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## Study of reaction-diffusion controlled mass transport in stopped-flow fluidics for spatiotemporal multiplexing

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## Abstract

1  
2 Integration of biological reaction networks (BRNs) with biosensor platforms has emerged as a technological  
3 niche overcoming the challenges related to the loss of sensitivity and selectivity in biological media. Optimal  
4 operation of BRNs in microfluidics requires control over reaction-diffusion dominated mass-transport,  
5 heavily influenced by fluidic parameters. In this work, we study and design an on-chip platform combining  
6 a programmable unique molecular amplification (PUMA) as BRNs with nanoscale biologically sensitive  
7 field-effect transistor (BioFET) arrays, which employs a physical diffusion-barrier to gain spatial and  
8 temporal control over mass-transport. Computational and numerical approaches such as finite element  
9 (FEM) and finite volume methods (FVM) were implemented to solve partial differential equations  
10 numerically after domain approximation by numerous finite elements. The focus on geometrical  
11 optimizations of fluidics is aimed at mass-transport to occur with precise spatial and temporal control  
12 towards BioFET-arrays. Adopting a 0.5 pM limit-of-detection (LoD) for biochemical monitoring of BRNs  
13 via single-stranded deoxyribonucleic acid (ssDNA) output, we show that it was possible to  
14 compartmentalize the mass-transport spatiotemporally without cross-talk, which can be of critical advantage  
15 for using biosensor-arrays in order to realize a simplified multiplexed point-of-care biosensors.

16

## 1 **1. Introduction:**

2 Miniaturization of fluidics, in its various forms, continues to play a vital role in the study of reactions  
3 and mass transport in chemical and biological systems <sup>1</sup>. While fluidic circuits and use of low Reynold  
4 number flows have become a mainstream for the study of mixing and separation, study of reaction-diffusion  
5 phenomena in miniaturized stopped-flow fluidics only begins to see a resurgence of interest due to newfound  
6 applications in future technology <sup>2,3</sup>. For example, regulation of biochemical/biomechanical conditions have  
7 high relevance for tissue engineering and development of Organ-on-a-Chip concepts for their dramatic  
8 influence on the vascularization and cell-growth <sup>4-7</sup>. The influence of three-dimensional (3D) geometry and  
9 various other physical parameters on the mass-transport of metabolites and biomolecules has been studied  
10 recently in various cell-lines, giving way to self-organization, differentiation patterns and novel approaches  
11 in developmental biology with precision biofabrication <sup>4,8-10</sup>. Beyond such topics related to self-organization  
12 of cells and tissues, spatiotemporal control of mass transport at nanoscale is also proving to be helpful in  
13 the study of various biomolecular systems of cell such as lipid and protein structure of cell membrane, gene-  
14 expression networks in relation to cellular heterogeneities and development of next generation microfluidics  
15 for dynamic single-cell spatial and multimodal transcriptomic <sup>11,12</sup>.

16  
17 Even before, spatiotemporal distribution of chemical species had received attention for the study of non-  
18 equilibrium reactions <sup>13-18</sup>. A famous example of such a non-equilibrium systems that has continuously  
19 attracted scientific attention is the Belousov-Zhabotinskii (BZ) reaction as a type of chemical oscillations  
20 and self-organization in chemical waves<sup>19</sup>. Ever since, temporal and spatial variation of reaction constituents  
21 and products of such non-equilibrium reactions in homogeneous conditions has been a topic of great interest,  
22 as a simplified model of self-organization in complex biochemical and biological systems <sup>20</sup>. More recently,  
23 study of such out of equilibrium systems in miniaturized fluidics helps mimicking complex systems such as  
24 biochemical reaction networks (BRNs), biochemical oscillators (BOs), self-assembly and molecular motion  
25 and advancing our understanding of systems chemistry <sup>2,16,21-25</sup>. At the same time, scientific interest in the  
26 study of heterogeneous non-equilibrium reactions began with the discovery of oscillatory kinetics at  
27 interfaces. A well-studied example of such heterogeneous reaction system is the catalytic oxidation of  
28 carbon monoxide (CO) at Pt(110) surface, also catalysing the development of experimental methods such  
29 as scanning photoelectron microscopy and photoemission electron microscopy for the imaging such systems  
30 with high temporal and spatial resolutions <sup>17</sup>. Eventually, development of theoretical models for the  
31 heterogeneous oscillatory reactions elucidating the underlying microscopic mechanism gave a significant  
32 boost for the study of such systems at the solid-liquid interface where reaction-diffusion patterns of reaction  
33 constituents play a pivotal role in self-organization <sup>18</sup>.

34 Interestingly, the reaction-diffusion regulated spatiotemporal mass transport has a direct relevance for  
35 technologies such as nanopores, miniaturized point-of-care (PoC) biosensors and micro-reactors for

1 biological and chemical processes <sup>26-28</sup>. On-chip biosensors based on nanoscale transducers such as  
2 semiconductor nanowires (s-NWs), microelectrode arrays (MEAs) and two-dimensional (2D) materials  
3 where biological interactions take place at the solid-liquid interface, are suitable examples where stopped-  
4 flow fluidics provide an easy solution for sample handling and are prone to influences from diffusion related  
5 aspects <sup>29-32</sup>. Such biosensor platforms typically employ volumes in the range of tens of microliters and  
6 generate different mass-transport regimes based on the molecular concentrations in the bulk and on the  
7 surfaces, density of the medium, retention time and the shape of the fluidic volumes <sup>33,34</sup>. At the same time,  
8 new strategies of integrating BRNs in microfluidics for molecular recognition and programmable unique  
9 molecular amplification (PUMA) are getting popular for advantages such as enhanced selectivity and  
10 reliable transduction <sup>35,36</sup>. Similar to the well-known polymer chain reaction (PCR) technique the PUMA  
11 can be used to amplify nucleic acid sequences. In contrast to the PCR technique, the PUMA utilizes  
12 isothermal conditions for the amplification of nucleic acid sequences. The molecular reaction mixture  
13 consists of multiple DNA templates and an enzyme mixture for the amplification. The onset of the  
14 amplification cascade is depending on the input concentration of the targeted nucleic acid sequence (e.g.  
15 miRNA). Therefore, the amplification onset as a function of time can be used to determine the input  
16 concentration of the targeted nucleic acid sequence. A detailed step by step description of the mechanisms  
17 behind the PUMA reaction is provided in the supplementary materials. Such BRNs, after modifying their  
18 recognition template sequence, are also able to provide modular mechanisms for multiplexed detection of  
19 low-concentration biomarkers such as microRNAs and signalling proteins <sup>36,37</sup>. Here, optimal operation of  
20 BRNs requires study of 3D mass-transport profiles in stopped-flow fluidics on chip at moderately higher  
21 temperatures.

22  
23 Biologically sensitive ion-sensitive field-effect transistors arrays (Bio-FET arrays) are classified as  
24 highly sensitive biological transducers for biomedical applications <sup>38</sup>. The possibility of micromachined  
25 fabrication ensures a low-cost production of such sensors. However, one of the most prominent bottlenecks  
26 of such near-field charge sensitive devices is the highly decreasing sensitivity in biological relevant analytes.  
27 Such liquids contain a high amount of salts which results in a lowering of the Debye-screening length – one  
28 of the most critical parameters in near-field charge detection – and, thus, results in a drastically decrease in  
29 sensitivity of the biosensor. Therefore, an on-chip amplification of the targeted nucleic acid sequence is of  
30 high interest to overcome this fundamental limitation, which was demonstrated in the literature <sup>39, 40</sup>.  
31 However, when it comes to miRNA profiling, a multiplexed readout scheme is mandatory to determine the  
32 health condition of a patient. For instance, the miRNA Let-7a level expression is affected by multiple types  
33 of cancer (e.g. breast, lung, or prostate) <sup>41</sup>. Therefore, multiple miRNA target sequences need to be detected  
34 simultaneously. To tackle the need for on-chip amplification in combination with a multiplexed readout, we  
35 performed numerical simulations as described in the following.

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A BioFET-arrays platform based on Si NWs, dedicated for the integration of PUMAs for biodetection can be seen in **figure 1**. The simulation design is based on recently published biosensor platform from our group combining a Si NW array with on-chip temperature sensors and metal or graphene oxide/polymer hybrid reference electrodes <sup>42,43</sup>. The platform includes a 4 mm wide stopped-flow fluidic chamber placed on top of biosensor chip having an array of BioFETs, arranged in a straight line. Different PUMA-BRN unique to micro ribonucleic acid (miRNA) biomarkers are surface immobilized on the distal ends of the fluidic ceiling, from where they release a common ssDNA sequence, upon recognition of desired miRNA. The PUMAs can be modified such that they recognize different microRNA sequences and cascade this molecular recognition to production of a common short DNA sequences. Programming PUMAs as such allows BioFETs having the same receptor-DNAs for the electrical detection of ssDNA and thereby simplifying the assembly of the biosensor chips for real applications. Therefore, stopped-flow conditions are required to ensure a spatiotemporal multiplexed readout using a common ssDNA output for multiple PUMA networks. Stopped-flow conditions ensure that diffusion is the prominent mode of mass transfer in the fluidic system, and hence, the transport of the PUMAs to the biofunctionalized surface is governed by the concentration gradients developed. Further, to ensure multiplexing capabilities of the proposed sensor system a local starting point of the diffusion front is needed to detect the spatiotemporal spread of the diffusion wave. This can be realized by immobilizing the recognition template of the PUMA at both sides of the fluidic channel (e.g. at the top glass cover). Without an external triggered flow, the generated nucleic acid sequences would diffuse through the channel with a uniform velocity and bind to the surface of the BioFET arrays <sup>44</sup>. Due to the binding of the generated ssDNA sequences a change in the surface potential of the BioFET would result in a change in the current flow. Stopped-flow conditions are realized when no external pressure gradient is applied. Therefore, the mass-transport inside the fluidic volume only consists of diffusion. In this work, we present numerical investigations of the reaction-diffusion regulated mass transport of ssDNA inside such a complex microfluidic volume operating BRNs in biological conditions and study the impact of fluidics shape on spatiotemporal multiplexing. We show that geometrical optimizations of the fluidic volumes by implementation of simple diffusion barriers significantly retard the mass-transport process. Thus, with simple barrier geometries too, the mass transport can be controlled and retarded to prevent cross-talk in scenarios where multiple different ssDNAs are to be detected. Further, we show that by changing the shape of such diffusion barriers, it is possible to tune the reaction-diffusion profiles (wave fronts) and set specific periods for the onset of hybridization process at the BioFET-arrays.

34 **2. Materials and Methods**

35 **2.1. The reaction-diffusion system:**

1 Diffusion as a mass transport phenomenon involves an entity of interest (e.g. biomolecules) moving  
2 from a point of higher concentration (or higher pressure) to that of a lower concentration (or lower pressure)  
3 in a given medium, thereby forming a concentration gradient. When the concentrations are also dependent  
4 on the rate and/or order of a chemical reaction involved (the diffusing species also participates in a chemical  
5 reaction), the system is called a reaction-diffusion system. Typical examples of such systems are chemical  
6 reaction-diffusion networks such as BZ reactions and autocatalytic BRNs such as PEN-DNA and PUMA  
7 molecular programs<sup>36,45,46</sup>. Such systems, governed by diffusion equation, can be mathematically described  
8 by the Kolmogorov-Petrovskii-Piscuno (KPP) equation<sup>47</sup>. The KPP equation describing the reaction-  
9 diffusion front in a fluidic volume is defined as

10 
$$\frac{\partial c}{\partial t} = D \frac{\partial^2 c}{\partial x^2} + R(c) \dots \dots \dots (1)$$

11 - where,  $c$  denotes the molecular concentration as a function of space and time  $c(x, t)$ ,  $D$  is the  
12 diffusion coefficient of candidate biomolecules with concentration  $c$ , and  $R$  represents the local reaction  
13 term that describes the reaction rate and order. In the absence of convection and bulk fluid motion, equation  
14 1 does not include the term for the velocity field of the fluid. Such a formulation also assumes isotropic  
15 diffusion conditions where  $D$  does not depend on the location in the fluidic volume.

16 **2.2. Molecules under spatial reaction-diffusion:**

17 The autocatalytic PUMA-BRN considered for this work were designed for the detecting the presence  
18 of miRNAs that are specific biomarkers for neurodegeneration disorders<sup>37,48</sup>. Briefly, PUMA employs an  
19 exponential molecular amplification cascade after the recognition of a miRNA target sequence at the  
20 converter template, which results in the synthesis of 12bp ssDNA. As this autocatalytic BRN is maintained  
21 by the use of ligase, nickase and polymerase enzymes, a buffer medium and elevated temperature of 45 - 50  
22 °C is required in the fluidic volume to ensure enzymatic activity. When the PUMA starts at a certain position  
23 in a microfluidic channel such as shown in the figure 1b, the trigger will create a reaction-diffusion front,  
24 which are expected to propagate along the fluidic volume. The maximum PUMA output (12bp ssDNA) was  
25 assumed to be at a concentration of 1 μM, and thus the maximum capacity of the system too was considered  
26 to be 1 μM.

27 **2.3. Fluidic Simulation Framework:**

28 A computational model of stopped-flow fluidic volume under study (4 mm length, 50 μm width, and 800  
29 μm height) was developed to simulate the diffusion mass transport and the reaction dynamics.  
30 Computational and numerical techniques such as Finite Element Method and Finite Volume Method were  
31 applied to solve the complex partial differential equations and domain approximation by numerous finite  
32 elements. The 2D and 3D design of fluidic volumes were carried out in SOLIDWORKS™ and imported to  
33 the COMSOL™ Multiphysics™ interface. The modules used for simulations of diffusive mass-transport in

1 COMSOL™ Multiphysics comprised of the ‘Transport of Diluted Species’ and ‘Reaction Engineering’  
2 which accounted for the diffusion and the reaction rates, both from equation 1. The reactive term was used  
3 to couple the two modules and model the complete system.

4 The system modelled in the work is governed by reaction-diffusion physics. The mass transfer  
5 occurs through diffusion, the system being of stopped-flow nature, and the convection being absent. Further,  
6 the concentration gradient that drives the mass transfer by diffusion is also impacted by the autocatalytic  
7 reaction of the PUMAs, making it a reaction-diffusion system. Simulation of time domain variation in the  
8 diffusion profile was monitored for a constant supply of 1 μM DNA from the release spots 1 and 2 (figure  
9 1). DNA concentration in the fluidic volume shall then vary with time based on KPP form of the Partial  
10 differential equation for reaction-diffusion and this variation was studied. To reduce the complexity of the  
11 simulations the reactions of the molecular program products with the biofunctionalized surface (surface  
12 reaction kinetics at the Si NW interface) were neglected. Only the diffusion profile of the trigger was  
13 investigated, after initiation of the autocatalytic reaction-diffusion front from the inlet positions as shown in  
14 Fig 1

15 In order to retard or restrict the diffusion of certain species in a reaction-diffusion system thin films have  
16 been studied and applied as a diffusion barrier in many instances <sup>49</sup>. Taking the concept of diffusive mass  
17 transfer in the microchamber further, the work intended to model such a diffusion barrier concept and study  
18 the impact of the same on the diffusion profile in the microfluidic chamber. The geometries of a possible  
19 barrier, based on feasibility from a fabrication point of view were modelled and investigated (figures 3, 4  
20 and 5). These structures can be easily fabricated using additive manufacturing processes like  
21 stereolithography, fused filament fabrication and standard polydimethylsiloxane processes.

22  
23 The temperature was set to 50°C that suits the functioning of the PUMA-BRN. The reaction rate  
24 constants and carrying capacities were set as global variables, and the domain properties were assigned  
25 along with concentration and no flux boundary conditions. As the model pertained to a stopped-flow system  
26 with no bulk flow, convection effects were not taken into account in these simulations. The medium of  
27 diffusion was set to a buffer with a 150 mM initial concentration, and the DNA strand diffusion coefficient  
28 was estimated from empirical relations from literature for a 12-base pair DNA <sup>50</sup>. The rate expression applied  
29 based on the Fisher KPP form of the reaction-diffusion system was:

$$R = K_f A \left(1 - \frac{A}{C}\right)$$

30 .....(2)

31 where,  $K_f$  is the forward rate constant,  $A$  is the concentration of species, and  $C$  is the maximum nucleic acid  
32 carrying capacity of the system (in other words: the maximum generated amount of the ssDNA output of  
33 the PUMA reaction system). To perform the simulations we assumed a carrying capacity of 1 μM, which  
34



1 creates the constant output of the PUMA. Here, we only considered the forward rate constant  $K_f$  since the  
2 reverse reaction constant  $K_r$  can be neglected for specific target receptor combinations<sup>50</sup>.

### 3 **3. Results and Discussion**

#### 4 **3.1. ssDNA mass-transport in the fluidic volume:**

5 According to the Fisher KPP rate law and reaction kinetics parameters for a DNA autocatalytic replication  
6 in BRN, the diffusion was simulated in a time dependent 3D model for up to about 2 hours (>120 minutes)  
7<sup>44</sup>. Implementing the simulation of reaction-diffusion of single species (12bp DNA with 1 $\mu$ M conc.) at the  
8 release spot (surface functionalized PUMA), a time dependent diffusion profile for the given fluidic volume  
9 is shown in the figure 3. In order to speed up the simulation, a two-dimensional vertical profile simulation  
10 was carried out to study the vertical spread of diffusion front produced by PUMA-BRNs. As shown in figure  
11 3 the diffusion front spread out along the whole channel within 36 minutes. Assuming that the bottom part  
12 of the channel contains an array of receptor-DNA modified BioFETs, the spatiotemporal diffusion could be  
13 monitored in real-time.

#### 14 **3.2 ssDNA mass-transport with a diffusion barrier:**

15 As mentioned earlier, in order to retard the diffusion of PUMA-BRN output (12 bp DNA), introduction of  
16 diffusion barrier and simulation of mass transport was attempted. Several geometric iterations were carried  
17 out to find an optimal geometry of such a diffusion barrier. On the introduction of a diffusion barrier, the  
18 simulation domain was divided geometrically, and distinct properties were assigned to each part. The barrier  
19 itself was assigned transport properties such that the diffusion through it would be absent. At first, the barrier  
20 was conceptualised as a cube, and then geometric changes to engineer the mass-transport in the fluidic  
21 volume were evaluated as follows:

22 a. *Cuboid Diffusion Barrier*: As shown in the illustration in figure 3a, a cuboid diffusion-barrier with  
23 dimensions of 1 mm length and 0.78 mm depth was placed under the ceiling of the fluidic volume, virtually  
24 partitioning it while leaving a fluidic capillary with 1 mm length, 50  $\mu$ m in width and a height of 20  $\mu$ m.  
25 The graphs 3b-3e as shown in figure 3 depict of the resulting diffusion patterns when DNA is injected from  
26 the left inlet (PUMA1) and observed in the form of a 2D simulations evaluating the effect of the barrier in  
27 comparison to fluidic volume with no barrier (figure 2). The barrier is found to be effective in preventing  
28 fast diffusion throughout the microfluidic volume for up to 30 to 50 minutes. With more time elapsed,  
29 however, the build-up of DNA concentration across the diffusion barrier progresses very fast, which is  
30 undesirable. With PUMA-BRNs amplification profiles typically longer than 50 minutes, this quick build-  
31 up of the DNA output after 50 minutes would result in significant molecular cross-talk between PUMA1  
32 and PUMA2 BRNs, and therefore calls for optimization of barrier's geometry.

1 *b. Trapezoid Diffusion Barrier, Type 1:* In order to minimize the molecular cross-talk between different  
2 BRNs in the same fluidic volume, a trapezoidal diffusion barrier was studied as an alternate geometry. This  
3 configuration is shown in the figure 4a where the trapezoid barrier is placed in between and has 1 mm length  
4 at the base and 50  $\mu\text{m}$  width. The depth of the barrier is selected as 790  $\mu\text{m}$  leaving a gap of 10 micron to  
5 the BioFET chip underneath. This way the fluidic capillary has an effective dimension of 1.6 mm (length),  
6 50  $\mu\text{m}$  (width) and 10  $\mu\text{m}$  (height). The simulations were carried out in a similar way and the mass transport  
7 profiles are shown in the figures 4 images b-e from the beginning up to 44, 69 and 125 minutes. Here, the  
8 speed of the reaction-diffusion front along the diffusion channel was retarded in the comparison to the  
9 cuboid barrier. After about 120 minutes, the total DNA concentration, on the other side of the diffusion  
10 barrier, was reduced to approximately 0.5  $\mu\text{M}$ .

11 *b. Trapezoid Diffusion Barrier, Type 2:* In the final iteration, the height of the diffusion channel was further  
12 reduced to 5  $\mu\text{m}$  while keeping the overall trapezoidal shape of the barrier. The overall configuration is  
13 shown in figure 5. From the reaction-diffusion profiles as shown in figure 5b-e, at 0, 55, 100 and 120 minutes  
14 respectively, the speed of the diffusion front is clearly reduced, and a reduced DNA concentration (0.3  $\mu\text{M}$ )  
15 was reached after 120 minutes. The height of the diffusion channel, therefore, has a significant impact on  
16 the mass transfer along the diffusion channel. Overall, this configuration enabled an efficient retardation of  
17 the diffusion process for 12bp DNA optimal for the implementation of several BRNs on same chip.

### 18 **3.3. Spatiotemporal control and multiplexed read-out:**

19 In order to simulate spatiotemporal multiplexing using such a reaction-diffusion regulated fluidics  
20 system, two different DNA sequences were modelled to be continuously injected from the two release spots  
21 1 and 2 respectively as shown in the figure 6. Upon applying of identical physical properties e.g. diffusion  
22 coefficient and reaction rate expressions for each of them, the diffusion patterns were symmetrical depicting  
23 the qualitative accuracy of the model. To be more application specific, especially in case of biosensors where  
24 a spatiotemporal multiplexing is advantageous to create more versatile and adaptive sensor chip platforms,  
25 we considered the release spots 1 and 2 as the PUMA, which upon the presence of a target biomarker, trigger  
26 an enzymatically controlled exponential amplification reaction (EXPAR) providing an exponential supply  
27 of short DNA sequences as an output for a limited time. This EXPAR typically lasts for a few hours,  
28 saturates, and then decays exponentially. The PUMA can be surface immobilized as shown in this scheme  
29 and modified by changing the converter DNA template to recognize a specific biomarker such as miRNA.  
30 In our case, PUMA were optimized to give an exponential onset (readable by rtPCR) against 0.5 pM  
31 concentration analyte biomarker (miRNA) within 5 minutes and then saturation point occurring around half  
32 an hour. Given when reaction-diffusion regulated microfluidic volume is spatially engineered in order to  
33 distinguish the mass-transport from  $n$  number of release spots, with the help of nanowire arrays, modular  
34 sensor platforms can be developed. Such a modular sensor platform alleviates the requirement of surface

1 modifying the sensor-spots with different receptor/probe DNA sequences using complicated procedures.  
2 Ideally, tuning of the PUMA at release spots would allow a biomarker linked mass-transport that is detected  
3 by the sensors in an engineered time-domain. For example, higher concentration of a biomarker would lead  
4 to an earlier onset of PUMA and requires slowing down of the reaction-diffusion driven mass transport.  
5 Here, we applied our simulation framework to evaluate the PUMA output sequence concentrations at a  
6 specified sensor position (BioFET-array) on the chip (figure 6). In order to do this, a transverse sectional  
7 profile was drawn in the simulation model in order to extract the concentration data at the BioFETs interface  
8 closest to PUMA1 (figure 6b). The build-up of the output DNA concentration at a single BioFET located  
9 near the release spot 1 are shown in the graph (figure 6a). In this case, primary sensor requirements are to  
10 prevent a non-specific interaction due to a crosstalk (i.e. between the trigger from spot 2 and spot 1) to  
11 ensure that correct PUMA-specific output is encoded by the BioFETs. It was considered that the BioFETs  
12 are able to encode the DNA output concentrations greater than 0.5 pM set as the limit of detection (LoD).  
13 This LoD is represented by the horizontal line in the graph. Then the simulations evaluate the local DNA  
14 concentrations at the BioFET originating from PUMA1 and PUMA2, respectively. While the blue curve  
15 shows concentration profile evolution at the BioFET interface as a result of reaction-diffusion mass-  
16 transport from PUMA2, the red curves show evolution of concentration profiles at the BioFET interface  
17 when PUMA1 starting at the same time as PUMA2, i.e. 0 minutes delay. A comparison of these 2 curves  
18 demonstrates that up to 80 minutes, the BioFETs will detect the output from PUMA1 exclusively without  
19 any interference from PUMA2 due to slowing down of the mass-transport across the diffusion barrier. The  
20 yellow, purple and green curves also evaluate a situation, when the PUMA1 starts with a certain time delay  
21 given as 6, 35 and 60 minutes, respectively. The evaluation suggests that a delay of up to 60 minutes (typical  
22 amplification time) can be easily set-up between the onset of two PUMAs and exclusive detection of the  
23 output DNA sequences from PUMA1 or PUMA2 in a spatiotemporal manner (26). We intend to adopt such  
24 engineered fluidic volumes with our BioFET-array chips in order to virtually compartmentalize the  
25 molecular output from different PUMAs surface immobilized onto the ceiling of fluidic layer and carry out  
26 spatiotemporal detection of different biomarkers. In addition, spatiotemporal engineering of mass-transport  
27 on chip is expected to facilitate study of more complex programmable molecular cascades and help setting  
28 up robust platform for studies of molecular biocommunication strategies using nanoelectronics. Additional  
29 data for the time-dependent ssDNA propagation within the microfluidic channel can be found in the  
30 supplementary materials.

31  
32 **4. Conclusion:**  
33 In this work, we studied the mass-transport of small DNA sequences (12bp) as an output of programmable  
34 unique molecular amplification (PUMA) systems spatially arranged in a stopped-flow fluidic volumes. With  
35 an aim towards integration of a biosensor platform for multiplexed detection, biomarker-specific PUMAs

1 were considered, and a reaction-diffusion approach was adopted to simulate the evolution of DNA  
2 concentrations at BioFET-arrays at the bottom of the fluidic volume. For effective spatiotemporal  
3 multiplexing, it was required to engineer the mass-transport in the given fluidic volume by using physical  
4 barriers and optimize build-up of output DNA concentrations related to different PUMAs, for a mutually  
5 exclusive electrical detection by BioFETs. For this, septa with different shapes and sizes were considered  
6 tuning the reaction-diffusion controlled mass-transport. We demonstrate that use of such septa has a critical  
7 influence on the mass transport and can lead to an enormous retarded diffusion along the diffusion channel.  
8 We show that the cuboid septum resulted in a final DNA concentration of around  $0.8 \mu\text{M}$  after 120 minutes,  
9 while an optimized diffusion channel reduced the amount of DNA to approximately  $0.3 \mu\text{M}$ . The geometry  
10 of the diffusion channel determines the diffusion speed of the reaction-diffusion front along the channel.  
11 Firstly, we show that the length of the diffusion channel should be as high as possible to increase the  
12 diffusion length and thus slowing down the speed of the reaction-diffusion front. Secondly, the height of the  
13 diffusion channel should be minimized to further reduce the diffusion speed. Finally, we evaluate that in  
14 such a fluidic volume engineered for optimal operation of PUMAs, a delay of up to 60 minutes between the  
15 start of two molecular programs does not lead to any significant biochemical cross talk. It is expected that  
16 integration of spatiotemporal fluidics with PUMA powered biosensors will allow modular strategies for  
17 multiplexed detection in near future. Overall, spatiotemporal control over mass-transport in confined  
18 volumes like attempted in this work also opens up possibilities to realize on-chip platforms to implement  
19 and study complex BRNs, as a topic of fundamental interest in self-organized systems.

## 20 **5. Supplementary Material**

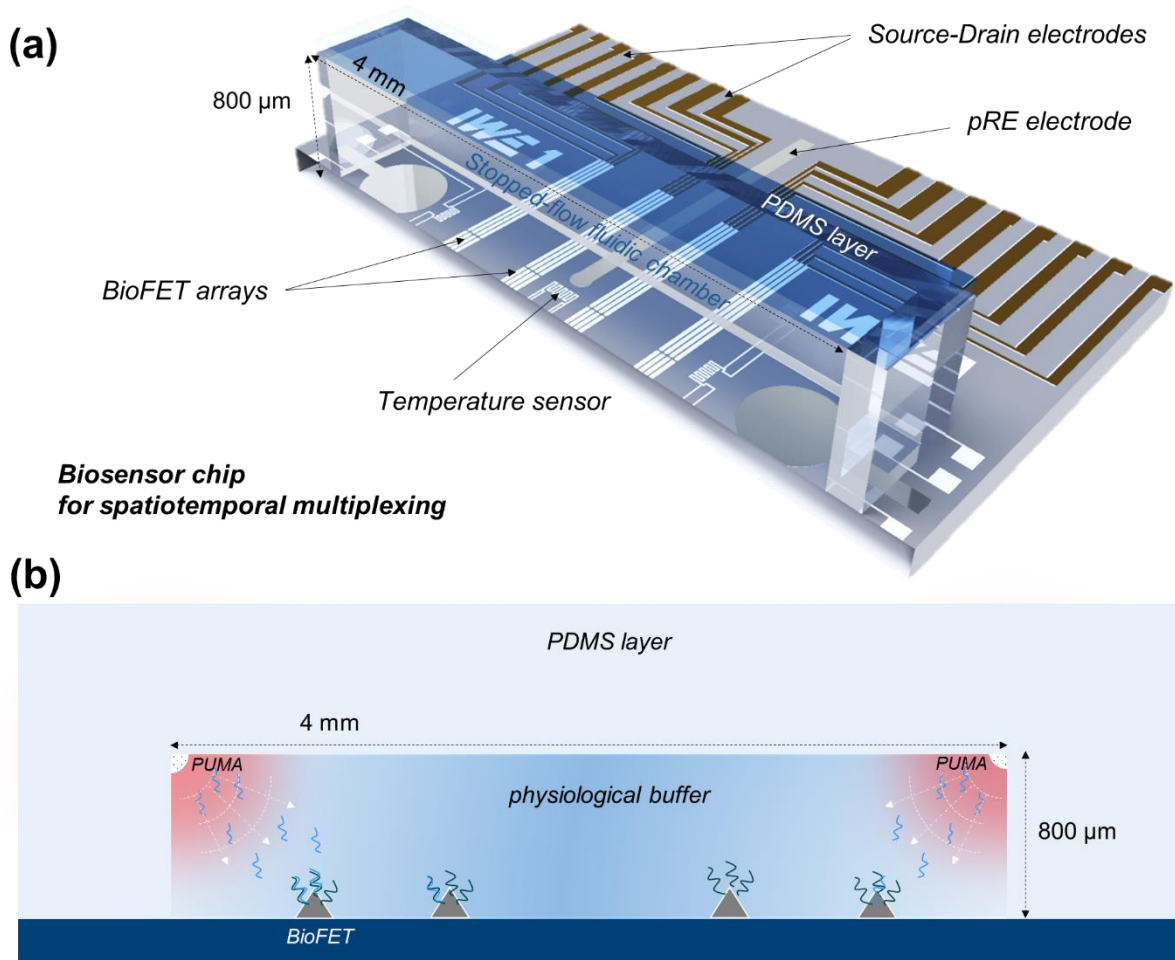
21 The PUMAs considered for the spatiotemporal multiplexing and further details on mass-transport profiles  
22 with and without the use of different kinds of diffusion barriers are discussed in the supplementary material.  
23 Link:

## 24 **6. Acknowledgments**

25 The authors thank the German Research Foundation (DFG) for funding the research project “Molecular  
26 Programs for neurodegenerative diseases markers Biosensing” (Project no. 391107823).

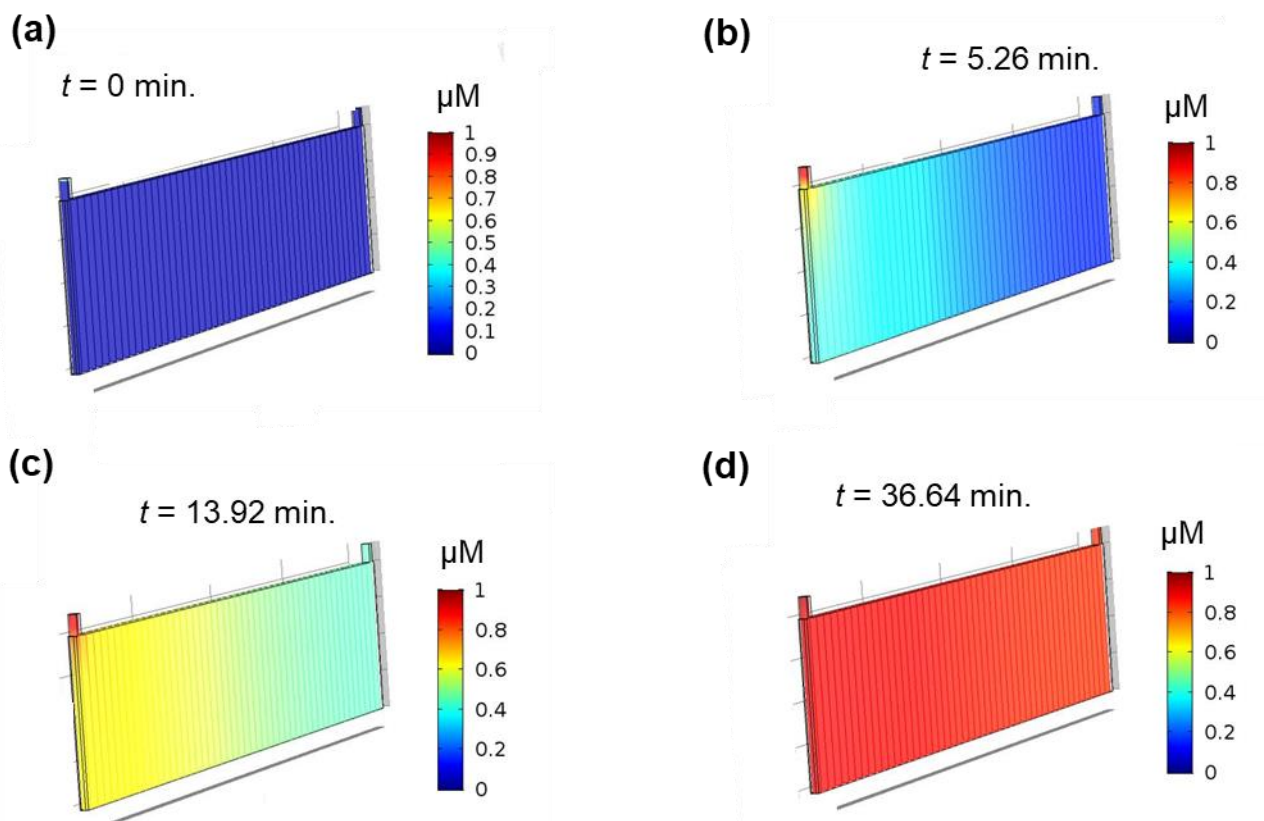
1

## FIGURES

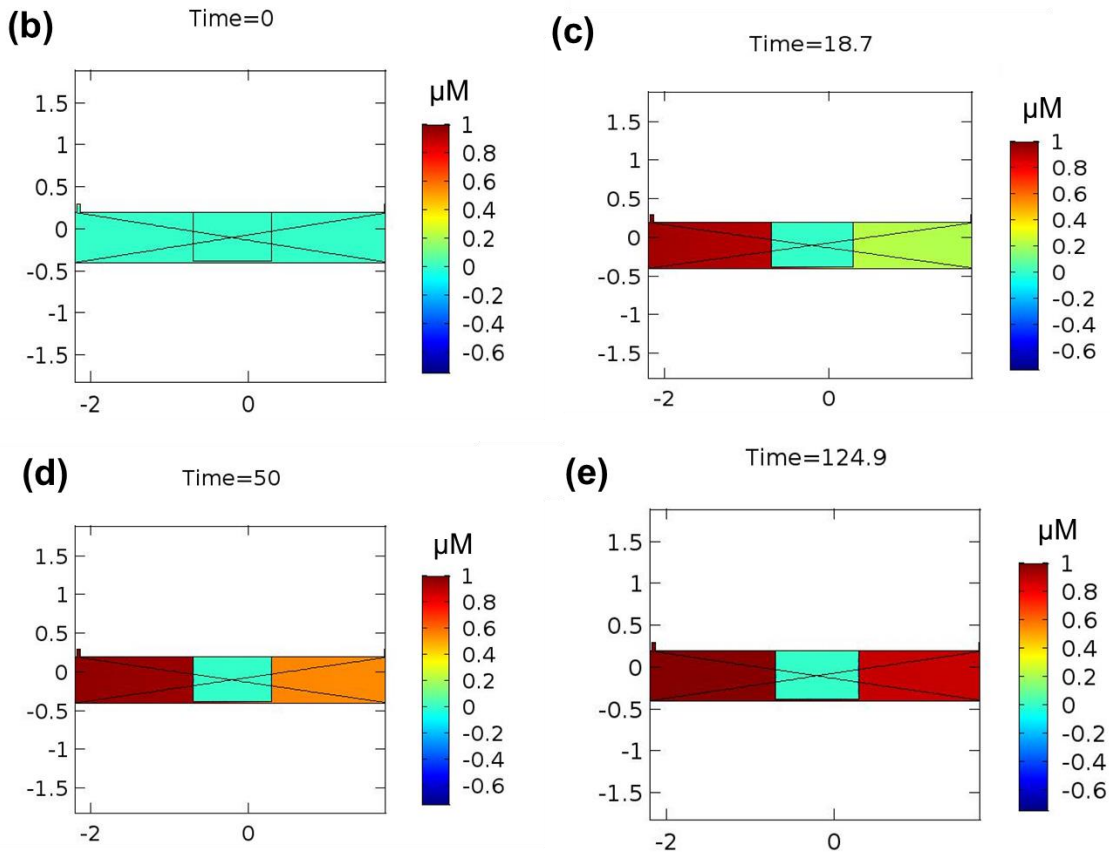
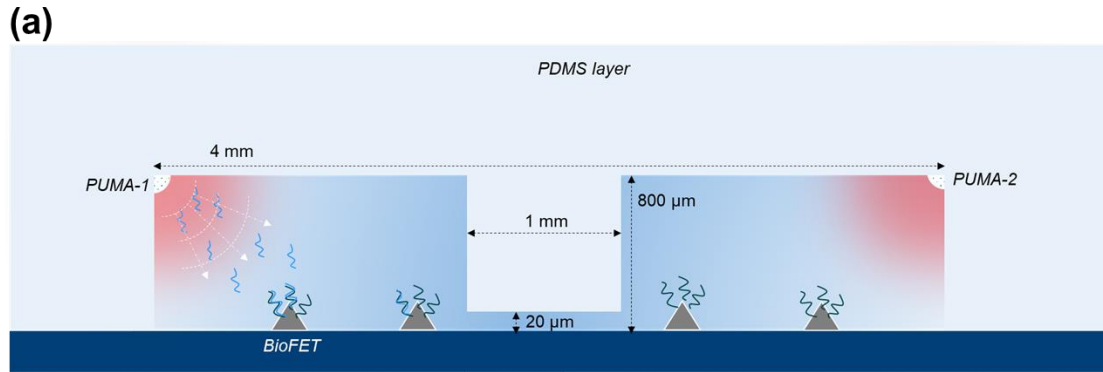


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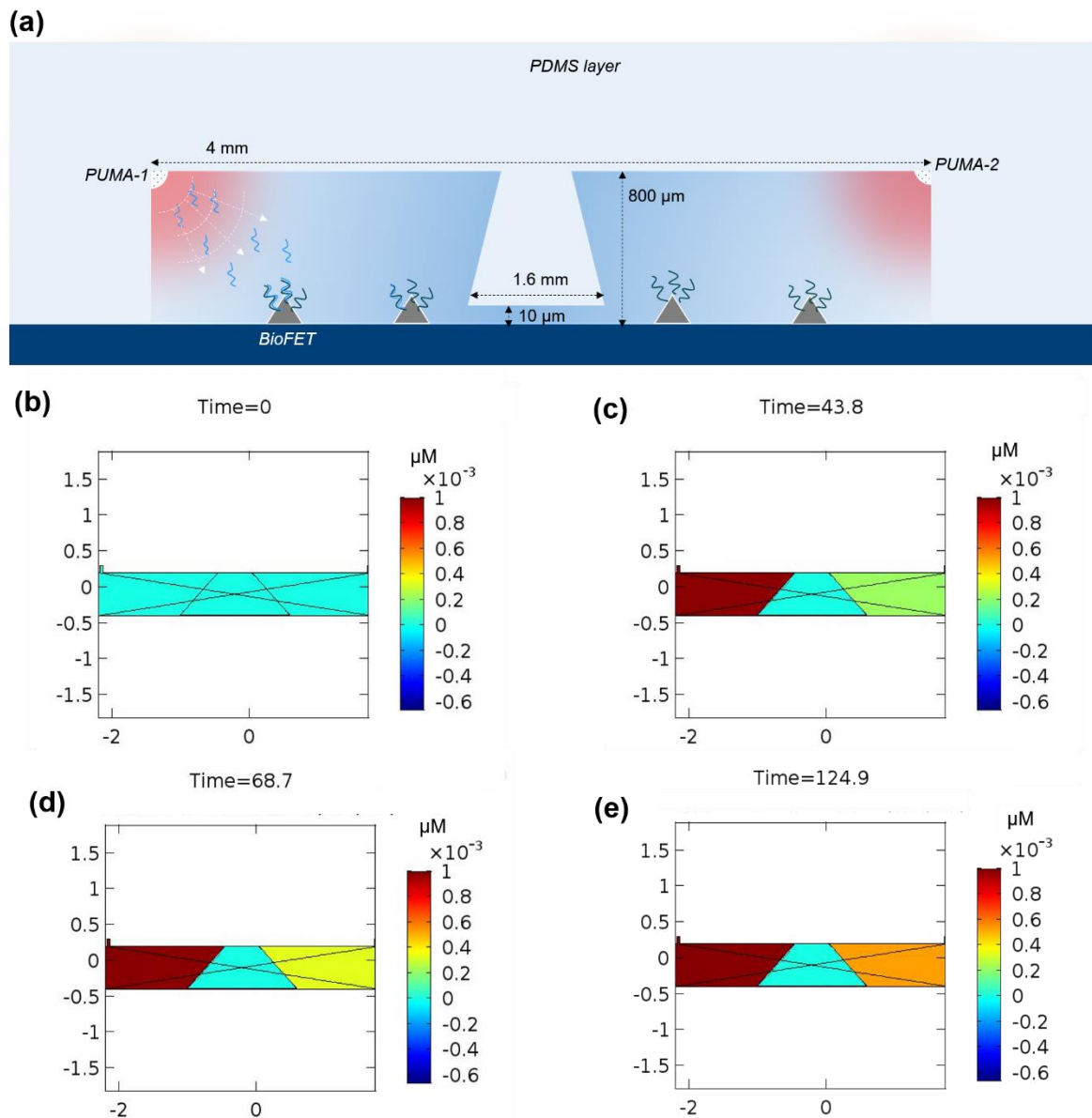
3 **Figure 1:** Schematic illustration of the biosensor platform modelled for spatiotemporal multiplexing with  
 4 the help of programmable ultrasensitive molecular amplification (PUMA) reactions and stopped-flow  
 5 fluidic chamber aimed at reaction-diffusion controlled mass transport. (a) Our biosensor chip with  
 6 biologically sensitive ion-sensitive field-effect transistors arrays (BioFET-arrays) dedicated for running  
 7 such PUMA in small fluidic volumes at elevated temperatures is shown with the fluidic layer on top. (b) A  
 8 vertical cross-section of the biosensor platform shows the fluidic volume filled with the physiological buffer  
 9 and the PUMA surface functionalised on the fluidic layer's ceiling towards left and right extremities. In the  
 10 presence of the analyte (trigger for PUMA), an amplification reaction starts with exponential onset of short  
 11 output DNA (12bp) sequences which are diffusing into the fluidic volume of dimensions  $4 \text{ mm} \times 800 \text{ μm} \times$   
 12  $50 \text{ μm}$  ( $l \times h \times w$ ). Optimal engineering of the spatiotemporal concentration profile of the output DNA  
 13 sequences and programming of PUMA for different analyte biomarkers facilitates biosensor multiplexing  
 14 where different BioFETs specifically sensitive to the PUMA output DNA provide an ultrafast measurement  
 15 of local concentration at the interface (bottom of the fluidic chamber).



1  
2 **Figure 2:** Three-dimensional spatiotemporal mapping of the reaction-diffusion dominated mass transport in  
3 stopped-flow fluidics integrated on top of biosensor chip. (a) In the beginning ( $t = 0$  min), the fluidic volume  
4 is filled with the background electrolyte (physiological buffer) and is devoid of any biomolecule under study  
5 (12bp ssDNA). (b) ssDNA being introduced at the virtual inlet with a concentration of 1  $\mu\text{M}$ . (c) Reaction-  
6 diffusion profiles at different time stamps: (top left) 0 minutes, (top right) 5.3 minutes, (bottom left) 13.9  
7 minutes, (bottom right) 36.6 minutes.

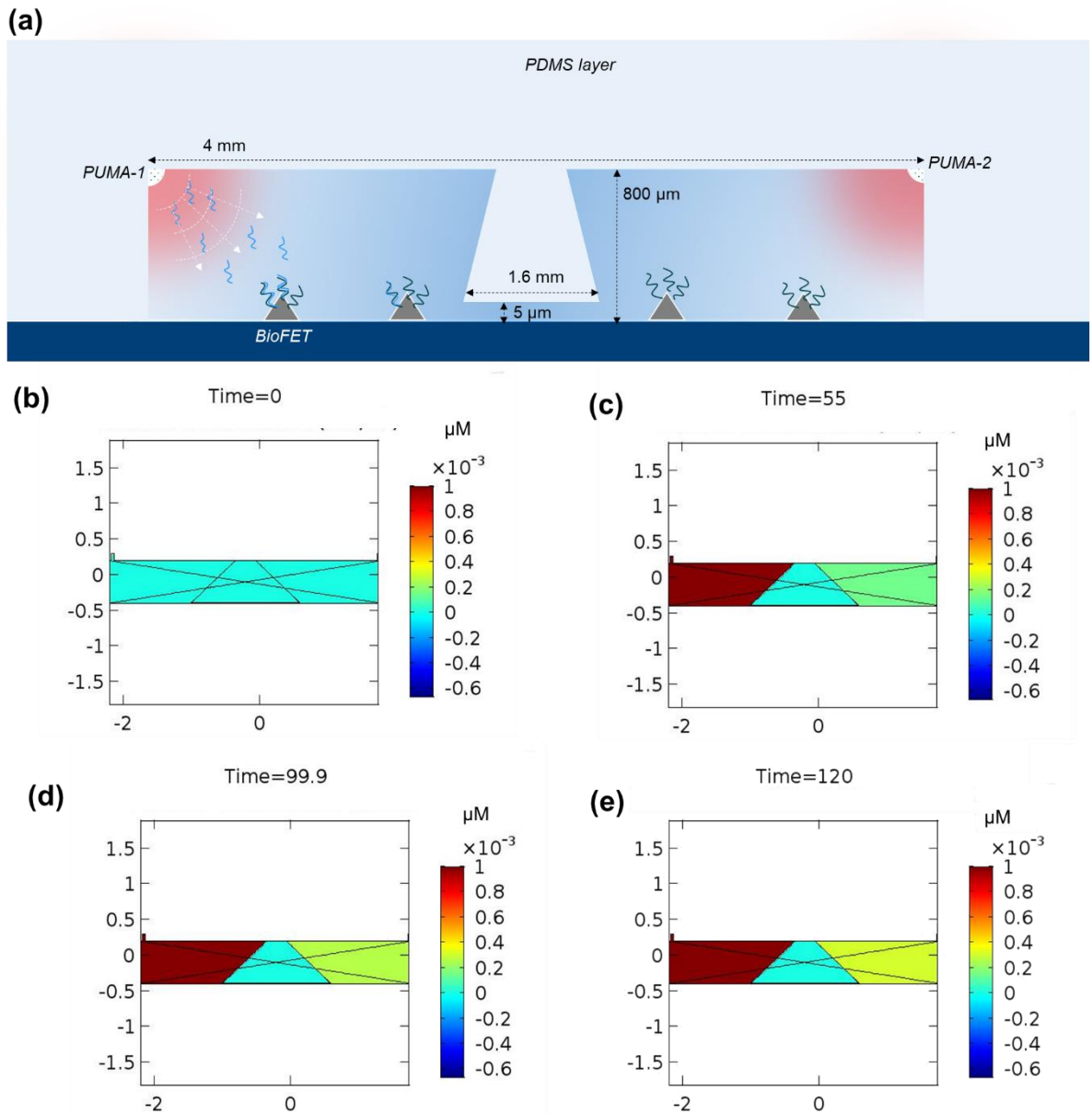


1  
2 **Figure 3:** Reaction diffusion controlled mass transport of 12 bp DNAs while introducing a rectangular shape  
3 septum in the middle of the fluidic volume creating a capillary of 1 mm (length)  $\times$  20  $\mu\text{m}$  (height)  $\times$  50  $\mu\text{m}$   
4 (width). (a) schematic illustration of the set-up, (b-d) DNA concentration due to reaction-diffusion mass  
5 transport after the start of PUMA-1 shown at 0, 18.7, 50 and 125 minutes.

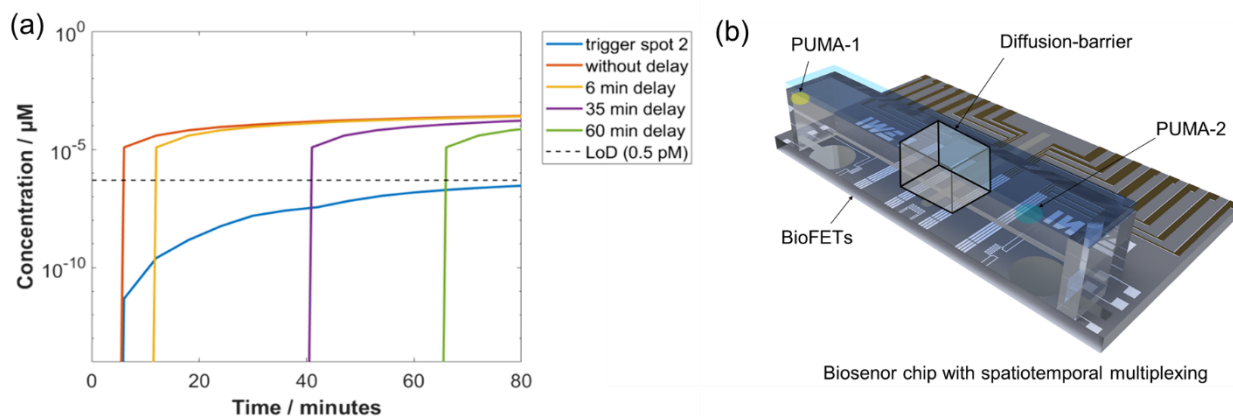


1  
 2 **Figure 4:** Reaction diffusion controlled mass transport of 12 bp DNAs while introducing a trapezoidal shape  
 3 septum in the middle of the fluidic volume creating a capillary of 1.6 mm (length)  $\times$  10  $\mu\text{m}$  (width)  $\times$  50  $\mu\text{m}$   
 4 (height). (a) schematic illustration of the set-up, (b-d) DNA concentration due to reaction-diffusion mass  
 5 transport after the start of PUMA-1 shown at 0, 18.7, 50 and 125 minutes, which is much slower than the  
 6 set-up with rectangular septum.





1  
2 **Figure 5:** Reaction diffusion controlled mass transport of 12 bp DNAs while introducing a trapezoidal shape  
3 septum in the middle of the fluidic volume creating a capillary of 1.6 mm (length)  $\times$  10  $\mu\text{m}$  (width)  $\times$  50  $\mu\text{m}$   
4 (height). (a) schematic illustration of the set-up, (b-d) DNA concentration due to reaction-diffusion mass  
5 transport after the start of PUMA-1 shown at 0, 55, 100 and 120 minutes, which is favourable for being  
6 slower than the previous two set-ups.



1  
 2 **Figure 6:** Reaction-diffusion regulated spatiotemporal multiplexing on chip. (a) The graph shows concentration of  
 3 PUMA output DNA sequence at BioFET interface closer to the release spot 1 (b) Illustration of the biosensor chip with  
 4 reaction-diffusion fluidic volume on top. The PUMA output DNA concentrations at different time intervals,  
 5 exponential increase of concentration at the interface due to reaction-diffusion regulated mass transport and saturation  
 6 is simulated. The blue curve shows the concentration evolution of output DNA sequence from release spot 2, which  
 7 for the given time domain remain below the limit-of-detection of the BioFETs.

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