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A Tunable Morris-Lecar Spiking Neuron in CMOS

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Abstract—This article describes a transistor-only tunable Morris-Lecar spiking neuron in CMOS. The tuning of the spiking frequency is accomplished by adjusting the voltage at the body terminal of a reset transistor in a standard 180 nm CMOS process. A tuning sensitivity of 47.85 kHz/V is achieved and can be used to compensate for changes in spiking frequency due to supply voltage variations. The proposed design consumes 1.06 fJ/spike, has a normalized area of 1,549, and has a spiking frequency of 18.37 kHz with a synchronization current of 10 pA.

I. INTRODUCTION

Neuromorphic chips use spiking neural networks (SNNs) to mimic the human brain. They have emerged as a promising computing architecture for artificial intelligence (AI) and have already been used in applications such as sensing [1], object avoidance [2], and speech recognition [3].

Analog spiking neural network (ASNN) is a subset of SNNs that uses analog circuits [4] to improve its energy efficiency. Recent studies have shown that by biasing transistors in the subthreshold region, the energy efficiency of a simplified Morris-Lecar (ML) neuron (Fig. 1) can be made as low as 1.2 fJ per spike [6]. Furthermore, the area occupied by a simplified Morris-Lecar neuron can be reduced by using a varicap-based design [7] or by removing the on-chip capacitors [8].

One challenge associated with the capacitorless Morris-Lecar neuron is that the spiking frequency (f_{spike}) and the energy efficiency (E_{spike}) of the spiking neuron are sensitive to variations in supply voltage, temperature, and process variations. *Takaloo et al.* [8] have shown that with 10 % variations in the supply voltage, the spiking frequency can deviate by as much as 33 %. It is therefore desirable to have a neuron implementation that compensates for changes in f_{spike} without changing the synaptic current I_{syn} .

It was shown in [9] that the biasing of the body-source junction can be changed to adjust the threshold voltage of MOS transistors in analog circuits. This paper evaluates the feasibility of adjusting f_{spike} by adjusting the body voltages of the reset transistors (M_3 and M_4 in Fig. 1) and shows that it can be used to compensate for the power supply sensitivity, and to a lesser extent sensitivity to temperature and process variations.

The article is organized as follows: Section II provides the background and simulation results for understanding the operation of a simplified Morris-Lecar neuron. Section III

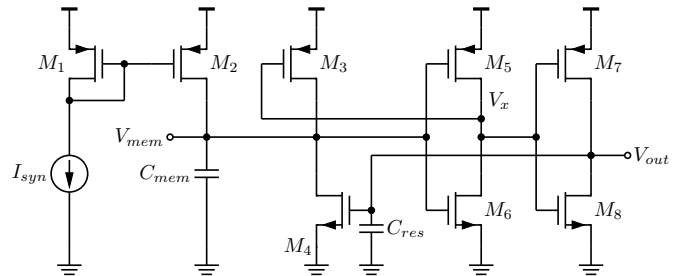


Fig. 1. A simplified spiking neuron based on the Morris-Lecar model [5].

describes the design considerations leading to the tunable transistor-only implementation. Section IV shows the post-layout simulation results. Conclusions are summarized in Sec. V.

II. BACKGROUND

The operation of the simplified Morris-Lecar neuron in Fig. 1 is as follows: M_1 and M_2 form a 1:1 current mirror. I_{syn} models the movement of neurotransmitters across the synaptic gap. For an initially uncharged C_{mem} , V_{mem} is 0 V. V_x is V_{DDA} , and M_3 is off. $V_{out} = 0$ V and M_4 is off. As charges accumulate across C_{mem} , V_{mem} increases gradually. V_{out} will increase rapidly once V_{mem} reaches the threshold voltage of the inverter formed by M_5 and M_6 . The falling voltage at V_x momentarily turns on M_3 . The rising V_{out} momentarily turns on M_4 and forces V_{mem} to return to 0 and V_x to rise, turning off M_3 . V_{out} is returned to 0 V, and a spike is generated. The waveforms of V_{out} and V_{mem} are shown in Fig. 2. f_{spike} is the spike frequency computed from V_{out} . And E_{spike} is the energy consumed to generate a spike.

C_{mem} integrates I_{syn} . Even though C_{mem} and C_{res} are small (e.g. C_{mem} and C_{res} are 4 fF and 8 fF, respectively, in [5]), they occupy a significant percentage of the area occupied by the neuron (e.g. 65 % of the neuron area in [5]). In 180 nm, C_g is 2 fF/ μm [10], and thus C_{mem} and C_{res} can be implemented using intrinsic gate capacitance and wire capacitance as was done in [8].

III. DESIGN CONSIDERATIONS

Figure 3 shows the proposed tunable Morris-Lecar spiking neuron. f_{spike} can be adjusted through either V_{BN} or V_{BP} . The advantage(s) and the disadvantage(s) of using V_{BN} and V_{BP} to adjust f_{spike} are discussed below.

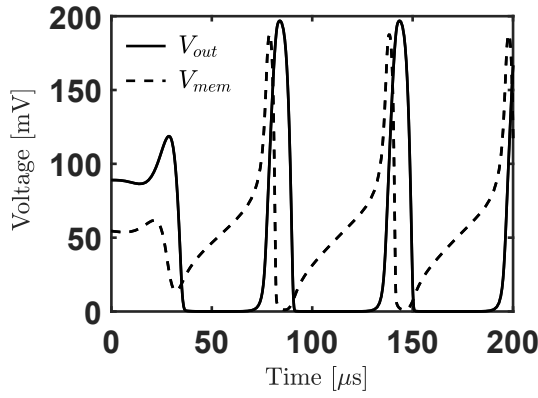


Fig. 2. Waveforms of V_{mem} and V_{out} .

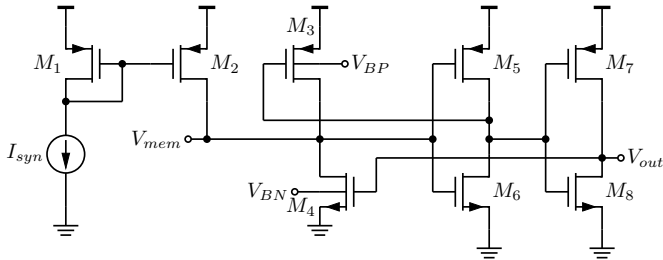


Fig. 3. The proposed tunable Morris-Lecar spiking neuron.

A. Adjust f_{spike} through V_{BN}

Figure 4 shows that the body voltage of M_4 can be adjusted to produce a significant change in f_{spike} . However, M_4 must be placed in a deep n -well, which requires a minimum area of $7 \times 8 \mu\text{m}^2$. The layout area of the spiking neuron is thus increased significantly.

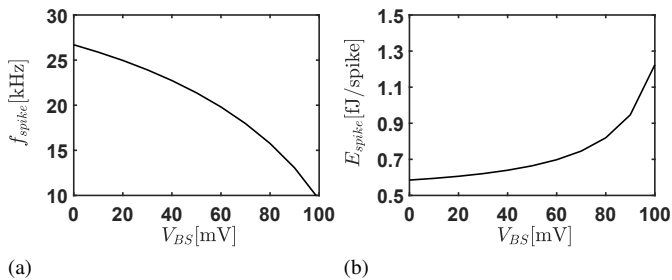


Fig. 4. (a) f_{spike} and (b) E_{spike} as a function of V_{BN} . $V_{BS} = V_{BN}$. V_{DDA} , the supply voltage, is 0.2 V. $V_{BP} = V_{DDA}$. $I_{syn} = 10$ pA.

B. Adjust f_{spike} through V_{BP}

Figure 5 shows that the body voltage of a M_3 can be adjusted to produce changes in f_{spike} . The body terminal of M_4 can be connected to ground and does not need to be placed in a dedicated n -well. M_3 and M_4 can be implemented using regular devices to minimize the active area of the spiking neuron. *It is therefore more desirable to adjust f_{spike} through V_{BP} than through V_{BN} .*

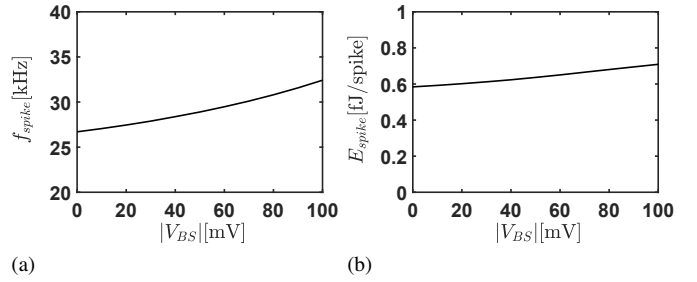


Fig. 5. (a) f_{spike} and (b) E_{spike} as a function of V_{BP} . $V_{BN} = 0$ V. $I_{syn} = 10$ pA. V_{DDA} , the supply voltage, is 0.2 V. $|V_{BS}|$ is $V_{DDA} - V_{BP}$.

C. Design Parameters

The parameters of the proposed tunable Morris-Lecar spiking neurons are as follows: V_{BN} is grounded. $V_{DDA} = 0.2$ V. V_{BP} is biased nominally at $V_{DDA}/2$ and can be adjusted to change f_{spike} . The aspect ratio of M_1 and M_2 is $1/0.18 \mu\text{m}/\mu\text{m}$. The aspect ratio of M_3 , M_5 , and M_7 is $0.44/0.18 \mu\text{m}/\mu\text{m}$. The aspect ratio of M_4 , M_6 , and M_8 is $0.22/0.18 \mu\text{m}/\mu\text{m}$. Instead of dedicated capacitors, C_m and C_{res} are implemented using parasitic wire capacitances and intrinsic transistor capacitances to reduce the layout area. Unless otherwise shown, the body terminals of the PMOS transistors are connected to V_{DDA} and the body terminals of the NMOS are connected to 0 V.

IV. POST-LAYOUT SIMULATION RESULTS

Figure 6 shows the layout created using Cadence Virtuoso. The parasitics are extracted with Quantus after checking the layout for DRC and LVS violations using Assura.

Figure 7(a) shows that f_{spike} is an increasing function of I_{syn} with $\Delta f_{spike}/\Delta I_{syn}$ equal to 0.9525 kHz/pA at $I_{syn} = 10$ pA. E_{spike} is calculated from simulations as discussed in [6] as follows. **First**, the instantaneous current supplied by V_{DDA} is calculated from simulation. **Second**, the instantaneous power consumed is calculated. **Third**, the period of spikes in V_{out} is calculated. **Fourth**, the instantaneous power is integrated over one period of a spike to calculate E_{spike} . Figure 7(b) shows that E_{spike} is a function of I_{syn} and has a minimum E_{spike} at $I_{syn} = 10$ pA.

Figure 8 shows that f_{spike} and E_{spike} are both decreasing functions of V_{BP} . Setting V_{BP} nominally at $V_{DDA}/2$ (i.e. 0.1 V) allows f_{spike} and E_{spike} to be adjusted as necessary. $\Delta f_{spike}/\Delta V_{BP}$ is -37.3 kHz/V with V_{BP} at $V_{DDA}/2$. The slope of E_{spike} is -2.7 fJ/spike/V with V_{BP} at $V_{DDA}/2$.

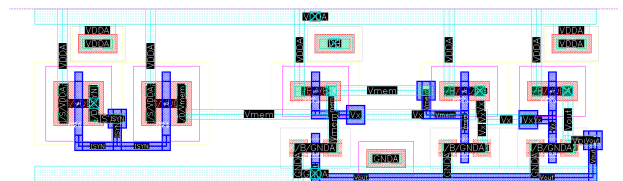


Fig. 6. Physical implementation of the tunable Morris-Lecar neuron. Area is $3.92 \times 12.8 \mu\text{m}^2$.

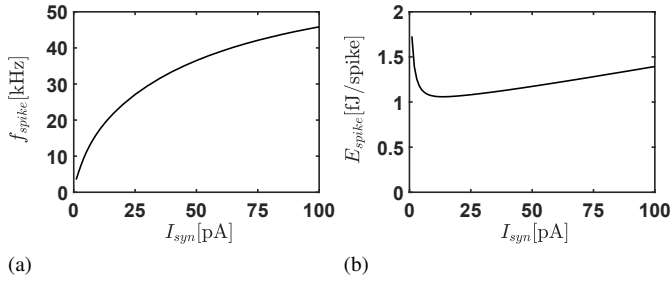


Fig. 7. (a) f_{spike} and (b) E_{spike} as a function of I_{syn} . V_{BP} is 100 mV and V_{DDA} is 200 mV. T is 27 °C.

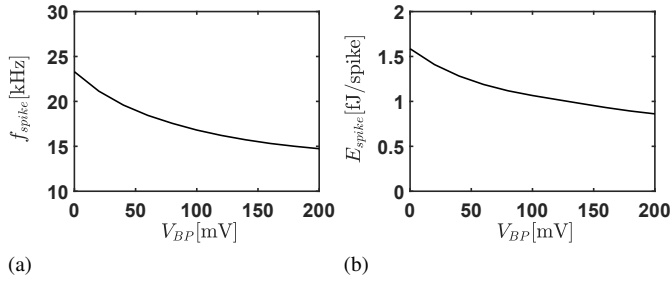


Fig. 8. (a) f_{spike} and (b) E_{spike} as a function of V_{BP} . I_{syn} is 10 pA and T is 27 °C.

Figure 9 shows the supply voltage sensitivities of f_{spike} and E_{spike} . The compensation is considered successful if Δf_{spike} after compensation is less than $\pm 1\%$ of f_{spike} at the nominal V_{DDA} . Table I shows that V_{BP} can be adjusted to compensate for $\pm 10\%$ changes in V_{DDA} . Simulations A, B, and C show that a drop in V_{DDA} by 10% can be compensated by reducing V_{BP} from 100 mV to 65 mV so that Δf_{spike} is less than 0.65%. Simulations A, D, and E show that an increase in V_{DDA} by 10% can be compensated by increasing V_{BP} from 100 mV to 135 mV so that Δf_{spike} is less than 0.1%.

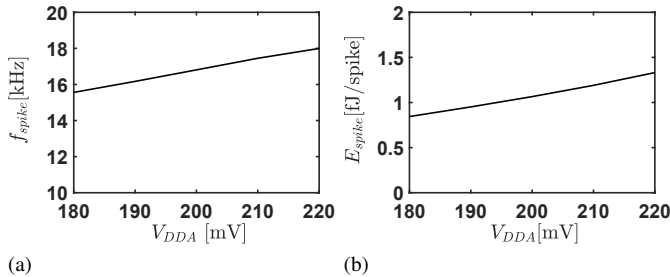


Fig. 9. (a) f_{spike} and (b) E_{spike} as a function of V_{DDA} . $V_{BP}=100$ mV, $I_{syn} = 10$ pA, and $T=27$ °C.

A. Limitations

1) *Temperature*: Figure 10 shows f_{spike} and E_{spike} between 0 °C and 70 °C—a temperature range for “commercial components” [11]. f_{spike} is an increasing function with a slope equal to 0.312 kHz/°C with V_{BP} at $V_{DD}/2$. Figure 10(b) shows that despite having a complex dependence on T , E_{spike} is an increasing function of T for $T > 20$ °C.

Table II shows V_{BP} can be adjusted to provide partial compensation for changes in T . Simulations A, B, and C show

TABLE I
 V_{BP} IS ADJUSTED TO COMPENSATE FOR $\pm 10\%$ VARIATIONS OF V_{DDA} .

	Temp. [°C]	V_{DDA} [mV]	V_{BP} [mV]	I_{syn} [pA]	f_{spike} [kHz]	E_{spike} [fJ/spike]
A	27	200	100	10	16.808	1.065
B	27	180	100	10	15.561	0.844
C	27	180	65	10	16.910	0.913
D	27	220	100	10	17.996	1.332
E	27	220	135	10	16.809	1.235

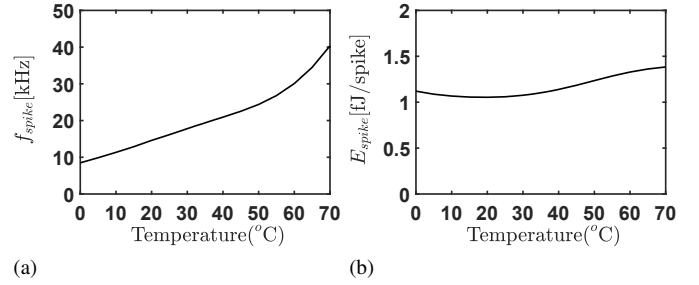


Fig. 10. (a) f_{spike} and (b) E_{spike} as a function of temperature.

that an increase of T from 27 °C to 43 °C can be compensated by increasing V_{BP} from 100 mV to 180 mV. Simulations A, D, E, and F show that a decrease in T from 27 °C to 0 °C cannot be adequately compensated by reducing V_{BP} to 0 V unless I_{syn} is also increased from 10 pA to 90 pA.

TABLE II
 V_{BP} IS ADJUSTED TO PROVIDE PARTIAL COMPENSATION FOR CHANGES IN TEMPERATURE.

	Temp. [°C]	V_{DDA} [mV]	V_{BP} [mV]	I_{syn} [pA]	f_{spike} [kHz]	E_{spike} [fJ/spike]
A	27	200	100	10	16.808	1.065
B	43	200	100	10	21.880	1.165
C	43	200	180	10	16.67	1.092
D	0	200	100	10	8.490	1.120
E	0	200	0	10	9.33	1.80
F	0	200	200	90	16.600	2.190

B. Process Variations

Figure 11 shows the sensitivities of f_{spike} and E_{spike} to process variations through a Monte Carlo simulation with one thousand samples. The mean value μ of f_{spike} is 18.37 kHz and the standard deviation σ is 6.17 kHz. The mean value of μ of E_{spike} is 1.06 fJ/spike and the standard of deviation σ of E_{spike} is 0.11 fJ/spike. The results indicate that V_{BP} can only provide partial compensation to changes due to process variations.

Figure 12 shows the average peak-to-peak output voltage is 191.25 mV with a σ of 14.17 mV and shows that most simulations of $V_{out,pp}$ produce swings greater than $V_{DDA}/2$.

C. Comparison

Table III shows the comparison of the state of the art. E_{spike} of 1.06 fJ/spike and f_{spike} of 18.37 kHz are obtained via a post-layout Monte Carlo simulation of one thousand samples

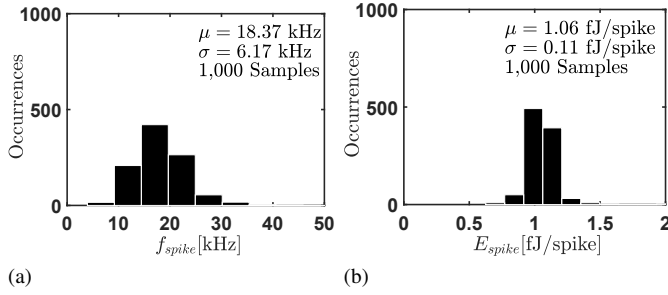


Fig. 11. Monte Carlo Simulations of (a) f_{spike} and (b) E_{spike} with V_{BP} at 0.1 V and I_{syn} at 10 pA.

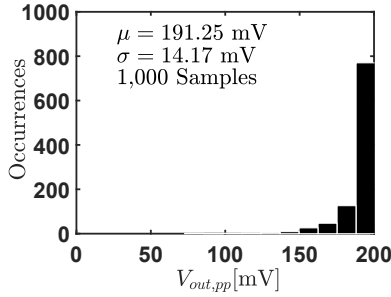


Fig. 12. Monte Carlo Simulations of $V_{out,pp}$ with V_{BP} at 0.1 V and I_{syn} at 10 pA.

with V_{BP} at $V_{DDA}/2$ and I_{syn} at 10 pA. Areas are normalized to L_{min}^2 for a technology-independent comparison as proposed by Takaloo *et al.* in [8]. L_{min} is the minimum length in a process. By using intrinsic transistor capacitances and parasitic wire capacitances as state capacitors as discussed in [8], a small normalized area of 1,549 is obtained.

The proposed design minimizes the normalized area through a capacitorless implementation and reduces its sensitivity to supply voltage and temperature variations by adjusting the body voltage of M_3 in Fig. 3.

TABLE III
COMPARISON WITH THE STATE-OF-THE-ART MORRIS-LECAR SPIKING NEURON DESIGNS.

	[6] ¹	[8] ¹	[7] ¹	[5] ²	This work ¹
V_{DDA} (V)	0.2	N/A ⁵	-0.1,0.1	0.2	0.2
Node (nm)	28	45	55	65	180
Area (μm^2)	34	3.91	98.6	35	50.2
Area/ L_{min}^2	39,540	1,930	32,595	8,284	1,549
f_{spike} (kHz)	343	6	400	25	18.37 ⁶
E_{spike} (fJ/spike)	1.2	N/A ⁵	1.95	4	1.06 ⁶
Tunability ⁴	No	No	No	No	Yes
C_m (fF)	3.4	N/A ³	varicap	4	N/A ³
C_f (fF)	3.4	N/A ³	varicap	8	N/A ³

¹ Post-layout simulation.

² Measurement.

³ Not applicable. Transistor-only designs.

⁴ Tunability is defined as the ability to adjust f_{spike} without changing I_{syn} .

⁵ Not available.

⁶ Obtained through a Monte Carlo simulation of 1,000 samples with V_{BP} at 0.1 V and I_{syn} at 10 pA.

V. CONCLUSION

This article examines the feasibility of adjusting the spiking frequency of a simplified Morris-Lecar neuron without changing its synaptic current. It was shown that by adjusting the body voltage of the PMOS reset transistor, the spiking frequency can be adjusted to compensate for $\pm 10\%$ change in the supply voltage and provide partial compensation for changes in temperature and process variations. The physical implementation of the design occupies an area of $50.2 \mu\text{m}^2$, a normalized area of 1,549, a spiking frequency of 18.37 kHz at 10 pA, and an energy efficiency of 1.06 fJ/spike in post-layout simulations.

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