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Thermal transport properties of porous silicon filled by ionic liquid nanocomposite system

Pavlo Lishchuk^{1✉}, Alina Vashchuk^{2,5}, Sergiy Rogalsky³, Lesia Chepela¹, Mykola Borovyj¹, David Lacroix⁴ & Mykola Isaiev⁴

This paper investigates thermal transport in a nanocomposite system consisting of a porous silicon matrix filled with ionic liquid. Firstly, the thermal conductivity and heat capacity of two imidazolium and one ammonium ionic liquids were evaluated using the photoacoustic approach in piezoelectric configuration and differential scanning calorimetry, respectively. Then, the thermal transport properties of the composite system "ionic liquid confined inside porous silicon matrix" were investigated with the photoacoustic approach in gas-microphone configuration. The results demonstrated a significant enhancement of the thermal conductivity of the composite system when compared to the individual components, i.e. (i) more than two times for pristine porous silicon and (ii) more than eight times for ionic liquids. These results provide new paths for innovative solutions in the field of thermal management, particularly in the development of highly efficient energy storage devices.

Ionic liquids (ILs) are a unique class of organic salts presenting melting temperatures below 100 °C. Among all their particular features, ILs show high-voltage stability windows, nearly null volatility, non-flammability, high ionic conductivity, thermal and radiation stability over a wide range of temperatures, corrosion resistance and recyclability¹. Moreover, the physicochemical characteristics of ILs can be easily tailored through an endless combination of cationic or anionic constituents, thus leading to labelling them as "designer solvents"^{2,3}.

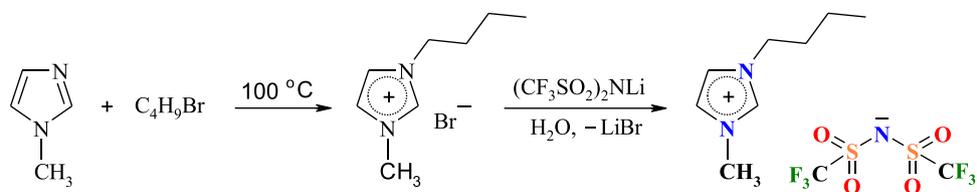
Most ILs tend to self-assemble due to competition between electrostatic and Van der Waals interactions of the charged and a-polar alkyl side-chain(s) moieties⁴. Moreover, the confinement of IL inside a solid porous matrix (host) causes unexpected effects on their physical properties, namely ionic mobility and viscosity^{5,6}. In particular, the integration of IL into pores of 20 nm induces a nanometric structuration of the IL molecules, which increases the ionic conductivity by one order of magnitude in comparison to the bulk state⁷. The latter was attributed to changes in ion packing under geometric confinement leading to higher mobility and electrical conductivity. The ILs confinement in unidirectional silica nanopores (7.5–10.4 nm) induces a change of thermal activation behavior from a Vogel-Fulcher-Tamman (VFT) to an Arrhenius-like trend resulting in an enhancement of diffusion coefficients by more than two orders of magnitude⁸. Noteworthy, the effect becomes more pronounced with decreasing pore diameter. Previous works have reported the importance of both the pore's size and the surface chemistry of the host⁹.

In designing advanced materials, the confinement of ILs inside porous materials seems to be a promising design strategy for comprehensive application sets. Shared solid porous hosts for ILs are nanoporous polymer⁷, nanoporous carbon^{10–12}, carbon nanotubes¹³, silicon^{14,15}, nanoporous silica¹⁵, silica glass nanocapillaries¹⁶ and metal–organic frameworks^{17,18}.

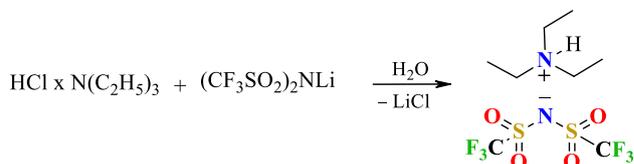
Liquids confined in porous matrix systems are promising for their application in various power sources and storage devices^{19,20}. In such applications, the systems can be significantly overheated during energy storage and operation. Therefore, understanding thermal properties features in such composite systems is essential for elaborating the new highly efficient energy storage devices.

Porous silicon (PSi) is very attractive as a host for ILs due to its wide diversity of pores^{21,22} and sizeable specific surface area that significantly impact heat and mass transfer of the fluid confined in the porous network. PSi is

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Scheme 1. Synthesis of aprotic ionic liquid [BMIm][TFSI].



Scheme 2. Synthesis of protic ionic liquid [TEA][TFSI].

stiffer than polymer matrix which could lead to significant confinement of the ILs. Moreover, the hydrophobicity of PSi makes it especially attractive as a model for studying the confinement effect of ILs since the water contamination absorbed from the atmosphere is negligible. Although the compatibility of ILs with PSi has been proven^{23,24}, their thermal transport properties have not yet been investigated. However, their application potential is excellent, as such materials allow the production of parts for cooling circuits, massive thermal isolators, etc. Therefore, the article's primary goal is to investigate the thermal properties of the ILs based nanocomposite systems.

In this work, the hosting matrix is porous silicon fabricated by electrochemical etching. Two imidazolium ILs (hydrophobic/aprotic, hydrophilic/protic) and ammonium IL (hydrophobic/protic) were chosen as fillers. In order to quantify the changes induced by the confinement of ILs on the thermal transport properties of resulting silicon-based composites, the photoacoustic approach was adopted.

Materials and methods

Following chemicals were used in this research: imidazole, 1-methylimidazole, lithium bis(trifluoromethylsulfonyl)imide (water solution) (for synthesis), triethylamine hydrochloride (99%), 1-bromobutane (99%), bis(2-ethylhexyl) phosphate (97%) (Sigma-Aldrich), ethyl acetate, methylene chloride (Uoslab, Ukraine).

Materials fabrication. *Synthesis of ionic liquids.* Synthesis of 1-butyl-3-methylimidazolium bis(trifluoromethylsulfonyl)imide ([BMIm][TFSI]). Hydrophobic aprotic ionic liquid [BMIm][TFSI] was synthesized according to Scheme 1. The mixture of 1-methylimidazole (10 g, 0.12 mol) and 1-bromobutane (25.5 g, 0.13 mol) was stirred at 100 °C for 2 h. After cooling, the viscous liquid was purified by washing with ethyl acetate (3 × 50 ml). Residual solvent was removed under vacuum 15 mbar at 60 °C.

To the stirred solution of crude 1-butylimidazolium bromide in 100 ml of water was added water solution of lithium bis(trifluoromethylsulfonyl)imide (29 g, 0.1 mol/100 ml). The mixture was stirred for 1 h, and the formed water-immiscible layer was extracted with methylene chloride (2 × 150 ml). The solution was dried with sodium sulfate overnight. Methylene chloride was distilled, the residual solvent was removed under vacuum 5 mbar at 70 °C for 12 h. The liquid product of light brown color was obtained.

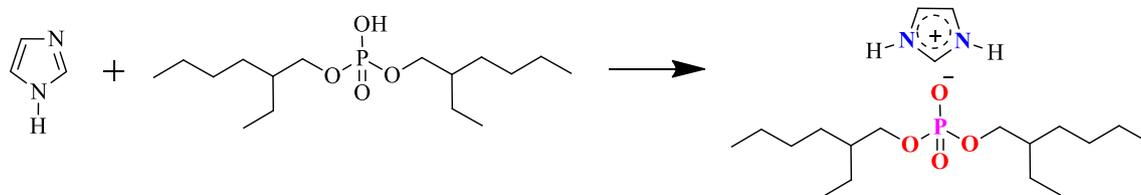
¹H NMR (400 MHz, CDCl₃) δ 8.72 (s, 1H, C₂-H), 7.32–7.29 (m, 2H, C₄-H, C₅-H), 4.16 (t, J = 7.4 Hz, 2H, NCH₂), 3.92 (s, 3H, NCH₃), 1.90–1.77 (m, 2H, NCH₂CH₂), 1.39–1.32 (m, 2H, NCH₂CH₂CH₂), 0.95 (t, J = 7.4 Hz, 3H, CH₃).

¹⁹F NMR (188 MHz, DMSO-d₆): δ = −79.92 (s, 6F, CF₃).

Synthesis of triethylammonium bis(trifluoromethylsulfonyl)imide ([TEA][TFSI]). Hydrophobic protic ionic liquid [TEA][TFSI] was prepared according to Scheme 2. To the stirred water solution of triethylamine hydrochloride (10 g, 0.07 mol/50 ml) was added water solution of lithium bis(trifluoromethylsulfonyl)imide (21 g, 0.07 mol/100 ml). The mixture was stirred for 2 h, and the formed water-immiscible layer was extracted with methylene chloride (2 × 150 ml). The combined organic solution was dried with sodium sulfate. Methylene chloride was distilled, the residual solvent was removed under vacuum 5 mbar at 70 °C. The transparent liquid product was obtained.

¹H NMR (400 MHz, CDCl₃): δ 6.87 (s, 1H, NH), 3.17 (q, 6H, CH₂), 1.31 (t, 9H, CH₃)

¹⁹F NMR (188 MHz, DMSO-d₆): δ = −79.97 (s, 6F, CF₃)



Scheme 3. Synthesis of protic ionic liquid [Im][BEHP].

Synthesis of imidazolium bis(2-ethylhexyl)phosphate ([Im][BEHP]). Hydrophilic protic ionic liquid [Im][BEHP] was prepared by stirring the mixture of imidazole (5 g, 0.07 mol) and bis(2-ethylhexyl)phosphate (23.5 g, 0.07 mol) at 50 °C for 6 h (Scheme 3).

^1H NMR (400 MHz, CDCl_3) δ 8.04 (s, 1H, $\text{C}_2\text{-H}$), 7.12 (d, $J=1.2$ Hz, 2H, $\text{C}_4\text{-H}$, $\text{C}_5\text{-H}$), 3.8 (q, $J=4.9$ Hz, 4H, OCH_2), 1.54 (h, $J=5.9$ Hz, 2H, CH_2CH), 1.47–1.19 (m, 16H, CH_2), 0.99–0.70 (m, 12H, CH_3).

The molecular structure and molecular weight of ILs used in this study are summarised in Table 1. ^1H NMR spectra of ILs are given in the Supplementary file.

Ionic liquid	Molecular structure		Molecular weight (g/mol)
	Cation	Anion	
1-butyl-3-methylimidazolium bis(trifluoromethylsulfonyl)imide [BMIm][TFSI]			419.36
Triethylammonium bis(trifluoromethylsulfonyl)imide [TEA][TFSI]			382.3
Imidazolium bis(2-ethylhexyl)phosphate [Im][BEHP]			390.5

Table 1. Molecular structure and molecular weight of ILs under investigation.

Porous silicon fabrication. As the initial porous matrix for ILs we used mesoporous silicon obtained by electrochemical etching of 500 μm boron-doped p^+ type silicon substrate (with a resistivity of 10–20 $\text{m}\Omega\text{ cm}$ and [100] orientation). The etching was done in a mixture of hydrofluoric acid (49%) and ethanol in a ratio of 1:1. The porosity (~65%) and thickness (50 μm) of PSi layer were controlled the etching current density and time and checked by gravimetric method and SEM microscopy, respectively. The mass of the removed silicon was equal to 20 mg, the balance used in this experiment had a resolution of 0.1 mg, which ensured the necessary level of accuracy. The mass of the IL inside the pores was estimated by calculating the mass difference between the dry and wet samples. This allows a direct evaluation of the volume of the pores filled by the ionic liquid. The same balance was used for these measurements, ensuring consistency and reliability of provided results.

Fabrication of the nanocomposites. The nanocomposite systems "porous silicon/ionic liquid" were obtained by filling the pores of PSi samples with ILs. This procedure was made by following steps:

- (1) The IL was added to the PSi surface;
- (2) The sample was heated to a temperature of 80 $^{\circ}\text{C}$ for 10 min;
- (3) The samples were passively cooled and kept as it with liquid remaining on the surface for 24 h;
- (4) Excess of IL was removed from the PSi surface.

The excess of IL was carefully blotted from the surface of the samples using a lint-free cloth, without touching the sorbent with the porous layer of silicon to avoid mechanical damage. This operation was performed under optical magnification using a microscope. The effectiveness of the process was statistically assessed by weighing the samples before and after the removal process.

For all the samples, the degree of pore filling was determined by the gravimetric method and was not less than 95%. It was supposed that the PSi matrix was filled completely and homogeneously, the geometry of PSi/IL samples was not modified. [BMIm][TFSI] and [TEA][TFSI] were hydrophobic. Thus, the effect of water contamination absorbed from the atmosphere on thermal conductivities was insignificant.

Experimental setups. *Proton nuclear magnetic resonance spectroscopy.* Proton Nuclear Magnetic Resonance (^1H NMR) spectroscopy was used to confirm the structure of synthesised compounds. The spectra were recorded on a Varian Gemini-2000 (400 MHz) NMR spectrometer.

Density and heat capacity measurements. Information about the structure's density and specific heat capacity plays an essential role in thermal conductivity evaluation by photothermal methods. The densities of all ILs (average value of three measurements) were determined directly from their weighing at room temperature ($T=25$ $^{\circ}\text{C}$).

Determination of specific heat of ILs was carried out by the differential calorimetry method. Two thermally insulated aluminium vessels were used so that heat losses to the surroundings can be kept as low as possible. The heat was supplied equally by heating nichrome coils which were immersed simultaneously in vessel with water and with studied liquid. The temperature changes in each vessel was recorded by K-type thermocouples connected to a 2-channel LCD data logger with a resolution of 0.1 $^{\circ}\text{C}$ in a broad range of monitoring applications. A schematic picture of the experimental setup is shown in Fig. 1.

The heat capacity of the studied liquid can be calculated using the known values for Al vessels (calorimeters) and water by the following formula based on the solution of the system of equations of the heat quantities obtained by the calorimeter with water and the calorimeter with the studied liquid:

$$c_l = \frac{1}{m_l} \left[\frac{(c_{Al}m_{Al} + c_w m_w)(t_2 - t_1)}{(t_4 - t_3)} \right] - c_{Al}m_{Al} \quad (1)$$

where c —is a specific heat; m —is a mass; indexes "Al", "w" "l" indicates that the respective parameters are taken for the Al calorimeters (vessels), water in the first calorimeter, and studied liquid in the second calorimeter, respectively; t_1 and t_2 are the initial and final temperature in the first calorimeter; t_3 and t_4 are the initial and final temperature in the second calorimeter.

The technique was tested on a control sample PEG 400E, from which the obtained value of the specific heat capacity (2300 $\text{J}/(\text{kg } ^{\circ}\text{C})$) correlates qualitatively with the literature data²⁵. The results obtained for the studied

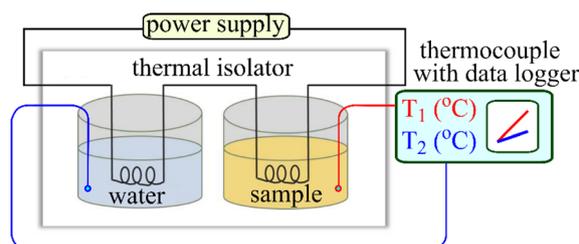


Figure 1. Schematic view of the experimental setup for heat capacity measurements of ILs.

ILs are shown in Table 2. As can be seen from the table, the specific heat values are within the range of values known from the literature for various ILs^{26,27}.

Photoacoustic technique for thermal conductivity (k) measurements. The photoacoustic technique was used to provide the thermal conductivity of ILs and «PSi/IL» nanocomposite systems²⁸. This technique refers to non-destructive methods for investigating the thermophysical properties of materials of different aggregate states and dimensions^{29–35}. The experimental setup is described in^{36,37}. In our case, installation includes a UV laser (405 nm) that, together with a square signal generator used as a source of modulated light. The UV irradiation is focused on the surface of the samples, creating thermoelastic stresses inside them. Samples inside the PA cell can record the response related to the PA effect. The design and type of PA signal recording depend on the studied object. Namely, the PA cell with a piezoelectric transducer (PZT) was used to study the thermal conductivity of ILs (see Fig. 2a), and a gas-microphone photoacoustic cell (PA GM cell) was used for the analysis of composite systems (see Fig. 3a). All the experiments by PA technique were done at room temperature.

(A) Thermal conductivity measurements of ILs

In this case, the PA cell is a multilayer structure that made of different layers distributed from the laser illumination side in the following order: optically transparent buffer—strongly absorbing layer—liquid sample layer ($l_s = 100 \mu\text{m}$)— $900 \mu\text{m}$ aluminium layer— $1000 \mu\text{m}$ buffer— $700 \mu\text{m}$ piezoelectric transducer. Thus, thermal energy

Liquid	ρ (kg/m ³)	c [J/(kg °C)]
[BMIm][TFSI]	1380 ± 80	1350 ± 110
[TEA][TFSI]	1380 ± 80	1380 ± 110
[Im][BEHP]	1000 ± 80	2060 ± 110

Table 2. Density and specific heat capacity of ILs.

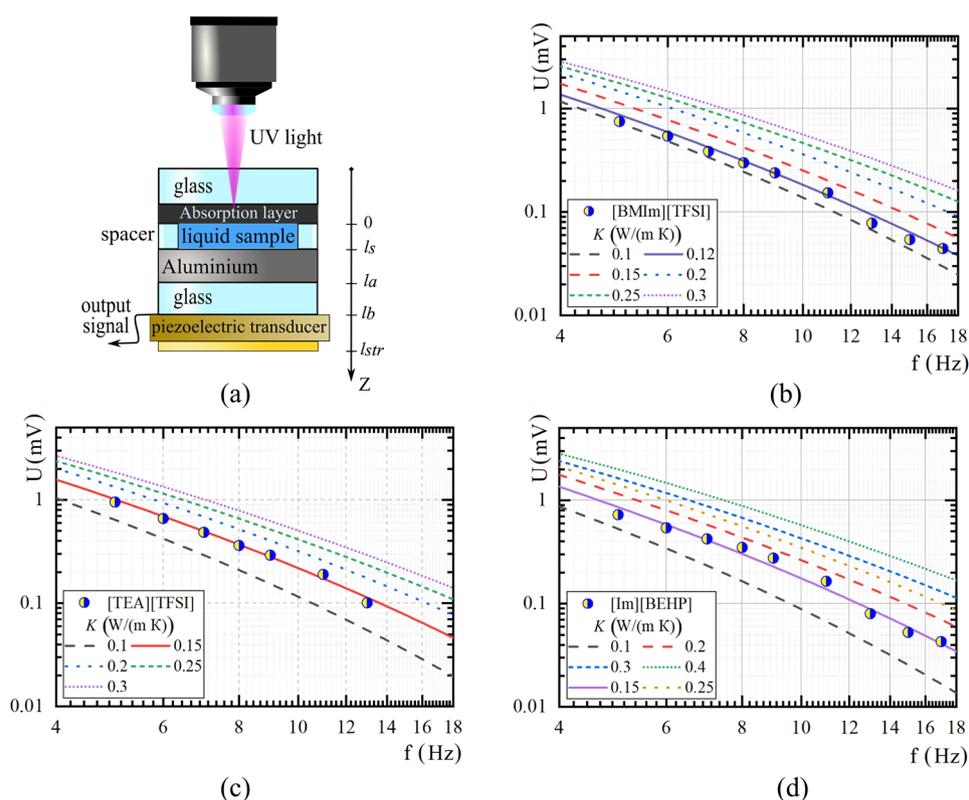


Figure 2. PA cell with piezoelectric registration employed (a), amplitude-frequency characteristics of a multilayer system with IL: [BMIm][TFSI] (b), [TEA][TFSI] (c), [Im][BEHP] (d). Circles indicate the experimental data, lines—the simulation of PA signal formation at different values of thermal conductivity of the liquid sample.

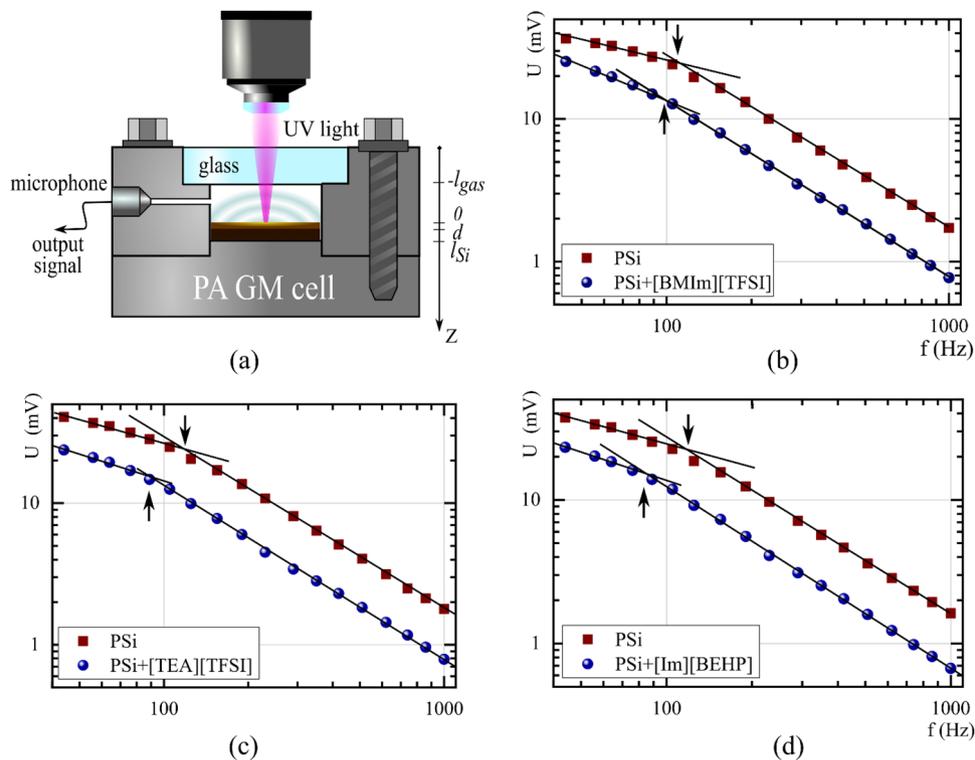


Figure 3. PA cell with gas-microphone registration employed (a), amplitude–frequency characteristics of PSi and “PSi/IL” composite systems with IL: [BMIm][TFSI] (b), [TEA][TFSI] (c), [Im][BEHP] (d). Arrows indicate the bending frequency.

arises and propagates in the system in the form of thermoelastic stresses due to the absorption of light by a thin absorbing layer located above the liquid. Thermoelastic stresses go through the studied liquid to a metal plate, and finally are recorded by a piezoelectric transducer. The time delay between the start of heating and the system’s bending depends on the fluid’s thermal conductivity. Thus, to estimate this value, one can use information about the dependence of the voltage on the piezoelectric transducer electrodes on the frequency of optical radiation.

(B) Thermal conductivity measurements of nanocomposite systems

To measure the thermal conductivity of composite systems “PSi/IL” we used the classical configuration of PA cell with gas microphone registration^{36,37}. This method belongs to the indirect PA research technology, since the signal is recorded in the gas isolated in the PA cell adjacent to the sample surface. Periodic heating of the sample leads to periodic heating of the gas and acoustic waves’ appearance, which are recorded by the microphone. Information regarding the frequency response of such a signal indicates the thermophysical properties of the sample under study.

Results and discussion

Thermal properties of ILs. The amplitude–frequency characteristics of the informative signal from the PA cell described in Fig. 2a were measured in the frequency range from 5 to 18 Hz. The obtained experimental results were analysed by modelling the spatial distribution of variable temperature in the multilayer structure (see Fig. 2b–d), as described briefly in³².

The frequency-dependent voltage $U(\omega)$ that occurs at the electrodes of the piezoelectric transducer, in this case, can be written as³²:

$$U(\omega) \sim \int_{l_b}^{l_{str}} \sigma(z) dz = \int_{l_b}^{l_{str}} \frac{E(z)}{1-\nu(z)} \int_{l_s}^{l_a} \frac{\alpha_T(s) E \theta(s, \omega)}{1-\nu(s)} G(z, s) ds dz \quad (2)$$

where $\omega = 2\pi f$, f is the modulation frequency of the UV light, $\sigma(z)$ is the spatial distribution of the thermoelastic stresses, $\alpha_T(s)$ —is the thermal expansion coefficient of the material, $\theta(s, \omega)$ is the temperature distribution, E —is Young’s modulus, ν —is Poisson’s ratio, l_{str} , l_b , l_a , l_s —are the thicknesses of the piezoelectric transducer, backing material, aluminium and liquid sample layers, respectively.

This equation was used to match the experimental amplitude–frequency characteristics of PA signal when we used some reference liquids as test samples. The thermal conductivity value of fluid was a fitting parameter in the simulation. Before considering ILs, test cases were achieved on water, oil and PEG. The values at which the

experiment qualitatively matches the simulation are as follows: for water $K=0.6 \pm 0.02$ W/(m K), for technical oil $K=0.15 \pm 0.02$ W/(m K), and for PEG 400E $K=0.2 \pm 0.02$ W/(m K). These values correlate with technical data of liquids and literature values. This demonstrates the ability of the setup and the inversion technique to recover the thermal conductivity of different liquids. When applied to ILs, the results of PA signal simulation from a multilayer system show that their thermal conductivity is within the range of 0.12–0.15 W/(m K), which is typical for ILs³⁸.

Thermal properties of nanocomposites. PA signal from PSi samples and corresponding "PSi/IL" composite systems were evaluated in the frequency range from 40 to 1000 Hz, in which the PA GM cell is working in the non-resonant mode. The obtained experimental results were analysed by the "critical frequency" method³⁷. This method models the thermal perturbations that occur when the sample is irradiated with modulated light by rapidly damped heat waves. They can be characterised by the thermal diffusion length, which depends on the frequency of light modulation and thermophysical properties of the structure³⁷:

$$\lambda_T = \sqrt{D_T(\pi f)} \quad (3)$$

where λ_T is the thermal diffusion length, D_T is the thermal diffusivity of the sample.

In our case, the critical frequency can be defined as "bending frequency" on the amplitude-frequency characteristics of PA signal for a two-layer system, where the upper layer is porous silicon with empty pores or filled with ILs, and the lower layer is monocrystalline silicon. This bending frequency corresponds to the case where the thermal diffusion length coincides with the size of the top layer, dividing the AFC into 2 characteristic frequency regions, according to which the bottom c-Si affects or does not affect the PA response. Thus, the thermal conductivity of the top layer can be obtained from the following expression for its thermal diffusivity³⁷:

$$\frac{K}{c\rho} = D_T = \pi f_c l^2 \quad (4)$$

where f_c —is a critical (bending) frequency.

It should be noted that the volumetric heat capacity of the samples was obtained using the following weighted formula³⁹:

$$\begin{aligned} c_{PSi} \rho_{PSi} &= c_{Si} \rho_{Si} (1 - \varepsilon) \\ c_{PSi/IL} \rho_{PSi/IL} &= c_{Si} \rho_{Si} (1 - \varepsilon) + c_{IL} \rho_{IL} \varepsilon \xi \end{aligned} \quad (5)$$

where $c_{PSi} \rho_{PSi}$ and $c_{PSi/IL} \rho_{PSi/IL}$ are the volumetric heat capacity of the PSi and "PSi/IL" composite; respectively. $c_{Si} \rho_{Si}$ and $c_{IL} \rho_{IL}$ are the volumetric heat capacity of monocrystalline silicon and ILs, respectively; ε is the porosity, ξ is the degree of filling of the pores with IL.

The experimental amplitude-frequency dependencies of the PA signal for PSi and PSi/IL composites and characteristic critical frequencies are shown on Fig. 3. The Fig. 3 shows the experimental amplitude-frequency dependencies of the PA signal for both PSi and PSi/IL composites. As depicted in Fig. 3, a distinct change in slope, referred as "the critical frequency"³⁷, can be observed in the amplitude-frequency dependencies. This critical frequency falls within the signal investigation range for all samples (as indicated by the arrows). At low frequencies, the thermal diffusion length (as described by Eq. 3) is greater than the thickness of the studied material layer, which is thus considered as thermally "thin" in this case, resulting in a thermal wave reaching the substrate. As the modulation frequency of the radiation increases, the thermal diffusion length decreases accordingly. At frequencies above the critical frequency value, the thermal wave dissipates within the porous layer, resulting in a layer becoming thermally "thick". The critical frequency values vary between the pristine samples and composites, as the presence of IL alters the effective thermal conductivity of the sample. It is worth to mention that, in all instances, the critical frequency of the composites occurs at lower frequencies than that of the porous silicon with empty pores, as its thermal conductivity is lower than the one of the composite systems based on it.

The estimated averaged thermal conductivity values of the studied ILs, initial PSi samples and the corresponding composite systems "PSi/IL" are shown in Fig. 4.

It was found that the thermal conductivity of the "PSi/IL" composite systems increases up to 2.5 times compared to the initial PSi samples. The difference can be explained by improved thermal contact between the Si crystallites and the IL as a filler³⁷ and the structuration of the liquid layer close to the interface of the porous matrix⁴⁰.

The assessment of these factors to the resulting thermal conductivity was carried out by simulating thermal transport in the original porous silicon and composite systems using COMSOL Multiphysics software. A 3D model reconstructed a porous matrix's morphological features before and after filling with an ionic liquid was created. As important markers for the simulation of the PSi structure, the average size of silicon nanocrystallites connected by narrow bridges, observed in several SEM images (see Fig. 5A), as well as the porosity of the system, were used. To evaluate the effective thermal conductivity, we generated the temperature gradient within the sample by applying the temperature difference between the top and bottom boundary of the simulated box. In lateral directions, we used periodic boundary conditions. Figure 5B demonstrates that the heat flow primarily runs along the surface of the crystallites, mostly localized at the necks connecting two crystallites, constituting the primary mechanism for reducing of thermal conductivity in porous silicon^{37,39,41}. However, when an IL is added with a structured layer adjacent to the Si surface, additional channels of heat transport emerge (e.g., between the silicon crystallites from neighbouring chains, as shown in Fig. 5C), leading to an increase in the system's thermal conductivity. At the same time, the layer of structured IL plays a significant role in the large rise of thermal conductivity.

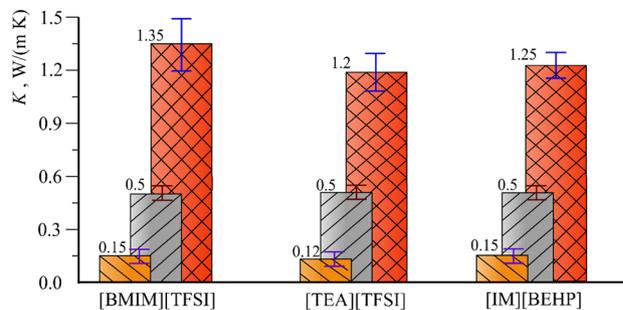


Figure 4. Thermal conductivity of IL (\\\\-line hatched columns), PSi (///-line hatched columns), "PSi/IL" composite system (#-line hatched columns).

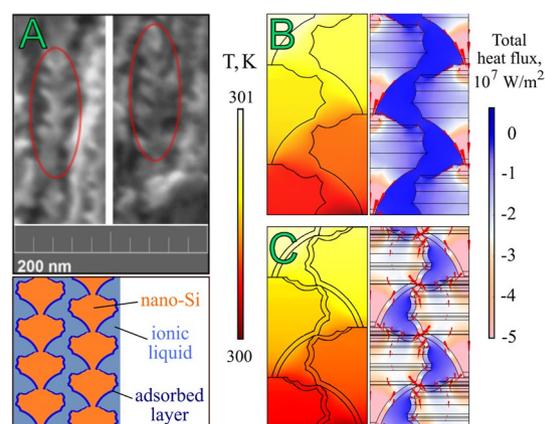


Figure 5. SEM cross-sectional images of PSi (highlighted areas show tentative markers indicating the features of the morphology of the porous structure of silicon) and below a schematic view of averaged by size Si nanocrystalline with a structured IL layer around it as the basis for modelling (A); schematic view of temperature distribution on the left half and cross-plane total heat flux q on the right half in PSi (B) and "PSi/IL" ([BMIM][TFSI]) composite system (C), respectively. Red arrows show the directions of heat fluxes.

According to the model, a temperature gradient was set in a system with known thermophysical properties of the components (nanostructured silicon with air or ionic liquid) to calculate the generated heat fluxes (see Fig. 5B and C). The effective thermal conductivity of the whole structure was evaluated from the following equation:

$$K_{eff} = (q \cdot l_z) / \Delta T \quad (6)$$

where K_{eff} —is an effective material's thermal conductivity, q —is a local heat flux density, ΔT —is a temperature difference between the top and bottom of the modelled structure along the (100)-direction, l_z —thickness of the modelled structure.

The thermal conductivity of Si nanocrystallites as a solid phase in the model material was evaluated according to the Minnich and Chen model, mentioned in⁴⁰:

$$K_{nano-Si} = \frac{K_{c-Si}}{1 + SSA \cdot \lambda_x / 4} \quad (7)$$

here K_{c-Si} —is the thermal conductivity of highly doped monocrystalline silicon, SSA —is the specific surface area^{42,43}, $\lambda_{ph} = 1 / \sqrt[3]{N}$ is the linear phonon mean free path, N —is the concentration of boron dopants in silicon structure ($N = (4-9.5) \cdot 10^{18} \text{ cm}^{-3}$).

The calculated values of the thermal conductivity of nanostructured silicon formed the basis for modelling the effective values of the PSi structure, which turned out to be close in magnitude to the experimentally obtained values within the error. However, in the case of modelling a "PSi/IL" composite system, its thermal conductivity depends on thermal contact resistance between solid/fluid interfaces.

In order to match the effective thermal conductivity of the composite with the experimental results, a liquid structuration effect close to the following interface was added in model calculations. As a fitting parameter, we vary the thermal conductivity value of ~1.5 nm thin boundary layer between Si and liquid, where the presence of the surface adsorbed layer of IL with higher density was predicted^{44,45}.

In framework of this model, the FEM simulation gives good agreement with experimental data for a thermal conductivity of the boundary layer in the range (0.5–1.5) W/(m K) and considering a perfect contact between PSi crystallites and IL with thermal contact resistance $R = (1-3) \text{ m}^2 \text{ K/W}$.

Conclusions

This paper investigates the thermal transport properties of the ILs based nanocomposites. In our study, two imidazolium and one ammonium ILs were chosen to combine with the mesoporous silicon fabricated by electrochemical etching of crystalline silicon substrate.

Firstly, we characterised the pristine ILs using differential scanning calorimetry, densimetry and photoacoustic approach with piezoelectric configuration. In such a way, the liquids' density, heat capacity and thermal conductivity were evaluated.

Then, the gas-microphone photoacoustic method was applied to measure the thermal transport properties of PSi/ILs nanocomposite systems. As the main results, the significant enhancement of thermal conductivity of the composite system compared to the pristine matrix and ILs was stated. The structuration of the liquid layer close to the interface of the PSi in composite systems is the most probable reason for this effect. Such structuration leads to modification of thermal transport of the ILs, precisely due to increasing thermal transport along the solid/liquid interface. More specifically, the thermal conductivity of PSi/ILs was $\sim 8-10$ times higher than bulk ILs and ~ 2.5 times higher compared to PS. Comparing the experimental data and the FEM simulations allow us to estimate the thermal conductance of the structured layer, which corresponds to lower limit of the known literature data regarding simulated interfacial boundary resistance between the ILs and solids. Thus, the results presented in the paper can be used to improve the thermal transport properties of the ILs-based nanocomposite system in various applications connected with energy production, storage, and conversion.

Data availability

The datasets used and/or analysed during the current study are available from the corresponding author upon reasonable request.

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Author contributions

M.I. and D.L. implemented supervision and project administration. P.L., L.C., and M.B. conducted main experiments. S.R. produced ionic liquids and summarized its structure. P.L., L.C. and M.B. produced porous silicon and corresponding composite systems. P.L., M.I., and D.L. made the simulations. P.L., A.V., and M.I. wrote the paper. All the authors contributed by editing the manuscript.

Competing interests

The authors declare no competing interests.

Additional information

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