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Iron-doped CaTiO₃ and Pd/YSZ dual bed catalytic system for CH₄ emission control from Natural Gas Vehicle.

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Abstract

The catalytic treatment of residual traces of refractory methane in the exhaust gas from NGV engines involves the use of expensive, highly loaded precious metal based catalysts. Recently, it was demonstrated that the association of a perovskite with a Pd/YSZ (Yttria-Stabilized Zirconia) catalyst improved both the oxygen exchange behavior on the YSZ support together with the methane oxidation on palladium. However, these interesting results were obtained in condition quite far from an exhaust pipe and this work aims to investigate the concept of this dual catalytic bed system in more realistic conditions. In this study, a mixed electronic/ionic conducting perovskite (CaTi_{0.7}Fe_{0.3}O_{3- δ}) was associated to a pure oxygen ion conductor (YSZ) impregnated with 1% palladium. This dual-bed configuration promoted CH₄ abatement in lean mixture, probably associated to the Pd/PdO active phase formation, but inhibiting effect of both CO₂ and H₂O was also observed.

Keywords: Methane, NGV, Palladium, YSZ, dual-bed

1. Introduction

To address the growing energy dependence on traditional fossil fuels and the environmental concerns, the use of natural (bio)gas, which mainly contains methane (90 %), becomes attractive. Pending the development of other clean energy sources, methane has a high energy efficiency that, associated with lower carbon dioxyde emissions than other hydrocarbon fuels, offers a viable alternative for combustion engines. Moreover, locally produced biogas also induce lower greenhouse gas emission. Interestingly, engines powered by natural gas (NGVs) also produce lower NO_X and particulate matter emissions than diesel or gasoline engines [1]. Compressed or liquefied natural gas also powers 23 million vehicles worldwide with an annual increase of 20 %, from heavy-duty buses and trucks to light-duty passenger cars [2]. However, the relevance of this option resides in the abatement of unburnt methane in the exhaust gas because of its global warming potential 23 times higher than CO₂. Hence, the removal of residual traces of refractory methane in the exhaust stream remains a technological challenge which currently implies the use of expensive active materials, which lowers the cost-effectiveness of such alternative systems. Concerning the lean-burn NGVs powered engines, the temperature of the exhaust gas is generally below 500-550 °C [3] and CH4 oxidation post-treatment should occur in the 320-420 °C temperature range [4] for automotive application. This condition makes the activation of the C-H bond of methane challenging due to its high stability (bond energy: 450 kJ/mol). Among the many catalytic formulations investigated (metal oxide, spinel, perovskite...), platinum-group metals (PGM), are predominant and Pd-containing catalysts have been recognized to be the most active candidate [5]. Still, substantial research efforts for low temperature efficiency must be achieved. Numerous studies were

therefore devoted to the determination of the active phase of the supported palladium materials, depending on the working temperature. The nature of the active sites of Pd catalysts for methane oxidation has been a matter of debate for a long time. It is now recognized that PdO→ Pd phase transformations interplay in the methane oxidation activity. Richard et al. [6] reported that the active species of palladium is rather an oxidized state, but the precise nature of the active sites is still controversy since it remains conflicting evidence on the activity of different oxidation states of Pd. For instance, it has been reported that methane is activated on a site pair consisting of an oxygen atom and an oxygen vacancy on the PdO_x surface, suggesting a redox mechanism [7,8] where surface oxygen on the palladium crystallites is more active for methane oxidation than bulk oxide due to the higher ability of the oxygen sorption processes [9]. Methane interacts with oxygen on the PdO surface which is rapidly restored by diffusion of bulk oxygen to the surface. This proposed mechanism avoids the need for the coexistence of a separate Pd metal phase in atomic contact with PdO_x for methane oxidation. To the opposite, methane oxidation over the metallic Pd surface is controlled by competitive adsorption of methane and oxygen. Overall, PdO catalyzes CH₄ oxidation via a redox Mars and van Krevelen (MvK) mechanism (with C-H bond activation as the rate-determining step), while metallic Pd catalyzes the reaction via the Langmuir-Hinshelwood mechanism. The nature of catalyst structure in respect to palladium is also discussed in the literature as Pd clusters, Pd clusters surface-saturated with chemisorbed oxygen (O*), and PdO clusters [10]. The development of active materials dedicated to low temperature application for promotive CH₄ oxidation refers to the necessity of the coexistence of Pd^{0} , Pd in a reduced state (PdO_X), or oxygen vacancies. The synthesis methods are a tool to control the structurefunction of Pd-based catalyst.

Recently Richard *et al.* [6,11,12] proposed an innovative approach in which the methane conversion is boosted by the formation of active oxygen species. With this aim, the catalytic bed was made *via* the association of LaMnO₃+ $0.2_{wt%}$ Pd/YSZ materials. Yttrium-stabilized zirconia (YSZ) presents oxygen vacancies due to the doping of ZrO₂ with Y³⁺ which exhibits a lower valence state than Zr⁴⁺. In oxidation catalysis, the improved catalytic performance of YSZ has been attributed to this high concentration of oxygen vacancies [13]. The oxygen exchange behaviour of the Pd/YSZ catalyst was dramatically improved in the presence of LaMnO₃. Methane conversion measured in the isotopic exchange set-up also showed a significant improvement. It was postulated that LaMnO₃ perovskite activated the O₂ molecule as singlet oxygen, which was then transferred to Pd/YSZ and promoted the methane oxidation *via* a MvK mechanism. However, these interesting results were obtained in conditions quite far from an exhaust pipe, *i.e.* in a recirculating mode with low pressures of methane and oxygen.

In this work, we studied the viability of the concept using a more common synthetic gas bench. Moreover, in order to improve the oxygen exchange behavior compared to the previously implemented perovskite material (LaMnO₃), a mixed ionic and electronic conducting (MIEC) perovskite was selected for this study. Based on CaTiO₃ material with partial substitution of iron for titanium [14], the CaTi_{0.7}Fe_{0.3}O_{3- δ} formulation was chosen after preliminary tests with various rate of titanium substitution for iron (0 to 40 %). The second implemented catalytic system was 1_{wt%}Pd/YSZ. Several YSZ supports were preliminary evaluated. The YSZ oxide provided by TOSOH (8 mol % Y₂O₃-stabilized ZrO₂) was selected for its perfect stability under the reactional mixtures at 600°C. In addition to evaluation of the proof of the dual-bed concept in a more realistic setup, the influence of both CO₂ and H₂O was also examined in this work. Additionally, Pd/YSZ behaviors were compared to usual Pd/Al₂O₃ sample to highlight the role of palladium active phase formation.

2. Materials and Methods

2.1 Catalyst preparation

To perform the synthesis of the perovskite CaTi_{0.7}Fe_{0.3}O_{3-δ} (denoted as CTF₃₀), calcium nitrate tetrahydrate (99 %, Sigma Aldrich), titanium (IV) isopropoxide (97 %, Sigma Aldrich), iron (III) nitrate nonahydrate (98 %, Sigma Aldrich), palladium (II) nitrate (40,1 %, Enrico Faggi), citric acid (99,6 %, Sigma Aldrich) and glycerol (99,5 %, Sigma Aldrich) precursors were used as received without further purification.

Based on the Pechini method [15], the perovskite was prepared using an adapted protocol to obtained a well crystallized material with no secondary phase and exhibiting a high specific surface area. Ethylene glycol is usually used as chelating agent because of its ability to form an extended covalent network throughout the solution [16]. Based on internal preliminary results, glycerol was used in this study. The desired stoichiometric amount of titanium (IV) isopropoxide was added to the proper amount of glycerol following a cation/ glycerol molar ratio of 1/15. Because of its viscosity, the solution with glycerol was heated to 80 °C. After 45 min of stirring, citric acid was added to the mixture following a molar ratio of 1/7.5 for cation/acid, heated to 80 °C and covered with a watch glass, and stirred for 1 h 30 to dissolve the acid. Calcium nitrate was then added to the mixture and stirred again for 1 h to dissolve the precursor. Iron (III) nitrate was finally added and stirred again for 1 h. The mixture was then heated to 120 °C for 2 h under stirring to ensure the polycondensation of the product until a viscous gel was obtained. The resulting polymer gel was calcined in air in muffle oven first at 100 °C for 1 h (5 °C/min) and at 600 °C for 6 h (1.6 °C/min). The resulting perovskite was grinded and sieved between 125 μ m and 250 μ m for the catalytic testing.

YSZ (8 mol % Y₂O₃-stabilized ZrO₂) oxide was provided by TOSOH. YSZ-supported metal catalyst (denoted Pd/YSZ) was prepared by wet impregnation of the appropriate amount of palladium (II) nitrate to obtain 1 wt%. The excess of water was evaporated at 60 °C and the resulting powder was dried at 120 °C overnight before calcination at 600 °C during 6 h (5 °C/min) under air flow (150 mL min⁻¹).

A reference palladium supported alumina catalyst, denoted Pd/Al₂O₃, was also prepared with the same impregnation procedure as for Pd/YSZ sample. The Al₂O₃ support was provided by Axens.

2.2 Catalyst characterizations

X-ray diffraction analysis were carried out with a Bruker D8 Endeavor using a Bragg-Bentano ($\theta - \theta$) geometry equipped with a CuK_{α} cathode radiation source (40 kV and 40 mA). Diffractogram were qualitatively analysed with EVA software from Bruker and ICDD 2016 database. The crystallites sizes were calculated from the Debye-Scherrer equation. To determine lattice parameters of well crystallised CaTi_{0.7}Fe_{0.3}O_{3- δ}, the structure was refined by a full-profile analysis method using Full-Prof software [17] and ICSD data corresponding from CTF₃₀ (ICSD: 93085).

The nitrogen physisorption was performed at 77 K in a Micromeritics Tristar II 3020 instrument. The sample was outgassed under vacuum at 280 °C for 5 h before measurement. Surface area was calculated using the Brunauer-Emmett-Teller [18] (BET) method and the pore size distribution with the Barrett-Joyner-Halenda [19] (BJH) method with Faas correction applied to Halsey equation.

SEM micrographs were obtained with a JEOL FEG JSM-7900F scanning electron microscope operating between 1 kV and 15 kV (special resolution of 0.7 nm) and equipped with an energy-dispersive X-ray spectroscopy (EDXS)

detector. Transmission Electron Microscopy (TEM) micrographs were recorded on JEOL 2100 instrument (operated at 200 kV with a LaB6 source). EDX spectroscopy was carried out with a Hypernine (Premium) detector (active area: 30 mm²).

The palladium dispersion was determined by H_2 chemisorption performed using AutoChem 2920 from Micromeritics and 100 mg of Pd/YSZ. After *in situ* reduction under 10 % H_2 at 300 °C (5°C min⁻¹) for 1 h, the sample was flushed at the same temperature under argon for 3 h. The hydrogen was dosed on the sample at 105 °C to prevent hydride formation. After saturation, the sample was flushed under argon for 10 min and exposed again to hydrogen. The amount of chemisorbed hydrogen was taken as the difference between the two hydrogen exposures and exploited as H/M molar ratio. Dispersion (%) and particle size (nm) were determined based on the statistical cuboctahedron clusters model of Drault et *al.* [20].

Temperature programmed reduction experiments were performed on Pd-containing samples with a Micromeritics Autochem 2920 apparatus. The Sample (50 mg) was placed in a U-shaped quartz reactor. Prior the reduction, the catalyst was *in-situ* calcined at 600 °C for 30 min under O₂ (heating rate: 5 °C min⁻¹). After cooling to room temperature under argon, the sample was cooling down to -50°C (coolant setup from Micromeritics, based on the evaporation of liquid nitrogen). The reduction was carried out under 10 % H₂/Ar up to 400 °C (rate: 10 °C min⁻¹). The reduction was followed by a thermal conductivity detector (TCD). Because this TCD is sensitive to water, a H₂O trap was added downstream the reactor, allowing the quantification of the H₂ consumption.

The Isotopic Exchange experiments were performed in a home-made closed recycling system set-up connected to a Pfeiffer Vacuum quadrupole mass Spectrometer (QMS 200) to monitor the gas phase composition (with Quadera software). The recycling pump placed in the system removes limitation due to gas-phase diffusion (recirculation rate = 170 cm³.s⁻¹). Tests were performed on catalyst powder sieved between 125 µm and 250 µm. The sample was placed into a U-shaped quartz reactor with quartz wool above and below the catalyst. The involved sample masse was calculated to get the same initial oxygen concentration inside the reactor for all measurements. The sample was first subjected to pure ${}^{16}O_{2(g)}$ at 600 °C (10 °C/min, 1 h) prior cooling to 150 °C for Temperature-Programmed Oxygen Isotopic Exchange (TPOIE). The system was then purged under vacuum for 30 min. Pressure of 58 mbar ${}^{18}O_{2(g)} (\ge 99 \text{ at%})$, ISOTEC) was introduced in the system and the isotopomer distribution was analysed following the intensities of m/z: 32 (${}^{16}O_2$), 34 (${}^{18}O_1{}^{6}O$) and 36 (${}^{18}O_2$). The m/z values of 28 (N₂), 44 (C ${}^{16}O_2$), 46 (C ${}^{18}O_1{}^{6}$) and 48 (C ${}^{18}O_2$) were also recorded to ensure the absence of atmosphere entrance into the system or desorption of residual carbonated species at the beginning of the exchange process. TPOIE analysis was performed by varying the temperature from 150 °C to 700 °C. The partial pressures of ${}^{16}O_2$, ${}^{18}O_1{}^{6}O$ and ${}^{18}O_2$ are calculated by the ratio of corresponding intensities of the m/z values of 32, 34, 36 for ${}^{16}O_2$, ${}^{18}O_1{}^{6}O$ and ${}^{18}O_2$ isotopes, respectively. The atomic fraction of ${}^{18}O$ in the gas-phase (α_g) is determined by Eq. 1 [21]:

$$\alpha_{g} = \frac{P_{36} + \frac{1}{2}P_{34}}{P_{32} + P_{34} + P_{36}} \tag{1}$$

2.3 Catalytic tests

The catalytic CH₄ oxidation tests were carried out in a fixed bed set-up. For single catalyst test, 100 mg of the catalyst sieved between 125 μ m and 250 μ m and 100 mg of SiC were mixed and placed inside a quartz reactor. For catalytic tests with a combination of CTF₃₀ and Pd/YSZ materials (or Pd/Al₂O₃ sample), 100 mg of each sample samples were implemented, without SiC. Three configurations involving the association of CTF₃₀ and Pd/YSZ were evaluated: the "dual-bed" noted CTF₃₀+Pd/YSZ was composed of a layer of CTF₃₀ (upstream) in contact with a layer Pd/YSZ (downstream); the "reverse dual-bed" noted Pd/YSZ+CTF₃₀ was composed of a layer of Pd/YSZ (upstream) in contact with a layer CTF₃₀ (downstream); the "mechanical mixture" denoted CTF₃₀/Pd/YSZ was obtained by an intimate mixing the two powders. The total flow was kept constant to 20 L h⁻¹. Catalytic tests are performed from RT to 600 °C (3° min⁻¹), followed by a 30 min step at 600 °C before the cooling step. The compositions of the feed gas and effluent stream were monitored continuously during the temperature ascent and descent using online MKS 2030 Multigas infrared analyzer. Various lean gaseous mixtures were examined according to Table 1 and the activities of the different catalytic systems for methane oxidation were recorded successively, corresponding to three consecutive tests starting with the simplified media and then incrementing by adding first CO₂ and then also H₂O.

Feed/gases	Simplified media	Simplified media +CO ₂	complex media
CH4	1500 ppm	1500 ppm	1500 ppm
O2	10 %	10 %	10 %
CO ₂	-	10 %	10 %
H ₂ O	-	-	8 %
N2	balance	balance	balance

Table1. Gas feed composition (20 L h⁻¹).

3. Results and Discussion

3.1 Samples characterization

3.1.1 CTF₃₀ catalyst

After the synthesis, the ICP elemental analysis showed that the expected compositions in Ca, Ti and Fe were obtained for the CTF_{30} sample. Additionally, XRD pattern revealed that the perovskite structure was obtained (Figure 1A). The Rietveld refinement indicated an orthorhombic P*nma*/P*bnm* phase (space group #62), with no secondary phases. The crystallite size was estimated at 30 nm from full width half maximum (FWHM) of the main diffraction peak. The specific surface area after ageing at 600 °C was 33 m² g⁻¹ (Table 2). The macroporosity of the material is evidenced on the SEM micrograph (Figure 1B).



Figure 1. (A) XRD pattern of CTF₃₀ and Rietveld refinement; (B) SEM micrograph.

The partial titanium substitution for iron induces the formation of oxygen vacancies because the ionic radius of 6coordinated Ti⁴⁺ (0.605 Å) is slightly bigger than for 6-coordinated Fe⁴⁺ (0.585 Å) [22]. Consequently, to maintain the structure and the stoichiometry, most of the iron species are Fe³⁺, with various coordination (Fe³⁺ 6-; 5-; 4coordinated species have ionic radii of 0.645 Å, 0.580 Å and 0.490 Å, respectively, while 6-coordinated Fe²⁺ is significantly bigger at 0.780 Å). The characterization by Mössbauer spectroscopy (results not shown) indicated that the Fe³⁺ 6-; 5-; 4-coordinated species distribution was 41 %, 46 % and 3 %, respectively, while 10 % Fe⁴⁺ was also detected. The formation of oxygen ion vacancies favours some oxygen exchange behaviour in the solid. This property is studied by isotopic exchange in section 3.1.3.

Samples	Specific surface area (m ² /g)	Pore volume (cm ³ /g)	Pore size (nm)	Pd loading* (%)	Molar H/M ratio**	D (%)	d (nm)
CTF ₃₀	33	0.134	14	-	-	-	-
Pd/YSZ	14	0.063	21	1.10	0.64	59	1.8
Pd/Al ₂ O ₃	180	0.453	8	1.05	0.51	50	2.2

Table 2. Specific surface area, pore volume and size, palladium loading and palladium dispersion of the studied samples.

* determined by ICP-OES; ** M is the total amount of palladium in the sample.

3.1.2 Pd/YSZ and Pd/Al₂O₃ catalysts

Due to the high synthesis temperature for the YSZ support (from TOSOH), the Pd/YSZ catalyst exhibited a low specific surface area, at $14 \text{ m}^2 \text{ g}^{-1}$. On the contrary, Pd/Al₂O₃ catalysts showed a high specific surface area (180 m² g⁻¹) which is constant with the support specific surface area, around 200 m² g⁻¹.

ICP analysis of Pd/YSZ and Pd/Al₂O₃ samples revealed that the palladium loadings were very close to the expected value of 1_{wt} % (Table 2). TEM images of the Pd/YSZ catalyst (Figure 2) shows palladium particles located at the borders of the crystallites of the support, allowing precise EDX analysis of the particles. Thus, the observed particles were in the form of PdO oxide. However, a precise count of the particle size distribution was challenging because the observed PdO particles appeared generally highly clustered, with sizes ranging from 5 nm to 10 nm.

However, isolated particles of larger diameter between 10 nm and 20 nm are occasionally observed. The average diameter of the PdO particles from TEM analysis was estimated at 11 nm. In addition, H₂-chemisorption gives an H/M ratio of 0.64 for the Pd/YSZ catalyst (Table 2). Based on the on the statistical cuboctahedron clusters model of Drault et *al.* [20], the palladium dispersion is estimated at 59 %, which correspond to a mean particle size of 1.8 nm. Compared to the TEM observations, it induces that small particles not identified by microscopy were predominant. The dispersion encountered over Pd/Al_2O_3 sample is around 50 % (mean particles size: 2.2 nm).



Figure 2. TEM images (associated with EDX analysis) at different scales of the Pd/YSZ catalyst.

H₂-TPR experiments were performed to evaluate the palladium reduction depending on the support, YSZ or Al₂O₃. Depending on support formulation, one or two hydrogen consumption peaks can be observed at low temperature [23]. The α peak is assigned to the reduction of PdO_X species highly dispersed on the support's surface. The β peak is attributed to stable PdO species having strong interaction with the support. A desorption peak is usually observed near 100 °C. It is related to the decomposition of palladium hydride. Recorded profiles reported Figure 3 shows that the H₂ consumption peak was observed at lower temperature with Pd/Al₂O₃ (4°C) than with Pd/YSZ (peaks at 32 °C and 77 °C). It results that PdO_X species supported on Al₂O₃ are more easily reduced and only one peak of hydrogen consumption was observed. The quantification of the H₂ consumption after subtraction of the H₂ desorption peak confirms that palladium was fully oxidized as PdO species for both samples, in accordance with the TEM-EDX analysis. It also induces that no spillover phenomenon from hydrogen adsorption on the metal to the support is denoted.



Figure 3. TPR profile of Pd/YSZ (A) and Pd/Al₂O₃ (B). The improperly control of the temperature ramp near 20 min was due to the transition between the cooling and the heating modes.

3.1.3 ¹⁸O₂ isotopic exchange

In this section, redox behaviors of the studied catalysts were studied by means of Temperature-Programmed Oxygen Isotopic Exchange (TPOIE). Remind that (i) the setup is made of a recirculating system and (ii) the catalyst masses implemented for the experiments were adjusted to have the same number of oxygen atoms in the solid phase. Consequently, all samples tend to the same equilibrium between the solid phase and the gas phase.

Figure 4A shows the atomic fraction of ¹⁸O in the gas-phase (α_g) plotted as a function of temperature obtained with the studies materials. For CTF₃₀, the isotopic exchange started at around 270 °C. This temperature is little lower than that previously reported with LaMnO₃ (300 °C) [11], the perovskite which was previously used to highlight the enhancement of O₂ activation on YSZ. The better oxygen exchange behavior of CTF₃₀ is also illustrated by the temperature recorded to reach 40 % of exchanged atoms in the solid, at 550 °C with LaMnO₃ [11] and 390 °C for CTF₃₀ (Figure 4A). This result emphasizes the difference in terms of ionic conductivity between LaMnO₃ which is purely electronic conductor and CTF30 recognized as a MIEC.

Compared to CTF₃₀, both Pd/YSZ and Pd/Al₂O₃ showed a starting exchange temperature shift of 200 °C, at 470 °C (Figure 4A). Palladium-based catalysts are known to be poorly active in isotopic oxygen exchange compared to other noble metal [24]. The exchange equilibrium between the gas phase and the solid (α_g around 40 %, *i.e.* 60 % of exchanged atoms in the solid) was reached at 650 °C on Pd/YSZ (\Box). In contrast, due to the poor behavior of Al₂O₃ support in direct oxygen exchange at low temperatures (T<500 °C), Pd/Al₂O₃ (Δ) did not reach the equilibrium at the end of the test (700 °C). Note that similar exchange onset temperatures were observed on Pd-free YSZ and Al₂O₃ supports. Consequently, Pd particles do not interfere with the activation of the O₂-exchange. However, the isotopic distribution was altered since partial pressures of ¹⁶O₂ and ¹⁶O¹⁸O were detected simultaneously for Pd-supported catalysts, in contrast to Pd-free supports.

The oxygen exchange behavior of the mixed system composed of mechanical mixture of CTF_{30} together with Pd/YSZ is also plotted in Figure 4A (\blacklozenge symbol). Interestingly, when the CTF_{30} is associated to Pd/YSZ, a shift of about 200 °C towards lower temperatures is observed compared to the single-bed Pd/YSZ (\Box), indicating that the isotopic exchange on Pd/YSZ is significantly improved (half of the exchangeable atoms are provided by YSZ in this test). The promotion of O₂ exchange over YSZ support was previously observed by Richard *et al.* [12] with LaMnO₃ as implemented perovskite. It was proposed that the formation of an active oxygen species on the

perovskite was involved to promote the exchange on YSZ at lower temperatures. The generated active species on the perovskite which promote the oxygen exchange on YSZ remains unclear but the assumption of singlet $({}^{1}\Delta_{g})$ oxygen formation over LaMnO₃ was speculated [11]. This highly reactive intermediate $({}^{1}\Delta_{g})O_{2}$ can thereafter enhance the oxygen exchange of YSZ.

Various configurations involving the same weight of CTF_{30} and Pd/YSZ, as described in section 2.3, were also evaluated: the "dual-bed" noted $CTF_{30}+Pd/YSZ$, the "reverse dual-bed" noted $Pd/YSZ+CTF_{30}$ and the "mechanical mixture" denoted $CTF_{30}/Pd/YSZ$. Note that the total weight of the catalytic bed was adjusted to get the same amount of oxygen atoms inside the reactor for all measurements. Oxygen exchange profiles plotted in Figure 4B are quite similar for all configurations. However, the mechanical mixture showed the best results.



Figure 4. Evolution of the atomic fraction of ¹⁸O in the gas-phase (α_g) (%) depending on temperature for (A): the comparison of single (CTF₃₀ (\bigcirc), Pd/YSZ (\square), Pd/Al₂O₃ (\triangle)) and mixed system (CTF₃₀/Pd/YSZ (\blacklozenge)).

(B): configurations involving the association of both CTF₃₀ and Pd/YSZ: dual bed CTF₃₀+Pd/YSZ(+); reverse dual bed Pd/YSZ+CTF₃₀ (\bigstar); mechanical mixture CTF₃₀/Pd/YSZ(\blacklozenge).

3.2 Catalytic tests

Note that the CO was never detected whatever the tests reported below, proving the total oxidation reaction of methane.

3.2.1 Single CTF₃₀ and Pd/YSZ catalysts

First, single CTF_{30} and Pd/YSZ catalysts were evaluated in simplified media with neither CO₂ nor H₂O, up to 600 °C, in both temperature rise and descent. Results are presented Figure 5. Note that the catalytic performances of single Pd/Al₂O₃ sample are discussed in section 3.2.3.

For CTF_{30} , the methane conversion started from 350 °C and it increased up 78 % at 600 °C. The conversion rate remained constant during the 30 min step at 600 °C and the profile recorded during temperature descent (dotted line) was similar to the ascent behavior. It appears that CTF_{30} remained very stable under reaction flow even after the 600 °C step for 30 min.



Figure 5. Methane conversion recorded during ascent (full line) and descent (dotted line) of temperature in simplified media (CH₄+O₂: —) for (A): CTF₃₀ (\bigcirc) and (B): Pd/YSZ (\square).

The YSZ support was not active in methane oxidation (results not shown) but, as expected, the Pd/YSZ catalyst (Figure 5B) was more active than the CTF₃₀ perovskite, with a start of conversion at 300 °C observed for the ascent test (full line). A conversion of 93 % was reached at 600 °C. To the opposite of CTF₃₀, higher performances was denoted during the temperature descent. For instance, the conversion observed at 400 °C was 66 % during the temperature decrease against 28 % during the temperature ascent. The conversion dropped to 0 % at around 225 °C, compared to the start of activation at 300 °C during the run-up test. This enhanced conversion after the 600 °C step can be attributed to a change in the palladium redox state under the reaction mixture. The total methane oxidation tests were performed without any pretreatment after the synthesis calcination step. It is therefore accepted, in agreement with the TEM and TPR analyses, that palladium was initially in the oxide form as PdO. The partial palladium oxide reduction would occur during the first light-off test together with the methane conversion. Indeed, Mahara et al. [25] demonstrated by in situ EXAFS analysis that the presence of CH₄ resulted in the partial reduction of the easily reducible surface PdO on the particle surface. At higher temperature under CH₄ media (600 °C), the decomposition/reduction of PdO was enhanced, generating additional Pd⁰ sites [26]. Su et al. [27] showed that the reduction of PdO under CH_4 led to a nucleation of Pd⁰ within the PdO particles, unlike the reduction under H_2 which generated a layer of Pd⁰ on the PdO surface. Finally, the highest CH₄ oxidation performances observed for the temperature descent can be attributed to a complex active Pd⁰/PdO phase formed during the ascent test and the step at 600 °C. In fact, the former generated Pd⁰ at 600 °C can be partially re-oxidized for temperature lower than approximately 500 °C, leading to migration and encapsulation of Pd⁰. Then, the highly active species of Pd/YSZ is revealed by a multi-step PdO reduction mechanism involving nucleation, growing and encapsulation. Finally, note that $PdO \rightarrow Pd^0$ phase transformations is subject to temperature.



Figure 6. Impact of the reactional mixture on methane conversion recorded during descent of temperature: (CH₄+O₂: —); (CH₄+O₂+CO₂: —); (CH₄+O₂+CO₂+H₂O: —) in for (A): single CTF₃₀ (\bigcirc) and (B): single Pd/YSZ (\square).

The impact of competing compounds such as CO₂ and H₂O on the activity of materials in the total oxidation of methane was studied depending on the fed mixtures reported in Table 1. For CTF₃₀ sample, the conversion profiles were similar for each evaluated reactional mixture for both successive ascent and descent tests, as illustrated in Table 3 which reports the variation in temperature for 20% methane conversion (T20). Then, CTF₃₀ catalyst remained stable whatever the composition of the reactional mixture. Figure 6A compares the conversion profiles recorded during the temperature descent. The addition of CO_2 in the reaction mixture led to a general decrease in CH₄ conversion over CTF₃₀. Indeed, the conversion started 50 °C higher compared with the simplified mixture and reached a maximum of 54 % at 600°C. Considering the high stability of the perovskite, the loss of conversion observed in Figure 6A can be directly associated only to the presence of carbon dioxide and not to deactivation due to the succession of catalytic tests. The basicity of calcium coupled with the acidic properties of carbon dioxide should induce the formation of carbonate species on the surface of CTF_{30} , thus limiting the adsorption and dissociation of methane on the active iron sites close to calcium. This assumption is supported by the fact that active sites for methane conversion on CTF samples are related to iron environment [28]. The catalytic test in the presence of H₂O in addition to CO₂ showed a further decrease in methane conversion. The onset was then observed at 475 °C and the conversion reached a maximum of only 21 % at 600 °C. The deactivation of catalysts in the presence of water has been widely observed by many authors on metal catalysts [29]. The addition of H₂O would lead to the formation of OH groups on the catalyst surface, preventing the oxidation reaction of methane on the active iron sites. Additional catalytic tests were performed in the presence of H₂O but without CO₂ and the resulting conversions (not shown) were similar than that observed in full complex media (CH₄+O₂+CO₂+H₂O, blue curve Figure 6A). Water is then mainly responsible for the inhibition of the activity when all gases are fed in the reaction mixture.

sample	CTF ₃₀			Pd/YSZ		
Reactional mixture	Ascent test	Descent test	Δ (descent-ascent)	Ascent test	Descent test	Δ (descent-ascent)
CH ₄ +O ₂	488 °C	488 °C	0°C	382 °C	326 °C	-56°C
CH ₄ +O ₂ +CO ₂	534 °C	537 °C	+3°C	340 °C	328 °C	-12°C
CH4+O2+CO2+H2O	596 °C	595 °C	-1°C	410 °C	396 °C	-14°C

Table 3. Temperature for 20 % of CH4 conversion (T20) depending on the inlet gas mixture.

Concerning single Pd/YSZ catalyst, the presence of CO₂ and H₂O had different impacts than those observed on CTF₃₀. Indeed, the methane conversion recorded during the temperature descent reaction in the presence of CO₂ globally followed the profile recorded with the simplified mixture (Figure 6B). However, the methane conversion returned to 0 % at around 225 °C in simplified media, while it started near 260°C in the successive test with addition of CO₂ in the reactional mixture (curve not shown). T₂₀ temperatures reported in Table 3 also illustrate the inhibiting effect of CO₂ on Pd/YSZ at low temperature (326°C in descant test in simplified mixture *vs*. 340°C for the successive ascent test in presence of CO₂). Note that the CO₂ poisoning effect appeared reversible since conversions curves were superposed from 550°C for ascent and descent tests. Moreover, data reported in Table 3 also illustrates that the palladium activation still occurred in presence of CO₂, but in a lower extent than that observed in simplified media, with a decrease of 12°C in T₂₀ between the ascent and descant test in presence of CO₂. Then, the palladium active phase was mainly generated under CH₄ during the first test proceeded in simplified condition.

Under wet media (CH₄+O₂+CO₂+H₂O), the methane conversion was strongly inhibited. It started near 340°C, *i.e.* at a much higher temperature compared to the previous inlet mixtures. Despite an improvement observed during the descent test, a shift of the methane conversion curve of approximately 70 °C to higher temperature was observed compared to tests performed without H₂O (Figure 6B, Table 3). Compared to the first run under simplified media (Figure 5B, full line), the recorded conversion in temperature cooling under wet media was lower in the 300-400 °C temperature range (until 8 conversion points at 380 °C) and a little higher in the 400-500 °C temperature range (maximum gap: 8 conversion points at 440 °C). This inhibiting effect of water is largely reported in the literature. For low temperature application (T<400 °C), both the recombination of surface hydroxyl and water desorption from the catalyst control reactivity of methane oxidation over PdO, making the water desorption from the surface the rate-limiting step for methane oxidation [30]. Therefore, the poisoning effect of water was proposed to be due to the formation of palladium (II) hydroxide where the breaking of the OH bond in the hydroxide is the determining-step [31]. At higher temperature, (T>400 °C), OH groups tend to desorb and the inhibiting effect of H₂O is attenuated.

The influence of CO_2 and H_2O on the structure-function relationship of Pd/YSZ catalyst was further investigated by recording the conversion of methane at 350 °C under different reaction mixtures. Results reported Figure 7 obviously confirms the previous statements. Under simplified media (CH_4+O_2), methane conversion increased during time on stream, associated to the continuous formation of the more active Pd⁰/PdO phase. CH₄ conversion started at 11 % to reach 20 % after 80 minutes due to PdO reduction by methane. With the addition of CO₂ to the reaction flow, the CH₄ conversion first dropped to 12 % and then increased continuously to 28 % after 90 minutes. This confirms that CO₂ does not limit the generation of the active phase of the catalyst but alters their accessibility. Finally, as expected, H₂O addition revealed a drastic decline in methane conversion confirming that carbon dioxide has a lower poisoning effect than water [32]. Note that the influence of water on the catalyst activity is reported to be sensitive to the type of host materials. Supports with high oxygen mobility show potential to moderate the inhibition by water, accelerating hydroxyl desorption [33].



Figure 7. Pd/YSZ (\Box) methane conversion at 350°C depending on the time on stream under various gaseous media (CH₄+O₂: -; CH₄+O₂+CO₂: -; CH₄+O₂+CO₂+H₂O: -)

3.2.2 Dual CTF $_{30}$ and Pd/YSZ system

As described in section 2.3, three configurations in the Pd/YSZ-CTF₃₀ association were studied, namely the dualbed (CTF₃₀+Pd/YSZ), the reverse dual-bed Pd/YSZ+CTF₃₀) and the mechanical mixture (CTF₃₀-Pd/YSZ). These configurations should highlight the specific function of CTF₃₀ toward Pd/YSZ. As mentioned in the introduction part, it was postulated that perovskite material can activate the O_2 molecule which can be used on Pd/YSZ *via* the oxygen mobility of the YSZ support, to promote the methane abatement. However, this assumption required confirmation in a more realistic catalytic setup.

First, the influence of the catalytic bed configuration was examined. The methane conversion recorded in simplified media during the temperature decrease is reported Figure 8A. The reversed bed configuration showed the lowest activity. Interestingly, the methane conversion was then similar to that recorded with the single Pd/YSZ sample (Figure 6B). This result can be explained by the facts that (i) CTF_{30} showed no activity at temperature lower than 400 °C and (ii) the postulated active species generated over CTF_{30} should not interact with Pd/YSZ placed upstream. On the contrary, a significant improvement was obtained with the mechanical mixture, which highlights the importance of the amount of contact points between CTF_{30} and Pd/YSZ in the activity improvement. The beneficial effect of the CTF_{30} +Pd/YSZ mechanical mixture was also evidenced during the isotopic exchange experiments (Figure 4B), but in a lower extent which can be attributed to the recirculating mode used for TPOIE experiments.

A focus on the methane conversion obtained at 400 °C is depicted Figure 8B to compare single and the mixed catalytic system. While CTF₃₀ alone was nearly inactive at 400 °C (2 % conversion), the association with Pd/YSZ led to an exaltation of the activity, with 62 % CH₄ conversion against only 29 % for single Pd/YSZ in the ascent test. It is then clearly evidenced that mechanical mixture of CTF₃₀ and Pd/YSZ (\blacklozenge) allowed higher CH₄ conversion in simplified media (CH₄+O₂) than the added contribution of each catalyst. The observed phenomenon was not cumulative but synergetic. Similar benefits were also observed during the descent tests reported, with 87 % methane conversion at 400 °C with the mechanical mixture CTF₃₀-Pd/YSZ, compared to 66 % and 2 % for single Pd/YSZ and CTF₃₀, respectively. Thus, the concept of a beneficial effect of CTF₃₀ toward Pd/YSZ for CH₄ abatement in simplified media is clearly evidenced.



Figure 8. (A): Impact of catalytic bed configuration on the CH₄ conversion recorded during the descent of temperature in simplified mixture (CH₄+O₂): dual bed CTF₃₀+Pd/YSZ(+); reverse dual bed Pd/YSZ+CTF₃₀ (*); mechanical mixture CTF₃₀/Pd/YSZ(\blacklozenge).

(B): CH₄ conversion at 400 °C recorded in simplified mixture during the ascent/descent temperature for single CTF₃₀ (\bigcirc), Pd/YSZ (\square) and the mechanically mixture CTF₃₀-Pd/YSZ (\blacklozenge) catalytic bed.

The influence of the reactional mixture composition was then investigated with the mechanical mixed bed configuration (CTF₃₀-Pd/YSZ). Only the results recorded during the descent tests are discussed in this section. Figure 9A shows that CO₂ addition shifted the CH₄ conversion curve toward higher temperatures, while results depicted in section 3.2.1 previously showed that for single catalysts, only CTF₃₀ was significantly CO₂ sensitive. For Pd/YSZ, the CO₂ inhibiting effect was compensated by the palladium activation occurring during the tests (Figure 6B). Consequently, the decrease in methane conversion recorded with the CTF₃₀-Pd/YSZ mechanical mixture with CO₂ in the feed stream is mainly attributable to the CTF₃₀ sample. Moreover, compared to the synergetic effect obtained using the simplified reactional mixture (Figure 9B), the gain in methane conversion was significantly attenuated by CO₂ (Figure 9C). Only a small improvement was still observed. Then, the availability of activated oxygen species responsible for methane conversion improvement became very limited. Since CTF₃₀ exhibited basic calcium sites, the formation of surface carbonates species is assumed. Carbonates species are well-known to favor oxygen exchange reactions [34]. The generated active oxygen species was postulated to be a singlet O₂. The exchange between the active oxygen species and the surface carbonates could explain the singlet O₂ relaxation, leading to the decrease in the availability of this species.

Figure 9A also shows that the water inhibition effect appeared more significant than the CO_2 one, in accordance with the results previously discussed for single CTF_{30} and Pd/YSZ catalysts (Figure 6). The gain in methane conversion with the CTF_{30} -Pd/YSZ association was then negligible (Figure 9C). The improvement observed for temperatures higher than 500 °C is attributable to the contribution of the CTF_{30} sample but no synergetic effect was then observed.



Figure 9. (A): Influence of the gaseous media composition (CH_4+O_2 : —; $CH_4+O_2+CO_2$: —; $CH_4+O_2+CO_2+H_2O$: —) on the methane conversion obtained with the Mechanically Mixture catalytic bed CTF_{30} -Pd/YSZ, recorded during the descent of temperature.

(B): CH₄ conversion under CH₄+O₂ (-) reactional mixture recorded during the descent of temperature for single CTF₃₀ (\bigcirc), Pd/YSZ (\square) and the Mechanically Mixture CTF₃₀-Pd/YSZ (\blacklozenge).

(C): CH₄ conversion under CH₄+O₂+CO₂ (-) reactional mixture recorded during the descent of temperature for single CTF₃₀ (\bigcirc), Pd/YSZ (\square) and the mechanically mixture CTF₃₀-Pd/YSZ (\blacklozenge).

(D): CH₄ conversion under CH₄+O₂+CO₂+H₂O (\longrightarrow) reactional mixture recorded during the descent of temperature for single CTF₃₀ (\bigcirc), Pd/YSZ (\square) and the mechanically mixture CTF₃₀-Pd/YSZ (\blacklozenge).

3.2.3 Mechanistic aspect- Role of the perovskite

In addition to the role of the CTF₃₀ perovskite, catalytic tests revealed an activation of the palladium phase in Pd/YSZ. Based on the bibliography [25,26,27], it is assumed that PdO Pd⁰ phase transformation initiated under the reactional mixture interplayed in the oxidation of methane. To date, the identification of the optimum palladium phase at temperature lower than 600 °C and the details of the mechanism remain a much-debated topic. PdO is generally admitted to be the more active phase at high temperature (T \geq 600 °C), while substantial evidences suggest the necessity of the coexistence of Pd⁰, PdO_X (Pd in a reduced state), or even oxygen vacancies (V₀). In this work, the association of CTF₃₀ with Pd/YSZ led to a significant CH₄ conversion enhancement in simplified reactional mixture, mainly for the mechanical mixing configuration with intimate contacts. As previously observed in [11], it is associated with the promotion of the O₂ exchange on Pd/YSZ, which was supposed to assist the methane oxidation reaction through a MvK mechanism. Interestingly, the conversion curve recorded using the simplified gas mixture (CH₄+O₂) with the CTF₃₀-Pd/YSZ mechanical mixture during the first ascent (first test, profile not shown) was very similar to that obtained for the descent with single Pd/YSZ catalyst (after palladium activation, Figure 5B). It could induce that the beneficial effect of CTF₃₀ also interfered with the palladium state. In fact,

palladium state and methane activation are linked since PdO reduction is assumed to occur together with methane oxidation, assuming that PdO was the initial palladium state as evidenced by the TPR measurements.

To highlight the role of CTF_{30} material in the enhancement of the catalytic activity, the association with Pd/Al_2O_3 was also examined. This sample was selected because it is a reference catalyst for this application and because alumina showed poor oxygen exchange properties, as described in Figure 4A. The palladium particle size determined by H₂-chemisorption was around 2.2 nm for Pd/Al₂O₃ catalyst, compared to 1.8 nm for Pd/YSZ (Table 2). This similar particle size close to 2 nm allows to rule out the possible structure sensitivity of the reaction. Single Pd/Al₂O₃ catalyst was evaluated in simplified CH₄+O₂ media and compared to Pd/YSZ Figure 10A. The methane conversion recorded during the first ascent test with Pd/Al_2O_3 (Δ , full line) was significantly higher than that observed with Pd/YSZ (□, full line). Again, the methane conversion recorded during the temperature descent with Pd/Al_2O_3 was higher compared with the ascent test (\triangle , dotted line), as previously evidenced for Pd/YSZ sample, indicating the formation of a more active palladium phase. Figure 10B compares the methane conversion recorded at 400 °C in simplified mixture depending on the catalytic system. Interestingly, the mechanical mixture CTF₃₀-Pd/Al₂O₃ allowed the same conversion during the first ascent experiment than single Pd/Al₂O₃ in descent test (observed on the whole temperature range). Then, the presence of CTF_{30} was also beneficial for the formation of the more active palladium phase on Pd/Al₂O₃. Unfortunately, it did not provide a supplementary enhancement of the methane conversion after the PdO/Pd⁰ active phase formation. Both Pd/YSZ and Pd/Al₂O₃ catalysts exhibited PdO as initial palladium state. However, the TPR experiments showed that PdO on Al₂O₃ is more easily reducible than on YSZ. This result is consistent with the assumption that the PdO/Pd^0 active phase formation occurred more rapidly on Pd/Al₂O₃ than on Pd/YSZ. Then, it is assumed that in CTF₃₀-Pd/YSZ association, active O₂ generation helped the methane conversion concomitantly with PdO partial reduction.

Figure 10B also shows that both single Pd/Al₂O₃ and mechanical mixture CTF_{30} -Pd/Al₂O₃ showed similar conversion during the descent test. It seems to indicate that the decisive step remains the generation of a Pd⁰/PdO_X phase, irrespective of the support properties. Nevertheless, the decomposition and reformation of Pd-based active phase for methane oxidation is strongly dependent on the nature of the support [26]. Over Pd/YSZ, mechanisms for the low temperature combustion of methane include steps for oxygen exchange between the palladium phase and the support [35]. As a consequence, it is postulated that PdO/Pd⁰ reciprocation on the Pd/YSZ catalyst is assisted by the synergetic effect of CTF_{30} material. As previously discussed, the assumption of active $(^{1}\Delta_{g})O_{2}$ formation by CTF_{30} enhances the oxygen transfer ability of YSZ involved in the methane conversion. It is then tentatively assumed that YSZ offers oxygen exchange to tune the valence state of palladium species by the redistribution of active palladium phase [36].



Figure 10. (A): Methane conversion recorded during ascent (full line) and descent (dotted line) of temperature in simplified media (CH₄+O₂: —) with single Pd/YSZ (\Box) and single Pd/Al₂O₃ (\triangle);

(B): Methane conversion recorded at 400°C in simplified media (CH₄+O₂) during ascent and descent tests depending on the catalytic system: single CTF₃₀; single Pd/YSZ; CTF₃₀-Pd/YSZ mechanical mixture; single Pd/Al₂O₃; CTF₃₀-Pd/Al₂O₃ mechanical mixture.

4. Conclusions

For the first time, the beneficial association of a perovskite with palladium-based catalysts for the total methane oxidation was confirmed using a synthetic gas bench setup dedicated to catalytic tests. The observed synergetic effect observed in simplified gas mixture was associated to the formation of active oxygen species on the perovskite, which were then transferred to the palladium-based catalyst allowing the promotion of the methane oxidation. This synergetic effect is favored by intimate contacts between $CaTi_{0.7}Fe_{0.3}O_{3-\delta}$ and Pd/YSZ, obtained by a mechanical mixture. The promoting effect of $CaTi_{0.7}Fe_{0.3}O_{3-\delta}$ perovskite is partially inhibited by the presence of 10 % CO₂ in the reactional mixture, and fully inhibited with the supplementary 8 % H₂O. Comparison with the association of the $CaTi_{0.7}Fe_{0.3}O_{3-\delta}$ perovskite with a Pd/Al₂O₃ catalyst indicates that the decisive step of the methane oxidation remains the generation of a Pd⁰/PdO_x phase, irrespective to the support properties.

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