum  $J_s^*$ .

Once the potential drop in the sheath is known, the heat flux from the plasma to the wall can be calculated as<sup>55</sup>:

$$Q_{pf} = \frac{1}{2}n_0c_s(2k_bT_i + e\phi_s + E_i - B_w) + \frac{n_0c_e}{8} \exp \left( -\frac{e\phi_s}{k_bT_e} \right) (2k_bT_e + B_w), \quad (8)$$

where we assumed that  $n_s = \frac{1}{2}n_0$ . In the space charge limited regime,  $Q_{pf}^*(\phi_s^*)$  reaches a maximum, and the heat flux conducted away from the wall, Eq. (4), becomes  $Q_c = Q_c(J_s^*)$ . In such a regime, the heat flux from the surface due to thermionic emission is maximum, even if  $T_s$  increases further, as explained in the previous section.

The variation of  $Q_{pf}$  with respect to  $T_s$  is depicted in Fig. 8a for a  $n_0 = 5 \times 10^{18} \text{ m}^{-3}$  hydrogen plasma and  $k_bT_i = k_bT_e = 35 \text{ eV}$  calculated thanks to Eqs. 6 to 8. A large increase of  $Q_{pf}$  between 2600 and 3000 K occurs and the plasma heat flux to the surface saturates for  $T_s > 3000 \text{ K}$  at  $17.18 \text{ MWm}^{-2}$ . This sudden augmentation of  $Q_{pf}$  around 2600 K is ascribed to the decrease of  $\phi_s$  (due to the thermionic current, Eq. (6)), which leads to a large increase of the plasma electron flux reaching the cathode (last term of Eq. (8)).

The determination of the surface temperature is possible by balancing the plasma heat flux to the cathode,  $Q_{pf}$ , and conducted away from it,  $Q_c$  (Eq. (4)), as shown in Fig. 8a. It appears that for a large thermal conductivity,  $\kappa = 100 \text{ Wm}^{-1}\text{K}^{-1}$ , or a reduced one,  $\kappa = 30 \text{ Wm}^{-1}\text{K}^{-1}$ , the surface reaches a stable low or high temperature. However, there is a range of  $\kappa$  where the equation of  $Q_{pf} = Q_c$  does not provide an unique  $T_s$  (see  $\kappa = 50 \text{ Wm}^{-1}\text{K}^{-1}$  in the figure). This behavior, already evidenced by other authors<sup>15,56,57</sup>, leads to a typical S curve of bifurcation where there is a coexistence between a cold and a hot phase of the tungsten surface, associated with the absence or the presence of a strong

thermionic emission respectively as shown in Fig. 6. The calculated S curves can be seen on the 3 plotted characteristics, from the sheath potential, the surface temperature to the emitted current crossing the surface and they are qualitatively in good agreement with the PIC results. It is important to specify that the fluid calculations were carried out with nominal plasma temperatures which may be different (larger) from the plasma temperatures in the PIC simulations as previously stated. This can explain the differences between the calculated surface temperature and the one from the simulations. Moreover, the transition into the space charge limited regime is calculated in the fluid model from the moment when the electric field on the surface cancels, which is not the case in the PIC simulations since a virtual cathode is established in the plasma close to the surface proximity. That is why the calculated  $\phi_s^*$  and  $J_s^*$  are larger and smaller respectively than the one derived from the PIC simulations. Finally, a similar good agreement is also found between the  $T_s$  bifurcation curves calculated for both  $\kappa$  and an increasing electronic plasma temperature  $T_e$ , Fig. 8b, and the PIC results, Fig. 7b.

In the range of  $\kappa$  (or  $T_e$ ) where two stable states coexist, it is obvious that the heat flux history matters in determining the final temperature  $T_s$ . In order to highlight this effect related to the history and the expected hysteresis associated with it, we have shifted in time the moment when the routine calculating the surface temperature and the number of emitted electrons is called in the code. Until now, this routine was launched at the beginning of the simulations, which led to large electron emission and to the creation of the virtual cathode from the first plasma periods as explained in section III A. Therefore we introduced in the code a waiting time of  $20 \times 2\pi/\omega_{pe}$  before this routine is called - waiting time which is large enough for the sheath to be formed for the working initial condition set - so that the sheath building arises without the effect of thermionic emission. The absence of injected electrons at the wall makes the sheath potential larger and the heat flux due to electrons smaller during the transient state with respect to the case without waiting time, Fig. 9. For a  $k_b T_e = 60$  eV plasma ( $\kappa = 100 \text{ Wm}^{-1}\text{K}^{-1}$ ,  $n_0 = 5 \times 10^{18} \text{ m}^{-3}$  and  $k_b T_i = 5$  eV), the final state of the system clearly depends on its history, i.e. on the temperature reached by the cathode during the transient regime. If the surface experienced transient high heat loads, a virtual cathode is build in its vicinity and the system remains stuck in this local minimum of the energy until the end of the simulations. If the electron plasma temperature is increased up to  $k_b T_e = 70$  eV, Fig. 9b, the waiting time does not change the final state of

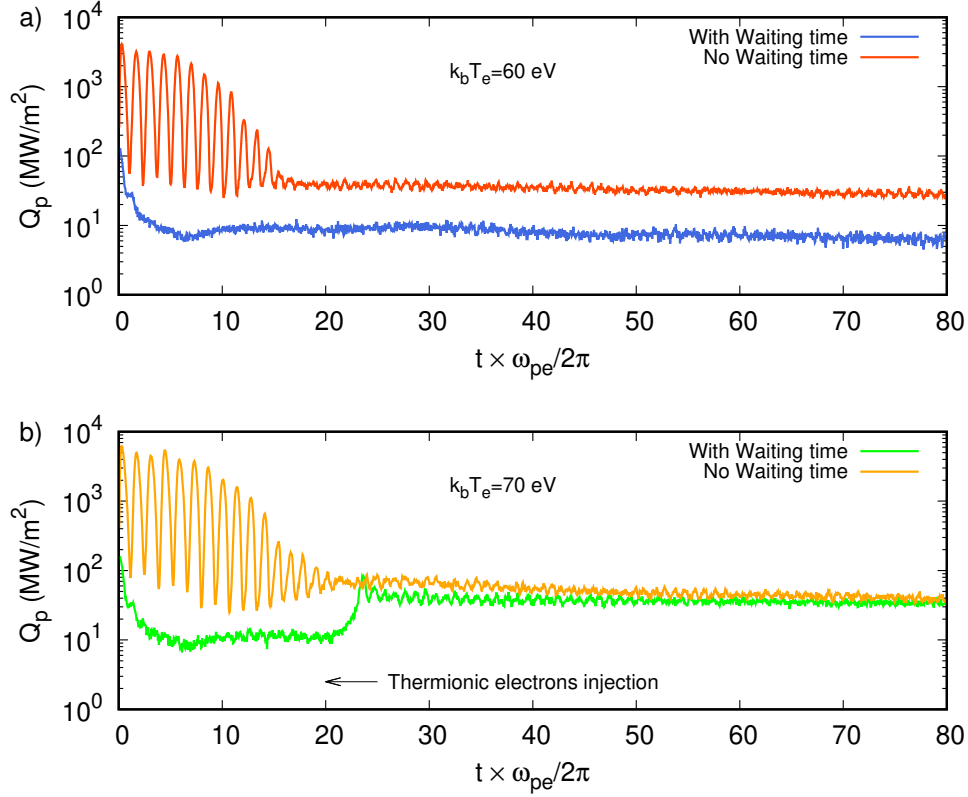


FIG. 9. a) Time variation of the plasma heat flux to the wall ( $Q_p$ ) for  $k_b T_e = 60$  eV. With the waiting time, the routine calculating the instantaneous surface temperature and the thermionic current to be injected into the plasma at each iteration is run after 20 plasma periods. b) Same than in a) for  $k_b T_e = 70$  eV.

the system because the heat flux received by the cathode is large enough to make it reach the high temperature regime.

This phenomenon induces a hysteresis on the different characteristics shown in Fig. 7 measured with and without a waiting time: the final  $T_s$  depends, for a certain range of  $T_e$ , on the history of the cathode, as evidenced by the fluid calculations. Note that the width of the hysteresis is smaller in the PIC simulations than the one expected by the model (compare Fig. 8b with Fig. 7b for instance). This can be ascribed to the variation of the heat flux to the surface from one iteration to another. While the fluid calculations are carried out with a constant heat flux to the cathode (Eq. (8)), the kinetic nature of the PIC simulations makes the heat flux vary around an average value. A small deviation of the heat flux associated with the deeply non linear dependence of the Richardson law on  $T_s$  can be enough to change



drastically the final situation of the cathode as depicted in Fig. 9b: in a few iterations, the system transits from a low temperature regime to a space charge limited one. Finally, the same hysteresis phenomenon is present when the simulations are conducted as a function of the thermal conductivity, with and without a waiting time, Fig. 6b.

#### IV. CONCLUSION

We have calculated thanks to PIC simulations the expected temperature of a tungsten surface  $T_s$  facing high heat plasma flux. The considered simulated plasma was a dense  $5 \times 10^{18} \text{ m}^{-3}$  hydrogen one with various electron and ion temperatures, conditions which can be found in the scrape-off-layer of actual fusion devices<sup>58</sup>. The heat conducted away from the tungsten surface was due to thermionic emission, surface radiation and heat conduction through the wall. For each time iteration, the heat flux from the plasma species to the cathode and the one conducted away from it was balanced in order to determine  $T_s$  and the number of thermionic electrons to be released in the system. The retained value of  $T_s$  was extrapolated at the end of the simulations by considering an average on the heat flux received by the surface. In order to take into account the surface condition, we have varied for each calculation the thermal conductivity, from a value close to a pristine tungsten down to  $\kappa = 35 \text{ Wm}^{-1}\text{K}^{-1}$ .

When the thermal conductivity  $\kappa$  was decreased, less heat was conducted away through the wall thickness so that the surface temperature was expected to increase. Its rise was at first modest, from a few hundred up to  $\simeq 1000 \text{ K}$  with a negligible thermionic current. But at a critical  $\kappa$ , whose value depends on plasma conditions (ion and electron temperature here), the system abruptly transited to a space charge limited regime with a high surface temperature ranging between 2500 and 3000 K. If the thermal conductivity was decreased further, the surface temperature kept increasing but the plasma sheath potential stayed at a minimum value and the thermionic current penetrating the plasma at a maximum one. It was about 3 times the Bohm current, which is of the same order of magnitude as the ion current reaching the wall. Other numerical experiments have been carried out for prescribed values of the thermal conductivity (15 and  $100 \text{ Wm}^{-1}\text{K}^{-1}$ ) and an increasing electron plasma temperature, yielding the same conclusions, ie. a transition from a cold surface temperature to a hot one for which the thermionic current is of the order of magnitude as the Bohm

current. For the case of a detached divertor plasma, our simulations showed that, for similar plasma parameters, the space-charge limited regime can be reached only on local defects where the thermal conductivity is quite reduced with respect to the pristine tungsten.

By changing the timing when the routine calculating the surface temperature and the thermionic electron to be injected at the wall at each iteration was launched during the simulations (a waiting time), we have shown that the final state of the system may have changed. With a waiting time, the building of the sheath is achieved without injection of thermo-electrons, and the heat flux to the surface is reduced because the potential drop in the sheath is larger than without a waiting time. The final state of the cathode can then depends on its heat flux history, i.e. the temperature it has reached before the steady state is established. We have shown that this hysteresis phenomenon, which has been also evidenced thanks to fluid calculations, arises for a certain range of  $\kappa$  (or  $T_e$ ). It was very similar to what was already experimentally measured on a tungsten plate<sup>59</sup> facing a variable and adjustable heat flow of He plasma. It will be interesting to study numerically in the forthcoming future the stability of the sheath subjected to a flux perturbation in order to check whether only one surface temperature solution is stable or both.

Our calculations will be extended soon to the case of magnetized sheaths, where a magnetic field is tilted with respect to the wall, in order to evaluate more precisely the temperature of a divertor surface in the presence of high heat loads<sup>2,60</sup> although the present calculations can be applied straightforward to misaligned W tiles with a magnetic field perpendicular to the surface, where experiments have already shown that the space-charge limited regime was achievable<sup>6</sup>.

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