

# Induced polarization of clay-rich materials. 2. The effect of anisotropy

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27 Abstract. We investigate the anisotropy in the complex conductivity of a clayrock formation 28 through both laboratory and in situ measurements. Laboratory measurements have been conducted 29 on four samples from two cores of the Callovo-Oxfordian formation from the Paris Basin (France). 30 This clay-rock formation is anisotropic with a well-defined bedding plane. Two of the cylindrical 31 core samples are taken in the transverse direction with respect to the bedding plane while two other 32 core samples are taken in the in-plane direction. The complex conductivity spectra are performed 33 in the frequency range 20 mHz to 45 kHz and in a broad pore water saturation range from near 34 saturation to a residual saturation of ~25%. The complex conductivity spectra are fitted with a 35 double Cole Cole model, the low-frequency contribution corresponding to induced polarization 36 effect while the high-frequency contribution is related to the Maxwell-Wagner polarization. The 37 six Cole Cole parameters are investigated as a function of saturation and we evaluate their degree 38 of anisotropy versus the effect of saturation. The low-frequency instantaneous conductivity and 39 normalized chargeability show a consistent degree of anisotropy with an anisotropy ratio equal to 40  $3.8\pm0.5$  for one core sample and  $6.5\pm0.9$  for the second core sample. These values represent a 41 substantial level of anisotropy. The low-frequency Cole Cole exponent and relaxation time do not 42 show substantial amount of anisotropy. The monitoring of the evolution of the weight in the 43 controlled humidity chamber seems to indicate that their relative permeabilities do not show a 44 strong anisotropic behavior. Finally, the laboratory data are discussed in the context of field data 45 obtained with an azimuthal array of 12 electrodes.

#### Introduction

Shale formations including clayrocks, mudstones, claystones, and argillites are low permeability formations that can be used for the geological storage of contaminants including nuclear wastes (Grambow et al., 2014). The development of an operating geological repository for highly radioactive wastes requires the development of research works dedicated to their long-term safety. In this context, the understanding of the properties of the clay formations in their ability to isolate radionuclides (especially most mobile radionuclides such as iodine-129 and chlorine 36) is of paramount importance.

55 Due to preferential orientation of minerals and finely laminated bedding planes, clay-rich 56 rocks are almost ubiquitously anisotropic in their macroscopic transport properties (Singh and 57 Sircar, 2014). This is especially true for their permeability (e.g., Ashworth and Doster, 2020), their 58 diffusion coefficients (e.g., Zhang et al., 2017) as well as for their mechanical properties (e.g., 59 Cheng, 1997; Coussy, 2003). In the case of the Collavo-Oxfordian clayrocks of the Paris Basin, 60 recent studies have demonstrated a weak anisotropy in their permeability and mechanical 51 properties (Giot et al., 2012, 2014).

62 Geophysical methods can be used to assess the anisotropy associated with the texture of 63 shales. Various studies have been dedicated to the anisotropy of the seismic velocities of rocks 64 (see for instance Zinszner et al., 2002; Yenugu, 2010; Singh and Sircar, 2014). The impact of the 65 fabric tensor on the electrical conductivity tensor has been investigated by Niu et al. (2017). 66 However, electrical conductivity tomography is difficult to interpret as a stand-alone alone 67 technique because the electrical conductivity of rocks depends on two contributions. These two 68 contributions are the bulk conductivity associated with the saline pore water located in the 69 interconnected pore space and the surface conductivity associated with conduction in the electrical

double layer and dependent on their Cation Exchange Capacity, CEC (e.g., Revil et al., 2019, and
references therein).

Induced polarization is a geophysical method that extend the electrical conductivity method by looking, in addition to conduction, at the low frequencies (<10 kHz) polarization of porous media. It is currently considered a hot topic in the realms of hydrogeophysics (e.g., Titov et al., 2002; Mwakanyamale et al., 2012; Revil et al., 2012; Kemna et al., 2012) and biogeophysics (e.g., Chen et al., 2009; Abdel Aal et al., 2010, Wainwright et al., 2016). In frequency-domain induced polarization, the conductivity tensor is replaced by a complex-conductivity tensor with components that are frequency-dependent (Revil et al., 2013).

79 Works dedicated to the study of the anisotropy of clay-rocks in terms of induced 80 polarization parameters are scarce. Zisser and Nover (2009) and Zisser et al. (2010a, b) presented 81 experimental data describing the polarization and anisotropy of tight (low-permeability) 82 sandstones. Revil et al. (2013) developed the first model describing the complex conductivity 83 tensor of transversely anisotropic clay-rocks and mudstones. Additional data were presented by 84 Woodruff et al. (2014, 2015) checking the validity of this model. The anisotropy of the complex 85 conductivity tensor of graphite-bearing rocks was also analyzed recently by Abdulsamad et al. 86 (2020). There is no paper investigating anisotropy of electrical conductivity and normalized 87 chargeability of clay-rocks presenting both laboratory and field data and a theoretical framework 88 to understand these data.

In the present paper, we analyze both laboratory and field low-frequency induced polarization properties of the Callovo-Oxfordian clayrock found in the Paris Basin (France). The anisotropy of this clayrock is analyzed both in the laboratory, at different degree of saturations, and in the in-situ condition of the underground laboratory operated by ANDRA in France (Paris Basin). Such data are critically needed to evaluate if the use of tomographic codes able to account
for anisotropy is needed or not in the context of the storage of radionucleides in the clayrock
formations.

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## Conductivity and normalized chargeability tensors

98 **Isotropic clayrocks** 

Electrical conductivity and normalized chargeability describe the ability of a rock to transfer electrical charges by conduction and to reversibly store electrical charges, respectively, both under the action of an applied electrical field. Revil (2013) developed a petrophysical model to describe the complex conductivity of clayey materials using a volume-average approach and the dynamic Stern layer concept. We consider below a partially saturated clay-rock at saturation  $s_w$ (dimensionless). For an isotropic clayrock, the instantaneous conductivity  $\sigma_{\infty}$  (in S m<sup>-1</sup>) of porous materials and the normalized chargeability  $M_n$  are given by,

106 
$$\sigma_{\infty}(s_w) = \frac{1}{F} s_w^n \sigma_w + s_w^{n-1} \left(\frac{1}{F\phi}\right) \rho_g B \text{CEC} , \qquad (1)$$

107 
$$M_n(s_w) = s_w^{n-1} \left(\frac{1}{F\phi}\right) \rho_g \lambda \text{CEC} , \qquad (2)$$

108 where  $\sigma_w$  (in S m<sup>-1</sup>) denotes the pore water conductivity,  $\rho_g$  denotes the mass density of the 109 grains (around 2700 kg m<sup>-3</sup>),  $n \ge 1$  is the saturation exponent (dimensionless, also called the second 110 Archie's exponent), and *F* (dimensionless) denotes the (intrinsic) formation factor. The formation 111 factor is related to the connected porosity  $\phi$  by Archie's equation  $F = \phi^{-m}$  where *m* (dimensionless) 112 denotes the porosity or first Archie's exponent. The CEC denotes Cation Exchange Capacity of 113 the material (expressed in C kg<sup>-1</sup> and often expressed in meq/100 g with 1 meq/100 g = 963.20 C

kg<sup>-1</sup>). It can be easily measured through titration experiments (e.g., Aran et al., 2008). A 114 115 dimensionless number R was introduced by Revil et al. (2017a, b, c) as  $R = \lambda / B$  where  $\lambda$  and B 116 are two apparent mobilities for polarization and conduction. From previous studies (e.g., Ghorbani et al., 2018), we have  $B(Na^+, 25^{\circ}C) = 3.1 \pm 0.3 \times 10^{-9} \text{ m}^2 \text{s}^{-1} \text{V}^{-1}$  and  $\lambda(Na^+, 25^{\circ}C) = 3.0 \pm 0.7 \times 10^{-10} \text{ m}^2 \text{s}^{-1}$ 117 <sup>1</sup>V<sup>-1</sup>. Both *B* and  $\lambda$  depends linearly with temperature at a rate of 2% per degree Celcius. Therefore 118 119  $R \approx 0.10 \pm 0.02$  (independent of saturation and temperature).

120 Another very useful relationship can be found between the quadrature conductivity at the geometric mean frequency of two frequencies  $f_1$  and  $f_2$  and the normalized chargeability. The 121 122 partial normalized chargeability is here defined as the difference between the in-phase conductivity 123 at the frequency  $f_2(>f_1)$  and the in-phase conductivity at the lower frequency  $f_1$ . This relationship 124 is given by (Van Voorhis et al., 1973; Revil et al., 2017a)

125 
$$\sigma''\left(\sqrt{f_1 f_2}\right) \approx -\frac{M_n(f_1, f_2)}{\alpha},\tag{3}$$

 $\alpha \approx \frac{2}{\pi} \ln A$ , 126 (4) 127

where A corresponds to the number of decades separating  $f_1$  and  $f_2$  (3 decades implies  $A = 10^3$ 128 129 and therefore  $\alpha \approx 4.4$ ). Equations (3) and (4) are independent of both the saturation state of the 130 material and temperature.

131 Finally, the permeability can be related to a mean pore size  $\Lambda$  and the formation factor F 132 by,

133 
$$k(s_w) \approx k_r(s_w) \frac{\Lambda^2}{8F},$$
 (5)

134 which can be considered as a generalized Kozeny-Carman equation (see Johnson et al. 1989 and 135 Revil et al. 2013). In Equation (5),  $k_r$  denotes the relative permeability of the rock and  $\Lambda$  is a 136 hydraulic pore radius. As discussed in Revil et al. (2023), the relative permeability is given by,

137 
$$k_r(s_w) = \left(\frac{s_w - s_w^i}{1 - s_w^i}\right)^{n+2},$$
 (6)

138 where  $s_w^i$  (dimensionless) is the irreducible water saturation.

139

#### 140 Complex conductivity: anisotropic case

All the anisotropy of the complex conductivity is associated with the anisotropy of the tortuosity tensor. Since porosity is a scalar, this means that the formation factor is a second-order symmetric tensor. The other quantities in the complex conductivity equations do not depend on the anisotropy of the material. A simple generalization of the above expressions to anisotropic media yields the following expression for the instantaneous conductivity tensor:

146 
$$\boldsymbol{\sigma}_{\infty} = \boldsymbol{\sigma}_{ij}^{\infty} \mathbf{X}_{i} \otimes \mathbf{X}_{j}, \qquad (7)$$

147 
$$\sigma_{ij}^{\infty} \approx F_{ij} \left( s_w^{\ n} \sigma_w + \frac{1}{\phi} s_w^{\ n-1} \rho_g B \text{CEC} \right), \tag{8}$$

148 where  $\mathbf{x}_i$  (i = 1, 2, 3) denote the basis vectors of the Cartesian frame of reference ( $\mathbf{x}_i \cdot \mathbf{x}_j = \delta_{ij}$ 149 where  $\delta_{ij}$  denotes the Kronecker delta),  $\mathbf{a} \otimes \mathbf{b}$  represents the tensorial product between vectors 150  $\mathbf{a}$  and  $\mathbf{b}$ . The formation tensor is given by  $\mathbf{F} = F_{ij}\mathbf{x}_i \otimes \mathbf{x}_j$ , where  $F_{ij}$  denotes the components of 151 the (symmetric second-rank) formation factor tensor for the conductivity, that we write as  $\mathbf{F}$ . In 152 the isotropic case  $F_{ij} = (1/F)\delta_{ij}$  with F the intrinsic formation factor. This model also assumes 153 that the saturation exponent remains more or less the same in the eigendirections and that the pore sizes are also the same in the eigenvector directions as discussed in the previous paper of this series. We will see later that these assumptions agree well with the experimental data but they should be considered as a simplifications. The tortuosity tensor is simply the formation factor tensors divided by the porosity  $\mathbf{T} = \tau_{ij} \mathbf{x}_i \otimes \mathbf{x}_j$  and  $\tau_{ij} = F_{ij} / \phi$ . The inverse of its component corresponds to the tortuosity of the current flow path in a given direction. Tortuosity is a quantitative measure of the effect of the deviation of the current streamlines from straight (not tortuous) paths in an electrolyte to tortuous paths in a complex porous body.

161 Neglecting the presence of pyrite, the normalized chargeability tensor can be written as

162 
$$\mathbf{M}_n = \boldsymbol{M}_{ij}^n \mathbf{x}_i \otimes \mathbf{x}_j, \qquad (8)$$

163 
$$M_{ij}^{n} \approx F_{ij} \frac{1}{\phi} s_{w}^{n-1} \rho_{g} \lambda \text{CEC} .$$
 (9)

164 Finally, equation (3) would be preserved for the anistropic case and the relationship between the165 quadrature conductivity component and the normalized chargeability components would be,

166 
$$\sigma_{ij}"\left(\sqrt{f_1 f_2}\right) \approx -\frac{M_{ij}^n(f_1, f_2)}{\alpha}, \qquad (10)$$

167 where  $\alpha$  is the same whatever the directions and given by equation (4).

In the context of the COx formation, we consider that unfractured COx core samples characterized by a bedding plane. The two eigenvectors along the bedding plane correspond to the in-plane direction (index i) while the normal direction is called the transverse direction (index t). If the function EV extracts the eigenvalues of a given tensor, then we have  $EV(\sigma_{\infty}) = (\sigma_i, \sigma_i, \sigma_i)$ and  $EV(\mathbf{M}_n) = (M_i^n, M_i^n, M_i^n)$ . The electrical anisotropy ratio is then defined as  $\lambda_e = \sigma_i / \sigma_i = M_i^n / M_i^n$ . Consequently, the electrical anisotropy ratio should be the same for the conductivity and the normalized chargeability, i.e., for conduction and polarization processes, which is an important feature of our model. This heuristic prediction can be easily tested withrespect to laboratory data.

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#### 178 **Permeability tensor**

Another question is to know if the relative permeability is just a function of saturation and if the effect of the bedding can be neglected. In other word, we write the permeability of the COx as

$$\mathbf{k}(s_w) = k_r(s_w)\mathbf{k}_s = k_r(s_w)k_{ij}\mathbf{x}_i \otimes \mathbf{x}_j, \qquad (11)$$

183 where  $\mathbf{k}_{s}$  denotes the permeability tensor at saturation with components  $k_{ij}$  and  $k_{r}(s_{w})$  is the 184 relative permeability function already defined above (equation 6), and  $s_{w}^{i} \approx 0.35 \pm 0.05$  denotes 185 the irreducible water saturation for the COx as obtained in the previous paper of this series (Revil 186 et al., 2023).

Assuming that the COx clayrock is characterized by a bedding plane, the eigenvalues of the permeability tensor are  $EV(\mathbf{k}_s) = (k_i, k_i, k_t)$  and the hydraulic anisotropy ratio is defined as  $\lambda_h = k_i / k_t$ . Then, one of the key questions we want to answer is to know if (and how) the electrical and hydraulic anisotropy ratios are related to each other. If we examine equation 5 and if we consider that the pore sizes are the same in the eigenvectors' directions, then we should expect  $\lambda_e \approx \lambda_h$  since  $k_{ii} = (\Lambda^2 / 8)F_{ii}$ .

193

### **Experiments and results**

194 Material and method

The Callovo-Oxfordian (COx) clayrock formation of the Paris Basin is mainly composed by clay minerals (20 to 55%, illite, micas, interstratified illite/smectite, kaoline and chlorite), silica (25 to 35%), calcite (15 to 30%) and secondary minerals (less than 5% of the total) including feldspar, dolomite, hematite and small proportions of pyrite (see Yven et al., 2007, Vinsot et al., 2014, see Paper 1). The Callovo-Oxfordian formation is weakly anisotropic due to a bedding plane (Figure 1) and the presence of small proportion of pyrite (Figure 2).

201 We consider in the experimental study 2 cores labelled EST59674 and EST59676, 202 respectively. Two samples are drilled in the direction along the bedding and two other samples 203 normal to the bedding plane. So we consider 4 samples in total. The physical properties of these 204 samples are summarized in Table 1. Frequency-domain complex conductivity measurements are 205 performed using the ZELSIP04-V02 impedance meter (Zimmermann et al., 2008) already used in 206 the previous paper of this series. The frequency range investigated is 20 mHz-45 kHz. The 207 measurements are made in a desiccation chamber in which the relative humidity is imposed as 208 described in the previous paper of this series (see Figures 3 and 4). The relative humidity is 209 imposed by using specific salts.

210 The measured complex conductivity spectra are shown in Figures 5 and 6. We use a 211 Bayesian technique to invert the Cole Cole parameters (Appendix A). The Cole Cole parameters 212 are collected in Tables 2 and 3 for the core sample EST59674 and in Tables 4 and 5 for the core 213 sample EST59676. We observe that both the amplitude of the conductivity and quadrature 214 conductivity decrease with the saturation. For these experiments, we use exactly the same 215 experimental protocol and sample holder as in Revil et al. (2017a) so the details of the experiments 216 will not be repeated here (see also Revil et al., 2023). The complex conductivity spectra are fitted 217 with a double Cole Cole model (see Appendix A). Fits of the complex conductivity spectra are

shown in Figures 5 and 6. The double Cole Cole model is clearly able to reproduce theexperimental data up to 10 kHz.

The permeability of COx samples to water at full saturation was assessed with the pulse decay method (Brace et al., 1968). This method allows determining both the intrinsic permeability  $k \text{ (m}^2)$  and the specific storage coefficient *Ss* (m<sup>-1</sup>) of low permeability materials. Initially, the sample is water-saturated and the fluid pressure inside the sample and the reservoirs is at equilibrium. A rapid increment of the fluid pressure (pulse) is imposed at the upstream reservoir, which create a one-dimensional flow through the saturated porous sample. The fluid pressure obeys a diffusion equation written as

227 
$$\frac{\partial^2 p}{\partial x^2} - \frac{S_s \mu_w}{k \gamma_w} \frac{\partial p}{\partial t} = 0, \qquad (12)$$

228 where p denotes the fluid pressure in the core sample of length L and for  $0 \le x \le L$ , x (m) is the 229 distance along the sample (x = 0: downstream face; x = L: upstream face),  $\gamma_w$  denotes the specific weight of the water (kg.m<sup>-2</sup>.s<sup>-2</sup>), and submitted to specific pressure boundary conditions. Classical 230 231 solutions have been proposed in the literature assuming uncoupled hydraulic and mechanical 232 behaviors (e.g., Hsieh et al., 1981). In the context of poroelasticity, Homand et al. (2004) proposed 233 an analytical solution for the hydromechanical problem assuming the skeleton of the porous 234 sample is elastic. We implemented this analytical solution in (Wolfram) Mathematica<sup>©</sup>) and using 235 an inverse method (based on Levenberg-Marquardt algorithm) we fit the pulse test data to obtain 236 the value of the permeability and specific storage. As a side note, Giot et al. (2011) proposed a 237 fully coupled analysis of the pulse test experiment through finite element modelling in 3D. An 238 inversion algorithm for the identification of the poromechanical parameters was also proposed in 239 this paper. By applying this complete solution on the COx claystone/clayrock, Giot et al. (2011)

found that the difference in estimating the intrinsic permeability between the two approaches was less than 15%. Since the 1D analysis gives good results, it was chosen in this study for the sake of simplicity.

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#### 244 Anisotropy of the electrical conductivity

The anisotropy of the instantaneous conductivity is shown in Figure 7. There is a clear anisotropy with a higher electrical conductivity along the bedding plane than with respect to conductivity in the normal direction to the bedding plane. This observation is consistent with our expectation that the bedding plane is more conductive with respect to the transverse direction. The obtained electrical conductivity anisotropy ratios are  $4.3\pm1.0$  and  $6.0\pm1.4$  for the cores EST59674 and EST59676, respectively. At the opposite, the saturation exponents are nearly the same in the in-plane and transverse directions. We obtain  $n = 3.2\pm0.3$  validating the assumption made above.

252

#### 253 Anisotropy of the normalized chargeability

254 The anisotropy of the (low-frequency) normalized chargeability is shown in Figure 8. The 255 normalized chargeability displays a clear anisotropy ratio with a higher normalized chargeability 256 in the bedding plane by comparison with the transverse direction. The normalized chargeability 257 anisotropy ratios are 3.1±0.7 and 7.0±1.0 for the cores EST59674 and EST59676, respectively. 258 These values are fairly consistent with the values obtained from the instantaneous conductivity 259 data ( $4.3\pm1.0$  and  $6.0\pm1.4$ ). The saturation exponent obtained from the normalized chargeability 260 data is also fairly consistent in the in-plane and transverse directions ( $n = 3.7 \pm 0.3$ ). Therefore the 261 value of the saturation exponent and the amplitude of the anistropy ratio are consistent between

the electrical conductivity and the normalized chargeability, which observations are in agreementwith the predictions of our model.

264

### 265 Anisotropy of the residual saturation

The residual saturation ( $s_w^i \approx 0.36 \pm 0.05$ ) is consistent with that obtained in the previous paper of this series. It is also the same for the instantaneous conductivity and the normalized chargeability and is independent of the direction of the core sample.

269

### 270 Anisotropy of the permeability

271 The COx clay rock shows anisotropy in its permeability (Giot et al., 2014). Mohajerani et 272 al. (2011) obtained a permeability for the COx of  $2.0 \times 10^{-21}$  m<sup>2</sup> along the bedding plane and 0.6  $\times 10^{-21}$  m<sup>2</sup> in the transverse direction. This yields a hydraulic anisotropic ratio  $\lambda_h = 3.3$ . Menaceur 273 et al. (2015) and Harrington et al. (2017) found permeabilities in the bedding plane of 9 -  $29 \times 10^{-21}$ 274 m<sup>2</sup> and in the range 4.5 - 7.0  $\times 10^{-21}$  m<sup>2</sup> in the transverse direction. These correspond to anisotropy 275 ratio  $\lambda_h$  in the range 2 to 4. Armand et al. (2017) obtained values of permeability of 3.0 and 6.0 276  $\times 10^{-20}$  m<sup>2</sup> for perpendicular and parallel directions to the bedding plane, respectively. This yields 277 again in an anisotropy ratio  $\lambda_h = 2.0$ . So the anisotropy of the permeability tensor is not very high. 278 279 The results of the permeability tests for our core samples are reported in Table 1 and are consistent with the estimates discussed above with estimate of  $\lambda_h$  in the range 1.9 to 3.7. In Figure 280

9, we plot the hydraulic anisotropy ratio of the two cores as a function of the electrical anisotropy ratio. We also add estimates from the literature. The data are fairly consistent with  $\lambda_e \approx \lambda_h$  and therefore also consistent with the findings of Maineult et al. (2018) on pore network simulations. In other words, the anisotropy of the induced polarization properties and permeabilities are related to an anisotropy of the tortuosity paths rather than a possible anisotropy in the pore sizes.

The previous argument can be checked independently. The low-frequency Cole Cole exponent described the broadness of the relaxation times for induced polarization. These relation times can be related to the pore sizes as discussed in Tartrat et al. (2019). Figure 10 shows that the (low-frequency) Cole Cole exponent  $c_1$  is independent of the direction indicating that the broadness of the relaxation times is the same in the bedding plane and normal to the bedding plane (Figure 11).

292 The next point to check is the validity of equation (11). In other words, can be separate the 293 permeability tensor at a given saturation as the product of a scalar function depending only on the 294 saturation and a permeability tensor at saturation. In order to reply to this question, we closely look 295 at the desaturation curves shown in Figure 2. In Figures 12 and 13, we look at the relaxation of the 296 mass of the core samples when the relative humidity is changed in the humidity chamber. We 297 observe that the relaxation times are nearly independent of the direction, which may indicate that 298 the relative permeability function can be considered as a scalar in first approximation. This is consistent with the fact that we have already demonstrated that n and  $s_w^i$  are independent of the 299 300 direction with respect to the bedding plane.

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### Field test

303 An experiment was carried out at the ANDRA Underground Research Laboratory (URL) 304 located near Bure in France (see Figure 14a., Armand et al., 2014). This URL is dedicated to 305 digging activities, technological demonstrations and scientific experiments for the design of the 306 geological disposal facility for radioactive waste. is The experimental galleries are located in the 307 COx formation at a depth of ~500m. We performed azimuthal measurements to characterize the 308 anisotropy of both the conductivity and normalized chargeability in the COx formation at Bure 309 inside the galleries of the URL. Four boreholes with a length of 22 m were drilling from the main 310 gallery. Figure 14b. shows a sketch of the position of each borehole from the main gallery.

311 For each borehole (labeled AHA1612 to AHA1615), two rings of electrodes allowing to 312 measure the anisotropy of the complex resistivity are installed at 17.9 and 18.2 meters from the 313 gallery wall. Each device therefore contains two ring composed by twelves stainless steel 314 electrodes (Figure 14c). The 10 mm-diameter electrodes are placed in a plastic cylinder of external 315 diameter 121 mm and spaced 30 degrees apart (Figure 14d). Each electrode ring is wired with a 316 multi-pair shielded cable. The purpose of this connection is to isolate each electrode by the 317 shielding of the pair and thus and therefore limit the effects of induction from one conductor to the 318 other. Resin coats all the cable and electrode connections. The device is finally placed inside the 319 borehole as close as possible to the inner walls (131 mm diameter), leaving a spacing of 320 approximately 5 mm. Indeed, the positioning of the rings is ensured by the use of benders. To 321 ensure electrical contact with the electrode and COx formation, the probes were sealed after 322 installation with a conductive bentonite cement grout.

The measurements were carried out using the SYSCAL Pro Impedance meter using a dipole–dipole array. The SYSCAL PRO include the current injection system, the potential difference measurement system, as well as a multiplexer allowing the acquisition of injection/measurement sequences programmed beforehand. The system also includes a stabilized and decoupled power supply, as well as a computer allowing the repetition over time of the measurement sequences, the remote control of the system and the storage of data. In this field experiment, the contact resistances were comprised between 4 to 10 k $\Omega$  and the injected current varies from 200 to 500 mA. The measurements are presented using radial figures. This is a representation of the conductivity and normalized chargeability measurements as a function of the orientation of the center of the quadrupole on the measurement ring.

333 For each ring, twelves measurement were carried out. Measurement 1 corresponds to the 334 measurement between electrodes 1-2-3-4 (45° azimuthal correspondence). Here the injection of 335 the current is carried out between electrodes 1 and 2 and the potential is measured between the 336 electrodes 3 and 4. Measurement 2 corresponds to the measurement between electrodes 2-3-4-5 337 (75° azimuthal correspondence) and so on until last measurement between electrodes 12-1-2-3 338 (15° azimuthal correspondence). Figure 15a., b., c. show the resistivity diagrams obtained on one 339 ring for this configuration acquired respectively for the rings 1, 4, 5 inside borehole 1612, 1613 340 and 1614. That said, since the rings behave differently in different boreholes, this indicates that 341 the effect of the heterogeneity associated with damage around the wells is important. As a first 342 approximation, we see that the diagrams show a marked anisotropic behavior with apparent conductivities on the order of 0.14 S m<sup>-1</sup> in the horizontal direction and around 0.08 S m<sup>-1</sup> in the 343 344 vertical direction as determined from the apparent resistivities. These values are fairly consistent with the conductivity data obtained in the laboratory experiments presented above (see also Figure 345 346 7). The different may be explained through the existence of cracks associated with damage of the 347 COx formation around the boreholes.

Figures 15d.e.f show the chargeability diagrams obtained on one ring for the same configuration as the electrical measurements and acquired respectively for the ring 1, 4, 5 inside borehole 1612, 1613 and 1614, respectively. The chargeability data is noisy because the EM noise is high in the underground laboratory. As electrical resistivity, the anisotropy highlight the effect of the heterogeneity associated with damage around the borehole. The shape of chargeability diagram is quite similar than the resistivity diagram. The diagram highlights a marked anisotropic behavior with apparent chargeability on the order of 15 mV/V in the horizontal direction and around 25 mV/V in the vertical direction. Figure 16a shows the mean chargeability of the 8 rings. This is expected since chargeability is a ratio between the normalized chargeability and the conductivity, which share the same eigenvectors and the same ratio of the eigenvalues. This is consistent with the laboratory data shown in Figure 16b.

359

## Conclusion

360 We have measured the complex conductivity spectra of two core samples from the Callovo-361 Oxfordian (COx) formation of the Paris Basin in the frequency range 20 mHz to 45 kHz. The 362 spectra were fitted with a double Cole Cole model with one contribution associated with the 363 polarization of the electrical double layer and a second polarization associated with the Maxwell-364 Wagner (interfacial) polarization. The measured were both performed in the direction and normal 365 to the bedding plane of the core samples. The two core samples exhibit a clear anisotropy in their 366 instantaneous conductivity and normalized chargeability. The instantaneous conductivity and 367 normalized chargeability of the first core sample exhibit an anisotropy ratio of 3.8±0.5 while the 368 second core sample is characterized by an anisotropy ratio of  $6.5\pm0.9$  in the saturation range 0.36 369 to 0.97. The Cole Cole exponent and the low-frequency Cole Cole relaxation times are independent 370 of the direction. The anisotropy ratio obtained from the electrical conductivity and normalized 371 chargeability can be related to the anisotropy ratio of the permeability. This indicates in turn that 372 the pore sizes do no depend on the direction in the COx formation. The saturation exponent and 373 the residual water saturation are found to be independent of the direction. This is consistent with the observation that the relative permeability is also independent of the direction with respect to the bedding plane. Finally, a field experiment is carried out to check the anisotropy of the conductivity and normalized chargeability directly in the COx formation at a depth of 500 m.

377

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## 512 Appendix A. Double Cole Cole parametric model

513 In each eigenvector direction, the complex conductivity data is fitted with a double Cole 514 Cole parametric model for which the low frequency polarization is labelled 1 while the higher 515 frequency polarization is labeled 2:

516 
$$\sigma^* = \sigma_{\infty} \left( 1 - \frac{M_1}{1 + (i\omega\tau_1)^{c_1}} - \frac{M_2}{1 + (i\omega\tau_2)^{c_2}} \right).$$
(A1)

517 where  $M_1$  and  $M_2$  (dimensionless)denote the chargeabilities,  $c_1$  and  $c_2$  (dimensionless) are the two 518 Cole-Cole exponents, and  $\tau_1$  and  $\tau_2$  are the (relaxation) time constants (in s). We consider that the 519 low-frequency contribution is the one associated with induced polarization.

We use a Monte Carlo Markov Chain (MCMC) sampling algorithm and a Bayesian approach (Mosegaard and Tarantola, 1995) to invert the in-phase and quadrature conductivity spectra shown in Figures 5 and 6. The model vector contained a form of the Cole Cole parameters is  $\mathbf{m} = [\log(\sigma_0); M_1; c_1; \log(\tau_1); M_2; c_2; \log(\tau_2)]$ . Then, the algorithm combines this information with the observed data vector and with the information provided by the double Cole-Cole model to obtain optimal realization of the model vectors. The Root Mean Square (RMS) error is given on the MCMC chain has converged as:

527 
$$\operatorname{RMS}^{2} = \frac{1}{N} \sum_{i=1}^{N} \left( \frac{g^{i}(\mathbf{m}) - d_{obs}^{i}}{d_{obs}^{i}} \right)^{2}, \qquad (A2)$$

where  $g(\mathbf{m})$  denotes the predicted in-phase or quadrature conductivity spectra and *N* denotes the number of data used in the fitting process. The fit are shown in Figures 5 and 6.

531

**Table 1.** Characteristics of four core samples investigated in the present study. CEC denotes the Cation Exchange Capacity, which is expressed here in meq/100 g (= 963.20 C kg<sup>-1</sup>). The porosity was computed by measuring the weight of the saturated and dry core samples and their volume. The permeability appears also anisotropic with a permeability anisotropic ratio  $\lambda_k = 1.06$  for the core EST59676 (electrical anisotropy ratio 6.5±0.9) and  $\lambda_k = 1.9$  for core EST59674 (electrical anisotropy ratio 2.0±0.2).  $\varphi_m$  denotes the volume fraction of pyrite from X-ray tomography. The grain density of the core samples is 2710 kg m<sup>-3</sup>.

| 5 | 4 | 0 |
|---|---|---|
|   |   |   |

| Sample      | Direction  | Porosity  | CEC         | BET         | k                      | $\varphi_m(-)$ |
|-------------|------------|-----------|-------------|-------------|------------------------|----------------|
|             |            | $\phi(-)$ | (meq/100 g) | $(m^{2}/g)$ | (m <sup>2</sup> )      |                |
| EST59676 42 | In-plane   | 0.122     | 16.83       | 29.95       | 1.31×10 <sup>-20</sup> | 0.25           |
| EST59676 41 | Transverse | 0.126     | 16.83       | 29.95       | 1.24×10 <sup>-20</sup> | 0.38           |
| EST59674 42 | In-Plane   | 0.130     | 16.97       | 30.46       | 2.93×10 <sup>-20</sup> | 0.29           |
| EST59674 41 | Transverse | 0.148     | 16.97       | 30.46       | 1.45×10 <sup>-20</sup> | 0.22           |

541

542

Table 2. Inversion of the Cole Cole parameters for the core sample EST59674-41 (tranverse
 direction). Index 1 is used for the low frequency contribution which is associated with the induced
 polarization contribution.

| Sw    | TI(S)    | 72(S)    | <i>c</i> <sub>1</sub> (-) | <i>c</i> <sub>2</sub> (-) | <i>M</i> <sub>1</sub> (-) | $M_{2}(-)$ | $\sigma_{\infty}$ (S/m) | RMS<br>(%) |
|-------|----------|----------|---------------------------|---------------------------|---------------------------|------------|-------------------------|------------|
| 0.965 | 0.00859  | 1.52e-05 | 0.550                     | 0.541                     | 0.0459                    | 0.0647     | 0.0321                  | 0.246      |
| 0.965 | 0.00670  | 4.34e-06 | 0.461                     | 0.456                     | 0.0260                    | 0.0859     | 0.0321                  | 0.240      |
| 0.781 | 0.0127   | 8.48e-07 | 0.465                     | 0.548                     | 0.0293                    | 0.214      | 0.0202                  | 0.574      |
| 0.781 | 0.0135   | 1.43e-06 | 0.501                     | 0.567                     | 0.0145                    | 0.267      | 0.0157                  | 0.212      |
| 0.768 | 0.00595  | 1.79e-06 | 0.450                     | 0.559                     | 0.0200                    | 0.186      | 0.0107                  | 0.152      |
| 0.723 | 0.00611  | 4.72e-06 | 0.462                     | 0.607                     | 0.0252                    | 0.129      | 0.0110                  | 0.276      |
| 0.691 | 0.00960  | 2.75e-06 | 0.453                     | 0.576                     | 0.0232                    | 0.175      | 0.0111                  | 0.350      |
| 0.691 | 0.0115   | 1.66e-06 | 0.483                     | 0.540                     | 0.0207                    | 0.204      | 0.0115                  | 0.333      |
| 0.675 | 0.0140   | 2.78e-06 | 0.501                     | 0.547                     | 0.0204                    | 0.184      | 0.0102                  | 0.271      |
| 0.675 | 0.0148   | 5.31e-06 | 0.518                     | 0.545                     | 0.0189                    | 0.142      | 0.0107                  | 0.173      |
| 0.666 | 0.00564  | 4.52e-06 | 0.424                     | 0.599                     | 0.0257                    | 0.160      | 0.00887                 | 0.112      |
| 0.661 | 0.00422  | 4.00e-06 | 0.422                     | 0.603                     | 0.0271                    | 0.170      | 0.00858                 | 0.111      |
| 0.654 | 0.00279  | 1.44e-06 | 0.399                     | 0.533                     | 0.0228                    | 0.221      | 0.00926                 | 0.102      |
| 0.642 | 0.00585  | 4.07e-06 | 0.458                     | 0.551                     | 0.0211                    | 0.160      | 0.00852                 | 0.143      |
| 0.642 | 0.00186  | 3.78e-06 | 0.405                     | 0.588                     | 0.0273                    | 0.156      | 0.00904                 | 0.126      |
| 0.630 | 0.00150  | 3.70e-06 | 0.381                     | 0.595                     | 0.0287                    | 0.160      | 0.00866                 | 0.101      |
| 0.615 | 0.00221  | 1.76e-06 | 0.388                     | 0.560                     | 0.0242                    | 0.212      | 0.00906                 | 0.139      |
| 0.604 | 0.000844 | 2.08e-06 | 0.361                     | 0.582                     | 0.0310                    | 0.185      | 0.00902                 | 0.0885     |
| 0.592 | 0.000937 | 1.11e-06 | 0.385                     | 0.559                     | 0.0262                    | 0.221      | 0.0111                  | 0.165      |
| 0.582 | 0.00167  | 1.58e-06 | 0.404                     | 0.562                     | 0.0235                    | 0.214      | 0.00909                 | 0.0931     |
| 0.541 | 0.00205  | 3.14e-06 | 0.415                     | 0.600                     | 0.0296                    | 0.188      | 0.00730                 | 0.102      |
| 0.489 | 0.00234  | 3.62e-06 | 0.432                     | 0.623                     | 0.0345                    | 0.214      | 0.00570                 | 0.154      |
| 0.461 | 0.00228  | 9.32e-06 | 0.471                     | 0.708                     | 0.0406                    | 0.169      | 0.00444                 | 0.199      |
| 0.394 | 0.00303  | 4.16e-06 | 0.459                     | 0.620                     | 0.0343                    | 0.310      | 0.00281                 | 0.171      |
| 0.394 | 0.00294  | 3.94e-06 | 0.445                     | 0.626                     | 0.0353                    | 0.319      | 0.00282                 | 0.173      |
| 0.358 | 0.00123  | 3.64e-06 | 0.430                     | 0.655                     | 0.0519                    | 0.294      | 0.00292                 | 0.0944     |
| 0.329 | 0.00148  | 5.10e-06 | 0.430                     | 0.687                     | 0.0596                    | 0.293      | 0.00221                 | 0.132      |
| 0.314 | 0.00204  | 2.90e-06 | 0.432                     | 0.655                     | 0.0525                    | 0.382      | 0.00214                 | 0.150      |
| 0.296 | 0.00252  | 5.20e-06 | 0.428                     | 0.680                     | 0.0589                    | 0.353      | 0.00165                 | 0.157      |
| 0.286 | 0.00135  | 5.78e-06 | 0.401                     | 0.726                     | 0.0748                    | 0.346      | 0.00149                 | 0.182      |
| 0.274 | 0.00107  | 4.33e-06 | 0.385                     | 0.729                     | 0.0757                    | 0.406      | 0.00141                 | 0.172      |
| 0.266 | 0.000781 | 5.16e-06 | 0.365                     | 0.755                     | 0.0841                    | 0.406      | 0.00122                 | 0.241      |
| 0.257 | 0.00216  | 5.93e-06 | 0.408                     | 0.710                     | 0.0699                    | 0.433      | 0.000975                | 0.262      |
| 0.253 | 0.00194  | 5.98e-06 | 0.406                     | 0.738                     | 0.0727                    | 0.471      | 0.000816                | 0.313      |
| 0.249 | 0.000848 | 9.22e-06 | 0.383                     | 0.817                     | 0.101                     | 0.407      | 0.000717                | 0.274      |
| 0.246 | 0.000719 | 7.96e-06 | 0.352                     | 0.784                     | 0.0964                    | 0.446      | 0.000705                | 0.243      |
| 0.242 | 0.000469 | 9.38e-06 | 0.332                     | 0.802                     | 0.111                     | 0.413      | 0.000674                | 0.326      |
| 0.239 | 0.000738 | 7.23e-06 | 0.356                     | 0.751                     | 0.0929                    | 0.466      | 0.000674                | 0.259      |
| 0.235 | 0.000855 | 8.14e-06 | 0.355                     | 0.787                     | 0.0909                    | 0.467      | 0.000655                | 0.277      |
| 0.230 | 0.000887 | 7.95e-06 | 0.350                     | 0.768                     | 0.0876                    | 0.489      | 0.000620                | 0.292      |
| 0.230 | 0.000442 | 1.15e-05 | 0.383                     | 0.825                     | 0.106                     | 0.345      | 0.000752                | 0.255      |

Table 3. Inversion of the Cole Cole parameters for the core sample EST59674-42 (in-plane
direction along the bedding plane). Index 1 is used for the low frequency contribution which is
associated with the induced polarization contribution.

| G              | $\tau_1(s)$       | 72(S)                | <i>c</i> <sub>1</sub> (-) | <i>c</i> <sub>2</sub> (-) | $M_{1}(-)$       | <i>M</i> <sub>2</sub> (-) | $\sigma_{\infty}(S/m)$ | RMS            |
|----------------|-------------------|----------------------|---------------------------|---------------------------|------------------|---------------------------|------------------------|----------------|
| Sw             |                   |                      |                           |                           |                  |                           |                        | (%)            |
| 0.967          | 0.0214            | 4.43e-05             | 0.688                     | 0.471                     | 0.0237           | 0.0493                    | 0.0975                 | 0.624          |
| 0.967          | 0.00990           | 1.22e-05             | 0.535                     | 0.533                     | 0.0206           | 0.0510                    | 0.0971                 | 0.194          |
| 0.780          | 0.0360            | 6.18e-06             | 0.577                     | 0.445                     | 0.0150           | 0.0956                    | 0.0654                 | 0.276          |
| 0.763          | 0.0169            | 3.06e-06             | 0.477                     | 0.454                     | 0.0138           | 0.110                     | 0.0666                 | 0.105          |
| 0.722          | 0.0414            | 8.35e-06             | 0.481                     | 0.511                     | 0.0173           | 0.0893                    | 0.0606                 | 0.188          |
| 0.694          | 0.0317            | 4.70e-06             | 0.524                     | 0.446                     | 0.0139           | 0.113                     | 0.0565                 | 0.296          |
| 0.678          | 0.0429            | 6.88e-06             | 0.466                     | 0.497                     | 0.0241           | 0.102                     | 0.0532                 | 0.237          |
| 0.678          | 0.0201            | 7.06e-06             | 0.490                     | 0.483                     | 0.0121           | 0.101                     | 0.0501                 | 0.177          |
| 0.669          | 0.0137            | 9.93e-06             | 0.444                     | 0.527                     | 0.0172           | 0.101                     | 0.0402                 | 0.162          |
| 0.664          | 0.0229            | 7.14e-06             | 0.517                     | 0.470                     | 0.0122           | 0.122                     | 0.0385                 | 0.252          |
| 0.664          | 0.00598           | 9.36e-06             | 0.439                     | 0.549                     | 0.0196           | 0.0964                    | 0.0392                 | 0.156          |
| 0.657          | 0.00828           | 1.06e-05             | 0.459                     | 0.533                     | 0.0187           | 0.0976                    | 0.0364                 | 0.126          |
| 0.645          | 0.00920           | 4.06e-06             | 0.465                     | 0.468                     | 0.0167           | 0.127                     | 0.0383                 | 0.104          |
| 0.645          | 0.00354           | 2.47e-06             | 0.386                     | 0.454                     | 0.0152           | 0.140                     | 0.0459                 | 0.0818         |
| 0.632          | 0.00985           | 5.34e-06             | 0.458                     | 0.478                     | 0.0119           | 0.120                     | 0.0443                 | 0.173          |
| 0.617          | 0.00141           | 3.57e-06             | 0.357                     | 0.529                     | 0.0259           | 0.113                     | 0.0472                 | 0.100          |
| 0.617          | 0.00583           | 1.43e-05             | 0.469                     | 0.583                     | 0.0204           | 0.0815                    | 0.0384                 | 0.238          |
| 0.599          | 0.00533           | 5.17e-06             | 0.427                     | 0.496                     | 0.0177           | 0.112                     | 0.0400                 | 0.107          |
| 0.587          | 0.00221           | 1.48e-06             | 0.347                     | 0.428                     | 0.0182           | 0.155                     | 0.0458                 | 0.188          |
| 0.587          | 0.000530          | 8.06e-06             | 0.353                     | 0.584                     | 0.0284           | 0.0808                    | 0.0545                 | 0.130          |
| 0.577          | 0.00828           | 2.16e-06             | 0.421                     | 0.429                     | 0.0105           | 0.156                     | 0.0488                 | 0.0897         |
| 0.541          | 0.00423           | 7.32e-06             | 0.421                     | 0.539                     | 0.0217           | 0.112                     | 0.0369                 | 0.0855         |
| 0.495          | 0.00966           | 8.22e-06             | 0.492                     | 0.516                     | 0.0188           | 0.132                     | 0.0305                 | 0.170          |
| 0.483          | 0.00948           | 1.48e-05             | 0.508                     | 0.567                     | 0.0212           | 0.118                     | 0.0269                 | 0.271          |
| 0.468          | 0.0248            | 1.25e-05             | 0.539                     | 0.510                     | 0.0149           | 0.137                     | 0.0266                 | 0.258          |
| 0.451          | 0.00918           | 9.74e-06             | 0.520                     | 0.504                     | 0.0177           | 0.148                     | 0.0247                 | 0.188          |
| 0.441          | 0.00248           | 8.05e-06             | 0.438                     | 0.553                     | 0.0277           | 0.144                     | 0.0232                 | 0.125          |
| 0.429          | 0.00453           | 6.05e-06             | 0.425                     | 0.493                     | 0.0210           | 0.169                     | 0.0218                 | 0.144          |
| 0.394          | 0.00679           | 1.12e-05             | 0.541                     | 0.529                     | 0.0196           | 0.169                     | 0.0139                 | 0.237          |
| 0.364          | 0.00608           | 1.40e-05             | 0.542                     | 0.560                     | 0.0245           | 0.166                     | 0.0109                 | 0.218          |
| 0.340          | 0.00519           | 1.56e-05             | 0.533                     | 0.591                     | 0.0308           | 0.165                     | 0.00919                | 0.250          |
| 0.326          | 0.00655           | 1.39e-05             | 0.544                     | 0.549                     | 0.0268           | 0.185                     | 0.00878                | 0.264          |
| 0.310          | 0.00657           | 1.83e-05             | 0.557                     | 0.601                     | 0.0323           | 0.174                     | 0.00760                | 0.397          |
| 0.300          | 0.0173            | 1.53e-05             | 0.625                     | 0.511                     | 0.0191           | 0.210                     | 0.00741                | 0.352          |
| 0.288          | 0.0140            | 1.16e-05             | 0.641                     | 0.510                     | 0.0199           | 0.234<br>0.242            | 0.00691                | 0.430          |
| 0.281          | 0.0132            | 1.17e-05             | 0.619                     | 0.497                     | 0.0199           |                           | 0.00618                | 0.402          |
| 0.272          | 0.00924           | 1.28e-05             | 0.595                     | 0.538                     | 0.0296           | 0.240                     | 0.00501                | 0.491          |
| 0.267          | 0.00863           | 1.89e-05             | 0.591                     | 0.574                     | 0.0359           | 0.227                     | 0.00397                | 0.450          |
| 0.263          | 0.00531           | 1.47e-05             | 0.553                     | 0.592                     | 0.0446           | 0.233                     | 0.00377                | 0.439          |
| 0.259          | 0.00881<br>0.0104 | 1.28e-05             | 0.614                     | 0.535                     | 0.0328           | 0.262                     | 0.00355                | 0.509          |
| 0.255<br>0.252 | 0.0104 0.0113     | 1.57e-05<br>1.40e-05 | 0.630<br>0.646            | 0.528                     | 0.0306 0.0311    | 0.262<br>0.275            | 0.00343<br>0.00326     | 0.440<br>0.465 |
| 0.252          | 0.0113            | 1.40e-05<br>1.78e-05 | 0.646                     | 0.547<br>0.577            | 0.0311<br>0.0364 | 0.275<br>0.252            | 0.00326                | 0.465 0.467    |
| 0.247          | 0.00863           | 1.78e-05<br>1.65e-05 | 0.626                     | 0.377                     | 0.0364 0.0288    | 0.252<br>0.275            | 0.00315                | 0.467<br>0.475 |
| 0.244 0.241    | 0.0132            | 2.01e-05             | 0.535<br>0.686            | 0.705                     | 0.0288           | 0.275<br>0.255            | 0.00285<br>0.00274     | 0.475 0.593    |
| 0.241          | 0.00741           | 2.016-03             | 0.000                     | 0.509                     | 0.0302           | 0.235                     | 0.00274                | 0.575          |

Table 4. Inversion of the Cole Cole parameters for the core sample EST59676-41 (transverse
 direction). Index 1 is used for the low frequency contribution which is associated with the induced
 polarization contribution.

| Sw    | $\pi(s)$ | 72(S)    | <i>c</i> <sub>1</sub> (-) | <i>c</i> <sub>2</sub> (-) | $M_{1}(-)$ | <i>M</i> <sub>2</sub> (-) | $\sigma_{\infty}(S/m)$ | RMS<br>(%) |
|-------|----------|----------|---------------------------|---------------------------|------------|---------------------------|------------------------|------------|
| 0.973 | 0.00818  | 2.97e-06 | 0.745                     | 0.402                     | 0.0181     | 0.0914                    | 0.0291                 | 0.661      |
| 0.973 | 0.00818  | 1.02e-06 | 0.743                     | 0.402                     | 0.0181     | 0.102                     | 0.0291                 | 0.001      |
| 0.973 | 0.0109   | 2.32e-06 | 0.312                     | 0.540                     | 0.0177     | 0.102                     | 0.0272                 | 0.403      |
| 0.810 | 0.0023   | 5.66e-06 | 0.530                     | 0.540                     | 0.0328     | 0.0984                    | 0.0181                 | 0.147      |
| 0.755 | 0.0128   | 4.36e-06 | 0.089                     | 0.331                     | 0.0108     | 0.107                     | 0.0210                 | 0.204      |
| 0.733 | 0.0200   | 4.24e-06 | 0.793                     | 0.400                     | 0.0113     | 0.107                     | 0.0198                 | 0.273      |
| 0.724 | 0.0328   | 3.76e-06 | 0.528                     | 0.518                     | 0.0132     | 0.102                     | 0.0165                 | 0.275      |
| 0.709 | 0.0155   | 3.55e-06 | 0.528                     | 0.667                     | 0.0132     | 0.219                     | 0.00337                | 0.200      |
| 0.693 | 0.0154   | 2.85e-06 | 0.604                     | 0.654                     | 0.0199     | 0.219                     | 0.00329                | 0.301      |
| 0.693 | 0.00134  | 9.50e-06 | 0.586                     | 0.660                     | 0.0199     | 0.103                     | 0.00329                | 0.331      |
| 0.686 | 0.00417  | 1.07e-05 | 0.580                     | 0.594                     | 0.0221     | 0.103                     | 0.00333                | 0.240      |
| 0.080 | 0.00840  | 1.01e-05 | 0.621                     | 0.594                     | 0.0185     | 0.0991                    | 0.00323                | 0.280      |
| 0.672 | 0.00164  | 1.32e-05 | 0.021                     | 0.907                     | 0.0240     | 0.0982                    | 0.00232                | 0.290      |
| 0.659 | 0.00254  | 1.05e-05 | 0.483                     | 0.907                     | 0.0240     | 0.110                     | 0.00232                | 0.234      |
| 0.643 | 0.00234  | 3.75e-06 | 0.652                     | 0.807                     | 0.0208     | 0.110                     | 0.00180                | 0.279      |
| 0.632 | 0.00675  | 1.02e-05 | 0.645                     | 0.694                     | 0.0103     | 0.104                     | 0.00431                | 0.213      |
| 0.619 | 0.00448  | 6.03e-06 | 0.514                     | 0.757                     | 0.0268     | 0.108                     | 0.00403                | 0.313      |
| 0.619 | 0.00269  | 1.78e-05 | 0.571                     | 0.858                     | 0.0200     | 0.0682                    | 0.00543                | 0.347      |
| 0.608 | 0.00256  | 1.03e-05 | 0.587                     | 0.797                     | 0.0275     | 0.100                     | 0.00459                | 0.155      |
| 0.563 | 0.00203  | 1.27e-05 | 0.387                     | 0.895                     | 0.0209     | 0.100                     | 0.00459                | 0.133      |
| 0.505 | 0.00203  | 8.52e-06 | 0.383                     | 0.895                     | 0.0422     | 0.107                     | 0.00352                | 0.748      |
| 0.492 | 0.00512  | 6.06e-06 | 0.376                     | 0.841                     | 0.0592     | 0.144                     | 0.00235                | 0.677      |
| 0.492 | 0.00148  | 7.37e-06 | 0.536                     | 0.721                     | 0.0332     | 0.219                     | 0.00213                | 0.168      |
| 0.405 | 0.00148  | 6.20e-06 | 0.603                     | 0.645                     | 0.0332     | 0.219                     | 0.00200                | 0.108      |
| 0.334 | 0.00808  | 7.47e-06 | 0.603                     | 0.696                     | 0.0243     | 0.225                     | 0.00110                | 0.285      |
| 0.317 | 0.0152   | 1.48e-05 | 0.592                     | 0.665                     | 0.0275     | 0.192                     | 0.000763               | 0.350      |
| 0.299 | 0.0132   | 1.03e-05 | 0.520                     | 0.005                     | 0.0342     | 0.192                     | 0.000597               | 0.550      |
| 0.288 | 0.0130   | 4.62e-06 | 0.545                     | 0.680                     | 0.0265     | 0.364                     | 0.000537               | 0.463      |
| 0.276 | 0.0270   | 1.24e-05 | 0.424                     | 0.809                     | 0.0405     | 0.321                     | 0.000395               | 0.558      |
| 0.268 | 0.0287   | 1.11e-05 | 0.421                     | 0.865                     | 0.0299     | 0.451                     | 0.000271               | 0.966      |
| 0.255 | 0.0207   | 8.98e-06 | 0.411                     | 0.862                     | 0.0332     | 0.521                     | 0.000224               | 0.842      |
| 0.255 | 0.0476   | 1.23e-05 | 0.461                     | 0.893                     | 0.0290     | 0.499                     | 0.000187               | 0.834      |
| 0.248 | 0.0470   | 6.31e-06 | 0.477                     | 0.848                     | 0.0182     | 0.671                     | 0.000255               | 0.908      |
| 0.244 | 0.0387   | 1.37e-05 | 0.423                     | 0.936                     | 0.0285     | 0.548                     | 0.000182               | 0.789      |
| 0.242 | 0.0319   | 8.13e-06 | 0.397                     | 0.930                     | 0.0250     | 0.634                     | 0.000202               | 0.887      |
| 0.238 | 0.129    | 1.19e-05 | 0.565                     | 0.867                     | 0.0181     | 0.604                     | 0.000176               | 1.37       |
| 0.235 | 0.0843   | 1.47e-05 | 0.513                     | 0.994                     | 0.0222     | 0.580                     | 0.000148               | 1.49       |
| 0.233 | 0.0683   | 9.45e-06 | 0.465                     | 0.844                     | 0.0189     | 0.659                     | 0.000178               | 1.55       |

| 559 | Table 5. Inversion of the Cole Cole parameters for the core sample EST59676-42 (in-plane            |
|-----|---|
| 560 | direction). Index 1 is used for the low frequency contribution which is associated with the induced |
| 561 | polarization contribution.  |

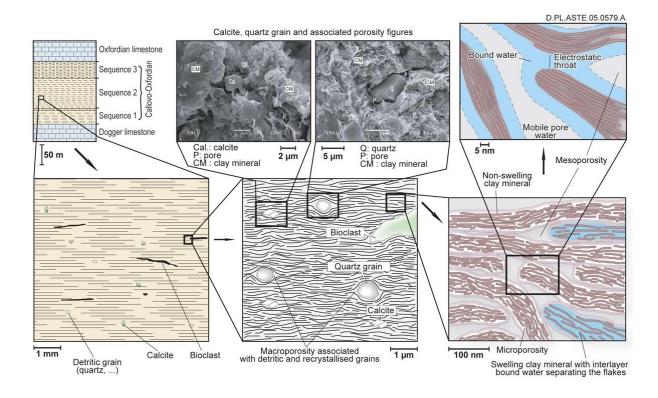
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RMS  $c_{1}(-)$  $c_2(-)$  $M_{1}(-)$  $M_{2}(-)$  $\sigma_{\infty}(S/m)$  $\pi(s)$  $\tau_2(s)$ Sw (%) 0.00716 1.42e-06 0.507 0.383 0.0366 0.0998 0.0987 0.268 0.965 0.0370 4.70e-07 0.807 0.530 0.361 0.0291 0.184 0.0587 0.272 0.789 0.0122 1.19e-06 0.425 0.448 0.0302 0.147 0.0652 0.166 0.752 0.0211 1.13e-06 0.467 0.440 0.0336 0.162 0.214 0.0615 5.91e-07 0.440 0.200 0.239 0.723 0.0450 0.435 0.0414 0.0582 9.25e-07 0.489 0.436 0.0518 0.192 0.708 0.0713 0.0529 0.163 8.52e-07 0.413 0.708 0.0147 0.415 0.0202 0.183 0.0513 0.117 0.694 0.0151 6.74e-07 0.436 0.414 0.0230 0.204 0.0441 0.137 0.679 0.0164 2.26e-06 0.427 0.473 0.0275 0.161 0.0385 0.157 0.679 0.0212 7.29e-07 0.441 0.396 0.0163 0.197 0.0482 0.110 0.668 0.0374 1.08e-06 0.481 0.374 0.0119 0.190 0.0441 0.103 0.653 0.0223 3.08e-06 0.432 0.425 0.0241 0.152 0.0451 0.103 0.00821 1.16e-05 0.385 0.536 0.0352 0.0844 0.0359 0.120 0.653 0.641 0.00436 1.60e-06 0.371 0.497 0.0364 0.159 0.0367 0.128 0.624 0.00164 3.89e-06 0.330 0.633 0.0520 0.104 0.0371 0.139 0.00770 1.99e-06 0.382 0.503 0.0321 0.624 0.153 0.0451 0.169 0.0268 9.00e-07 0.449 0.404 0.0205 0.198 0.0461 0.192 0.617 0.0334 9.50e-07 0.461 0.376 0.0117 0.189 0.0517 0.0971 0.603 0.509 0.603 0.0112 2.77e-06 0.429 0.0149 0.142 0.0645 0.228 0.590 1.41e-06 0.566 0.387 0.0117 0.175 0.223 0.0256 0.0531 0.552 0.0139 3.61e-06 0.466 0.485 0.0268 0.150 0.0382 0.231 0.503 0.0126 1.01e-06 0.434 0.436 0.0285 0.227 0.0335 0.148 0.490 0.0166 2.29e-06 0.438 0.476 0.0350 0.201 0.0286 0.218 7.96e-07 0.0276 0.474 0.0421 0.482 0.406 0.271 0.0292 0.151 0.456 0.0457 4.06e-07 0.417 0.392 0.0322 0.313 0.0284 0.208 0.299 0.445 0.0418 5.90e-07 0.416 0.414 0.0341 0.0263 0.246 0.433 0.0673 3.73e-07 0.561 0.382 0.0226 0.342 0.0246 0.236 0.396 0.000466 1.87e-06 0.422 0.600 0.0637 0.207 0.0163 0.350 1.31e-06 0.315 0.683 0.0980 0.243 0.208 0.396 0.000112 0.0143 1.12e-06 0.487 0.458 0.0292 0.294 0.353 0.364 0.00361 0.0137 0.339 1.18e-06 0.483 0.474 0.0330 0.315 0.366 0.00373 0.0116 0.324 0.506 0.481 0.0338 0.315 0.423 0.00485 1.37e-06 0.0106 0.308 0.00503 1.29e-06 0.493 0.495 0.0377 0.333 0.00963 0.416 0.298 8.60e-07 0.0340 0.389 0.00691 0.521 0.461 0.372 0.00957 0.285 0.00390 7.86e-07 0.495 0.0370 0.396 0.00858 0.406 0.486 1.79e-06 0.277 0.000636 0.429 0.683 0.0796 0.305 0.00688 0.419 0.269 0.000855 1.58e-06 0.411 0.659 0.0784 0.343 0.00578 0.341 0.264 2.69e-06 0.425 0.788 0.000498 0.100 0.307 0.00429 0.356 0.259 0.000267 2.55e-06 0.409 0.841 0.119 0.304 0.00403 0.403 0.000330 0.255 2.82e-06 0.421 0.846 0.113 0.312 0.00375 0.442 0.251 2.32e-06 0.391 0.835 0.120 0.331 0.00376 0.447 0.000191 0.248 0.000578 1.91e-06 0.424 0.764 0.0880 0.412 0.00367 0.477 0.243 0.411 0.843 0.384 0.499 0.000293 2.03e-06 0.108 0.00353 0.240 0.827 0.000300 1.93e-06 0.411 0.105 0.411 0.00325 0.624 0.238 0.000110 0.347 0.774 0.151 0.00485 0.270 1.76e-06 0.265 0.0594 0.238 0.00150 0.476 0.697 0.482 0.00334 0.572 1.58e-06

# **Figures**

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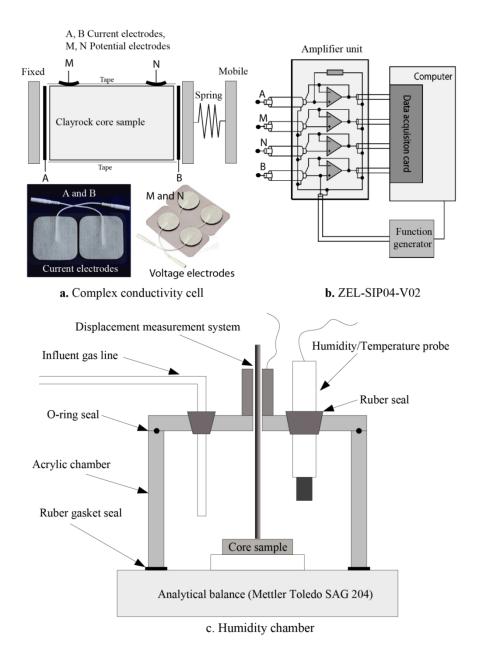
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**Figure 1.** Microstructure of the Callovo-Oxfordian formation illustrating the anistropy of this formation in association with a bedding plane (adapted from Yven et al., 2007). Note however that the anistropy of the Cox formation remains weak (<3 for the permeability).



**Figure 2.** X-ray tomography images of COx sample 59674-41 (cylinder axis perpendicular to the 575 bedding plane) showing the whole volume (left) and the volume of inclusions (pyrite-filled 576 bioturbations) which represents 0.29% of the total volume (right).



**Figure 3.** Equipment used to measure induced polarization for the Collavo-Oxfordian clayrocks. **a.** Sketch of the experimental setup. We used the carbon film electrodes-with hydrogel for injection (A and B) and non-polarizable Ag-AgCl electrodes for potential measurements (M and N). **b.** ZEL-SIP04-V02 impedance meter developed by Zimmermann et al. (2008). This equipment is operated in the frequency range from 1 mHz- to 45 kHz. **c.** Automated humidity system of the environmental chamber in which the measurements are performed (modified from Likos and Lu, 2003).

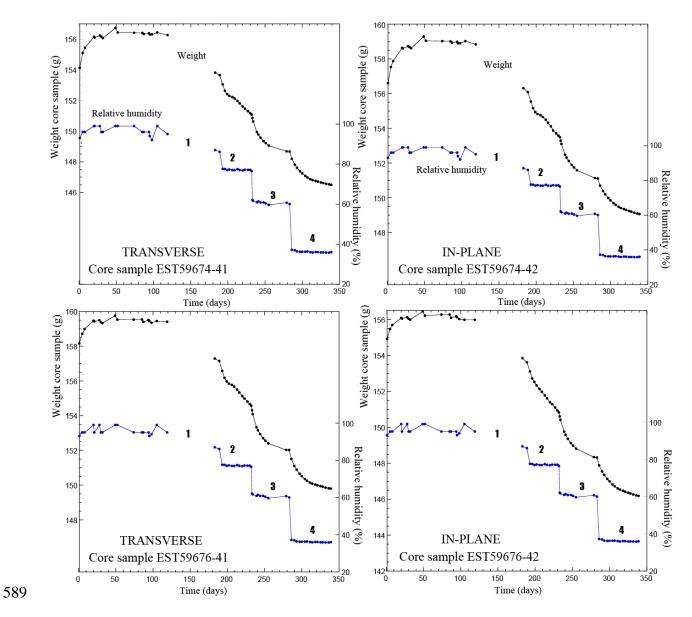


Figure 4. Evolution of the weight of the samples (Cores EST59674 and EST59676) for different
 relative humidities in a controlled humidity chamber. The saturation steps 3 and 4 is used to
 characterize the degree of anisotropy of the relative permeability curve of the COx.

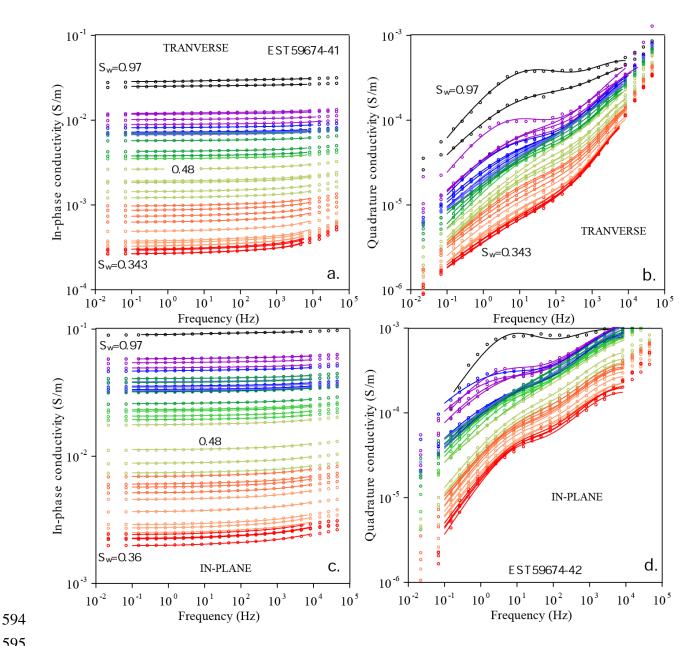




Figure 5. In-phase conductivity and quadrature conductivity spectra for core sample EST59674. a. In-phase conductivity, transverse component. b. Quadrature conductivity, transverse component. c. In-phase conductivity, in-plane component. d. Quadrature conductivity, in-plane component. The dots correspond to the measured data while the lines are the fit with a Cole Cole model using a Bayesian approach to optimize the values of the Cole Cole parameters. 

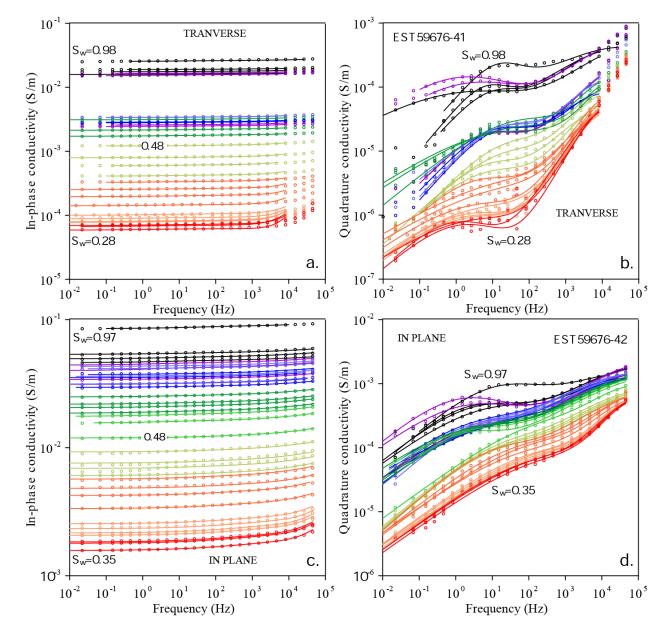
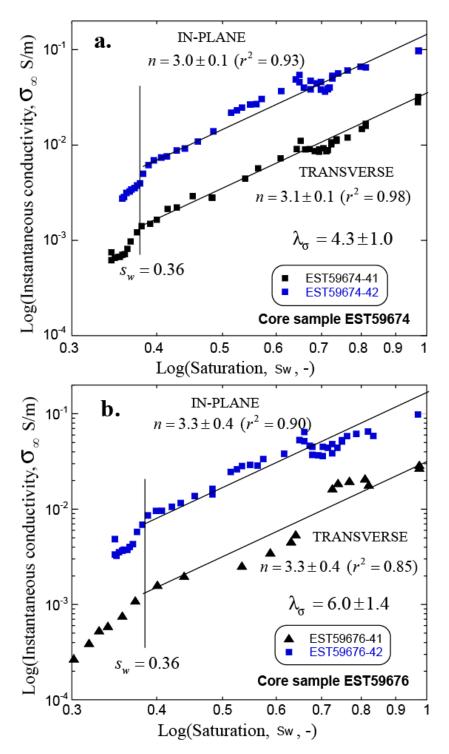




Figure 6. In-phase conductivity and quadrature conductivity spectra for core sample EST59676.
a. In-phase conductivity, transverse component. b. Quadrature conductivity, transverse component. c. In-phase conductivity, in-plane component. d. Quadrature conductivity, in-plane component.



**Figure 7.** Transverse and in-plane instantaneous conductivity versus pore water saturation in a desiccation experiment. **a.** Core sample EST59674. **b.** Core sample EST59676. Note that the anisotropy ratio is higher for the second core sample. The saturation 0.36 appears as the critical residual saturation, which appears to be independent of the direction of the core smaple.

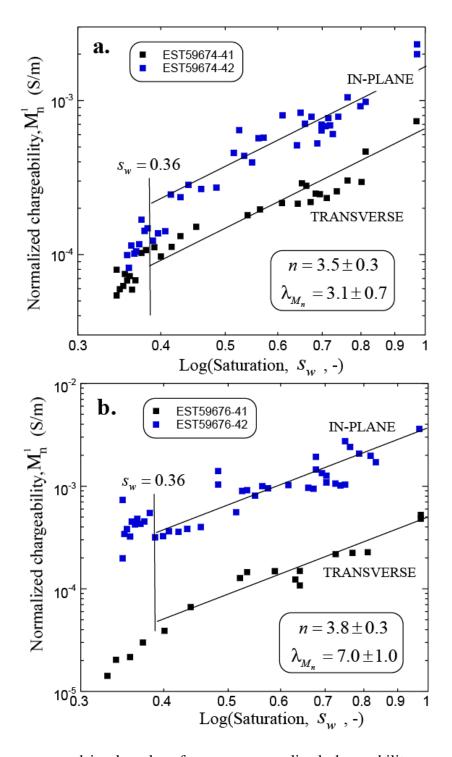
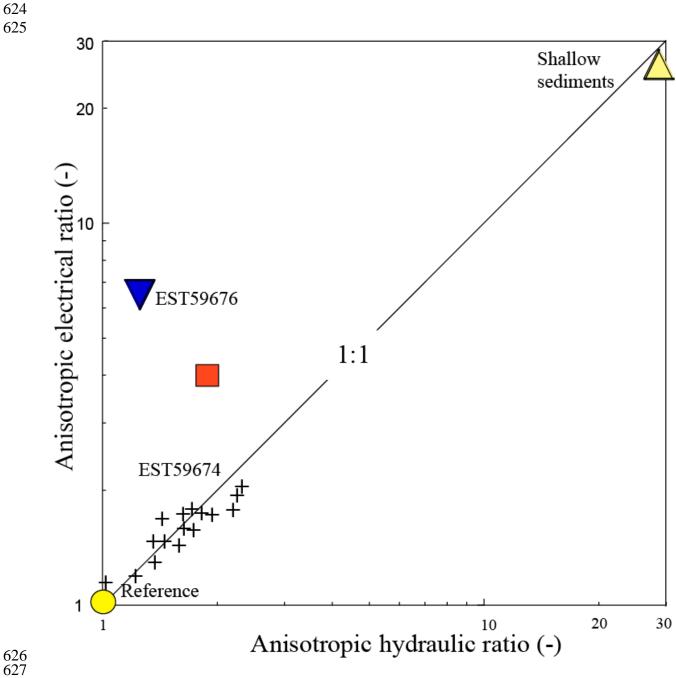


Figure 8. Transverse and in-plane low frequency normalized chargeability versus pore water saturation in a desiccation experiment. a. Core sample EST59674. b. Core sample EST59676. Note that the anisotropy ratio is higher for the second core sample. The saturation 0.36 appears as the critical residual saturation, which appears to be independent of the direction of the core smaple. 



**Figure 9.** Relationship between the electrical and hydraulic anistropic ratio. This trend should be confirmed with further analysis and data. The data corresponding to shallow sediments (yellowfilled triangle) is from the work of Gernez et al. (2019) based on hydraulic and electrical conductivity tomography. The crosses correspond to mudrocks (data from Adams et al., 2016).

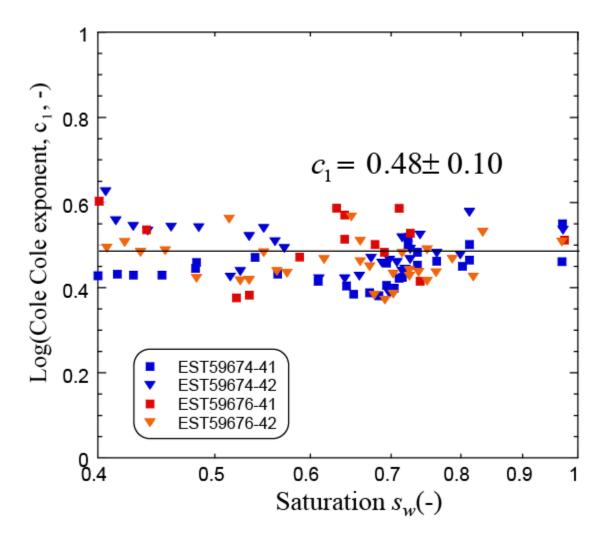
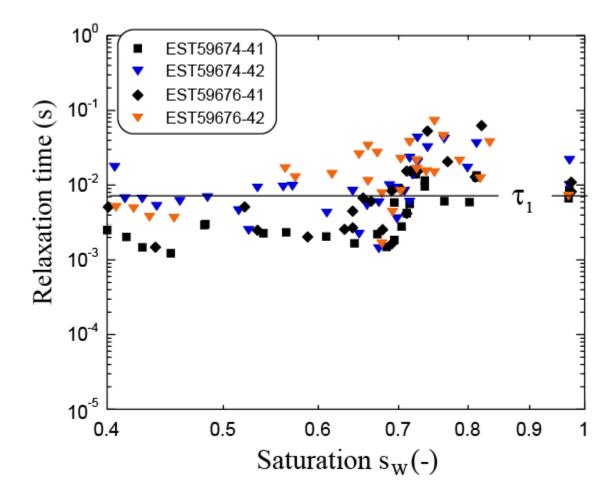
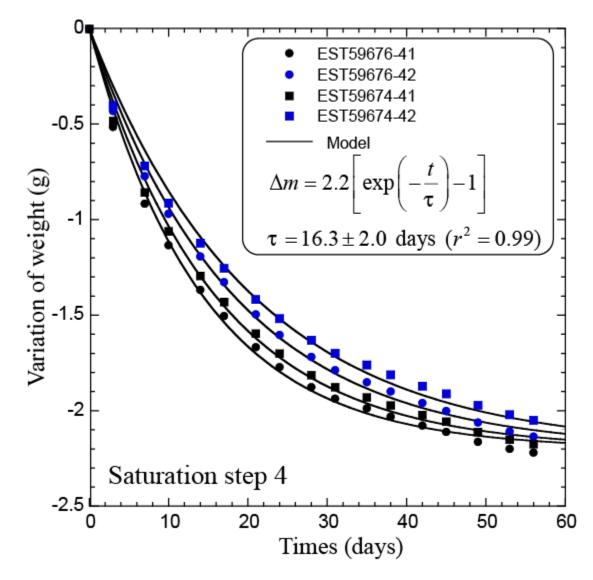


Figure 10. Transverse and in-plane low frequency Cole Cole exponent versus pore water saturation in a desiccation experiment. We use the data of the core sample EST59674 and EST59676.

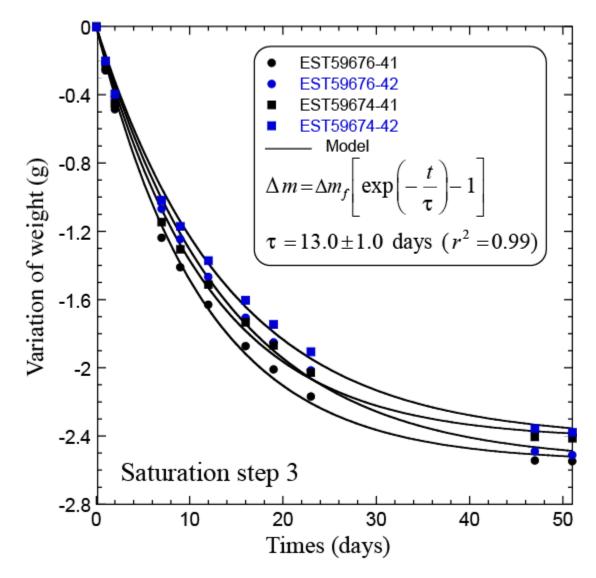


**Figure 11.** Low-frequency relaxation time versus saturation. The mean value of the relaxation 643 time  $\tau_1$  is close to  $7 \times 10^{-3}$  s independent of the direction.





**Figure 12.** Variation of the weight (in g) of the four core samples as a function of time when the relative humidity in the chamber is changed from 60 to 36% (Step 4 in the data shown in Figure 2). The inverted relaxation times are: (Sample EST59676-1, 14.4 $\pm$ 0.5 days), (Sample EST59676-2, 17.7 $\pm$ 0.6 days), (Sample EST59674-1, 15.4 $\pm$ 0.5 days), and (Sample EST59674-2, 18.3 $\pm$ 0.6 days). The data show a small anisotropic effect for the two cores but this effect can be safely neglected.





**Figure 13.** Variation of the weight (in g) of the four core samples as a function of time when the relative humidity in the humidity chamber is changed from 77 to 60% relative humidities (Step 3 in the data shown in Figure 2). The inverted relaxation times are: (Sample EST59676-1, 11.5±0.5 days,  $\Delta m_f = 2.6$  g), (Sample EST59676-2, 14.0±0.5, days,  $\Delta m_f = 2.6$  g), (Sample EST59674-1, 12.0±0.5 days,  $\Delta m_f = 2.4$  g), and (Sample EST59674-2, 14.1±0.6 days,  $\Delta m_f = 2.4$  g). The data show a small anisotropic effect for the two cores but this effect can be safely neglected.

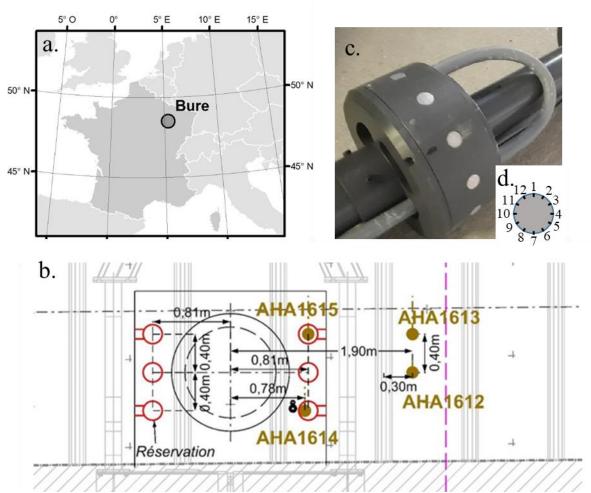
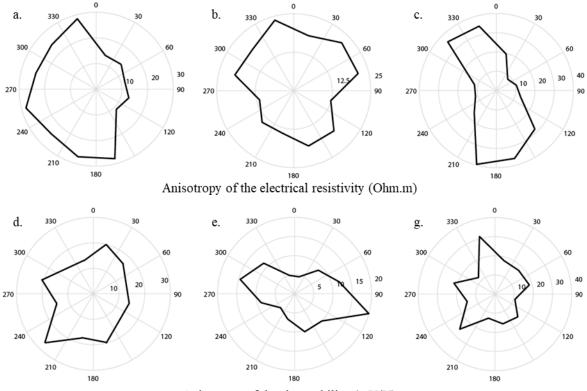


Figure 14. Location of Andra facility at Bure (France) a. Borehole location b. and Azymuthal
electrode system with stainless steel electrodes. This network is used to determine the anistropy of
the electrical conductivity and normalized chargeability of the COx formation in *in situ* conditions.
c. Azymuthal electrode array. d. Position of the 12 electrodes used for the study of the anistropy.



Anisotropy of the chargeability (mV/V)

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**Figure 15. a. b. c.** In situ electrical resistivity based on the azymuthal dipole dipole measurements respectively for the ring 1, 4, 5. The averaged anistropy ratio is  $2.3\pm0.7$ , which is on the same order of magnitude of the anistropy ratio discussed for the core samples. **d. e. f.,** In situ chargeability (expressed in mV/V) based on the azymuthal dipole dipole measurements respectively for the ring 1, 4, 5. The chargeability does not exhibit a clear anistropy ratio.

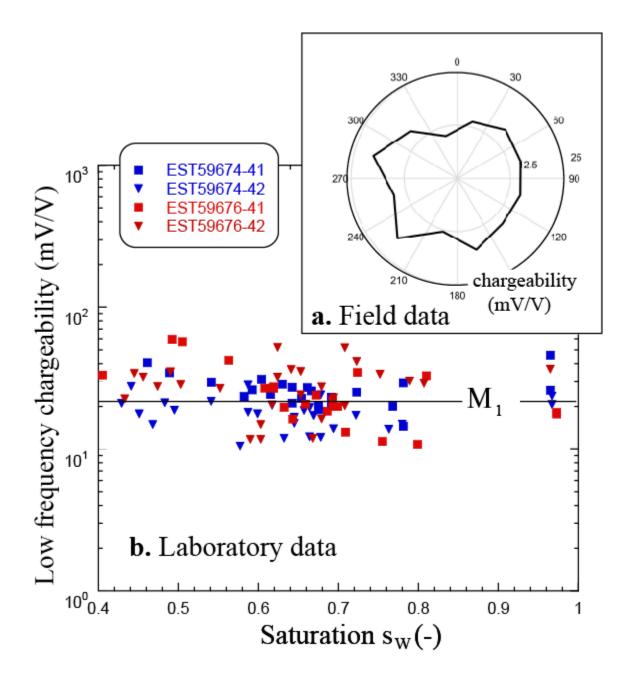


Figure 16. Anistropy of the chargeability. a. Field data showing no anistropy of the chargeability
 of the COx. b. Chargeability versus saturation for the four samples used in this study. The data
 show no anistropy of the chargeability field.