

# Homogenisation for waves in 1D periodic media: Effective models, boundary and transmission correctors Rémi Cornaggia

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# Theme 1: Homogenisation for waves in 1D periodic media Effective models, boundary and transmission correctors

Rémi Cornaggia<sup>1</sup>

Joint work with Bojan B. Guzina<sup>2</sup> and Bruno Lombard<sup>3</sup>

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<sup>1</sup>Institut ∂'Alembert, Sorbonne Université

<sup>2</sup>Department of Civil, Environmental & Civil Engineering, University of Minnesota

<sup>3</sup>Laboratoire de mécanique et d'acoustique, Aix-Marseille Université, CNRS, Centrale Marseille

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Waves in 1D periodic media

# Control of wave propagation using periodic structures



[Celli and Gonella, 2015]

 $\dots$  to design waveguides

- ${\ensuremath{\, \bullet }}$  with resonators for long wavelengths / low frequencies
- with Bragg effects for medium wavelengths / frequencies

... to design seismic protections (with resonators)



... and more (negative effective properties, cloaking ...)

# A motivation : dispersion and anisotropy in 2D elasticity [Rosi and Auffray, 2019]









#### Continuum model



### Effective (strain-gradient) model.



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Waves in 1D periodic media

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# Homogenisation and interface conditions

### How to model the wave propagation in periodic structures ?

- Accounting for all interactions  $\rightarrow$  costly (*dedicated numerical methods* out-of scope)
- Floquet-Bloch theory  $\implies$  See other lectures.
- Homogenization (/averaging/effective) methods and models
- Both lectures: asymptotic two-scale homogenization
  - Formal procedure to obtain effective models
  - Accuracy can be improved by pushing the expansion to higher orders
  - Extensions to high/finite frequencies [Craster et al., 2010, Guzina et al., 2019]
  - $\implies$  R. Craster and B. Guzina's lectures

### How to account for boundaries and interfaces ?

- In 2-3D, *boundary layers* must be accounted for at boundaries and interfaces [Dumontet, 1986, Moskow and Vogelius, 1997, Allaire and Amar, 1999, Gérard-Varet and Masmoudi, 2012, Armstrong et al., 2017, Cakoni et al., 2019] ...
- Equivalent boundary or transmission conditions preserving the asymptotics are difficult to build [Vinoles, 2016, Marigo and Maurel, 2017, Maurel and Marigo, 2018, Beneteau, 2021]
- This lecture: 1D waves, "interfaces" are points.

# Optimization

### How to obtain desired properties ?

- Known design (cylinders, spheres, cones, LEGO bricks ...) ⇒ parameter optimization [Huang et al., 2016, Palermo et al., 2016] ...
- Given materials, unknown design ⇒ topological optimization [Vondřejc et al., 2017, Kook and Jensen, 2017, Allaire and Yamada, 2018] ...

Next lectures: topological optimization of microstructured 2D media and interfaces (long wavelengths, no resonances)



what we will see

[Noguchi et al., 2018] high frequency, hyperbolic propagation, see R. Craster's lecture

## A preliminary example : 1D statics



- **Two-scale** problem : L (macro) and  $\ell$  (micro)
- Scale factor  $\varepsilon = \ell/L$
- $\ell$ -periodic properties  $E_{\ell}(X) = E(X/\ell) = E(x/\varepsilon)$  : *E* is 1-periodic
- Normalized coordinate x = X/L

$$\begin{cases} \partial_x \sigma(x) = 0 & x \in [0, 1] & \text{equilibrium} \\ \sigma(x) = E(x/\varepsilon) \partial_x u & x \in [0, 1] & \text{constitutive law} \\ u(0) = 0 & & \text{displacement BC} \\ \sigma(1) = \sigma_L & & \text{stress BC} \end{cases}$$

### See dedicated Jupyter Notebook.

### Examples: 2D statics [Dumontet, 1986]



Figure 4. — The (3, 3) components of the real stresses  $\sigma^t$ , of the micro-stresses  $\sigma^0$ and of the boundary layer stresses  $\sigma^{OBL}$  added to  $\sigma^0$ , ploted against  $y_3$ , at  $y_2 = 0.0416$  fixed.

## Examples: 2D time-harmonic dynamics [Beneteau, 2021] with S. Fliss, X. Claeys

 $\varepsilon = \ell/\lambda = 0.125$  $U_0$ u (exact) 1.0e+00 0.8 - 0.4 - 0.2 - 0.2 - -0.2 - -0.4 - -0.6 - -0.8 - 1.0e+00  $|u - U_0|$  $|u - (U_0 + \varepsilon u_1)|$  (bulk corrector) 0.06 0.04 -0.02 -0.04 -0.06 -9.7e-02 -9.7e-02

# 





 $|u - (U_0 + \varepsilon [U_1 + u_1 + u_1^{\text{BL}}])|$  (bulk, mean and boundary layer correctors)



(and then look for 2nd-order correctors ...)

Challenges for 1D waves : dispersion, interfaces and source points



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#### Second-order asymptotic homogenization for waves in 1D domains

- Second-order models
- Corrector functions and reciprocity identities
- Choosing a model

Boundary and transmission correctors for time-harmonic motion

#### Extension to transient waves

- Hyperbolic system
- Transmission conditions and first-order "hybrid" model
- Application to point sources

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## Two-scale asymptotic homogenization in a 1D periodic medium



Wave equation in a ℓ-periodic medium

$$\rho\left(\frac{X}{\ell}\right)\frac{\partial^2 u_\ell}{\partial t^2} - \frac{\partial}{\partial X}\left[E\left(\frac{X}{\ell}\right)\frac{\partial u_\ell}{\partial X}\right] = 0$$

• Reference wavelength  $\lambda$ 

[Sanchez-Palencia, 1974, Bensoussan et al., 1978, Cioranescu and Donato, 1999] ...

- Scale separation  $\varepsilon = \ell/\lambda \ll 1$
- Slow variable  $x=X/\lambda$  and fast variable  $y=X/\ell=x/\varepsilon$
- Look for  $u_\ell$  as a function of both variables:  $u_\ell(X,t) = \hat{u}(x,y,t)$ , 1-periodic in y
- $\frac{\partial}{\partial X} \to \frac{1}{\lambda} \left[ \frac{\partial}{\partial x} + \varepsilon^{-1} \frac{\partial}{\partial y} \right]$
- Ansatz:  $\hat{u}(x,y,t) = \sum_{j\geq 0} \varepsilon^j u_j(x,y,t) \implies$  cascade of equations for the  $u_j$
- Separated variable solution featuring mean fields  $U_j(x,t)$  and cell functions  $P_j(y)$ :

$$\begin{split} &u_0(x,y,t) = U_0(x,t) \\ &u_1(x,y,t) = U_1(x,t) + U_{0,x}(x,t)P_1(y) \\ &u_2(x,y,t) = U_2(x,t) + U_{1,x}(x,t)P_1(y) + U_{0,xx}(x,t)P_2(y) \end{split}$$

### Effective wave equations

• Equations satisfied by the mean fields:

$$\begin{split} \varrho_{0}U_{0,tt} - \mathcal{E}_{0}U_{0,xx} &= 0 & \left| \begin{array}{c} \varrho_{0} &= \langle \rho \rangle \\ \mathcal{E}_{0} &= \langle E(1 + P_{1,y}) \rangle \\ \varrho_{0}U_{1,tt} - \mathcal{E}_{0}U_{1,xx} &= 0 & \mathcal{E}_{1} &= \frac{\varrho_{1}}{\varrho_{0}}\mathcal{E}_{0} \Rightarrow \text{ no first-order contribution} \\ \varrho_{0}U_{2,tt} - \mathcal{E}_{0}U_{2,xx} + \varrho_{2}U_{0,xxtt} - \mathcal{E}_{2}U_{0,xxxx} &= 0 & \left| \begin{array}{c} \varrho_{2} &= \langle \rho P_{2} \rangle \\ \mathcal{E}_{2} &= \langle E(P_{2} + P_{3,y}) \rangle \end{array} \right| \end{split}$$

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- Second-order total mean field  $U = U_0 + \varepsilon U_1 + \varepsilon^2 U_2$ :  $\underbrace{\varrho_0 U_{,tt} - \mathcal{E}_0 U_{,xx}}_{0} + \varepsilon^2 \left( \underbrace{\varrho_2 U_{0,xxtt}}_{0,xxtt} - \mathcal{E}_2 U_{0,xxxx} \right) = 0$
- "Boussinesq trick": using (i)  $\varrho_0 U_{0,tt} = \mathcal{E}_0 U_{0,xx}$  and (ii)  $U_0 = U + o(1)$ :

$$\frac{1}{c_0^2}U_{,tt} - U_{,xx} - \varepsilon^2 \left(\beta_x U_{,xxxx} - \frac{\beta_m}{c_0^2}U_{,xxtt} - \frac{\beta_t}{c_0^4}U_{,tttt}\right) = 0, \text{ with } \beta_x - \beta_m - \beta_t = \beta$$

[Fish et al., 2002, Lamacz, 2011, Wautier and Guzina, 2015]

- Effective properties:  $c_0^2 = \frac{\mathcal{E}_0}{\rho_0}$  and  $\beta := \left[\frac{\mathcal{E}_2}{\mathcal{E}_0} \frac{\varrho_2}{\rho_0}\right]$
- 2 degrees of freedom to choose  $(\beta_x, \beta_m, \beta_t)$ .

### Cell functions: displacement/velocity and stress correctors

Velocity-stress system:

$$\begin{cases} \partial_t v_\ell - \frac{1}{\rho_\ell} \partial_x \sigma_\ell = 0\\ \partial_t \sigma_\ell - E_\ell \partial_x v_\ell = 0 \end{cases}$$

with  $v_{\ell} = \partial_t u_{\ell}$ and  $\sigma_{\ell} = E_{\ell} \partial_x u_{\ell}$ . • Displacement/velocity correctors  $(P_1, P_2, P_3)$  using  $V = \partial_t U$ :

$$\begin{cases} u_{\ell}(x,t) \approx U(x,t) + \varepsilon U_{,x}(x,t) P_1(x/\varepsilon) + \varepsilon^2 U_{,xx}(x,t) P_2(x/\varepsilon) \\ v_{\ell}(x,t) \approx V(x,t) + \varepsilon V_{,x}(x,t) P_1(x/\varepsilon) + \varepsilon^2 V_{,xx}(x,t) P_2(x/\varepsilon) \end{cases}$$

• Stress correctors  $(\Sigma_1, \Sigma_2)$  using macroscopic stress  $S := \mathcal{E}_0 \partial_x U$ :  $\sigma_\ell(x, t) \approx S(x, t) + \varepsilon S_x(x, t) \Sigma_1(x/\varepsilon) + \varepsilon^2 S_{xx}(x, t) \Sigma_2(x/\varepsilon)$ 

**Static equilibrium problems** posed in the unit cell Y = [0, 1] for  $(P_j, \Sigma_j)$ 

$$\begin{cases} \partial_y \Sigma_j = f_j [E, \rho, P_{j-1}, \Sigma_{j-1}] \\ \mathcal{E}_0 \Sigma_j = E \left( P_j + \partial_y P_{j+1} \right) \end{cases} \quad (P_j, \Sigma_j) \text{ are 1-periodic}, \quad \langle P_j \rangle = 0 \end{cases}$$



# Reciprocity identities on effective coefficients

• Classical expression of effective coefficients:

$$\rho_j = \langle \rho P_j \rangle, \qquad \mathcal{E}_j = \langle E(P_j + P_{j+1,y}) \rangle = \mathcal{E}_0 \langle \Sigma_j \rangle, \qquad \beta := \left[ \frac{\mathcal{E}_2}{\mathcal{E}_0} - \frac{\varrho_2}{\varrho_0} \right]$$

 $\Rightarrow$  a priori needs  $P_j$ , j = 1, 2, 3 for second-order effective properties.

• Weak form of cell problems:

$$\mathsf{Find}\ {P_j} \in H^1_{\sharp 0}, \quad \int_0^1 E(\partial_y P_j)(\partial_y w) \ \mathrm{d} y = F_j(w) \quad \forall w \in H^1_\sharp, \quad j \in \{1,2,3\},$$

**Reciprocity identities** are obtained by "testing" one cell problem with another. [Fish et al., 2002, Abdulle and Pouchon, 2020] ...

First reciprocity identity: using  $F_1(P_2) = F_2(P_1)$ ,

 $\frac{\mathcal{E}_1}{\mathcal{E}_0} - \frac{\varrho_1}{\varrho_0} = 0 \quad \Rightarrow \begin{cases} \text{No need for } P_2 \text{ to compute } \mathcal{E}_1. \\ \text{Cancels first-order contribution in effective wave equation.} \end{cases}$ 

Second reciprocity identity: using  $F_1(P_3) = F_3(P_1)$  (and after some work):

$$\beta = \frac{\mathcal{E}_2}{\mathcal{E}_0} - \frac{\varrho_2}{\varrho_0} = \frac{1}{2} \left\langle \left[ P_1 - \Sigma_1 \right]^2 \left( \frac{\mathcal{E}_0}{E} + \frac{\rho}{\varrho_0} \right) \right\rangle \qquad \Rightarrow \begin{cases} \text{No need for } P_3 \text{ to compute } \beta \text{ (or } \mathcal{E}_2). \\ \text{Important positivity property: } \beta \ge 0. \end{cases}$$

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# Choosing a model : link with gradient elasticity models

$$\frac{1}{c_0^2} \left[ 1 + \varepsilon^2 \beta_m \partial_{xx} + \varepsilon^2 \frac{\beta_t}{c_0^2} \partial_{tt} \right] U_{,tt} = \left[ 1 + \varepsilon^2 \beta_x \partial_{xx} \right] U_{,xx}, \quad \text{with} \quad \beta_x - \beta_m - \beta_t = \beta > 0$$

	Gradient elasticity	Two-scale homogenization	Properties
	(see [Askes and Aifantis, 2011])		
(x)	[Mindlin, 1964]	"natural" result when $ ho=1$	unstable if $\beta_x > 0$
		[Fish and Chen, 2001]	[Allaire et al., 2016]
(m)		[Fish et al., 2002, Lamacz, 2011]	stable if $\beta_m < 0$
(t)	?	?	?
(xm)	[Mindlin, 1964]	"natural" result for $\rho \neq 1$	
		Used to stabilize $(x)$	
(mt)	[Pichugin et al., 2008]	[Cornaggia and Guzina, 2020]	stable if $\beta_m < 0$
	[Forest and Sab, 2017]	[Cornaggia and Lombard, 2023]	and $\beta_t > 0$
(xmt)	[Dontsov et al., 2013]	[Wautier and Guzina, 2015]	

 $\beta_x \neq 0 \Longrightarrow$  additional boundary conditions for bounded domains

- Well-posedness of the problem ? [Askes et al., 2008, Kaplunov and Pichugin, 2009]
- Difficult to deal with in homogenization theory (proofs when  $\varepsilon \to 0$  ?)
- Not very useful to fit dispersion curves [Schwan et al., 2021].

Choosing a (mt) model from dispersion relations in layered media



• Bloch wave  $u_{\ell}(X,t) = \tilde{u}(x)e^{i(\kappa x - \omega t)} \implies \text{dispersion relation } \omega = f(\kappa).$ About  $(\omega, \kappa) = (0,0)$  (on the acoustic branch):

$$\frac{\omega}{c_0} = \kappa \left[ 1 - \frac{\beta}{2} (\kappa \varepsilon)^2 + \frac{\beta \left( 2 - 27\beta - 8\overline{\beta} \right)}{40} (\kappa \varepsilon)^4 + O(\varepsilon^6) \right],$$

( $\overline{\beta}$  known for layered media)

• Plane wave  $U(x,t) = \tilde{U}e^{i(\kappa x - \omega t)}$  in the (mt) homogenized model:

$$\frac{\omega}{c_0} = \kappa \left[ 1 + \frac{\beta_m + \beta_t}{2} (\kappa \varepsilon)^2 + \frac{(\beta_m + \beta_t)(3\beta_m + 7\beta_t)}{8} (\kappa \varepsilon)^4 + O(\varepsilon^6) \right].$$

- Second-order approximation of  $\omega/c_0$  obtained for any  $(\beta_m, \beta_t)$  satisfying  $-\beta_m \beta_t = \beta$ . Also true in 2-3D [Allaire et al., 2016].
- Fourth-order approximation for  $\beta_m = \frac{-1 4\beta + 4\overline{\beta}}{10}$  and  $\beta_t = \frac{1 6\beta 4\overline{\beta}}{10}$ Similar approximation for spring-mass lattice in [Pichugin et al., 2008]

# Choosing a (mt) model by fitting dispersion curves



$$\begin{array}{ll} \text{Material contrasts:} & \frac{E_2}{E_1}=6, \quad \frac{\rho_2}{\rho_1}=1.5\\ \text{Phase ratio:} & \frac{\ell_2}{\ell_1}=3\\ (\approx \text{ maximal dispersion [Santosa and Symes, 1991]} \end{array}$$



- Bloch wave:  $u(x, y, t) = \phi(y)e^{i(\kappa x \omega t)}$  $\implies$  Dispersion relation  $\kappa = f(\omega)$
- Oth-order:  $U_{,tt} c_0^2 U_{,xx} = 0$  $\implies$  non-dispersive
- 2nd-order (m):  $\implies O((\kappa \varepsilon)^2)$  approximation
- Optimized (mt):  $\implies O((\kappa \varepsilon)^4)$  approximation [Pichugin et al., 2008, Cornaggia and Guzina, 2020]

### Recap: second-order homogenization in one slide



2 - Choose a model (e.g. (mt)) and compute effective coefficients (e.g.  $c_0^2, \beta, \beta_m, \beta_t$ )

$$\frac{1}{\frac{2}{c_0}}U_{,tt} - U_{,xx} + \varepsilon^2 \left(\frac{\beta_m}{c_0^2}U_{,xxtt} + \frac{\beta_t}{c_0^4}U_{,tttt}\right) = 0,$$

- 3 Solve the effective wave equation to find the macroscopic field U
- 4 Add bulk correctors to obtain approximations :

$$\begin{cases} u_{\ell}(x,t) \approx U(x,t) + \varepsilon U_{,x}(x,t) P_{1}(x/\varepsilon) + \varepsilon^{2} U_{,xx}(x,t) P_{2}(x/\varepsilon) \\ \sigma_{\ell}(x,t) \approx S(x,t) + \varepsilon S_{,x}(x,t) \Sigma_{1}(x/\varepsilon) + \varepsilon^{2} S_{,xx}(x,t) \Sigma_{2}(x/\varepsilon) & \text{with } S = \mathcal{E}_{0} U_{,x} \end{cases}$$

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# Model problem and leading-order approximation



• Time-harmonic model problem:

$$\begin{vmatrix} [E(x/\varepsilon)u_{,x}]_{,x} + \rho(x/\varepsilon)\,\omega^2 u = 0 & x \in Y_L := ]0,L \\ u = 0 & x = 0 \\ \sigma = E(x)u_{,x} = \sigma_L & x = L \end{vmatrix}$$

• Leading-order homogenization:  $(u, \sigma) \rightarrow (U, \mathcal{E}_0 U_{,x})$ 

$$\begin{array}{ll} U_{,xx} + k_0^2 \, U = 0 & x \in Y_L, & k_0 := \omega/c_0 \\ U = 0 & x = 0 \\ U_{,x} = \sigma_L/\mathcal{E}_0 & x = L \end{array}$$

Boundary correctors using full-field approximations [Cornaggia and Guzina, 2020] First-order approximations of displacement and stress  $(u, \sigma)$ :

$$\begin{cases} \tilde{u}^{(1)}(x) = U(x) + \varepsilon P_1\left(\frac{x}{\varepsilon}\right)U_{,x}(x) \\ \tilde{\sigma}^{(1)}(x) = \mathcal{E}_0\left[U_{,x}(x) + \varepsilon \Sigma_1\left(\frac{x}{\varepsilon}\right)U_{,xx}(x)\right] \end{cases}$$

Using cell stress functions:  $\Sigma_j := (E/\mathcal{E}_0) [P_j + P_{j+1,y}]$ 

Boundary-value problem for the mean field U:

$$\begin{aligned} &U_{,xx} + k_0^2 U = 0 \quad x \in Y_L \\ &\tilde{u}^{(1)} = 0 \quad x = 0 \\ &\tilde{\sigma}^{(1)} = \sigma_L \quad x = L \end{aligned}$$

$$\begin{array}{ll} U_{,xx} + k_0^2 \, U = 0 & x \in Y_L \\ U + \varepsilon P_1(0) U_{,x} = 0 & x = 0 \\ U_{,x} + \varepsilon \Sigma_1(0) U_{,xx} = \sigma_L / \mathcal{E}_0 & x = L \\ U_{,xx} + k_0^2 \, U = 0 & x \in Y_L \\ U + \varepsilon P_1(0) U_{,x} = 0 & x = 0 \\ U_{,x} - \varepsilon \Sigma_1(0) k_0^2 \, U = \sigma_L / \mathcal{E}_0 & x = L \end{array}$$

### Second-order approximation

• Approximations of the displacement and stress  $(u, \sigma)$ :

$$\begin{split} \tilde{u}^{(2)}(x) &= U(x) + \varepsilon P_1\left(\frac{x}{\varepsilon}\right) U_{,x}(x) + \varepsilon^2 P_2\left(\frac{x}{\varepsilon}\right) U_{,xx}(x), \\ \tilde{\sigma}^{(2)}(x) &= \mathcal{E}_0\left[U_{,x} + \varepsilon \Sigma_1\left(\frac{x}{\varepsilon}\right) U_{,xx}(x) + \varepsilon^2 \Sigma_2\left(\frac{x}{\varepsilon}\right) U_{,xxx}(x)\right] \end{split} \right\} U = U_0 + \varepsilon U_1 + \varepsilon^2 U_2$$

 $\bullet$  Boundary-value-problem for the second-order mean field  $U{:}$ 

$$|U_{,xx} + k_{mt}^2 U = 0 \qquad \qquad x \in Y_L$$

$$\begin{split} & \left[ 1 - \varepsilon^2 k_{mt}^2 P_2(0) \right] U + \varepsilon P_1(0) U_{,x} = 0 \qquad x = 0 \\ & \left[ 1 - \varepsilon^2 k_{mt}^2 \Sigma_2(0) \right] U_{,x} - \varepsilon k_{mt}^2 \Sigma_1(0) U = \sigma_L / \mathcal{E}_0 \quad x = L. \end{split}$$

using the (mt) dispersive model:

$$k_{mt}^2 := k_0^2 \frac{1 - \varepsilon^2 \beta_t k_0^2}{1 + \varepsilon^2 \beta_m k_0^2}$$

Lemma 2:  $\exists C > 0$   $\|u - \tilde{u}^{(2)}\|_{H^1} \leq C\varepsilon^2 \|U\|_{H^1}.$ 

Theorem 1:  $\exists C > 0$   $\|u - \tilde{u}^{(1)}\|_{L^2} \leq \|u - \tilde{u}^{(2)}\|_{L^2} + \|\tilde{u}^{(2)} - \tilde{u}^{(1)}\|_{L^2} \leq C\varepsilon^2 \|U\|_{H^2}.$ 

- No need for 2nd order BC to prove these results
- BCs surely needed for the next step : we hope that  $||u \tilde{u}^{(2)}||_{L^2} = O(\varepsilon^3)$

## Example for a layered material - mean fields U

 $\varepsilon = \ell / \lambda_0 \approx 0.3$ 



### Example for a layered material - total displacement u

 $\varepsilon = \ell / \lambda_0 \approx 0.3$ 



### Example for a layered material - axial stress $\sigma$

 $\varepsilon = \ell / \lambda_0 \approx 0.3$ 



Errors for fixed  $\omega$  and  $\ell \to 0$ 





# Application to a transmission problem ( $\varepsilon \approx 0.3$ )



### Transmission problem - errors for fixed $\omega$ and $\ell \to 0$



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Equivalent hyperbolic system for the (mt) model  $(\beta_x = 0$  because we don't want  $U_{,xxxx}$  and additional BC/TC it brings)

Second-order homogenization, (mt) model:

$$\frac{1}{c_0^2} \left[ 1 + \varepsilon^2 \beta_m \partial_{xx} + \varepsilon^2 \frac{\beta_t}{c_0^2} \partial_{tt} \right] U_{,tt} = U_{,xx},$$

"Stress gradient" system [Forest and Sab, 2017]:

$$\begin{cases} \sigma = E\partial_x(u+\phi) \\ r = D\phi \end{cases} \begin{cases} \rho\partial_{tt}u = \partial_x\sigma \\ \rho J\partial_{tt}\phi = \partial_x\sigma - r \end{cases}$$

So that: 
$$\frac{\rho}{E} \left[ 1 - \frac{E(1+J)}{D} \partial_{xx} + \frac{\rho J}{D} \partial_{tt} \right] u_{,tt} = u_{,xx}$$

$$\Rightarrow \begin{cases} \partial_t V - \frac{a}{\varrho_0} \partial_x S &= -\frac{a-1}{\varrho_0} r \\ \partial_t S - \mathcal{E}_0 \partial_x V &= 0 \\ \partial_t \varphi - \frac{a-1}{\varrho_0} \partial_x S &= -\frac{a-1}{\varrho_0} r \\ \partial_t r &= \frac{\mathcal{E}_0}{\varepsilon^2 \beta} \varphi \end{cases}$$

- Macroscopic fields  $V = \partial_t (u + \phi)$  and  $S = \sigma$
- Auxiliary fields  $\varphi = \partial_t \phi$  and r
- Parameter  $a = -\beta_m / \beta_t$  to select a (mt) model.

Well-posedness (hyperbolicity, stability, conserved positive energy) for:

$$oldsymbol{eta} \geq 0 \; (oldsymbol{\checkmark}), \quad oldsymbol{eta}_{oldsymbol{m}} < 0 \quad ext{and} \quad oldsymbol{eta}_{oldsymbol{t}} > 0$$

### Hyperbolicity and stability (See B. Lombard's first lecture)

• Matricial form of system:

 $\partial_t \boldsymbol{U} + \boldsymbol{A} \cdot \partial_x \boldsymbol{U} = \boldsymbol{S} \cdot \boldsymbol{U}, \quad \text{where} \quad \boldsymbol{U} := (V, S, \varphi, r)^{\mathsf{T}}$  $\boldsymbol{A} = \begin{bmatrix} 0 & -a/\varrho_0 & 0 & 0\\ -\mathcal{E}_0 & 0 & 0 & 0\\ 0 & -(a-1)/\varrho_0 & 0 & 0\\ 0 & 0 & 0 & 0 \end{bmatrix} \quad \text{and} \quad \boldsymbol{S} = \begin{bmatrix} 0 & 0 & 0 & -(a-1)/\varrho_0\\ 0 & 0 & 0 & 0\\ 0 & 0 & 0 & -(a-1)/\varrho_0\\ 0 & 0 & \mathcal{E}_0/(\varepsilon^2 \beta) & 0 \end{bmatrix}.$ 

• Hyperbolicity : real eigenvalues of  $oldsymbol{A}$ 

$$\mathsf{Sp}(\boldsymbol{A}) = \left\{0, 0, \pm \boldsymbol{c_0}\sqrt{a}\right\}$$

• Stability : imaginary eigenvalues of  ${old S}$ 

$$\mathsf{Sp}(\boldsymbol{S}) = \left\{ 0, 0, \pm \boldsymbol{c_0} / \left( \varepsilon \sqrt{-\beta_t} \right) \right\}$$

$$\begin{cases} \mathsf{Hyperbolicity:} & a > 0 \\ \mathsf{Stability:} & \boldsymbol{\beta_t} > 0 \end{cases} \implies \begin{cases} -\frac{\boldsymbol{\beta_m}}{\boldsymbol{\beta_t}} > 0 \\ \boldsymbol{\beta_t} > 0 \end{cases} \implies \begin{cases} \boldsymbol{\beta_m} < 0, \\ \boldsymbol{\beta_t} > 0. \end{cases}$$

# Symmetrizer and energy conservation for $\partial_t U + A \cdot \partial_x U = S \cdot U$

• Symmetrizer matrix:

$$M = \begin{bmatrix} \frac{\varrho_0 & 0 & -\varrho_0 & 0\\ 0 & 1/\mathcal{E}_0 & 0 & 0\\ -\varrho_0 & 0 & a\varrho_0/(a-1) & 0\\ 0 & 0 & 0 & \varepsilon^2\beta/\mathcal{E}_0 \end{bmatrix},$$

So that:

• Multiplying the system by  $U^{\mathsf{T}} \cdot M$ :

$$\partial_t \frac{1}{2} (\boldsymbol{U}^{\mathsf{T}} \cdot \boldsymbol{M} \cdot \boldsymbol{U}) + \frac{1}{2} \partial_x (\boldsymbol{U}^{\mathsf{T}} \cdot \boldsymbol{M} \cdot \boldsymbol{A} \cdot \boldsymbol{U}) = 0.$$

Integrating over  $\Omega \times [0,T]$ , (large  $\Omega$  so that  $U(\cdot,T) = 0$  on  $\partial \Omega$ )

**Energy conservation:**  $\mathcal{E}^{\text{vol}}(T) = \mathcal{E}^{\text{vol}}(0).$ 

$$\mathcal{E}^{\text{vol}} = \frac{1}{2} \int_{\Omega} \boldsymbol{U}^{\mathsf{T}} \cdot \boldsymbol{M} \cdot \boldsymbol{U} \, \mathrm{d}x = \frac{1}{2} \int_{\Omega} \varrho_0 \left( v^2 + \frac{\beta_t}{\beta} \varphi^2 \right) + \frac{1}{\mathcal{E}_0} \left( \sigma^2 + \varepsilon^2 \beta r^2 \right) \, \mathrm{d}x \ge 0 \text{ if } \beta \ge 0$$
  
(with  $v = V - \varphi$ )

# Outline

### Introduction

#### Second-order asymptotic homogenization for waves in 1D domains

- Second-order models
- Corrector functions and reciprocity identities
- Choosing a model

#### Boundary and transmission correctors for time-harmonic motion

### Extension to transient waves

- Hyperbolic system
- Transmission conditions and first-order "hybrid" model
- Application to point sources

### 5 Conclusions and perspectives

# First-order transmission conditions



• Fields of interest:

$$\begin{cases} (V,S) = (\partial_t U, E_- \partial_x U) & x < 0 \\ (V,S,\varphi,r) & x > 0 \end{cases}$$

• Transmission conditions from total fields continuity:

$$\begin{cases} V(0^{-}) = V(0^{+}) + \varepsilon P_1(0)V_{,x}(0^{+}) \\ S(0^{-}) = S(0^{+}) + \varepsilon \Sigma_1(0)S_{,x}(0^{+}) \end{cases}$$

• Energy analysis : interface terms when integrating  $\partial_x (\boldsymbol{U}^{\mathsf{T}} \cdot \boldsymbol{M} \cdot \boldsymbol{A} \cdot \boldsymbol{U})$  over  $\Omega_- \cup \Omega_+$ 

 $\partial_t (\mathcal{E}_-^{\mathrm{vol}} + \mathcal{E}_+^{\mathrm{vol}}) + \mathcal{D}^{\mathrm{int}} = 0,$ 

$$\mathcal{D}^{\text{int}} = \llbracket V \rrbracket_0 \langle S \rangle_0 + \langle V \rangle_0 \llbracket S \rrbracket_0$$
  
=  $-\varepsilon \left[ P_1(0)(\partial_x V)^+ \langle S \rangle_0 + \Sigma_1(0)(\partial_x S)^+ \langle V \rangle_0 \right]$   
= ???

• We would like  $\mathcal{D}^{int} = \partial_t \mathcal{E}^{int}$  with  $\mathcal{E}_1^{int} \ge 0$ 



### First-order transmission conditions - stabilization

Spring-mass conditions across a thin interface  $I_d = [-d\varepsilon, d\varepsilon]$  (additional  $o(\varepsilon)$  error):



• New expression of interface term:

$$\partial_t (\mathcal{E}_-^{\text{vol}} + \mathcal{E}_+^{\text{vol}}) + \mathcal{D}_d^{\text{int}} = 0,$$
$$\mathcal{D}_d^{\text{int}} = \partial_t \mathcal{E}_d^{\text{int}} \quad \text{with} \quad \mathcal{E}_d^{\text{int}} = \frac{\varepsilon}{2} \left[ A_1 \langle S \rangle_{I_d}^2 + B_1 \langle V \rangle_{I_d}^2 \right]$$

• Stability of {Hyperbolic system + transmission conditions} for  $A_1 \ge 0$  and  $B_1 \ge 0$ 

$$\Rightarrow \quad \mathsf{Choice of } d \ge d_{\min} := \max\left(\frac{E_-P_1(0)}{E_- + \mathcal{E}_0}, \ \frac{\varrho_0 \Sigma_1(0)}{\rho_- + \varrho_0}, \ 0\right)$$

Well-posed "hybrid" model:

- dispersive system from 2nd-order bulk homogenization
- transmission conditions (1st-order for now)

## Transmission conditions for $arepsilon=\ell/\lambda_{ m c}pprox 0.04$ (Numerics by B. Lombard)

 $E_{-}\rho_{-} = \mathcal{E}_{0}\varrho_{0} \Longrightarrow$  reflected wave is a 1st-order effect



## Transmission conditions, increasing central frequency, $\varepsilon \approx 0.09$



### Transmission conditions, increasing central frequency, $\varepsilon \approx 0.13$



## Transmission conditions, increasing central frequency, $\varepsilon \approx 0.17$



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n (m)

### Transmission conditions, errors on velocity and stress fields

- Fields emitted at source  $x_{\rm s} < 0$ , measured at receiver  $x_{\rm r} > 0$  during time T.
- Increasing frequency f, constant microstructure periodicity  $\ell$ .
- Positions  $(x_{\rm s}, x_{\rm r})$  and time T accordingly rescaled for each frequency.



 $(v_1, \ \sigma_1)$ : Adding 1st-order bulk correctors  $(P_1, \Sigma_1)$  and 1st-order TC  $(v_2, \ \sigma_2)$ : "Hybrid" dispersive system (but still 1st-order TC)

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# In 1D, source points $\Leftrightarrow$ interfaces with stress jumps

$$\begin{cases} \partial_t v_\ell - \frac{1}{\rho_\ell} \partial_x \sigma_\ell = \delta_{\mathbf{s}} g(t) & x \in \mathbb{R} \\ \partial_t \sigma_\ell - E_\ell \, \partial_x v_\ell = 0 & x \in \mathbb{R} \end{cases} \iff \begin{cases} \partial_t v_\ell - \frac{1}{\rho_\ell} \partial_x \sigma_\ell = 0 & x < x_{\mathbf{s}} \text{ and } x > x_{\mathbf{s}}, \\ \partial_t \sigma_\ell - E_\ell \, \partial_x v_\ell = 0 & x < x_{\mathbf{s}} \text{ and } x > x_{\mathbf{s}}, \\ \|v_\ell\|_{\mathbf{s}} = 0 & x = x_{\mathbf{s}}, \\ \|\sigma_\ell\|_{\mathbf{s}} = -\rho_{\mathbf{s}} g & x = x_{\mathbf{s}}, \end{cases}$$



### First-order correction

• Same tools (and no need for an enlarged interface):

$$\begin{cases} \llbracket V \rrbracket_{\mathrm{s}} = \varepsilon P_{1}(x_{\mathrm{s}}/\varepsilon) \frac{\rho_{\mathrm{s}}}{\varepsilon_{0}} \partial_{t} g_{\mathrm{s}} \\ \llbracket S \rrbracket_{\mathrm{s}} = -\rho_{\mathrm{s}} g, \end{cases}$$

- First-order corrector on V involving  $\partial_t g$  and the local values  $\rho_s$  and  $P_1(x_s/\varepsilon)$ .
- Already given by [Capdeville et al., 2010] with another argument.
- Equivalent system with Dirac notation:

$$\begin{cases} \partial_t V - \frac{a}{\varrho_0} \partial_x S &= -\frac{a-1}{\varrho_0} r + \frac{a}{\varrho_0} \rho_{\rm s} \, g \, \delta_{\rm s}, \\ \partial_t S - \mathcal{E}_0 \partial_x V &= -\varepsilon \, \rho_{\rm s} P_1(x_{\rm s}/\varepsilon) \, \partial_t g \, \delta_{\rm s}, \\ \partial_t \varphi - \frac{a-1}{\varrho_0} \partial_x S &= -\frac{a-1}{\varrho_0} r + \frac{a-1}{\varrho_0} \rho_{\rm s} \, g \, \delta_{\rm s}, \\ \partial_t r &= \frac{\mathcal{E}_0}{\ell^2 \beta} \varphi. \end{cases}$$

## Back to the initial motivation



# Velocity fields in a slab with a source point



# Velocity fields in a slab with a source point



# Slab with a source point - errors at several frequencies receiver in left homogeneous domain



### Key ideas

- The second-order asymptotic homogenization accounts for dispersive effects.
- Reciprocity identities between cell problems are a big help.
- Boundary and transmission conditions can be designed to complement the inner expansion. (including in 2-3D [Vinoles, 2016, Maurel and Marigo, 2018, Cakoni et al., 2019, Beneteau, 2021] ...)
- For transient waves, **stability** can be adressed using (i) hyperbolic formalism and (ii) enlarged interfaces (in 1D for now).
- Source points can be addressed using the same tools (specific to 1D).

### Perspectives

- Pursue the transient case up to *full second-order model* (as done in the time-harmonic case [Cornaggia and Guzina, 2020])
- Apply the built framework to other 1D configurations:
  - High-frequency homogenization [Craster et al., 2010, Guzina et al., 2019, Assier et al., 2020] Solids with inner imperfect interfaces [Assier et al., 2020] Non-linearities [Bellis et al., 2021]
- Reciprocity identities for higher dimensions and elasticity [Boutin and Auriault, 1993] (ongoing).
- Hyperbolic formalism for higher dimensions and other models ? (2D acoustics, elasticity ...)

# Thanks for your attention !

Second-order homogenization of boundary and transmission conditions for one-dimensional waves in periodic media Rémi Cornaggia, Bojan B. Guzina International Journal of Solids and Structures, 2020

An homogenized model accounting for dispersion, interfaces and source points for transient waves in 1D periodic media Rémi Cornaggia, Bruno Lombard ESAIM: Mathematical Modelling and Numerical Analysis (M2AN), 2023

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