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# Some aspects of beech biomechanics: juvenile wood properties, sapwood pre-stress and growth forces. 

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## Keywords

Beech; Growth stress; Wood properties; Variability; Radial variation


#### Abstract

The building of a tree is the result of wood growth through successive division, expansion and maturation of living cells at the periphery of the trunk and branches. During this process, diameter growth is combined with sapwood pre-stress to allow posture control by the generation of growth forces in the living wood cells. These mechanical aspects of tree building can be characterised at each peripheral position by parameters describing the amount of material produced, wood rigidity and the strain induced by the maturation process. In-situ assessment of maturation strains at the trunk periphery of beech trees, combined with laboratory measurements of ring width $(R W)$, wood density $(D)$ and wood specific modulus $(S M)$, was used to examine biomechanical aspects of juvenility corresponding to young stages of the tree, as well as the correlation or trade-off between sapwood pre-stressing and the generation of forces in the living wood layer used to control tree posture. The radial variations of $R W, D$ and $S M$, averaged over 86 trees, were close to the "typical radial pattern" of juvenile wood for softwood plantation trees: decrease in $R W$ and increase in $D$ and $S M$ from pith to bark in the juvenile phase. But $D$ only increased in the very first rings, then remained more or less constant. Furthermore, for all three parameters there were many discrepancies in the pattern of variation between trees and even between plots. This is a good indication that the mechanical juvenility of the wood was more related to the biomechanical conditions experienced by the trees in the young ages than to the age of the tree as such (which is the case for fibre length). The level of pre-stress and posture control forces were strongly dependent on the maturation strain as the first explanatory factor. But pre-stress is independent of $R W$, whereas posture control force is strongly dependent on this growth parameter. This opens the way to trade-offs between these two biomechanical functions of wood fibres.


## 1. Introduction

Wood growth is the process used for tree building (Thibaut 2019) including simultaneously primary growth by elongation or creation of twigs (bud role) and secondary growth by thickening of existing woody axes (cambium role). Primary growth is mostly assessed by the trunk slenderness relating primary growth (HT, total height) to secondary growth (DBH, diameter at trunk basis) at each growth step. Trunk, as a first-order axis, plays the major role in tree biomechanics and its building process is the most studied, mainly through secondary growth (Fournier et al 1991, Thibaut et al 2001, Alméras \& Clair 2016). The variation of growth parameters characterizing wood structure and properties is dependent on tree ontogeny and adaptation to changes in the environment of the tree during its life. Juvenility, in particular, describes the evolution of wood parameters during the early years of tree life. But the environment of the tree (access to light, wind influence, etc.) also changes during the young period of tree growth and mechanical adaptation of wood growth occurs in answer to these changes. In this paper, the data obtained on a large panel of beech trees in the context of a European collaborative program "Stresses in beech" (Becker \& Beimgraben 2001) will be exploited to characterize the patterns of radial variation of wood properties. The study will be preceded by the presentation of typical patterns observed in trees according to the literature.

## 2. State of the art on the spatial variations of wood properties

### 2.1 Secondary growth descriptors and mechanical parameters

Secondary growth performed by living wood cells (Raven et al 2007, Savidge 2003, Thibaut 2019) consists of the following successive steps: division of the cambium stem cells into daughter cells; expansion of daughter cells until the end of primary wall formation; thickening of the fibre (or tracheid) cell walls until the end of secondary wall formation; lignification of the whole cell wall, including the compound middle lamella; programmed cell death.
During this living period of wood cells, basic wood features are achieved. They can be described by ring width ( $R W$ in m ), result of combined cell division and expansion, density ( $D \mathrm{in} \mathrm{kg} / \mathrm{m}^{3}$ ) expressing cell wall thickening, specific modulus ( $S M$ in $\mathrm{Mm}^{2} / \mathrm{s}^{2}$ ) determined by the cellulose micro-fibril organisation in the cell wall, and maturation strain ( $\alpha_{m}$, no unit) resulting from the final polymerization of lignin and other macromolecular processes (Thibaut \& Gril 2021).
Some useful mechanical parameters can be calculated from these basic growth descriptors for an elementary growth unit (Fig. 1):
$R W(\mathrm{~mm})$ : local ring width, used as secondary growth layer width $\Delta \mathrm{r}$;
$R S=10 . \Delta \theta \cdot R \cdot R W$ (in $\mathrm{cm}^{2}$ ): ring portion surface for a distance to pith $R$ and angular sector $\Delta \theta$;
$R M=R S . D$ (in $\mathrm{kg} / \mathrm{m}$ ): mass per unit length of the ring portion;
$M O E=S M . D$ (in GPa): longitudinal modulus of elasticity;
$\sigma_{m}=$ MOE. $\alpha_{m}$ (in MPa): maturation stress, the pre-stressing of the peripheral layer in the sapwood, mostly made of dead fibres or tracheids;
$R F=100 . R S . \sigma_{m}(R F$ in N$)$ : local ring force.


Fig. 1: Local elementary growth unit in a trunk.
(L, r, $\theta$ ) : cylindrical coordinate system associated to the trunk
(L, R, T): Cartesian coordinate system associated to the elementary growth unit

### 2.2. Secondary growth variations within a trunk section.

All secondary growth descriptors display spatial variation within a portion of trunk, in the 3 cylindrical directions: transversely across radii (Tar), around the perimeter (Ap) and longitudinally along the stem (Las), called variation "TarApLas" within the tree by Savidge (Savidge 2003). These variations are linked either to the effect of tree age (called juvenility) or to the adaption of the wood growth to external conditions (climate, light availability, accidental leaning ...).
Variations around the perimeter in a given ring are related to a mechanical adaption in the control of posture, i.e. oblique growth in a given direction (in the case of coppice or for the search of light) or progressive change of axis curvature, either to restore verticality after accidental inclination of the tree (Alméras et al 2009) or to change the orientation of the branches after the death of the apex (Fournier et al 1994). Maturation strain asymmetry is the growth parameter most involved in posture regulation (Alméras et al 2005) and there are often large variations between the two sides of the axis (Thibaut \& Gril 2021).
The variations along the stem deals with primary growth: i) succession of connected zones and free-from-branching portions of the axis and ii) ageing of the terminal bud in the successive growth unit. Apart from the vicinity of the branching zones, the variations are rather slow (Savidge 2003).
Radial variations, from pith to bark at a given height level can be divided in two types: i) intraring short distance changes mostly due to intra-annual climatic changes and ii) variations of mean intra-ring properties linked both to cambium ageing (juvenility) and to the adaption of secondary wood growth to tree mechanics at each growth step (gravity and wind forces depending on tree slenderness and crown development). It is not easy to separate the effects of age per se (time since birth of cambium in the growth unit) and of the mechanical situation of the tree at different growth ages (light availability, wind protection).

The biggest variations in dimensions and environment for a given tree over time occur during the young ages, and so are the variations of wood properties showing higher radial gradients in the inner part of the axis. This inner part, where gradients are monotonously higher (in algebraic value), is called juvenile wood or core wood depending on the authors (Lachenbruch 2011) and their opinion concerning the main factor (juvenility or adaptation).
A good description is given in (Bendtsen \& Senft 1986) for a softwood and a hardwood. Loblolly pine (Fig. 2) is an example of the typical radial pattern (TRP) of juvenility (Lachenbruch et al 2011): i) initial increase of tracheid length, specific gravity and specific modulus, initial decrease of ring width and microfibril angle (MFA); MFA variations are closely, negatively related to those of SM. This is the general case in softwood plantation trees (Crown \& Dowling 2015, Larson et al 2001).


Fig. 2: Radial variations for Loblolly pine, after Bendtsen \& Senft (1986).

For Eastern cottonwood (Fig. 3), the ring width initially increases and there is no variation in specific gravity. The variations in fibre length and specific modulus are similar to those of TRP. There is again a highly significant, negative relationship between MFA and SM.


Fig. 3: Radial variations for Eastern cottonwood, after Bendtsen \& Senft (1986).
Variations in tracheid or fibre length always share the same initial positive gradient for all trees, whether softwood or hardwood (Koubaa et al 1998, Larson et al 2001, Bhat et al 2001, Bao et al 2001, Kojima et al 2009). This parameter is important for the paper industry (Koubaa et al 1998) but is not cited as a factor influencing the mechanical properties of wood (Kollmann \& Côté 1968, Kretschman 2010). The results of initial variations of $R W, S G$ and $S M$ can vary considerably from tree to tree, with flat, positive or negative initial gradients (Bhat et al 2001, Mc Lean et al 2011).

There is very little data on the variation of the average maturation strain within a ring as a function of cambium age or radial position in a log. It has been suggested that the maturation strain can change from positive values (compression stress) in the most juvenile rings compared to negative values (usual tension stress) in older rings, for softwoods (Fournier et al 1990). For hardwoods (Eucalyptus and poplar), plantations of clones at different ages ( 3 trees per age) for the same clone in the same environment have been used for in-situ measurements of maturation strains (Baillères 1994, Gérard 1994, Thibaut et al. 1996). No clear influence of age was found (see data for poplar).
In order to know, a-posteriori, the values of the maturation strains for each ring of a log, the relationships between local maturation strain and wood parameters at trunk periphery were investigated (Thibaut \& Gril 2021). Longitudinal shrinkage is a good parameter in case of reaction wood (compression or tension wood). But, until now, no relationship has been established to estimate the maturation strains from wood parameters (cell wall structure of chemical composition) for normal wood, although there are important variations of maturation strain within normal wood around the periphery of the trunk (Jullien et al 2013).
It can be hypothesized that initial fibre length gradient is mainly related to age per se (true juvenility) while adaption is often the dominant causality for $R W, S G$ and $S M$, and probably also for maturation strain.

## 3. Material and methods

### 3.1. Material

Within the framework of a European collaborative programme called "Stresses in beech", nine beech forests, representative of European forest management, were selected in 5 countries (Austria, Denmark, France, Germany and Switzerland) (Becker \& Beimgraben 2001). The age of the selected trees varied from 70 to 200 years. Maturation strain at 8 peripheral positions was measured on 440 standing beech trees from the 9 plots (Jullien et al 2013).
In each plot, 10 trees ( 86 in total) were selected for the measurement of wood properties. One small $\log$ of 50 cm length was cut at a height of 4 m for each tree. Each small $\log$ was cut into radial boards, through the pith, from North to South. These boards were air-dried to an average moisture content of $13.5 \%$ (equilibrium at $20^{\circ} \mathrm{C}$ and $65 \% \mathrm{RH}$ ) and cut into 1259 rods of 20 mm in radial, 20 mm tangential and 360 mm longitudinal direction, from the pith outwards (Fig. 4). Those with irregularities or cracks were discarded.


Fig. 4: Diagram of the sawing of the rod after the sawing of a North-South diametrical board. Numbering both for Northern and Southern parts of the board start with pith position. The coloured parts evoke the case of redheart occurrence.

The rods were numbered according to their position in the board and their distance to pith (DP) was measured. At the same time, the number of rings at both ends of the samples was recorded and the mean annual ring width of the rod $(R W)$ was calculated as the ratio of the mean radial dimension to the number of rings. The presence of red heartwood was also noted for the rods located in the core, in relation to a previously published work (Liu et al 2005).

### 3.2. Measurement of density and specific modulus.

All measurements were done in a regulated room at a temperature of $20^{\circ} \mathrm{C}$ and a relative humidity of $65 \%$.
The density $(D)$ was calculated by measuring the weight ( $W$ ) and the dimensions $R, T, L$ of the rod in direction R, T, L, respectively: $D=W /($ R.T.L). The specific gravity $(S G)$ is the ratio between $D$ and water density.
To measure the specific modulus ( $S M, 10^{6} \mathrm{~m}^{2} / \mathrm{s}^{2}$ ), each rod is positioned on fine wires and set in free vibration by a hammer stroke. The analysis of the sound vibration by fast Fourier transform gives the values of the three highest resonance frequencies which are interpreted using Timoshenko solution (Brancheriau \& Baillères 2002, Brancheriau 2006). The modulus of elasticity $(M O E)$ can be calculated as: $M O E=D . S M$.

### 3.3. Statistical analysis

Basic statistical analyses were performed using XLSTAT software. The data description table includes the number of data, the minimum, maximum and mean values for each parameter, as well as the coefficient of variation $(C V)$. The normality of the distribution is verified by ShapiroWilk test. A Pearson correlation analysis is used in the case of a normal distribution, and a Spearman correlation analysis in the case of a non-normal distribution, which is the majority of cases.

## 4. Results and discussion

### 4.1. Radial variations of properties

By giving positive values for the distance to the pith on the North side and negative values on the South side, it is possible to draw the South-North profile of each parameter ( $R W, S G, S M$, $M O E)$ for each tree, as a function of the diametrical position $(D P)$. If there was an increase of the parameter from pith position, the profile is noted "Up", "Down" for the reverse case and "Flat" when the variation was not clearly up or down. In case of clear asymmetry between the Southern and Northern parts by visual observation, the sample was noted as asymmetric (Fig. 5).


Fig. 5 Examples of clearly asymmetric North-South profiles.
There was a large majority of symmetrical patterns (Table 1).

Table 1 Percentage of profile types per plot within each or wood parameter.

| Para. | Ring width |  |  |  | Density |  |  |  | Specific modulus |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| PLOT | Up | Down | Flat | Sym | Up | Down | Flat | Sym | PLOT | Up | Down | Flat |
| 1 | $57 \%$ | $43 \%$ | $0 \%$ | $70 \%$ | $0 \%$ | $25 \%$ | $75 \%$ | $40 \%$ | 1 | $57 \%$ | $43 \%$ | $0 \%$ |
| 2 | $67 \%$ | $11 \%$ | $22 \%$ | $90 \%$ | $11 \%$ | $0 \%$ | $89 \%$ | $90 \%$ | 2 | $67 \%$ | $11 \%$ | $22 \%$ |
| 3 | $63 \%$ | $0 \%$ | $38 \%$ | $80 \%$ | $30 \%$ | $0 \%$ | $70 \%$ | $100 \%$ | 3 | $63 \%$ | $0 \%$ | $38 \%$ |
| 4 | $70 \%$ | $10 \%$ | $20 \%$ | $100 \%$ | $20 \%$ | $0 \%$ | $80 \%$ | $50 \%$ | 4 | $70 \%$ | $10 \%$ | $20 \%$ |
| 5 | $43 \%$ | $14 \%$ | $43 \%$ | $70 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $60 \%$ | 5 | $43 \%$ | $14 \%$ | $43 \%$ |
| 6 | $86 \%$ | $0 \%$ | $14 \%$ | $88 \%$ | $50 \%$ | $0 \%$ | $50 \%$ | $100 \%$ | 6 | $86 \%$ | $0 \%$ | $14 \%$ |
| 7 | $22 \%$ | $56 \%$ | $22 \%$ | $90 \%$ | $43 \%$ | $14 \%$ | $43 \%$ | $70 \%$ | 7 | $22 \%$ | $56 \%$ | $22 \%$ |
| 8 | $67 \%$ | $17 \%$ | $17 \%$ | $60 \%$ | $100 \%$ | $0 \%$ | $0 \%$ | $70 \%$ | 8 | $67 \%$ | $17 \%$ | $17 \%$ |
| 9 | $14 \%$ | $57 \%$ | $29 \%$ | $88 \%$ | $40 \%$ | $0 \%$ | $60 \%$ | $63 \%$ | 9 | $14 \%$ | $57 \%$ | $29 \%$ |
| Mean | $54 \%$ | $23 \%$ | $23 \%$ | $82 \%$ | $44 \%$ | $4 \%$ | $52 \%$ | $71 \%$ | Mean | $54 \%$ | $23 \%$ | $23 \%$ |

Para.: Wood parameter; Up: initial increase of the parameter from pith to bark; Down: initial decrease of the parameter from pith to bark; Flat: no clear initial increase or decrease; Sym: proportion of globally symmetrical profiles between North and South directions.

Globally there were no noteworthy difference between the Northern and Southern samples (Table 2).

Table 2 Comparison of parameter values North and South.

| Position (Nb) | $R W(\mathrm{~mm})$ | $S G\left(\mathrm{~kg} / \mathrm{m}^{3}\right)$ | $S M\left(10^{6} \mathrm{~m}^{2} / \mathrm{s}^{2}\right)$ | $M O E(\mathrm{GPa})$ |
| :--- | :--- | :--- | :--- | :--- |
| North (637) | 2.32 | 0.695 | 22.06 | 15.33 |
| South (622) | 2.28 | 0.694 | 22.39 | 15.54 |
| \% Sym. | $82 \%$ | $71 \%$ | $76 \%$ | $70 \%$ |

$R W$ : mean ring width; $S G$ : mean specific gravity; $S M$ : mean specific modulus;
MOE: mean longitudinal modulus of elasticity; Nb : number of rods;
\%Sym: proportion of diametrical patterns considered symmetrical for each parameter.
In each case, the occurrence of rods for each successive radial position within the trees or plots was examined (Fig. 6). Up to 18 cm from the pith, all the plots are concerned and there are always more than $70 \%$ of the trees concerned, values lower than $100 \%$ being due to defect occurrence close to the pith. This proportion decreases rapidly for larger distances from the pith, due to variable log size. It is therefore preferable not to use rods with a radial distance of more than 18 cm to calculate the mean values of the parameters at the global scale.


Fig. 6 Percentage occurrence of rods for each successive radial position within trees or plots $100 \%$ means that there are used rods at a given radial position in every tree or every plot.

There are notable differences between trees for each parameter, both in value and in pattern. Globally, there is no significant difference between the Northern and Southern samples (Fig. 7). It is thus allowable to mix the beech rods of the Northern and Southern specimens for further analysis of the mean radial variation patterns at the global or plot level.


Fig. 7 Number of rods and parameter values for all trees as a function of diametrical position (DP) Bolt dots: mean value; thin dashes: mean value + or - standard deviation.

Moreover, some trees have a part of red core-wood portion and the effect it may have on properties was investigated. All trees (25) without any red rod (except sometimes one near the pith) were considered as white beech while all trees with more than two red rods were considered as red beech. The mean radial variations for red and white beech trees were calculated (Fig. 8). Due to the variability between the trees, no clear difference could be observed between the mechanical properties of red and white beech wood.


Fig. 8 Values of parameter for all red and no-red hearted trees as a function of radial position. Bolt dots: mean value; thin dashes: mean value + or - standard deviation.

Red dots: red heartwood; black dots white heartwood
It is thus allowable to mix Northern and Southern specimens of red and white beech rods for further analysis of the mean radial variation patterns at the global or plot level.
The global mean radial patterns for these beech trees were as follows (Fig. 9):

- $\quad R W$ decreases regularly ( 2.6 to 2.2 mm ) from pith to bark;
- $S G$ increases a little ( 0.703 to 0.709 ) at the beginning (up to about 4 cm radius) and decreases thereafter ( 0.709 to 0.686 ), but the variations are small;
- $S M$ increases ( 20.8 to $22.8 \mathrm{~m}^{2} / \mathrm{s}$ ) for a rather long time (up to about 12 cm radius) and then decreases ( 22.8 to $22.2 \mathrm{~m}^{2} / \mathrm{s}^{2}$ ) regularly;
- the MOE pattern is very similar to the $S M$ pattern.


Fig. 9 Mean radial distribution of indicators and modulus of elasticity for all rods.
Bolt dots: mean value; thin dashes: mean value + or - standard deviation.
A ratio of 3 has been set for all graphs between maximum and minimum values of the ordinate axis.
The variability between trees (standard deviation values) is high for $R W$ but low for $S G$. It is slightly higher for $S M$ and $M O E$ (Table 6).
The mean patterns of the plots (Fig. 10) are more irregular due to the smaller number of rods, but, more or less, the global mean pattern is the most frequent. There are differences between plots, in the mean level of properties and sometimes in the pattern, mainly for $R W$, with some plots having increasing $R W$ (plot 7 and 9).


Fig. 10 Mean radial variations of properties at the plot level
Mean: mean values for all rods at each radial position.
It is interesting to look at the evolution of the ring surface from pith to bark, using the radial position (PoRa) and the mean ring width of each rod:
RSra $=2 \pi$.PoRa.RW
The evolution of the mean values of all $R S r a$ at the same radial position for all trees in a plot, from pith to bark (Fig. 11), is a signature of the trunk surface growth for the plot. For these beech plots, the ring surface can be considered proportional to the distance from the pith with a regression coefficient $\left(\mathrm{R}^{2}\right)$ always above 0.96 (Table 3):
$\mathrm{RSra}=\mathrm{K} . \mathrm{PoRa}$
K has a mean value of $1.43 \mathrm{~cm}^{2} / \mathrm{cm}$, and ranges from 1.09 to 1.88 . This kind of linear growth quasi proportional to distance to pith together with K values can be considered as a result of forest management in these European plots.

Table 3 Proportional coefficient $(\mathrm{K})$ and $\mathrm{R}^{2}$ values for linear regressions

| Plot | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Mean |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| K | 1.25 | 1.14 | 1.69 | 1.47 | 1.28 | 1.44 | 1.88 | 1.09 | 1.63 | 1.43 |
| $\mathrm{R}^{2}$ | 0.98 | 0.96 | 0.99 | 0.98 | 0.98 | 0.96 | 0.98 | 0.98 | 0.98 | 0.99 |



Fig. 11 Variation of ring surface $\left(\mathrm{cm}^{2}\right)$ with distance to pith ( cm ) for each plot.
Mean: regression for mean values

### 4.2. Global results

### 4.2.1. Global results at rod level

Table 4 and 5 give global description and correlation within the data for all samples ( 1259 rods).
Table 4 Parameter description for all rods

| 1259 rods | RW | SG | SM | MOE |
| :--- | :--- | :--- | :--- | :--- |
| Minimum | 0.67 | 0.55 | 11.08 | 8.00 |
| Maximum | 6.67 | 0.83 | 27.49 | 21.30 |
| Mean | 2.30 | 0.69 | 22.22 | 15.44 |
| Max/min | 10.00 | 1.51 | 2.48 | 2.66 |
| C. V. | $35.0 \%$ | $6.2 \%$ | $10.9 \%$ | $13.0 \%$ |

$R W(\mathrm{~mm})$ : ring width; $S G$ : specific gravity; $S M\left(10^{6} \mathrm{~m}^{2} / \mathrm{s}^{2}\right)$ : specific modulus;
MOE (GPa): longitudinal modulus of elasticity.
The variations of $S G$ between samples are very low (coefficient of variation $6 \%$ ).
Table 5 Correlation table for all rods

| 1259 rods | RW | SG | SM | MOE |
| :--- | :--- | :--- | :--- | :--- |
| RW | 1 | 0.215 | -0.313 | -0.167 |
| SG | 0.215 | 1 | 0.047 | 0.506 |
| SM | -0.313 | 0.047 | 1 | 0.884 |
| MOE | -0.167 | 0.506 | 0.884 | 1 |

$R W$ : ring width; $S G$ : specific gravity; $S M$ : specific modulus; $M O E$ : longitudinal modulus of elasticity. Bold numbers: correlation significant at $0.1 \%$ level.

There is no significant correlation (at the $5 \%$ level) between $S G$ and $S M . R W$ has a very significant correlation (at the $0.1 \%$ level) positively with $S G$ and negatively with $S M$. Thus, the correlation between $R W$ and $M O E$ is negative with a lower coefficient of determination (3\%). In the determination of $M O E$ from $S M$ and $S G$, the coefficient of determination (square of the correlation coefficient given in Table 5) is three times higher for $S M(78 \%)$ than for $S G(26 \%)$.

### 4.2.2. Global results at tree level

Tables 6 and 7 give the description and correlation table for tree dimension and mean per tree. Variability of parameters is significantly lower for tree mean values, and notably low for $S G$.

Table 6 Parameter description for tree mean values

| 86 trees | RW | D | SM | MOE |
| :--- | :--- | :--- | :--- | :--- |
| Minimum | 1.29 | 0.63 | 17.6 | 12.0 |
| Maximum | 4.78 | 0.78 | 25.6 | 19.3 |
| Mean | 2.28 | 0.70 | 22.4 | 15.6 |
| Max/min | 3.70 | 1.24 | 1.46 | 1.60 |
| C.V. | $24.9 \%$ | $4.8 \%$ | $7.6 \%$ | $9.5 \%$ |

$R W(\mathrm{~mm})$ : ring width; $S G$ : specific gravity; $S M\left(10^{6} \mathrm{~m}^{2} / \mathrm{s}^{2}\right)$ : specific modulus; $\operatorname{MOE}(\mathrm{GPa})$ : longitudinal modulus of elasticity.

Except for $R W$, the mean wood properties per tree show rather low variations between trees (very low for $S G$ ).

Table 7 Correlation table for all trees

| 86 Trees | RW | D | SM | MOE |
| :--- | :--- | :--- | :--- | :--- |
| RW | 1 | 0.122 | -0.388 | -0.252 |
| D | 0.122 | 1 | 0.140 | 0.602 |
| SM | -0.388 | 0.140 | 1 | 0.874 |
| MOE | -0.252 | 0.602 | 0.874 | 1 |

$R W$ : ring width; $S G$ : specific gravity; $S M$ : specific modulus; $M O E$ : longitudinal modulus of elasticity. Bold numbers: correlation significant at $0.1 \%$ level.

Among the wood properties, $R W$ and $S M, S M$ and $M O E, S G$ and $M O E$ remain highly significantly correlated ( $0.1 \%$ level) at the tree level.

### 4.2.3. Global results at plot level

Table 8 gives the description of tree dimensions and mean wood properties per tree for the 9 forest plots and Table 9 the correlation table for all plots. Except for $R W$, the mean wood properties per plot all show very little variation between plots.

Table 8 Parameter description for the 9 plots mean values

| Plot | Nb trees | RW | D | SM | MOE |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | 10 | 2.06 | 0.70 | 21.5 | 15.0 |
| 2 | 10 | 1.80 | 0.71 | 23.1 | 16.4 |
| 3 | 10 | 2.63 | 0.70 | 22.2 | 15.6 |
| 4 | 10 | 2.50 | 0.71 | 21.2 | 15.1 |
| 5 | 10 | 2.12 | 0.68 | 21.9 | 14.8 |
| 6 | 8 | 2.57 | 0.73 | 23.7 | 17.3 |


| 7 | 10 | 2.84 | 0.68 | 22.0 | 15.1 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 8 | 10 | 1.63 | 0.68 | 24.1 | 16.4 |
| 9 | 8 | 2.50 | 0.67 | 21.7 | 14.6 |
| Max |  | 2.8 | 0.7 | 24.1 | 17.3 |
| Min |  | 1.6 | 0.7 | 21.2 | 14.6 |
| Mean |  | 2.29 | 0.70 | 22.4 | 15.6 |
| Max/min |  | 1.74 | 1.08 | 1.14 | 1.18 |
| CV |  | $16.9 \%$ | $2.6 \%$ | $4.2 \%$ | $5.5 \%$ |

$R W(\mathrm{~mm})$ : ring width; $S G$ : specific gravity; $S M\left(10^{6} \mathrm{~m}^{2} / \mathrm{s}^{2}\right)$ : specific modulus; $\operatorname{MOE}(\mathrm{GPa})$ : longitudinal modulus of elasticity.

At the plot mean level, only the causal relationship between $M O E$ and SG or between $M O E$ and $S M$ remains significant at the $0.1 \%$ level (Table 9).

Table 9 Correlation table for all plots

| 9 Plots | RW | D | SM | MOE |
| :--- | :--- | :--- | :--- | :--- |
| RW | 1 | 0.154 | -0.446 | -0.266 |
| D | 0.154 | 1 | 0.252 | 0.671 |
| SM | -0.446 | 0.252 | 1 | 0.886 |
| MOE | -0.266 | 0.671 | 0.886 | 1 |

$R W$ : ring width; $S G$ : specific gravity; SM: specific modulus; MOE: longitudinal modulus of elasticity. Bold numbers: correlation significant at $0.1 \%$ level.

### 4.3. Pre-stressing and growth forces

In situ measurements on standing trees give values of GSI for North and South sides at breast height for each tree (Jullien et al 2013). $R W, S G$ and $S M$ values are measured in laboratory for the last rods (farthest away from pith) at North and South positions and 4 m high in the tree. We can expect that these 3 wood parameters are good estimations for the values at breast height level.

All the North and South values labelled with the subscript last for wood parameters were gathered in the same sheet (Maturation): distance to pith ( $D P_{\text {last }}$ in cm ), ring width ( $R W_{\text {last }}$ in mm ), specific modulus ( $S M_{\text {last }}$ in $10^{6} \mathrm{~m}^{2} / \mathrm{s}^{2}$ ), longitudinal modulus of elasticity ( $M O E_{\text {last }}$ in GPa ) of the last rod (North \& South), GSI (North \& South) for the 86 trees.
Firstly, the calculation of maturation stress (pre-stressing value) and growth force needs green wood values for parameters such as $D P, R W$ and $M O E$. In the literature (Cirad 2015) we can find a mean value for radial shrinkage ( $R S=5.7 \%$ ) and fibre saturation point $(F S P=32 \%)$ of beech wood. The moisture content of the rods was $13.5 \%$, which is $18.5 \%$ below FSP. The increase in radial dimension between the air-dry and green state of the wood can be estimated by the shrinkage proportion ( $P S$ ):

$$
P S=5.7 \% \times 18.5 \% / 32 \%=3.3 \%
$$

Thus the width of the green ring $\left(R W_{g}\right)$ and green distance to pith $\left(D P_{g}\right)$ can be obtained from the air dry values ( $R W$ and $D P$ ) by the formulas:

$$
R W_{g}=1.033 R W: D P_{g}=1.033 \mathrm{DP}
$$

and ring portion surface $\left(R S_{g}\right)$ is calculated as $R S_{g}=\Delta \theta \times D P_{g} \times R W_{g}$, where the angular sector $\Delta \theta$ corresponding to a given $G S I$ value is taken as $\pi / 4$.

Air dry (MOE) and green $\left(\mathrm{MOE}_{g}\right)$ longitudinal modulus of elasticity are proportional according to the formula (Thibaut \& Gril 2021):

$$
M O E_{g}=0.8943 \times M O E
$$

It is also necessary to convert GSI values into maturation strains ( $\alpha_{m}$ ) using the conversion factor FI (Thibaut \& Gril 2021):

$$
\alpha_{m}=F I \times G S I
$$

$F I$ can be calculated from the formula:

$$
F I=-0.475 \times S M_{b}+25.24
$$

$S M_{b}$ is the basic specific modulus which is proportional to the specific modulus $S M$ (Thibaut \& Gril 2021):

$$
S M_{b}=1.1068 \times S M ; \text { so } F I=-0.5257 \times S M+25.24
$$

Using the values of the maturation strain $\alpha_{m}$ and green $M O E$, the value of the maturation stress (which is the value of the tensile pre-stress at the periphery of the trunk) can be calculated:

$$
\sigma_{m}=M O E_{\mathrm{g}} \times \alpha_{m}
$$

Then, the local force generated on the unit ring portion ( $\Delta F$ in N ) by the maturation process can be calculated:

$$
\Delta \mathrm{F}=\mathrm{RS}_{\mathrm{g}} \times \sigma_{\mathrm{m}}
$$

For the 3 explaining factors $\left(R S_{g}, M O E_{g}, G S I\right)$, the variability is rather low for $M O E$, high for local ring surface and very high for GSI. Thus it is also very high for local maturation strain, maturation stress (pre-stressing value) and growth force (Table 10).

Table 10 Statistical description of maturation parameters

|  | $\Delta \mathrm{S}_{\mathrm{g}}$ | MOEg | GSI | FI | $\square_{\mathrm{m}}$ | $\square_{\mathrm{m}}$ | $\square \mathrm{F}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Mean | 4.04 | 13.7 | 83 | 13.6 | 1109 | 15.4 | 6025 |
| Median | 3.60 | 13.9 | 70 | 13.4 | 941 | 12.3 | 4335 |
| Minimum | 0.77 | 8.4 | 0 | 10.8 | 0 | 0.0 | 0 |
| Maximum | 10.80 | 19.1 | 251 | 18.6 | 3103 | 47.6 | 23342 |
| CV | $45 \%$ | $15 \%$ | $68 \%$ | $10 \%$ | $66 \%$ | $70 \%$ | $79 \%$ |

$R S_{g}\left(\mathrm{~cm}^{2}\right)$ : local ring surface; $M O E_{g}(\mathrm{GPa})$ : longitudinal modulus of elasticity of the last ring; GSI $(\mu \mathrm{m})$ growth stress indicator measured in situ on standing tree;
$F I$ conversion factor between $G S I$ and maturation strain; $\alpha_{m}$ : maturation strain $\left(10^{-6}\right)$; $\sigma_{m}(\mathrm{MPa})$ : maturation stress; $\Delta F(\mathrm{~N})$ : local growth force. $C V$ : coefficient of variation.

Both pre-stressing and growth force are strongly related to maturation strain ( $\mathrm{R}^{2}=92 \%$ and $62 \%$ respectively) through proportional laws. Growth force and pre-stressing are very significantly correlated but $35 \%$ of growth forces variations are not explained by pre-stressing variations (Fig. 12).


Fig 12: Relationships between growth forces, maturation strain or growth stress indicator, and maturation stress.

### 4.4. Discussion and conclusion

There are few published results relating to radial variations of mechanical parameters in large trees of high forests that are not the result of plantation. In Europe, old growth beech forests can have different forest origins: i) even-aged (France or Germany) or uneven-aged high forest (Switzerland), coppicing with standards (France) or conversion of coppice forest into high forest (Ciancio et al 2006) (Germany, France) but are very rarely the result of plantations (none in the 9 plots). Fagus is known for its shade tolerance and ability to grow very slowly under a closed canopy (Collet et al 2011) and most forest plots undergo more or less severe thinning before final harvesting, which leads to an increase of $R W$ due to better access to light (Noyer et al 2017). This is reflected in the different mean $R W$ radial patterns for the 9 plots (Fig. 10). For plots 7 and 9 , a clear increase of $R W$ is observed in the young ages, while the reverse and classical pattern is true for plots 2,4 and 6 . Similar results were found on younger beech trees (Bouriaud et al 2004).
As a mean for these high forest beech trees, the radial patterns of variations are partly similar to the typical radial pattern for $R W$ and $S M$. $S G$ has a very small decreasing variation. But looking tree by tree, there are all types of patterns (increasing or decreasing at the beginning) for all parameters ( $R W, S G$ and $S M$ ). This supports the hypothesis of an "adaptation" for "mechanical" juvenility.
Due to the very low variability of the $S G$ of beech wood, the variations of $S M$ are much more important than those of $S G$ in order to explain the variations of $M O E$.

The high level of inter-tree variability ( $\mathrm{CV}=66 \%$ ) for pre-stressing $\left(\sigma_{m}\right)$ is massively due to variations in maturation strains combined with variations in $M O E$, while for growth forces ( $\triangle F$ ), the high level of variability between trees ( $\mathrm{CV}=79 \%$ ) is also mainly linked to variations in maturation strains combined with variations in local ring surface and MOE (Table 11). Although growth force and maturation stress are very significantly linked ( $\mathrm{R}^{2}=64 \%$ ) due to the influence of the maturation strain, the ring width has no influence on pre-stressing and appears to be a possible trade-off parameter between the two mechanical functions of growth forces: pre-stressing of trunk periphery and posture control of axis position.

Table 11 Contribution of several factors to the variance of local growth force and maturation stress

| $\mathrm{R}^{2}$ | $\alpha_{\mathrm{m}}$ | $\mathrm{MOE}_{\mathrm{g}}$ | $D P_{\text {last }}$ | $R W_{\text {last }}$ | $\mathrm{RS}_{\mathrm{g}}$ |
| :---: | :---: | :--- | :--- | ---: | ---: |
| $\Delta \mathrm{F}$ | $61.8 \%$ | $5.0 \%$ | $9.4 \%$ | $11.7 \%$ | $17.2 \%$ |
| $\sigma_{\mathrm{m}}$ | $92.5 \%$ | $11.6 \%$ | $0.4 \%$ | $0.6 \%$ | $0.9 \%$ |

$\mathrm{R}^{2}$ : coefficient of determination; $\Delta F$ : local growth force; $\sigma_{m}$ : maturation stress; $\alpha_{m}$ : maturation strain; $M O E_{g}$ : modulus of elasticity in green state; $D P_{\text {last: }}$ distance to pith of last ring; $R W_{\text {last: }}$ width of last ring; $R S_{g}$ : ring portion surface.

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## Data

The original data used in this paper are available at: https://zenodo.org/record/8103568.

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