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Article

Degree of Polarization of Cathodoluminescence from a GaAs Facet in the Vicinity of an SiN Stripe

Daniel T. Cassidy^{1,*}, Jean-Pierre Landesman², Merwan Mokhtari³ , Philippe Pagnod-Rossiaux³, Marc Fouchier⁴ and Christian Monachon⁴

¹ Department of Engineering Physics, McMaster University, Hamilton, ON L8S 4L7, Canada

² Institut FOTON-UMR 6082, Université de Rennes, INSA Rennes, CNRS, 35000 Rennes, France

³ 3SP Technologies, Route de Villejust, CEDEX, 91625 Nozay, France

⁴ Attolight AG, 1015 Lausanne, Switzerland

* Correspondence: cassidy@mcmaster.ca

Abstract: Measurements of the cathodoluminescence (CL) and the degree of polarization (DOP) of (CL) from the facet of a GaAs substrate and in the vicinity of a SiN stripe are reported and analyzed. The deformation induced by the SiN stripe is estimated by fitting the measured DOP to 3D finite element method (FEM) simulations. The deformation is found to be more complex than an initial condition of biaxial stress in the SiN. A ratio of fit coefficients suggests that the dependence of DOP on strain is described by equations presented in Appl. Opt. 59, 5506–5520 (2020). These equations give a DOP that is either proportional to a weighted difference of the principal components of strain in the measurement plane, or proportional to the shear strain in the measurement plane, depending on the chosen orientation of the measurement axes.

Keywords: degree of polarization (DOP); cathodoluminescence (CL); GaAs; SiN stripe; stress; strain



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1. Introduction

Strong interest exists for the characterization of devices and materials, with new approaches to extract material and device parameters [1]. Our interest lies in estimation of strain in III–V materials and devices by analysis of the degree of polarization (DOP) of luminescence, for which engagement is strong and current [2–10]. The DOP of luminescence from InP and GaAs, and related compounds, is a sensitive function of the strain in these III–V materials [11–13].

In this paper, we analyze cathodoluminescence (CL) [14,15] from the facet of a GaAs substrate and in the vicinity of an SiN stripe, which was deposited on the top surface of the GaAs substrate. Most previous DOP work has analyzed electroluminescence (EL) or photoluminescence (PL).

The ever-increasing level of the device integration of semiconductor materials into complex micrometer-scale structures, for instance, in photonic integrated circuits (PICs) as well as in solid-state lasers, makes the availability of a technique capable of revealing small strains at micrometer scales highly desirable. A DOP measurement based on cathodoluminescence is interesting in this context because CL has a probe diameter that is not determined by optical diffraction, which enables DOP measurements with sub-micrometer spatial resolution.

Ultimately, we fit, using a least squares approach, 3D finite element method (FEM) simulations of the DOP of luminescence of a strained SiN-stripe-on-GaAs system to the measured DOP of the CL. To obtain the parameters needed in the fits of the FEM simulations to the data and to obtain insights into the CL, we investigated aspects of the measured CL in the vicinity of the edge of the sample.

The results from fits of the 3D FEM simulations of the DOP of luminescence to the measured data are consistent with the theoretical work reported in [16]. This theoretical work, which is based on Bahder’s analytic expressions for the strain dependence of the

conduction and valence band dispersions [17,18], gives an expression for the strain dependence of the DOP that is more complicated than the expression that previously was thought to hold [13]. A confirmation of the applicability of [16] for the strain dependence of the DOP of luminescence from GaAs has not, to our knowledge, been reported.

The importance of the work lies in the approach of using fits to luminescence and of using accurate expressions for the strain dependence of the DOP of luminescence to determine parameters that are important for understanding device performance. Strain has long been understood to affect not only the reliability but also the operation of devices [19]. With accurate estimations of strain through fits to DOP measurements, it should be possible to provide input for accurate simulations for device design and for the understanding of operation.

The DOP of luminescence is measured as

$$DOP_{\hat{n}} = \frac{L_{\hat{h}} - L_{\hat{v}}}{L_{\hat{h}} + L_{\hat{v}}} \quad (1)$$

where $L_{\hat{h}}$ and $L_{\hat{v}}$ are the detected luminescences that are emitted along the normal \hat{n} to the surface under study and polarized along two orthogonal directions, \hat{h} and \hat{v} , where h stands for horizontal and v stands for vertical [20]. $L_{\hat{h}} + L_{\hat{v}}$ is the total detected luminescence, i.e., the luminescence yield.

A second independent measurement of the DOP of luminescence, which we call ROP for rotated degree of polarization, is made for \hat{h}' and \hat{v}' rotated by -45 deg about the external normal to the surface \hat{n} . This defines the measured ROP of luminescence as

$$ROP_{\hat{n}} = \frac{L_{\hat{h}'} - L_{\hat{v}'}}{L_{\hat{h}'} + L_{\hat{v}'}} \quad (2)$$

where $L_{\hat{h}'}$ and $L_{\hat{v}'}$ are the detected luminescences that are emitted along the normal \hat{n} to the surface under study and polarized along the \hat{h}' and \hat{v}' directions [11,21,22]. The luminescence yield as determined from $ROP_{\hat{n}}$ or from $DOP_{\hat{n}}$ should be the same.

1.1. DOP as a Function of Strain

The strain dependence of the degree of polarization (DOP) of luminescence from GaAs or InP can be written as a function of the shear deformation potentials b or d if one assumes a value for the ratio d/b , i.e., $d = \zeta b$. To reduce the number of variables in the equations that follow, numerical values are substituted for the remaining physical constants that describe the band structure [23] and for the three independent elastic stiffness constants ([24], Chapter VIII) of the GaAs substrate.

For the luminescence from the normal to a GaAs {110} facet and assuming that $d = \zeta b$, the predicted relationships between the degree of polarization (DOP), the rotated degree of polarization (ROP), and strain ([16], Section 3.D.4) are

$$DOP_{110} = -|K_e| \left(0.3659 (\zeta + 1.0218) e_1 + 0.1140 (\zeta - 9.5356) e_3 \right) \quad (3)$$

and

$$ROP_{110} = |K_e| 0.5867 \zeta (2 e_5) \quad (4)$$

with the calibration constant $K_e = -3b/(4k_B T)$ ([16], Equation (26)), ([25], Equation (16)), where k_B is the Boltzman constant and T is the absolute temperature, and where the normal \hat{n} to the facet is a $\langle 110 \rangle$ direction, \hat{h} and e_1 are in the plane of the facet and along a $\langle 1\bar{1}0 \rangle$ direction, and \hat{v} and e_3 are in the growth or $\langle 001 \rangle$ direction. e_5 is a tensor shear strain in the plane of the facet. Note that a Voigt notation is used to reduce the number of subscripts: $e_1 = e_{11}$, $e_3 = e_{33}$, and $e_5 = e_{13}$ in terms of components of the strain tensor.

Equations (3) and (4) give the dependence of the degree of the polarization of luminescence on strain as a function of the deformation potential b (K_e is a linear function of b) and the ratio $\zeta = d/b$ of the deformation potentials. The deformation potentials are experimentally determined parameters, are different for GaAs and InP, and have uncertainties associated with them [23]. These two equations give the strain dependence in a somewhat

general form. Expressed in this form, one can see that DOP_{110} depends on a weighted difference of the principal components of strain in the horizontal and vertical directions and that ROP_{110} depends on the shear strain, regardless of the value of ζ .

For luminescence from the normal to a GaAs {110} facet and assuming the recommended relationship of $d = 2.4b$ ([23], Table I, p. 5825), the predicted relationships between the degree of polarization (DOP), the rotated degree of polarization (ROP), and strain ([16], Section 3.D.4), are

$$DOP_{110} = -|K_e| (1.252 e_1 - 0.8132 e_3) \quad (5)$$

and

$$ROP_{110} = |K_e| 1.408 (2 e_5). \quad (6)$$

Under the simplifying assumption that the material is isotropic, then ([16], Section 4.A.1)

$$DOP_{110} = -|K_e| (e_1 - e_3) \quad (7)$$

and

$$ROP_{110} = |K_e| (2 e_5). \quad (8)$$

These expressions permit estimation of the DOP and ROP for a given strain field. These expressions also provide a route to estimate the strain field by fitting DOP and ROP values obtained through the FEM simulations of strain fields to measured degree of polarization data.

In this paper, 3D finite element method (FEM) simulations [26] were fit, using a least squares approach, to measurements of the degree of polarization of cathodoluminescence from a cleaved {110} facet of a GaAs substrate in the vicinity of an SiN stripe.

The constants 1.252, 0.8132, and 1.408 of Equations (5) and (6) were included in the 3D FEM simulations. Thus, the ratio of the ROP_{110} to DOP_{110} fit coefficients should equal unity if Equations (3) and (4) are accurate descriptions of the dependence of the DOP and ROP on strain and if $d = 2.4b$.

1.2. Least Squares Fits

Least squares fits to the measured DOP data $Y_{DOP}(h, v)$ and ROP data $Y_{ROP}(h, v)$ were obtained by minimizing reduced chi-square with respect to fitting parameters $\{a_i, b_i\}$. Note that a subscripted b, b_i , indicates a fitting parameter and should not be confused with the deformation potential b , which is not subscripted. The meaning of the variable should be clear from context and by the presence of the subscript.

Three-dimensional FEM simulations for the strain field in the vicinity of a SiN stripe on a GaAs substrate were performed to obtain N_s 'basis functions' $f_i^{(DOP)}(h, v)$ and $f_i^{(ROP)}(h, v)$ using Equations (5) and (6). These N_s basis functions are the DOP and ROP fields obtained from the 3D FEM simulations for the given initial conditions in the SiN stripe or GaAs substrate. The initial conditions are estimates of the state of stress or strain in the materials prior to the attachment of the SiN to the GaAs substrate. The (final) state of stress or strain in the SiN and GaAs is determined with the FEM solver. If the least squares fit of a basis function to the measured data was perfect, then we would conclude that the stress or strain in the SiN was the initial condition that led to the perfectly fitting basis function.

Reduced chi-squares for DOP and ROP fits were defined as

$$\chi_{DOP}^2 = \sum_{h,v} \left(Y_{DOP}(h, v) - \sum_{i=1}^{N_s} a_i f_i^{(DOP)}(h, v) - \sum_{i=N_s+1}^{N_f} a_i f_i(h, v) \right)^2 / (\sigma^2 \nu_{DOP}) \quad (9)$$

and

$$\chi_{ROP}^2 = \sum_{h,v} \left(Y_{ROP}(h, v) - \sum_{i=1}^{N_s} b_i f_i^{(ROP)}(h, v) - \sum_{i=N_s+1}^{N_f} b_i f_i(h, v) \right)^2 / (\sigma^2 \nu_{ROP}) \quad (10)$$

where h and v are the parameters that give the horizontal and vertical position of the measurement, σ is the rms noise for each data point, ν_{DOP} and ν_{ROP} are the number of degrees of freedom for χ_{DOP} and χ_{ROP} , N_f is the number of fit parameters, and $f_i(h, v)$ are polynomials in h and v that describe the background, which is composed of the offsets, birefringence, and polarization dependence of the optics, and other unavoidable artifacts that are not in the FEM simulations.

The background basis functions were taken as

$$\begin{aligned} f_{N_s+1}(h, v) &= 1 & f_{N_s+2}(h, v) &= v & f_{N_s+3}(h, v) &= h \\ f_{N_s+4}(h, v) &= (v - \bar{v})^2 & f_{N_s+5}(h, v) &= (h - \bar{h})^2 & f_{N_s+6}(h, v) &= (v - \bar{v})(h - \bar{h}) \end{aligned} \quad (11)$$

with \bar{v} equal to the average value of v and \bar{h} equal to the average value of h .

A total reduced chi-square, χ_T , was defined as

$$\chi_T^2 = \frac{\nu_{DOP} \chi_{DOP}^2 + \nu_{ROP} \chi_{ROP}^2}{\nu_{DOP} + \nu_{ROP}} \quad (12)$$

and it was χ_T that was minimized with respect to the fit parameters $\{a_i, b_i\}$, subject to the constraint that $b_i = R_a \times a_i$, for $i \leq N_s$ where R_a was set to a number and was not minimized in the least squares fitting procedure.

If Equations (5) and (6) are correct, and if $d/b = 2.4$, then $R_a = 1$. If $R_a \neq 1$, then either the equations are incorrect, or $d/b \neq 2.4$, or both. The inclusion of R_a as a constraint expresses the fact that DOP_{110} and ROP_{110} should scale together. If the influence that causes the strain distribution is increased by a factor of, e.g., ten, then DOP_{110} and ROP_{110} should scale by the same factor and the ratio b_i/a_i should equal R_a , for $i \leq N_s$.

2. Sample and SEM Measurements

2.1. SiN Stripes on GaAs

Compressive, 290 nm-thick SiN layers were deposited on (100) GaAs substrates by a standard PECVD technique, using SiH_4 , N_2 , and He as precursors. After deposition, a stress of -220 MPa was measured at the wafer level through the measurement of the wafer bow. Wafers were then processed with standard UV contact lithography to define the stripes of various widths and groupings by the reactive ion etching of the SiN layers and the removal of the photoresist. Bars of 3 mm width in the \hat{n} direction and of 368 μm thickness in the \hat{v} direction were cleaved for scanning electron microscope (SEM) and CL analysis. The backside of the wafer was not polished.

2.2. SEM Data

CL experiments were conducted at room temperature on an Attolight Allalin spectroscopy platform with a beam current in the 10–15 nA range [27]. During the measurements, a focused electron beam scans the sample while the optical emission is collected and detected by an Si detector, enabling the simultaneous acquisition of secondary electron (SE) and CL intensity images. The e-beam energy was 5 keV, leading to a penetration depth of primary electrons in GaAs of approximately 150 nm. It was found that 5 keV was a good compromise between signal intensity (to improve the signal to noise ratio, which is especially important as DOP is a differential ratiometric technique, and is therefore especially prone to noise), and spatial resolution, as a higher accelerating voltage would result in a larger interaction depth as well as a lower resolution.

The degree of polarization data was obtained by adding a wire grid polarizer before the Si detector as in Ref. [15] but mounted on a motorized holder. Images with the polarizer oriented in the vertical \hat{v} and horizontal \hat{h} directions were acquired sequentially to calculate the DOP. Afterwards, images were acquired with the polarizer rotated by ± 45 deg from \hat{h} to obtain the ROP data. The number of pixels per image was set to 1024×1024 and the integration time per pixel to 10 μs , leading to a time per image of approximately 11 s.

Figure 1 is a schematic diagram of the measurement system and Figure 2 displays a cropped SEM image of a cleaved facet in the vicinity of an SiN stripe.

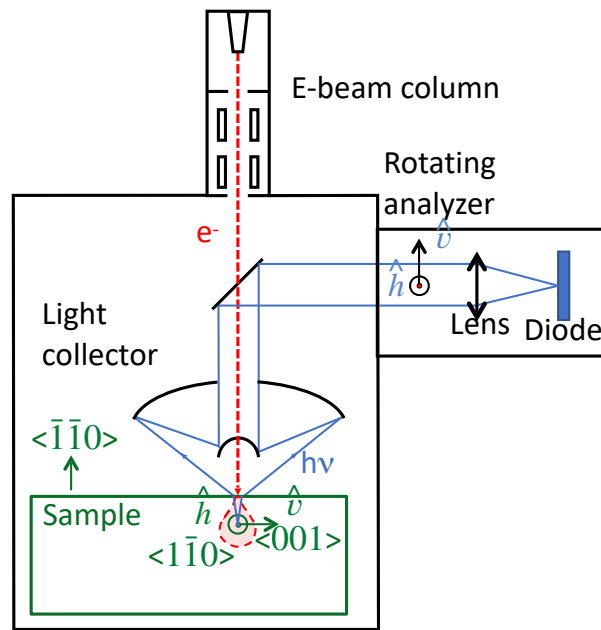


Figure 1. Schematic diagram of the CL measurement system.

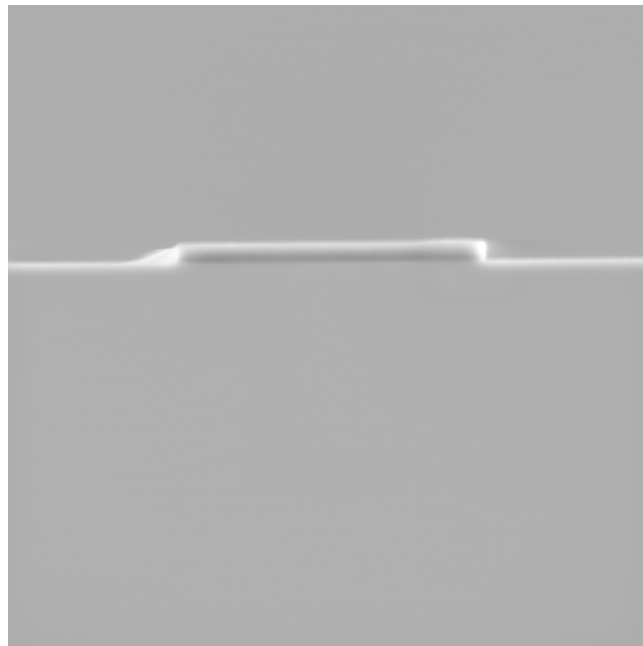


Figure 2. A cropped SEM photo of the SiN stripe and GaAs facet. The SiN is on top of the GaAs.

Panels (a), (b), and (c) of Figure 3 display the measured CL yield, DOP, and ROP using a false color mapping, respectively. The DOP and ROP displays were thresholded at 4% of the maximum value of the CL yield, i.e., at $0.04 \times CL_{\max}$. This value corresponds to $\approx 5 \times$ the rms value of the bottom fifty rows of the CL yield. Areas for the DOP and ROP that were calculated for the CL yield < 0.04 of the maximum value of the CL yield are displayed in a magenta color. The low threshold allows the estimation of the location of the top of the substrate.

The color bar, (g) of Figure 3, shows the linear, false color mapping that was used. The top and bottom squares of (g) are colors that were used to display off-scale values. The black/red colors at the bottom of the color bar display smaller values of the signal than the blue/white colors at the top of the scale. For signed signals such as the DOP and

ROP, a green color at the mid-point of the color bar represents zero. If g is the display gain, then the just off-scale colors represent a DOP or a ROP value of $\pm 29.16/g\%$ relative to the midpoint of the color bar. For the data presented in the figures, the DOP display gain $g = 10$ and the ROP display gain $g = 15$, giving just off-scale values of $\pm 2.92\%$ and $\pm 1.94\%$, relative to the center of the color bar.

Panels (d), (e), and (f) of Figure 3 display the same data as in (a), (b), and (c), but with the DOP and ROP thresholded at 0.6 of the maximum value of the CL yield. This threshold should remove edge effects, i.e., it should remove artifacts in the calculated DOP and ROP for measurements that are of low CL yield and thus dominated by noise, or for measurements that are too close to the edge of the sample and are thus corrupted by polarized reflections, and is the threshold that was used for the least squares fits of 3D FEM simulations to the DOP and ROP data.

Each panel of Figure 3 displays the same area of $5.46 \mu\text{m}$ in the \hat{v} or vertical direction by $8.92 \mu\text{m}$ in the \hat{h} or horizontal direction. Similarly to Figure 2, the SiN stripe is approximately centered left–right and is near the top. In panels (a) and (d) of Figure 3, which display the CL yield, the cleaved facet of the GaAs substrate shows as blue or white. The top edge of the GaAs substrate lies in the black-red-green bands, which indicate the CL yield increasing (note the colors in the color bar, panel (g)) as the GaAs is approached from above, as is shown later in Figure 4. The SiN sits on top of the gray areas in panels (b) and (e) and in between the blue and red lobes of panels (c) and (f). The effects of the SiN stripe on the CL yield, the DOP, and the ROP are readily apparent in the panels of Figure 3 by comparing the colors at the bottom of each panel to the colors near the top of each panel.

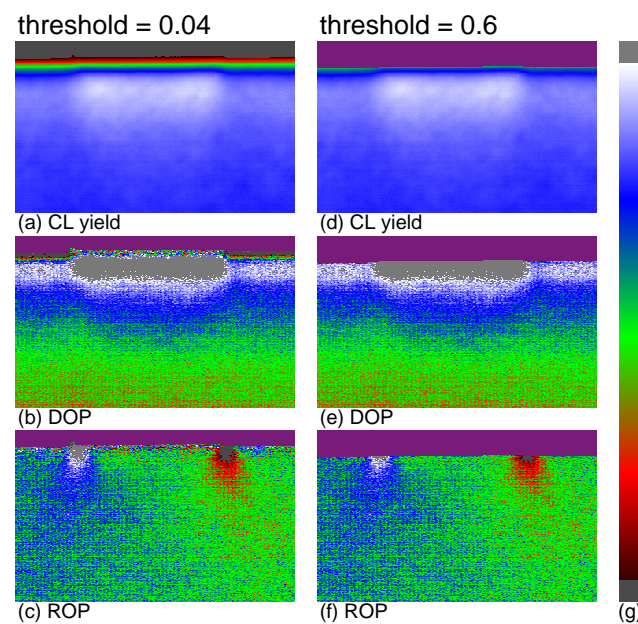


Figure 3. CL yield as calculated from P_1 and P_2 (top panel), DOP (middle panels), and ROP (bottom panels), displayed using a false color mapping. The same DOP and ROP data are displayed in the two columns but for different thresholds of $0.04 \times CL_{\text{max}}$ and $0.6 \times CL_{\text{max}}$. The color bar (g) shows the false color mapping that was used to display the data.

Measurements of the polarized CL were made for four different angles of the polarizers. The polarized CL yield along one axis, P_1 , was made for the polarizer transmission axis along the \hat{h} direction (i.e., the $\langle 1\bar{1}0 \rangle$ direction). P_2 was measured for the transmission axis along the \hat{v} direction (i.e., the $\langle 001 \rangle$ direction). P_3 and P_4 were measured for the polarizer transmission axis at ± 45 deg to the \hat{h} direction.

P_1 , P_2 , P_3 , and P_4 were zero corrected by subtracting the average value of the raw data for 200 full rows of data that were off the sample. These rows are not visible in Figure 2 as these rows were at the top of the file (rows 824–1023) and are not displayed.

With these definitions, using the zero-corrected versions, and using the supplied constants as determined from an unstrained sample,

$$CL_{DOP} = P_1 + 0.94328 P_2 \quad (13)$$

$$DOP = \frac{P_1 - 0.94328 P_2}{CL_{DOP}} \quad (14)$$

and

$$CL_{ROP} = P_3 + 1.00385 P_4 \quad (15)$$

$$ROP = \frac{P_3 - 1.00385 P_4}{CL_{ROP}}. \quad (16)$$

Equation (14) is the defining equation for the experimentally determined DOP, Equation (7), with $L_{\hat{h}} = P_1$ and $L_{\hat{\theta}} = 0.94328 P_2$. Equation (16) is the defining equation for the experimentally determined ROP, Equation (8), with $L_{\hat{h}'} = P_3$ and $L_{\hat{\theta}'} = 1.00385 P_4$.

The constants 0.94328 and 1.00385 account for the polarization-dependent transmission of the measurement system.

The identification of Equations (13) and (15) as the CL yields follows from the measurements of the CL at two orthogonal directions, as pointed out below the defining equations for the experimentally measured DOP and ROP, Equations (7) and (8). CL_{DOP} should equal, within experimental uncertainty, CL_{ROP} .

The field of view was specified as 8.949 μm , with 1024×1024 equally spaced measurements on a horizontal–vertical grid. This gives $x_{step} = y_{step} = 8.949 \times 10^3 / 1023 = 8.748 \text{ nm}$ where the step sizes are the distances between measurements in the horizontal (\hat{h}) or vertical ($\hat{\theta}$) directions.

To reduce the size of the files, the cropped P_1 , P_2 , P_3 , and P_4 files were averaged over a rectangle with height of 3 (raw) data points in the vertical direction and a width of 5 (raw) data points in the horizontal direction. This reduced the files sizes to 204 points in the horizontal direction and 208 points in the vertical direction. This gives an $h_{step} = 5 \times x_{step} = 0.04374 \mu\text{m}$ and a $v_{step} = 3 \times y_{step} = 0.02624 \mu\text{m}$. Note the use of h_{step} and v_{step} to distinguish from x_{step} and y_{step} .

3. Fits to the CL Yield

The CL yields (CL_{DOP} and CL_{ROP}) were analyzed to provide values needed in the least squares fitting of FEM simulations of the SiN stripes on GaAs to the measured degree of polarization data.

Complementary error functions as functions of vertical distance v and for a chosen h ,

$$\frac{A}{2} \operatorname{erfc}\left(\frac{v_e - v}{\sigma_v \sqrt{2}}\right), \quad (17)$$

were fit to the CL yields to determine the best-fit estimates of the locations of the top edges of the samples, v_e , and the full-width half-maximum (FWHM) resolutions. For a Gaussian function with scale parameter (i.e., standard deviation) σ_v , the $\text{FWHM} = 2.35482 \sigma_v$. The parameter A gives the best-fit value of the CL yield for the substrate away from the top edge of the sample. h specifies which column of vertical data is fit to the complementary error function. $h \times h_{step}$ is the horizontal distance from the left-hand edge of the full measurement area.

The complementary error function in Equation (17) is proportional to the area of a Gaussian function over the interval $(v_e - v, \infty]$ and is a function of $v_e - v$ where v_e is a number and gives the location in the vertical direction of the top edge of the sample. If the electron beam of the SEM is Gaussian in the cross-section and if the CL yield is proportional to the fraction of the electron beam that is on-the-sample, then Equation (17) should provide an accurate description of the CL yield.

Equation (17) is particularly useful near the edge of the sample, in cases for which the electron beam is not fully on-the-sample and not fully off-the-sample, i.e., when $v \approx v_e$. For the electron beam fully off-the-sample, $v = -\infty$, $\operatorname{erfc}(\infty) = 0$ and there is no CL yield.

For $v = v_e$, the electron beam is half on the sample, $\text{erfc}(0) = 1$, and the CL yield is $A/2$, which is half the maximum value. If the electron beam is fully on the sample, $v = +\infty$, $\text{erfc}(-\infty) = 2$, and the CL yield is a maximum and equals A .

Table 1 lists values found from fits of a vertical column of CL yield data to Equation (17). $h \times h_{step}$ specifies the vertical column by the distance from the left hand edge. The value of χ is the rms value of the residue, where the residue is the difference between the data points and the best fit curve. A is the best fit CL yield far from the location of the top edge v_e of the sample. The $\text{FWHM} = 2.35482 \sigma_v$ is a measure of the diameter of the CL probe and shows that sub-micrometer resolution is achieved with the CL measurement system.

Table 1. Fit parameters for fits of Equation (17) to the CL yields, CL_{DOP} and CL_{ROP} , for vertical planes specified by h . The SiN stripe is in the interval $57 \leq h \leq 156$.

File	h	χ	A	v_e	v_e (nm)	σ_v (nm)	FWHM (nm)
CL_{DOP}	18	464	20,817.0	28.45	747	201	473
CL_{DOP}	98	630	19,465.2	29.87	785	203	477
CL_{DOP}	102	630	19,463.4	29.76	782	203	478
CL_{DOP}	106	673	19,452.2	28.46	748	205	482
CL_{DOP}	190	480	20,990.3	29.18	766	204	480
CL_{ROP}	18	464	21,549.1	26.87	705	204	481
CL_{ROP}	98	664	20,073.7	28.24	740	203	479
CL_{ROP}	102	659	20,087.5	28.13	737	203	478
CL_{ROP}	106	705	20,268.2	26.92	706	207	487
CL_{ROP}	192	461	21,603.6	27.70	727	206	486

Figure 4a shows a fit of Equation (17) to the CL yields for $h = 102$, where h is a horizontal distance and has units of h_{step} . The top left edge of the sample occurs at the ordered pair $(h = 1, v_e)$, the top right edge occurs at $(h = 204, v_e)$, and the middle of the SiN stripe is roughly $(h = 102, v_e)$.

Note that the horizontal axis of Figure 4 gives the distance in units of v_{step} from the top of the file and along the line $h = 102$. The point with vertical index = 20 is 20 rows below the top row of the CL data file, i.e., $20 \times v_{step} = 0.5258 \mu\text{m}$ below the top of the file.

Figure 4b displays a fit of Equation (17) to the CL yields for $h = 18$, a region that is well away from the SiN stripe. By the comparison of Figure 4a to b, one can see that the fits differ for values near the vertical index equals 20 and 40. The vertical index = 40 is $40 \times v_{step}$ below the top of the data file and is close to the beam being fully on the GaAs substrate. The values for the vertical index near 20 are for the beam mostly off the sample. The near-zero values for the CL yield for the vertical index $\lesssim 20$ in Figure 4a suggest that the SiN might be blocking the tail of the beam. For Figure 4b, which is a region away from the SiN stripe, the CL yield rises smoothly from zero.

The rms of the residue for fits of CL_{DOP} to an error function, χ in Table 1, rises sharply at $h = 61$ and falls sharply at $h = 152$, and remains above 600 in this interval between $h = 61$ and $h = 152$. This is the region of the SiN stripe: $(152 - 61) \times h_{step} = 4 \mu\text{m}$, which is the nominal width of the SiN stripe. In the region of the stripe, χ has a mean value of 628 ± 6 and a sample standard deviation of 27. Outside of the SiN stripe, $\chi < 500$, with a mean value of 439 ± 6 and a sample standard deviation of 25. The quality of a fit of an error function to CL_{DOP} is different depending on whether the fit is for a value of h that is inside or outside of the SiN stripe. Clearly the SiN stripe influences the CL yield.

The fits of error functions to the CL data are not particularly good. It is possible that band bending at the surface of the substrate leads to a reduction in the CL yield near the top surface, and that this reduction in CL yield is not well described by an error function. Nevertheless, one can glean some useful information from the plots and the fits.

Observe from panels (a) or (d) of Figure 3 that the CL yield is different under the SiN as compared to the regions away from (i.e., to the left and right of) the SiN stripe. These data also suggest that the SiN plays a role in the CL yield.

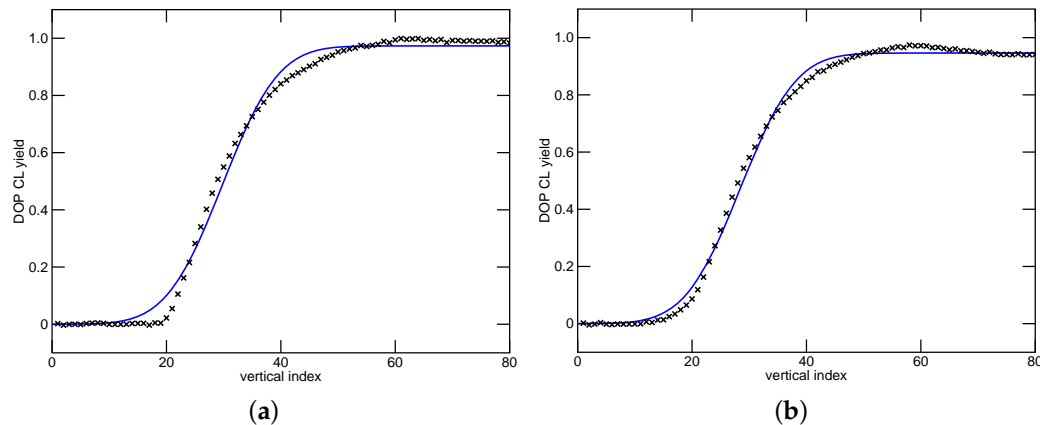


Figure 4. Fits of complementary error functions to the CL_{DOP} data as a function of v for: (a) near the mid-point of the SiN stripe, $h = 102$; and (b), far from the SiN stripe, $h = 18$.

Registrations of the DOP and ROP images are, not surprisingly, slightly different.

Figure 5 shows a portion of Figure 4 on an expanded scale and with both DOP and ROP data. The expanded scale shows a mis-registration of several v_{step} in the vertical direction; the red data rise sharply for smaller values of the vertical index, than the blue data rise for. The mean mis-registration, as calculated over all 204 columns of CL data, was $1.51 v_{step}$ with a standard error of the mean of $0.006 v_{step}$.

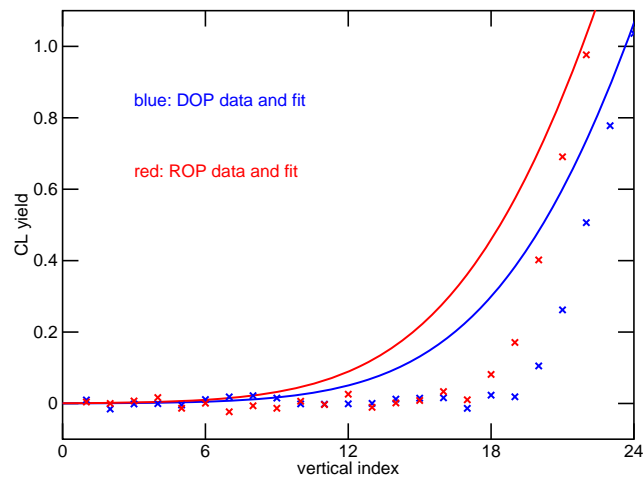


Figure 5. Fits of complementary error functions to the CL_{DOP} and CL_{ROP} data as a function of v near the mid-point of the stripe, i.e., at $h = 102$, and on an expanded scale.

Table 1 shows a similar value for the vertical mis-registration. The table shows the fit parameters for different horizontal locations, h , for the CL yields as determined from the ROP and DOP. Note that the difference in the values of v_e for the DOP and ROP at the same values of h are approximately 1.5, in units of the v_{step} . The values of v_e occur at roughly $A/2$.

In the horizontal direction, the mis-registration is, from best fits, of the order $2 \times h_{step}$.

4. Fits of FEM Simulations to the DOP and ROP Data

The width of the SiN stripe was taken to be $4.35 \mu\text{m}$. This value was obtained by comparison of the ROP from 3D FEM simulations [26] of various widths with the ROP data. The horizontal centroids of the ROP lobes near the edges of the SiN were calculated as

$$h_c = \frac{\sum_{i=h_c-12}^{h_c+12} \sum_{j=168}^{175} h_i \text{ROP}(h_i, v_j)}{\sum_{i=h_c-12}^{h_c+12} \sum_{j=168}^{175} \text{ROP}(h_i, v_j)} \quad (18)$$

for both data and simulations, with $\text{ROP}(h, v) = Y^{\text{ROP}}(h, v)$ for calculation of the centroid of the data, and $\text{ROP}(h, v) = \sum_{i=1}^{N_s} b_i f_i^{\text{ROP}}(h, v) + \sum_{i=N_s+1}^{N_s+6} b_i f_i(h, v)$ for the calculation of the centroid of the best fit FEM simulation. The ROP lobes are readily apparent in the bottom panels of Figure 3.

The width as determined from the centroids of the ROP data was 4.75 μm . Three-dimensional FEM simulations for an SiN stripe width of 4.35 μm gave the same distance between the centroids of the simulated ROP lobes as for the data. It is clear, from Figure 3 and from the calculation of the centroids, that the ROP lobes lie slightly to the left and to the right of the edges of SiN stripe.

The rms noise for CL_{DOP} and CL_{ROP} measurements was $\approx 6 \times$ greater than a low-noise measurement of the DOP (or ROP) of PL using the equipment and technique described in [13]. The noise sources of the PL measurement system [13] were studied in detail and reported in [28]. The rms noise was 3.1×10^{-3} for the DOP of CL and 3.0×10^{-3} for the ROP of CL, as opposed to 5×10^{-4} for the DOP or ROP from the PL measurement system. The CL noise values were calculated from the averaged data. Assuming white noise, the noise for the raw CL data should be $\sqrt{15} = 3.873$ times larger than for the averaged CL data.

The 3D FEM simulations were interpolated on the same $h_{\text{step}} \times v_{\text{step}}$ rectangular grid as the DOP and ROP data, and were then convolved with a unit-area Gaussian function

$$G(h_i, v_j) = Z^{-1} \exp\left(-\left(\frac{h_i^2}{2s_h^2} + \frac{v_j^2}{2s_v^2}\right)\right) \quad (19)$$

to mimic the effects of the finite SEM beam width and the averaging of the data that was performed to reduce the file size. In the equation for the unit-area Gaussian response function, Z is the sum of $G(h_i, v_j)$ on the $h_{\text{step}} \times v_{\text{step}}$ grid and over the assumed extent of the function (21×33 points), and $s_h = 209.3$ nm and $s_v = 201.1$ nm are scale factors as determined by fits of a Gaussian to the sum of the Gaussians, with scale parameters of 200 nm, in the averaging process that was used to reduce the file size.

4.1. Some Details on the FEM Simulations

The SiN stripe was taken to be 4.35 μm -wide (in the \hat{h} direction), 286 nm-thick ($=2 \mu\text{m}/7$, in the \hat{v} direction), and to exist from front to back (along the \hat{n} direction) of the GaAs substrate. Coordinate scaling in the \hat{v} direction, with a scale factor of 7, was used to permit efficient meshing of the SiN–GaAs structure [29].

The elastic constants for the SiN were taken to be $E_{\text{SiN}} = 270$ GPa and $\nu_{\text{SiN}} = 0.30$. The value for E_{SiN} is consistent with E_{SiN} found for similarly prepared films [6] and a shallow but smooth minimum in plots of χ_T versus E_{SiN} was found at 270 GPa. No well was found for the plots of χ_T versus ν_{SiN} . The quality of the fits as visually determined did not seem to depend on the values that were used.

The three non-zero components of the stiffness matrix for a cubic crystal (p. 140, [24]) were taken to be $c_{11} = 118$ GPa, $c_{12} = 53.5$ GPa, and $c_{44} = 59$ GPa for GaAs [30]. The stiffness matrix was converted into a tensor and this tensor was rotated by 45 deg about \hat{v} and then converted back to matrix form ([24], Chapter VIII) to find the stiffness matrix for GaAs in the plane of a $\{110\}$ facet. These values for the stiffness constants ([31], Table 3.4), which were found by the rotation of the stiffness tensor, were used in the 3D FEM simulations.

Symmetric boundary conditions and coordinate scaling were used to create a rectangular parallelepiped of GaAs that was 200 μm -wide (in the \hat{h} direction) by 368 μm -thick (in the \hat{v} direction by 150 μm -deep (in the \hat{n} direction) from a 100 μm -wide by 100 μm -thick by 75 μm -deep piece.

The DOP and ROP patterns were calculated for 23 different basis functions, or initial conditions, as explained in Section 1.2. These basis functions included uniaxial and biaxial

stresses and strains in the SiN, in the areas beside the SiN, polishing stresses and strains, interface stresses, and the curvatures of the substrate. The approach was to simulate multiple influences and to use the results of the least squares fitting of the simulations to the data to determine the dominant explanations for the measured data.

The first basis function, or dominant explanation, was chosen based on expectations and minimization of χ_T . It was expected that the SiN was biaxially strained. To obtain the second dominant explanation, χ_T was calculated for each basis function acting with the first one for a total of two basis functions. The basis function that led to the minimum value of χ_T was selected. The third and fourth basis functions (or dominant explanations) were selected in a similar manner. Note that selection of the second, third, and fourth basis functions was based solely on the reduction in χ_T . There were choices for the second, third, and fourth dominant explanations that were statistically degenerate (i.e., well within one confidence interval) but were not chosen.

The basis functions were not chosen nor made to be orthogonal. Thus, the responses, which were fit to the data, are not expected to be orthogonal. It is expected and observed that there will be correlations between the responses, and that the fit coefficients will change as basis functions are added to the fit ([32], Section 7.3). This makes it difficult to assign a physical interpretation to individual fit coefficients. One needs to interpret the results based on the overall fit.

To ensure that the correlations were not masking the selection of the last three dominant explanations, χ_T was calculated for $C(22,3) = 22!/3!/19! = 1540$ combinations of three basis functions along with the chosen first dominant explanation of biaxial stress in the SiN.

4.2. Fits to the Data

Figure 6 shows the DOP and ROP data, the fits to the data for four basis functions, and $5\times$ the residue, where the residue is defined as the data minus the best fit. The DOP and ROP residues are displayed with gains of $g = 50$ and $g = 75$, respectively.

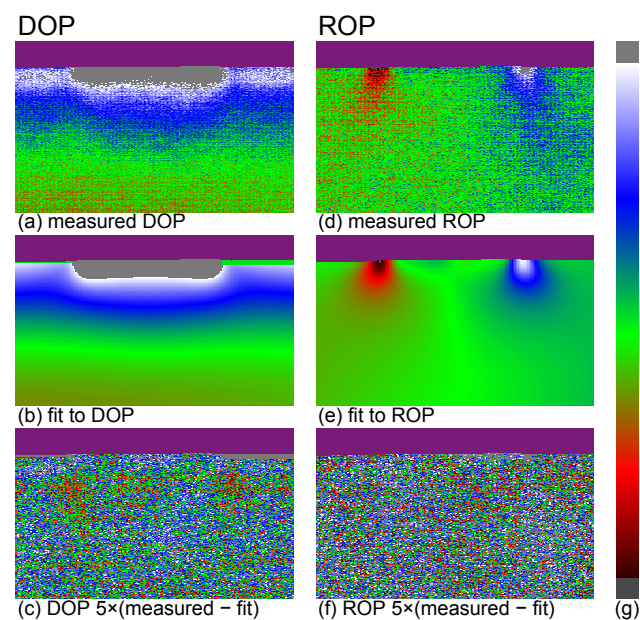


Figure 6. DOP and ROP data, the fits to the data, and $5\times$ the residues. The same area of $208 \times v_{step} = 5.46 \mu\text{m}$ by $204 \times h_{step} = 8.92 \mu\text{m}$ is displayed in each panel. The colour bar (g) shows the false colour mapping that was used to display the data and has the same explanation as the colour bar of Figure 3.

Figure 7 shows the development of the DOP and ROP residues for the addition of a fitting function. The top panels show the residues for the DOP data and the residue for the ROP data, for a fitting function composed of biaxial stress in the SiN stripe plus background

terms. The background terms are polynomials in h and v , as described in Section 1.2, and account for dc offsets in the data and unavoidable artifacts owing to imperfections such as defects, misalignments, birefringence, and polarization-dependent reflections. The just off-scale values for false color images of the DOP and the ROP residues are $\pm 0.6\%$ and $\pm 0.4\%$, respectively.

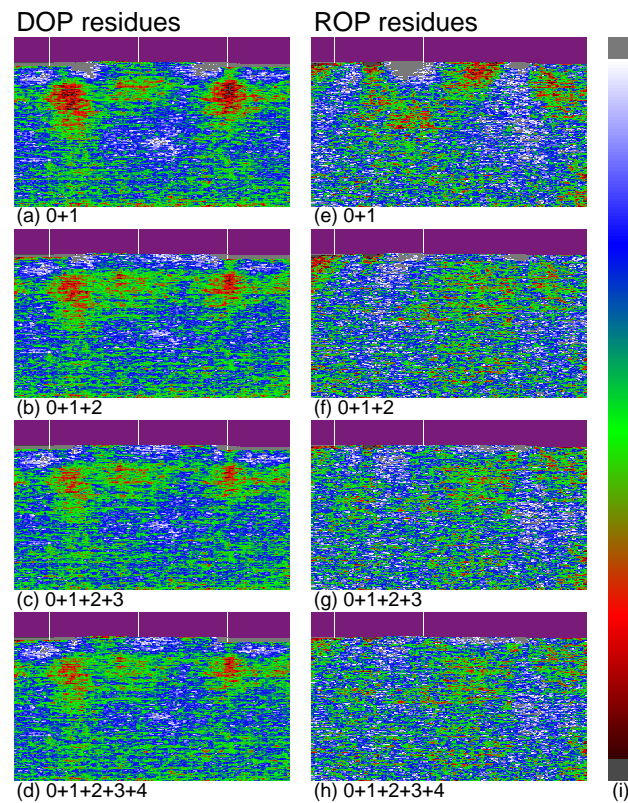


Figure 7. From top to bottom, residues for fits with 1, 2, 3, and 4 basis functions plus background functions. A 3×3 point smoothing (unit-area convolution) was used to reduce the noise and thus enhance the ability to see patterns in the residue. Compare panels (c,f) of Figure 6 with panels (d,h) to observe the noise reduction caused by the smoothing. The colour bar (i) shows the false colour mapping that was used to display the data and has the same explanation as the colour bar of Figure 3.

The second panel from the top shows the residues for uniaxial \hat{n} SiN stress plus a biaxial stress in the SiN (plus background terms). The addition of the uniaxial stress reduces the red ‘blobs’ under the edges of the SiN stripe, and thus appears to improve visually the quality of the fit.

The third panel from the top shows the residues for biaxial plus uniaxial SiN stress plus a biaxial interface stress between the SiN and the GaAs. The addition of the interface stress appears to reduce slightly the DOP and ROP residues. The changes in the ROP residue are most noticeable in the upper left as compared to the panel above.

The bottom panel shows the residues for the addition of a biaxial stress to the GaAs surface outside of the SiN. This biaxial etch stress does not appear to improve visually the plots of the DOP and ROP residues, and thus does not appear to be a physically significant component in the description of the DOP and ROP patterns.

It should also be noted that the basis functions are not necessarily unique. For the choice of the second basis function, there were eight choices that reduced χ_T by the same amount, within four-tenths of one 95% confidence interval, $CI_{0.95}$. The common effect for these choices was to produce a radius of curvature (i.e., a bowing) on the top surface.

It is clear from the false color images of the residues in Figure 7 that more than one basis function is required to explain the DOP and ROP patterns caused by the presence of

the SiN stripe. The DOP and ROP cannot, for example, only be explained by biaxial stress in the SiN.

Table 2 lists the values of $\chi_T = \sqrt{(\chi_{DOP}^2 + \chi_{ROP}^2)/2}$, χ_{DOP} , and χ_{ROP} for 1, 2, 3, and 4 basis functions plus background terms. The first four rows of the table correspond to the rows of the panels in Figure 7. χ_{DOP} and χ_{ROP} are the reduced chi values for the fits, and are equal to the rms values of the residues. Assuming that the residues are normally distributed, the 95% confidence interval for χ_T , $CI_{0.95}$, is estimated as $CI_{0.95} = 5.2 \times 10^{-3}$ for 71,316 degrees of freedom ([25], Section 2B).

The bottom row of Table 2 lists the reduced chi values for the background terms only. This row shows that the biaxial SiN stress basis function reduces the rms DOP and ROP residues by large amounts. For example, χ_T reduces by $(2.43 - 1.0943 \approx 258 \times CI_{0.95})$ with the addition of the biaxial SiN stress basis function. This reduction puts the changes caused by the other terms in perspective. The addition of the second basis function changes χ_T by $8.9 \times CI_{0.95}$, some $29 \times$ less than the first basis function. It can also be observed from the last row of Table 2 that the DOP signal, as measured by the DOP rms residue between the biaxial basis function and the background fit, is $3.20/1.28 \approx 2.5 \times$ larger than the ROP signal. The difference in the magnitudes and extents of the DOP and ROP lobes can be observed by comparing the appropriate panes of Figure 3 and noting that the ROP is displayed with a display gain of $15 \times$ as compared to the $10 \times$ for the DOP.

An analysis of the χ_T values of Table 2 shows that the addition of uniaxial \hat{n} stress to biaxial SiN stress reduces χ_T by a statistically significant amount ($1.0485 - 1.0943 = -0.0458 \approx -8.9 \times CI_{0.95}$), that the addition of a biaxial interface stress produces a statistically significant ($-0.0195 \approx -3.8 \times CI_{0.95}$) change in χ_T , and that the addition of a biaxial etch stress causes a statistically insignificant ($-0.0016 \approx -0.3 \times CI_{0.95}$) change. These pronouncements on the significance of the change introduced by the addition of a fitting function are similar to the discussions of the preceding paragraphs, which were based on the visual changes in the residues of Figure 7.

Table 2. χ values for fits of the DOP and ROP data to FEM simulations for a $4.35 \mu\text{m}$ -wide SiN stripe on GaAs for $R_a = 1.2$.

Elements	Influence	χ_T	χ_{DOP}	χ_{ROP}	$\delta\chi_T/CI$
0 + 1	1: biaxial SiN stress	1.0943	1.1248	1.0633	−258.4
0 + 1 + 2	2: uniaxial \hat{n} stress	1.0485	1.0757	1.0210	−8.9
0 + 1 + 2 + 3	3: biaxial interface stress	1.0290	1.0498	1.0082	−3.8
0 + 1 + 2 + 3 + 4	4: biaxial etch stress	1.0274	1.0513	1.0033	−0.3
0	0: background only	2.43	3.20	1.28	

The parameter R_a , which is the ratio of the ROP to DOP fit coefficients, was taken to be 1.2. The value for R_a of 1.2 gave a minimum value of χ_T . $R_a = 1$ is expected if $d = 2.4b$, as recommended by Vurgaftman et al. ([23], Table I, p. 5825), and if the analysis presented in Ref. [16] is correct.

A plot of χ_T as a function of R_a shows that the minimum is smooth, shallow, and broad. For $\chi_T = \pm 1.5 \times 10^{-3} = \pm 0.3 CI_{0.95}$, $R_a = 1.2 \pm 0.16$. Clearly χ_T is not a sensitive function of R_a .

Monte-Carlo analyses were performed to estimate the precision in the value of R_a as obtained from the fitting procedure. Gaussian white noise was added to the best-fit DOP and ROP functions to create synthetic data. These synthetic data were used as input to the fitting routine, and fits for $R_a = 1.15, 1.16, \dots, 1.25$ were performed. The R_a value that gave the minimum value of χ_T was selected. For noise which gave a $\chi_T = 1.0$ for fits to the synthetic data, the average value for R_a obtained from 101 different fits with different noise was 1.20 with a standard deviation of zero. A similar result was obtained if the noise was added to the measured data (which already has noise and thus χ_T increased to 1.43) and the fitting procedure was run. If the rms value of the noise was increased by a factor of 10,

the mean value for R_a stayed the same but with a non-zero standard deviation, with 88 of the 101 values equal to 1.20, and with all values in the range $1.19 \leq R_a \leq 1.21$.

It seems that additive noise is not the limiting factor in the ability to determine R_a from fits to the data. It is likely that the precision in a determination of R_a will be determined by the quality of the substrate and the accuracy of the FEM simulations. Defects in the substrate or on the measurement surface, which show as non-uniform regions of DOP and ROP, will likely set limits on the precision of an estimation of the ratio R_a from fits to the data. Similarly, FEM simulations with grossly inadequate basis functions or material parameters might lead to bad determinations of R_a .

For the fits presented in this work, a value of $R_a = 1$ is expected if $d/b = 2.4$ and if the simple model [16] underlying Equations (5) and (6) is correct for GaAs. The value of R_a found in this work is consistent with the model and the suggested value for d/b ([23], Table I, p. 5825). However, this result is from fits of FEM simulations to single maps, with each map composed of $\approx 36\,300$ measurements. Confirmation by additional measurements and fits is indicated.

Fits of FEM simulations to measurements of loaded v-grooves etched into an InP substrate gave a value of R_a close to unity [25] and this suggests that the combination of the model of strain dependence of DOP [25] and the suggested d/b ratio for InP ([23], Table VI, p. 5829) are reasonable. The InP work comprised fits to multiple independent measurements.

5. Conclusions

The impact of a 4.35 μm -wide SiN stripe on the local strain of a GaAs substrate was investigated using degree of polarization (DOP) measurements conducted by cathodoluminescence (CL) spectroscopy in a scanning electron microscope. The 3D FEM simulations [29] of 23 different strain states (or basis functions) were made and compared to the measured DOP and four of these basis functions were identified to be the most relevant.

The top four basis functions for the fits were found to be biaxial stress in the SiN, an uniaxial \hat{n} SiN stress, a biaxial SiN interface stress between the SiN and GaAs, and a biaxial etch strain. The stresses induce a bowing of the GaAs, and this introduces a DOP that varies from the top to the bottom of the substrate. The contribution of the etch stress does not appear to be statistically significant and choices for the influences are not necessarily unique. There were other influences that caused reductions in χ_T that were the same within one confidence interval.

The fits are not excellent in that extended red lobes remain under the edges of the SiN stripe and there is a blue band at the top of substrate. These features can be seen in the panels of Figure 7. This suggests that not all influences have been considered in the basis functions that were considered. However, it should be noted that the magnitudes of these influences are likely of the order $<1\%$ of the magnitude of the influence of the biaxial stress in the SiN, and thus should not significantly change the values of the dominant fit coefficients. The estimate of 1% is based on the relative magnitudes of the changes in χ_T that are caused by addition of a basis function, c.f., Table 2.

It is interesting to note that the magnitude of the ratio R_a of the ROP fit coefficient to the DOP fit coefficient is ≈ 1 . A value of $R_a = +1$ is expected if the expressions for DOP and ROP as presented in (Ref. [16], Section 3.D.4) are employed and if the same convention for the direction for $DOP = 1$ and $ROP = 1$ is also employed. For loaded v-grooves on InP, the ratio of the ROP and DOP fit coefficients was found [25] to be consistent with the analysis presented in Ref. [16]. The results for fits to GaAs are consistent with the strain dependence of DOP and ROP that is reported in [16] and displayed in this work as Equations (5) and (6).

The results presented here and in [25], although in need of corroboration, appear to indicate that the dependence of DOP on strain [16], as given in this work by Equations (5) and (6) for GaAs, or as given in [25] for InP, should be used.

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