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REAL-TIME VISUALISATION OF THE MUSICAL TIMBRE BASED ON THE SPECTRAL ESTIMATES OF THE SNAIL-ANALYSER

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ABSTRACT

This article presents a real-time software solution that allows musicians to visualise the timbre content of their musical tones. The timbre representation is based on the spectral estimates of the Snail-Analyser, for a high frequency precision, and on a harmonic-like representation. After a short reminder on the derivation of these estimates, some second-stage estimates and the mapping used for the timbre representation are described. The visual representations in the application have been prototyped using the MAX software and developed with the Juce framework.

1. INTRODUCTION

The Snail-Analyser is a real-time software that allows the spectral analysis of a sound with a high frequency precision [1, 2]. It delivers a visual rendering on a musical scale made of a spiral (one turn is one octave, one angle is one chroma).

The ATRIM project¹ aims to design reliable tools with reactive visual renderings adapted to high precision pitch and timbre analysis of musical wind instruments. It is devoted to provide musicians with accurate and informative feedback in real time for tuning and timbre assessment, during performance and in several contexts such as: expert testing and improvement of manufactured instruments, tuning or comparison of instruments, musical practice by helping musicians adjust their motor control to reach their own or a teacher's target (intonation, timbre, vibrato, glissando, playing effects, etc).

A first tuning application has been designed in the ATRIM project to assess the frequency-deviation from the target pitch, in Hertz [3]. Its technology involves demodulated phase signals, low-pass filtered phase-constancy indicators, and other complementary signals calculated in the spectral estimates of the Snail-Analyser. The visual rendering mimics electro-mechanical strobe-tuners that exploit a stroboscopic technology (see e.g [4, 5] for original work and [3] and references therein for some brief descriptive historical elements and more recent non-mechanical versions). A second version of this application has been designed to assess a more comfortable deviation, in cents [6]. It involves a reactive local-in-time constancy indicator of the demodulated phase.

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This paper addresses the assessment of timbre. This issue has a long history from the point of view of perception, cognition and signal processing (see e.g. [7, 8, 9]) and learning algorithms (see e.g. [10] and references therein for a recent work integrating results on timbre and instrumental playing techniques). A resulting general statement is that timbre is related to spectrotemporal indicators and their modulations, and that it intimately covaries with pitch and amplitude.

The paper is organised as follows. First, section 2 presents a brief reminder on some spectral estimates used in the Snail-Analyser, the spiral visual rendering, a tuning spinner and in a rendering with harmonic structure that provides a starting basis to address musical timbre representation. Then, the analyser is complemented by an indicator overbuilt on that of local-in-time constancy of the demodulated phase, that characterises the harmonic synchronicity, in order to provide a set of spectrotemporal timbre indicators adapted to quasi-harmonic signals. Second, section 3 presents the software prototype and the designed visual rendering based on these indicators. Section 4 ends with conclusive remarks and perspectives.

2. ANALYSIS METHOD

This section first presents a brief reminder on the principle used in the Snail-Analyser [1] with its spectral estimates and their use in the spiral rendering (\S 2.1) and in a harmonic view (2.2) of interest to represent timbre. It complement the set of spectral estimates by an overbuilt one, the harmonic synchronicity (\S 2.3).

2.1. Reminder on the Snail-Analyser

The analysis process of the input sampled signal is based on (see [2, § 3.1] for more details) a spectral transform (here, a short time Fourier transform) for successive frames, the complex values of which are interpolated according to a vector Freq_v of tuned frequencies that are exponentially spaced to correspond to equally spaced midi codes, and spectral estimates introduced in [1], some of them being recalled below to make this paper self-contained. Typical parameters are: $F_s = 44.1 \, \rm kHz$ (sampling frequency), $T_{\rm frame} = 50 \, \rm ms$ (duration of a classic-shape window) associated with the next power of 2 of the corresponding number of samples (number of FFT points), $T = 5 \, \rm ms$ (incremental time step for overlap) and $R_m = 20$ frequency points per half tone (midi resolution) for Freq_v over the analysed midi range.

The downstream indicators of the Snail analyser are derived from the spectrum modulus and phase, for all frames starting at time $t \in T\mathbb{N}$ and all frequencies f with value in Freq_v, as follows.

¹ATRIM is the French acronym for "Analyseur Temps-Réel haute précision de justesse et de timbre pour Instruments Musicaux" (High precision real-time pitch and timbre analyser for musical instruments). This project is supported by the plan "France Relance" (see acknowledgements at the end of the paper).

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Figure 1: Spiral renderings of the spectrum of an ideal harmonic signal (harmonics synthetised with uniformly distributed amplitudes). From left to right: Fourier transform (50ms, Hanning), Snail-Analyser (frequency precision: 6 Hz), Snail-Analyser (cent precision: 5 cents).

Demodulated phase (ϕ_d) : this signal is defined by

$$\phi_d(t, f) = \phi_{Fourier}(t, f) - 2\pi f t, \qquad (1)$$

where $\phi_{Fourier}(t, f)$ denotes the spectrum phase.

Phase constancy indicator $(C_{f_c}, \text{set by } f_c)$: this signal is defined as the modulus of the output of a low-pass filter (e.g. of Butterworth type) with cutoff frequency f_c , excited by the input complex signal $u_f : t \mapsto \exp(i \phi_d(t, f))$, namely,

$$\underbrace{u_f(t) = e^{i \phi_d(t,f)}}_{\text{Low-Pass}(f_c)} \xrightarrow{|\cdot|} \underbrace{C_{f_c}(t,f)}_{(2)}$$

This indicator is used as a factor multiplying the spectrum loudness (ISO226:2003) to form the thickness represented on the spiral representation². Compared to the Fourier spectrum (see fig. 1 left), this improves the frequency accuracy by contracting the lobes to a precision of about $\pm f_c$ ($f_c = 6$ Hz in center figure and $f_c(f) = 2\frac{\kappa}{1200}f$ with $\kappa = 5$ cents in the right figure). Due to the low-pass filter, this indicator also rejects time-varying components faster than f_c , which is of interest for tuning tasks in noisy environments. To capture fast components (glissando, vibrato, etc) with the

same precision $(\pm f_c)$, a third (reactive) indicator is introduced.

Local-in-time constancy $(\delta \Phi_d)$: this signal is defined by

$$\delta\Phi_d(t,f) = M[\phi_d(t,f) - \phi_d(t-T,f)], \qquad (3)$$

where M denotes the 2π -modulo centered on $(-\pi, \pi)$.

This deviation indicator is local-in-time, at the scale of the incremental time step T. It quantifies a deviation-speed indicator that can be converted in Hertz (frequency deviation δF), in cents (cent deviation $\delta \kappa$) and used to contract the spectral lobes (factor \tilde{C}_{f_c}) according to the shape inherited from the low-pass filter chosen to compute C_{f_c} : **Frequency deviation** (δF): this signal defined by

$$\delta F(t,f) = \delta \Phi_d(t,f)/(2\pi T), \tag{4}$$

estimates a frequency deviation from f to the central frequency $F \approx f + \delta F$ of the spectral lobe of a stationary component (see e.g. [11] for an overview of other estimates used for spectrum reallocation). Its robustness (to perturbations or an unsteady frequency component) is achieved through the averaging of the demodulated phase evolution over the frame duration $T_{\rm frame}$. Its reliability is limited to the range $\frac{1}{2T}(-1,1)$ of unaliased frequency deviations (100 Hz for T = 5 ms).

Cent deviation ($\delta \kappa$): this signal is defined by

$$\delta\kappa(t,f) = 1200\log_2\left(1 + \frac{\delta F(t,f)}{f}\right),\tag{5}$$

a good approximation of which is given by $\frac{1200}{\ln 2} \frac{\delta F(t,f)}{f}$ for $|\delta F/f| \ll 1$. Note that according to the definition of δF , the unaliased range in cents depends on f and is given by $1200 \log_2 \left(1 + \frac{1}{2T f}\right)$.

Contraction factor (factor \tilde{C}_{f_c}): this signal defined by

$$\tilde{C}_{f_c}(t,f) = \left| H(\delta F(t,f)/f_c) \right|, \tag{6}$$

restores the same shape as C_{f_c} for a stationary sound input signal, choosing $f \mapsto H(f/f_c)$ as the transfer function of the low-pass filter used to compute C_{f_c} .

The indicator ϕ_d mapped to the angle of a spinning pattern is the one used in the Snail-Analyser and in the strobe-tuner application [3], and that $\delta\kappa$ mapped to the angle velocity of the same pattern is the one used in the cent-sensitive version [6]. The contraction factor \tilde{C}_{f_c} can be used in the Snail-Analyser: the combination of its high time reactivity and frequency precision makes it particularly suitable for enhancing real-time spectrogram-like rendering.

²The spiral skeleton (+1 round from the center is +1 octave, so that one angle is one chroma) is defined in polar coordinates by $\rho(f) =$ $1 + \log_2(f/f_{min}), \theta(f) = \theta_{ref} + 2\pi \log_2(f/f_{ref})$ where f_{min} and f_{max} are the lowest and highest frequencies to be displayed and f_{ref} is the tuning reference displayed at angle θ_{ref} .

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Figure 2: Harmonic representation ($f_c = 6$ Hz): (left) ideal harmonic signal of fig. 1; (right) inharmonic string (acoustic upright piano).

2.2. Harmonic view

The Snail-Analyser integrates (for future distributions) a harmonic viewer that makes harmonic components aligned (see fig. 2). Given a fundamental frequency F_1 , each stage n represents a spectral area of harmonics $n \ge 1$ on a midi-code-scaled axis centered according to the abscissa

$$m_{F_1}^n(f) = m(f) - m(nF_1) = 12\log_2\frac{f}{nF_1},$$
 (7)

where a frequency f is converted into midi code as $m(f) = m_{ref} + 12 \log_2 \frac{f}{f_{ref}}$ (with typical values $m_{ref} = 69$, $f_{ref} = 440$ Hz).

This representation is chosen as one of the bases of the timbre representation described in section 3.

2.3. Harmonic synchronicity

It is complemented by descriptors of harmonic synchronicity in Hertz (ν_n) or in cents (σ_n), for each harmonic $n \ge 1$.

Harmonic frequency synchronicity (ν_n) : it is defined by

$$\nu_n(t,f) = \delta F(t,nf) - n\,\delta F(t,f). \tag{8}$$

This descriptor provides a local-in-time estimation of the harmonic synchronicity for nearly harmonic signals in the following sense.

Assume that an input signal is composed of nearly harmonic partials of frequencies $F_n = n(1+\epsilon_n)F_1$ (with $\epsilon_1 = 0$), where F_1 denotes the fundamental frequency and $\epsilon_n = (F_n - nF_1)/(nF_1)$ encodes the relative deviation of F_n compared to the expected harmonic frequency nF_1 . Then, consider an analysis frequency f and assume that nf is in the frequency range of the spectrum lobe of the partial of frequency F_n . In this case, $\delta F(t, nf) \approx F_n - nf$ estimates the frequency deviation between the ground-truth frequency F_n and the analysis frequency nf, and $\nu_n(t, f) \approx n(1 + \epsilon_n)F_1 - nF_1 \approx n\epsilon_nF_1$ estimates the deviation from the harmonic frequencies, independently from the analysis frequency f.

A conversion of ν_n into cents (relative to nf) is below.

Cent harmonic synchronicity (σ_n) : it is defined by

$$\sigma_n(t,f) = 1200 \lfloor \log_2(nf + \delta F(t,nf) - n \,\delta F(t,f)) \\ -\log_2(nf) \rfloor$$
$$= 1200 \log_2\left(1 + \frac{\delta F(t,nf) - n \,\delta F(t,f)}{nf}\right),$$

a good approximation of which is given by $\sigma_n(t, f) \approx \frac{1200}{\ln 2} \frac{\delta F(t, nf) - \delta F(t, nf)}{nf}$ for small frequency deviations.

Note that a version into cents, relative to an estimate of the target harmonic frequency $nF_1 \approx n(f + \delta F(t, f))$, is $\tilde{\sigma}_n(t, f) = 1200 \log_2 \left(1 + \frac{\delta F(t,nf) - n \, \delta F(t,f)}{n(f + \delta F(t,f))} \right) \approx \frac{1200}{\ln 2} \, \frac{\delta F(t,nf) - \delta F(t,nf)}{n(f + \delta F(t,f))}.$

3. VISUAL RENDERING AND SOFTWARE

3.1. Description of the visualisation

The software is a first prototype integrating a tuning spinner [6] and a harmonic representation inspired from fig. 2 complemented by spinners cent-sensitive to the harmonic synchronicity (σ_n). The visual rendering is organised in two main parts (see fig. 3).

The left part displays a vertical representation of the harmonics, with the fundamental (of target pitch F_1) at the bottom of the representation and higher harmonics superimposed in tiers above. Note that this vertical harmonic representation is not the spectrum unrolled on the frequency Y-axis but a superposition of visual windows, centered around these harmonics, extracted from the Snail analysis kernel. Each visual window covers a range of ± 1 semitones around the target harmonic frequency (nF_1) , the target being represented by a pink line in the middle of the window.

The right part of each window displays a rotating spinning hexagon, that conveys pitch and harmonic synchronicity information. In the lowest one (pitch window), the rotation speed indicates the pitch deviation from the target F_1 . Its color linearly varies from red (50 cents or more deviation) to green (0 cent). In the staged upper windows (harmonics $n \ge 2$), the rotation of the haxagons (of fixed blue color for now) indicates the harmonic synchronicity estimate, with an angular speed proportional to $\nu_n(t, nF_1)$.

The figure 3 shows a sawtooth wave playing a E3 (normally 164.81Hz) slightly detuned to +20 cents (=166.73Hz). Each F0 spinner on the right has a yellow color due to the +20 cts deviation from the target frequency (E3=164.81Hz). Consistently, we can see that the center of the lobes are also a little below the reference pink line because of the slight detune. The figure on the right shows that the Snail kernel analysis uses the cents scale for the phase processing, using the contraction factor \tilde{C}_{fc} where f_c is set to 5 cents (as in fig. 1-right). This method greatly improves the accuracy, and force the size of the lobes to be equal for each frequency, as opposed to what we see in the center figure which displays the same signal but with $f_c = 6$ Hz (as in fig. 1-center).

To compare the precision stemming from the Snail analysis to the Fourier approach, figure 3-left shows the loudness of the Fourier spectrum of the same signal. Proceedings of the 26th International Conference on Digital Audio Effects (DAFx23), Copenhagen, Denmark, 4 - 7 September 2023



Figure 3: Harmonicity renderings of a Sawtooth wave with a fundamental frequency at 166.73Hz (E3 +20 cents), 8 visible harmonics. From left to right: Fourier (50ms, Hanning), Snail-Analyser (frequency precision: 6 Hz), Snail-Analyser (cent precision 5 cents).

3.2. Rapid prototyping with MAX

The prototype Software and the visualisation have been developed using the Max environment [12], a visual programming paradigm for interactive multimedia applications. A max external object (MXO), loaded as a dynamic library in the environment at startup, encapsulates the Snail kernel library and computes for the signal processing chain. The real-time visualisation is then built using the Javascript for User Interface (or JSUI [13]) in Max, which has internal bindings to the Max graphics engine. Each analysis signal from the Max object is passed on to the JSUI object to build the rendering. This first approach proves reliable enough for the design of proof of concept real-time renderings, running approximately at 25 frames per second and requiring fast development iterations [6]. Thus, other views for future developments are yet to be tested. Once the user interface prototypes reach a final state, a desktop version of the prototype should also be converted to the JUCE environment [14].

4. CONCLUSION AND PERSPECTIVES

The Snail analysis process appears to relevant to design applications dedicated to real-time representations of the timbre of nearly harmonic sounds. The proposed visual rendering integrating reactive descriptors of the amplitude of spectral components, of tuning and harmonic synchronicity, all frequency accurate provides a first reliable prototype. Further work will focus on the exploration of this tool with expert musicians, the integration of new descriptors to enhance the information legibility, and the design of a desktop application.

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