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Using thermodynamical modelisation to predict the evolution of Co-base superalloys' microstructures at high temperature P. BERTHOD, S. MICHON, L. ARANDA, S. MATHIEU, J.C. GACHON



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# **INTRODUCTION**

High temperature properties of superalloys more depends on their chemical composition. It's especially true for cast cobalt-based alloys: several characteristics of the interdendritic carbides network govern their mechanical resistance. Quantities, morphologies and natures of carbides do not remain like they were just after solidification or heat treatment when exposed to high temperature for a long time. Indeed, they are evolving to reach the thermodynamically stable state corresponding to the considered temperature. Thermodynamical calculations are very useful to know the final microstructure the alloys are converging to, or to target the chemical compositions leading to thermodynamically-stable microstructures suitable to the wanted properties.

The agreement between predicted stable metallurgical states and real microstructures was assessed. For this purpose, the natures and quantities of the different phases of several selected alloys held few hours at high temperatures were compared to those calculated by Thermo-Calc.

# CHARACTERISTICS OF THE STUDIED ALLOYS

Five different alloys were prepared by high frequency induction melting in a cold crucible and under argon gas, then heat treated in two stages :

- homogenized 2h at 1200°C,
- aged 10h at 1000°C, and air quenched.

Their compositions were chosen in order to represent a large panel of cobalt-base superalloys strengthened by carbides. Nickel and chromium contents are equals for all the alloys, but different carbon and tantalum contents were selected.



Chemical Composition (weight percent)	Со	N i	Cr	С	W	Та
Alloy 1	bal.	8.6	28	0.22	5.8	3.0
Alloy 2	bal.	8.7	28	0.37	1	5.8
Alloy 3	bal.	8.9	29	0.49	1	8.5
Alloy 4	bal.	8.5	29	0.38	5.8	3.0
Alloy 5	bal.	8.9	29	0.98	1	5.8





The obtained microstructures exhibit different carbides types and densities. Tantalum carbides (TaC), and/or chromium carbides such as  $Cr_7C_3$  or  $(Cr,W)_{23}C_6$ , are present at grain boundaries. Their density is governed by the carbon content.

### **COMPARISON CALCULATIONS <-> EXPERIENCES**

Groupe sfim Fig. :	Experiment : BCo84	A	tm.: Ar	Crucible: AI2O3 10

1000°C. which Except corresponds to the ageing treatment applied initially, all the alloys were exposed during 5 hours to high temperature, then air quenched. It ov 1 after 10 hours at 1000°C Alloy 1 after 5 hours at 1100°C that the higher the appears temperature, the lower the area fraction of each type of carbides. Moreover, for Alloy 5, a change of the nature of chromium carbides 5 hours at 1200°C takes place at 1100°C and above. Thermo-Calc calculations were made for all the alloys and three different temperatures. Usually, the mass fraction (or volumic fraction obtained with the following formula) of each type of carbide decreased with temperature, as it can also be seen on alloys.  $f_m(\phi_j)$ 







Alloy 2 Alloy 3 Alloy 4 Alloy 5 **T**<sub>solidus</sub> 1284°C 1288°C 1281°C 1288°C from DTA Heating **T**<sub>solidus</sub> 1270°C 1249°C 1250°C 1263°C from DTA Cooling T<sub>solidus</sub> 1277°C 1277°C 1253°C 1287°C from TC calculation

Experimental results consisted first in a determination of solidus temperatures by Differential Thermal Analysis (DTA), then compared to those issued from Thermo-Calc N version using a completed SSOL database. The calculated solidus values are all located in the interval:  $[T_h, T_c]$  where  $T_h$  is the temperature obtained during heating and T<sub>c</sub> during cooling].

For the comparisons with the microstructural Thermo-Calc predictions, the alloys were exposed in a muffle furnace at several high temperatures, then quenched by air cooling. Different heat treatment durations were applied to the alloys to be closed to the stable microstructural state: five hours appeared sufficient.

	In the state of the		a factor		a hada		a hada		a landal		a landes	$f_{vol}(\phi_i)$	$=$ $ \phi_j$	— with	$\rho_{T_{2}C} = 14.5$
	carbides'	Alle	oy 1	Alle	oy 2	All	oy 3	Alloy 4 Alloy 5		Vor <+ j>	$\sum (\underline{\mathbf{f}_{m}}(\boldsymbol{\varphi}))$	$(\underline{p_i})$	, rae		
	area fractions	exp. (% <sub>surf</sub> )	calc. (% <sub>vol</sub> )	exp. (% <sub>surf</sub> )	calc. (% <sub>vol</sub> )	exp. (% <sub>surf</sub> )	calc. (% <sub>vol</sub> )	exp. (% <sub>surf</sub> )	<b>calc.</b> (% <sub>vol</sub> )	exp. (% <sub>surf</sub> )	calc. (% <sub>vol</sub> )		$\sum_{i} \rho_{\varphi_i}$	,	
New Y	1200°C	22	1 4 9	54	314	75	4 6 5	29	1 4 9	49	3 31	$\rho_{M7C3} =$	= 6.94 and	$\rho_{M23C6} =$	6.95 g/cr
	M <sub>7</sub> C <sub>3</sub>	2.2	/	/	/	/.5	1.05	?	/	5.8	7.95			- 11 25 0 0	the second
	M <sub>23</sub> C <sub>6</sub>	1	0.03	1	1	1	1	?	3.72	1	1	<b>A</b> 1 1			and the
	1100°C											Calcul	lations a	lso sho	wed the
	MC	1.9	1.54	7.1	3.35	10	4.81	2.4	1.54	5.2	3.40	M.C	->M_C	change	in Alloy
N.	$M_7C_3$							?	/	5.3	8.33	1123 6	-117C3	enange	
			0.07						4.37			5, and	revealed	l the pre	sence of
	MC	2.4	1.59	4.8	3.47	8.9	4.92	2.5	1.58	5.6	3.43	rare c	hromium	carbide	s which
	M <sub>7</sub> C <sub>3</sub>	/	/	/	1	/	1	?	/	/	1	iaic c	111 Onnum	carolac	
N.	M <sub>23</sub> C <sub>6</sub>	/	1.01	/	0.10	/	- 1 -	?	4.70	5.3	13.6	were n	not observ	red in the	e alloys.
'	The cal	culat	ted	vo	lume										
	fractions	' V8	lues	do	not	-									
	correspo	nd to	o the	e sui	rface		f <sub>su</sub>	rf Φi		Allov	1	Allov 2	Allov 3	Allov 4	Alloy 5
fractions ones but it can						$\frac{f_{\text{vol}} \phi_i}{f_{\text{vol}} \phi_i}$					11110 y -	intog e	11105	into y c	
	inactions				· Can	1	200°C	Μ	С	1.48		1.72	1.61	1.95	1.48
be explained by a relation					M <sub>7</sub> C <sub>3</sub>								0.73		
	that seer	ns e	xist	bety	ween	1	100°C	M	C	1.23		2.12	2.08	1.56	1.53
-	the tru	10	σο	mot	rical			$M_7$	C <sub>3</sub>						0.64
	the tw	/0	gei	JIIC	inca	1	000°C	M	C	1.51		1.38	1.81	1.58	1.63
-	fractions	:						<b>M</b> <sub>23</sub>	C <sub>6</sub>						0.39
	%v0	= lc	1.65	%s	urf										
-	for the T	C a	orhi	dec				S. H.L.							
3	tor the I	al c	ardio	ues											

Alloys followed different evolutions. For example, at 1300°C, Alloy 1 lost all its MC carbides. At the opposite, MC network remained stationary for the Alloy 3.



Alloy 3 reaching 1300°C after 20 hours at 1300°C

Surprisingly no beginning of fusion was evidenced at this temperature, despite of the measured or calculated solidus value.

carbides' area fractions	Alloy 1	Alloy 2	Alloy 3
reaching 1300°C	0.8% MC	4.0% MC	7.6% MC
5 hours at 1300°C	0.1% MC	4.0% MC	6.7% MC
20 hours at 1300°C	/	3.9% MC	6.9% MC

## ONCLUSION

Good fits were found for five different cobalt-based alloys, especially for the solidus temperatures. Concerning the nature of the phases, the expected carbide types were observed. Moreover, thermodynamical modelisation revealed for some compositions the presence of small quantities of others carbides not evidenced in the synthesised alloys. The rarefaction of carbides with an increasing exposition temperature is also confirmed by the simulation. Nevertheless values of carbides fractions are not similar, but it can be explained, at least for TaC carbides, by geometrical considerations.