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# 2 Effect of compatibilizers on polyethylene-eucalyptus

## 3 lignin blends

- 4 Jérôme Vachon,<sup>1,\*</sup> Derar Assad-Alkhateb,<sup>1</sup> Laura de Araujo Hsia,<sup>2</sup> Jairo H. Lora,<sup>3</sup> Stéphanie
- 5 Baumberger<sup>4</sup>

- <sup>1</sup> SABIC Europe B.V., Urmonderbaan 22, 6160 AH Geleen, The Netherlands;
- <sup>2</sup> Suzano S/A; Estrada do Lageado, Lageado Limeira, SP; CEP: 13486-199 Brazil
- <sup>3</sup> Lora Consulting LLC, 7 Camby Chase Rd, Media PA 19063, USA
- 9 4 Institut Jean-Pierre Bourgin, INRAE, AgroParisTech, Université Paris-Saclay, 78000 Versailles, France
- 10 \*Correspondence to: J. Vachon (E-mail: <u>jerome.vachon@sabic.com</u>)

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**Abstract:** Eucalyptus Kraft lignin was blended in various proportions with two different types of PE (LDPE and PCR), with or without compatibilizer (PE-GMA or PE-HEMA copolymers). Materials prepared by injection molding or extrusion casting were characterized for their thermal, antioxidant, antibacterial and mechanical properties. In addition, the photo-permeability was assessed, as this property is specifically relevant to mulching applications. The use of compatibilizers enhanced the antioxidant properties which reached more than 3 h OIT when lignin was present at 20 wt% and beyond. Good antibacterial properties were obtained on Gram-positive bacteria when using PE-GMA as compatibilizer. The photo-permeability of the materials was also reduced, reaching a transmittance lower than 5% throughout the whole measurement range (200 - 800 nm) in PCR. However, higher lignin contents led to a more brittle material and the overall processability of the material became more difficult, features that were not improved by compatibilizers. These materials are promising candidates for mulching film application, especially with PCR which still lacks high-volume market applications.

Keywords: Lignin, LDPE, Post-Consumer Recycled plastics, Compatibilizer, Antioxidant, Antimicrobial, Mulching.

1. Introduction

In the last couple of decades, research efforts were concentrated on using ligno-cellulosic biomass as feedstock for the sustainable production of energy, chemicals and materials. Indeed, this ligno-cellulosic biomass can be recovered from forestry and agricultural residues as well as from dedicated energy crops, plants grown as a low-cost and low-maintenance harvest, which makes them a source of renewable carbon not competing directly with the supply of food resources for human and animal consumption.<sup>1</sup> Additionally, the ligno-cellulosic biomass has multi-million ton potential capacity, in particular its lignin component with a presence in biosphere estimated at ~ 350 billion tons.<sup>2</sup>

Lignin mass content determined by the Klason method reaches 25-35% in softwoods, 20-25% in hardwoods and 15-25% in herby plants.<sup>3</sup> It consists of a polymer built on phenylpropane-type monomers linked through various carbon-carbon and ether bonds making this raw material more resistant to chemical and enzymatic attacks than the other biomass components.<sup>4,5</sup> Several lignin isolation processes have been developed up-to commercial scale to valorize the carbohydrate fractions of wood and straws while producing a by-product so-called "technical lignin", recognized nowadays as high-value functional bio-based polymer with a wide range of applications.<sup>5,6,7</sup> Among these technologies, the Kraft process has the advantage to be versatile (applicable to both softwood and hardwood), to generate cellulosic fibers suitable for paper production, and to have the potential to produce large volumes of high purity lignin (less than 5% of carbohydrate contaminants). During the previous decade, worldwide Kraft lignin production capacity more than tripled reaching 120 kt

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in 2016.8 The main challenge for the industry and the scientific community remains the actual valorization of technical lignins and their use in high volume markets.9 Promising markets are those of aromatics, carbon fibers, phenolic resins and additives for plastics, these last applications exploiting the multifunctionality of lignins.

In a previous paper, the use of specific lignin extracts as additives in high density polyethylene (HDPE) was reported. 10 It was observed that a fraction from annual plant soda lignin that possessed a high phenolic content (~ 4.2 mmol/g), conferred to the material specific attributes, when blended and co-extruded with HDPE at a few wt% level (ranges from 2 to 5). Besides antioxidant and antimicrobial properties (especially on Gram positive Staphylococcus Aureus bacteria), this lignin extract gave to the material repellent properties towards two types of insects, an invader (Sitophylus oryzae) and a penetrator (Plodia interpunctella). However, an issue when using lignins is the dark color and smell they confer to the material they are blended with, which constitutes a hurdle for potential application in food packaging (e.g as insect repellent films for protecting food). Another issue encountered is the poor compatibility of polyolefins with lignin, which can negatively affect the thermal and mechanical properties of polyolefins/lignin blends. 11 In the previous study, a poor compatibility between HDPE and the lignin fraction with low phenolic content (≤ 3.4 mmol/g) was observed, leading to visible lignin agglomerates and film cracks even when lignin was used in low amounts (2 wt%). This phenomenon could be even more exacerbated when using higher lignin content and/or LDPE which is known to have a poorer compatibility with lignins than HDPE due to the interaction with branching, an entropically unfavorable feature. 12 To solve the compatibility problem, chemical modification of lignin is a potential route where the polarity of the lignin is modified, <sup>1a</sup> yet, the lignin functionality such as its antioxidant properties can be strongly altered. An advantageous alternative is the use of compatibilizers, materials that, through covalent bonding or polar interaction, act as a binder between materials of different polarities. 11b,13

An interesting application for PE-lignin composites that could be targeted is for agricultural mulching films. Indeed, already colored material (with dyes or carbon black) are used and smell is not a limiting factor since the films are implemented in open space. Mulching is the practice of covering the soil surface with a thin plastic film around plants in their first growth stage for a rather short period, typically from 2 to 4 months but can be up to a couple of years depending on the quality of the material.<sup>14</sup> The films used for mulching are the second most important agricultural film applications after covers. The benefits achieved are soil moisture retention, heat trapping and controlling, improving cultivation conditions, enabling reduction of weeds and plant diseases, reducing the use of pesticides and preventing insects from attacking plants.<sup>15</sup> The most common material used for producing mulching films is LLDPE, sometimes used in combination with LDPE. Post-consumer recycled (PCR) materials that contain various sources of PE coming from mechanical recycling processes are increasingly used. Other materials such as EVA and EBA copolymers are also used for higher added value crops. Mulching films are commonly produced through an extrusion blown film process. The general procedure is to feed PE granules to a single screw extruder where material is melted and exits the die in the form of a tube. This tube is subsequently blown in a shape of a bubble which is collapsed and drawn upwards by two nip rolls. Finally, the obtained flattened tube is wound on a winder. The film thickness can range between ~15 to 80 µm with a width up to 3 m. 16 During the blown film process, the material is stretched in both the transverse and draw directions thus requiring that the material possesses a good mechanical strength which shall not altered by the addition of lignin. Additionally, puncture, impact strength resistance and ductility,17 as well as a good UV and thermal stability are necessary during the lifetime of the film but also to sustain the blown film process which operates at high temperatures (≥ 190 °C). To be attractive in a mulching application, the addition of lignin should not be detrimental to the original PE mechanical properties while conferring additional functionalities. For instance, photo-permeability is an important property for mulching films where blocking visible light transmission is key to prevent from an undesired high growth of weeds.<sup>18</sup> Carbon black, tannins and humic substances can be used to reduce the transmitted light.<sup>19</sup> Light transmittance also has an effect on soil temperature and

 moisture retention. Furthermore, UV absorption may impact the kinetics of polymer degradation by sun exposure, which could result in premature mechanical film failure.

The objective of this paper was to show that materials with enhanced properties (thermal stability, mechanical strength, UV protection) can be prepared by blending LDPE with a lignin fraction having a high phenolic content, in combination with compatibilizers. A eucalyptus Kraft lignin was blended in various proportions with two different types of PE (LDPE and PCR), with or without any compatibilizer (PE-copolymers). Materials prepared by injection molding or extrusion casting were characterized for their thermal, antioxidant, antimicrobial, optical and mechanical properties, as well as puncture resistance and photo-permeability, as these properties are specifically relevant to mulching applications.

#### 2. Materials and methods

#### 2.1 Materials

SABIC® LDPE 2101N0W grade (MFR 0.85 dg/min at 190 °C and 2.16 kg) was used. The material contains no additives. PCR-PE (RYMO W122 from Rymoplast) is a recycled PE that contains ~ 40% LLDPE and ~60% LDPE, amounting overall to more than 99% recycled polymer content. NEWProd-FP101 (provided by Suzano SA) is a high purity, low moisture renewable aromatic biopolymer derived from eucalyptus wood pulped by the Kraft process and produced in a pilot plant using proprietary technology (more technical specifications in Table 1). LOTADER® AX8840 or "PE-GMA" (provided by Arkema) is a random copolymer of ethylene and glycidyl methacrylate (GMA), polymerized by high-pressure autoclave process. The GMA content is ~8.0 wt% (determined by FT-IR). PE-HEMA (provided by SABIC) is a copolymer based on a high-pressure free radical copolymerization of ethylene and 2-hydroxyethyl methyl acrylate (HEMA) (Figure 1). The HEMA content is ~17.6 wt% (determined by ¹H-NMR).

PE-GMA PE-HEMA

Figure 1. Chemical structures of PE-GMA and PE-HEMA. The ethylene and methacrylate blocks are randomly distributed

#### 125 Table 1. Characteristics of NEWProd-FP101

SOLID CONTENT	wt%	>95
LIGNIN	wt%	>95
HEMICELLULOSE	wt%	<2
ASH	wt%	<3
AROMATIC OH	mmol/g	4.2
T <sub>G</sub>	°C	~135
APPARENT DENSITY	kg/L	0.44 ± 0.04
<b>COMPACT DENSITY</b>		0.61 ± 0.07
REAL DENSITY		$1.40 \pm 0.02$
PH (10% AQ.		3 to 5
SOLUTION)		

#### 2.2 Polyethylene-lignin blends preparation

Polyethylene (LDPE and PCR), lignin and compatibilizers were ground by using cryogenic conditions (with liquid nitrogen). The grinding and mixing process was performed by using an Ultra Centrifugal Mill ZM 200. The lignin was dried in vacuum oven at 50 °C overnight prior to compounding. PE and lignin mixtures were fed to a micro compounder machine (Xplore) with two conical fully intermeshing mixing screws (capacity of 3 - 15 mL of material). The processing temperature is controlled in 2 times 3 separate barrel-heating zones. The micro compounder was fed with PE/lignin/compatibilizers ground mixtures through a powder feeder. All the samples were processed at a maximum rotor speed of 170 RPM for 5 min at 150 °C. The following materials were made with LDPE and PCR-PE base polymers at varying concentration of each constituent (Table 2).

Table 2. List of compounded materials

Sample name	Composition
LDPE-1	LDPE (95 wt%) + FP101 (5 wt%)
LDPE-2	LDPE (94 wt%) + FP101 (5 wt%) + PE-GMA (1 wt%)
LDPE-3	LDPE (94 wt%) + FP101 (5 wt%) + PE-HEMA (1 wt%)
LDPE-4	LDPE (88 wt%) + FP101 (10 wt%) + PE-GMA (2 wt%)
LDPE-5	LDPE (76 wt%) + FP101 (20 wt%) + PE-GMA (4 wt%)
LDPE-6	LDPE (64 wt%) + FP101 (30 wt%) + PE-GMA (6 wt%)
PCR-PE1	PCR-PE (95 wt%) + FP101 (5 wt%)
PCR-PE2	PCR-PE (94 wt%) + FP101 (5 wt%) + PE-GMA (1 wt%)
PCR-PE3	PCR-PE (94 wt%) + FP101 (5 wt%) + PE-HEMA (1 wt%)
PCR-PE4	PCR-PE (76 wt%) + FP101 (20 wt%) + PE-HEMA (4 wt%)

Xplore micro-injection molder was used to obtain materials in desired shapes (plaques and bars). The molder consists of a temperature-controlled mold, connected with a heated removable injection nozzle unit. PE/lignin/compatibilizers were injected into the temperature-controlled mold with a plunger powered by compressed air (pressure ~10 bars, mold temperature 40 to 60 °C).

Films from PE/lignins/compatibilizers blends were produced by extrusion casting process (thickness ~ 60 to 70  $\mu$ m in the middle and 100 to - 120  $\mu$ m at the edge of the films, width = 70 mm). The prepared pellets were let to dry at 70 °C for 2 h. All films were prepared by using the following parameters: extrusion temperature = 150 °C, temperature at the shaping die = 174 °C, extruder speed = 135 RPM and films thickness = 60-100  $\mu$ m.

#### 2.3 Material characterization

Thermogravimetric Analyses (TGA) were performed by using a TA instruments equipment. All measurements were performed under nitrogen from 30 to 300  $^{\circ}$ C with 10  $^{\circ}$ C/min heating rate. Isothermal TGA was performed at 200  $^{\circ}$ C.

Differential scanning calorimetry (DSC) measurements were performed on a TA Instruments Q20 equipped with a RCS 90 cooling system. About  $3-5\,\mathrm{mg}$  of polymeric sample was weighed inside an aluminum pan and subjected to DSC measurements under nitrogen atmosphere. Unless otherwise noted, polymers were scanned twice from -100 °C to 200 °C at a constant heating/cooling rate of 20 K/min. The  $T_m$ , and the melting enthalpy ( $H_m$ ) were determined from the second heating.

Oxidation Induction Time (OIT) was measured by DSC on molten polymer according to standard ASTM D3895. About 3 – 5 mg of polymeric sample was weighed inside an aluminum pan and subjected to DSC measurements under nitrogen atmosphere (50 mL/min). The polymer was heated until 200 °C at 10 °C/min heating rate and left at this temperature for 5 min. Nitrogen was switched to oxygen and the time before an exothermal peak is detected was recorded.

#### 2.4 Optical properties

Haze measurements of the cast films were performed according to the "Standard Test Method for Haze and Luminous Transmittance of Transparent Plastics" ASTM D1003-C using a BYK Gard-i device where the opening angle of the beam passing through the sample is less than 3°. The roll was clamped on the holder in front of the detector. The average of 5 measurements is reported where random spots on the films were chosen at different height and length of the film. For the gloss, BYK-micro-gloss 45° (typical angle used for films) was used where a black felt was placed below the film as background to diffuse the light during measurement. The average of 5 measurements is reported where random spots on the films were chosen at the same height. Due to the width of the device which is close to the one of the film, and to be sure that the device fully covers the film, the device was placed in the middle of the film thus only measuring the middle part and not at the edges.

Photo-permeability (UV-Vis) measurement were performed to determine the percentage of light transmittance at different wavelengths between (200 and 850 nm) by using an ultraviolet-visible (UV-Vis) spectrophotometer. The transmission (in %) is shown with sample thickness correction to account for variations.

#### 2.5 Mechanical properties

Mechanical properties (tensile strength, Young's modulus, maximum elongation at break) were measured by using ISO 527 (Plastics — Determination of tensile properties) and Zwick-Roell machine for both tensile bars and cast films. Tests were performed on five specimens for both tensile bars and cast films. The films were cut with the following dimension: thickness =  $60-110 \mu m$ , width = 15 mm, length = 50-53 mm. Measurements were performed on both TD direction and MD direction at room temperature (test speed = 50 mm/min). Sample thickness was taken into account in the calculation to get rid of variations due to this parameter. The same tensile bars were used to measure Izod Pendulum Impact Resistance. Tests were performed on three specimens at -30 °C, both on notched and un-notched samples according to ASTM D256 ("Standard Test Methods for Determining the Izod Pendulum Impact Resistance of Plastics").

Puncture resistance of the films were measured according to the "Slow Rate Penetration Resistance of Flexible Barrier Films and Laminates" test ASTM F1306. Experiments were performed at 23 °C using a clamping fixture diameter of 34.9 mm, a pre-load of 0.2 N and a test speed of 25 mm/min. Specimens with approximate dimensions of 60x60 mm were cut from the films and clamped. The penetration hole was ~35 mm in diameter and a hemispherical penetration probe of 3.2 mm diameter was used. Reported results are the average measurement of 5 specimens.

#### 2.6 Antibacterial properties

Antimicrobial activity measurements were performed following ISO 22196 "Measurement of antibacterial activity on plastics and other non-porous surfaces" and was performed at Industrial Microbiological Services LTD using the following conditions. The films were cut into ~50 ×50 mm squares. An aliquot (225 μL) of a log phase cell suspension of either Escherichia coli (4.2 x 105 cells/mL;ATCC 8739) or Staphylococcus aureus (4.1 x 105 cells/mL; ATCC 6538p) prepared using the method described in ISO 22196:2011 was held in intimate contact with each of the three replicates of films supplied using a 30 x 30 mm PE film (cut from a sterile Stomacher bag). The temperature of incubation was set to  $35 \pm 2$  °C. The size of the surviving population was determined using the method described in ISO 22196: 2011. The viable cells in the suspension were enumerated by spiral dilution on to Trypcase Soya Agar and by the pour plate method described in ISO 22196. These plates were then incubated at 35 °C + 2 °C for 24 h and then the colonies present are counted. An additional three replicates of unfortified surfaces (LDPE films) were also inoculated in the manner described above but were then analysed immediately for the size of microbial population present to provide 0time control data). Antimicrobial activities are given in logarithmic reduction R. R is calculated according to the bacterial concentration in the negative control and the concentration after 24 h of contact with the treated products. All data were converted to colony forming units (CFU) cm-2 and

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then transformed (Log10) to provide a data set that conformed to a Gaussian distribution. Potential outliers were tested using Dixon's Q-test (P = 0.05). Statistical significance of any effects in the dataset was tested by analysis of variance (ANOVA, P = 0.05) and the confidence intervals of the means were calculated and displayed as Box and Whisker plots (see Sup. Info. for further details).

#### 3. Results and Discussion

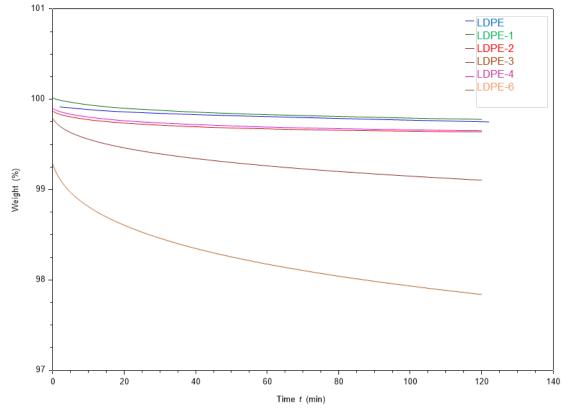
In order to investigate the benefit of compatibilizers on the properties of PE-lignin blends, a pilot-plant pre-commercial eucalyptus Kraft lignin sample (NewProd-FP101, Suzano SA) was used. This sample was selected for its (i) high lignin content, (ii) low content of moisture, sugars and ash, (iii) low molecular weight, and (iv) low softening temperature compared to other commercially available Kraft lignins and lignosulfonates (Table 1), which made it a good candidate for the preparation of homogeneous blends. Lignin incorporation rate up to 30% was tested, since it is the limit mentioned in literature at which most of polymer-lignin blends lose their mechanical properties. The two compatibilizers tested (PE-GMA and PE-HEMA) were incorporated at 1:5 wt. ratio with respect to lignin. The compatibilizers were selected due to their difference in polarity and reactivity. While the HEMA group can participate in both hydrogen donor and acceptor, GMA can only participate as hydrogen acceptor. Additionally, the epoxide from the glycidyl group can undergo an opening reaction with nucleophilic groups such as hydroxyl and, carboxyl groups which are present in lignins. This section reports on the properties of the different materials obtained.

#### 3.1. Thermal stability

The thermal stability of the films made out of lignin is key for assessing the processability of such materials. Technical lignins are known to have limited thermal stability which is indicated by TGA by some weight loss when temperature exceeds 190 °C as has been reported previously, 10 and confirmed for the lignin sample used in this study (Figure S1). An isothermal TGA at 200 °C for 2 h was thus performed on the PE-lignin blends to evaluate their relative thermal stability under temperature and time more severe than those used in normal processing, for instance in extrusion or film blowing (Figure 2). Under these conditions, the lignin FP101 experienced an 8.2% weight loss while both reference PE materials (LDPE and PCR-PE) only showed 0.2% weight loss (Table 3). When ramping up the temperature to 200 °C, before starting the isothermal TGA experiment, the lignin already lost ~4 wt%, while the LDPE and PCR-PE materials were mostly unaffected (Figure S2 and S3). Lignin being somewhat moisture sensitive, this could be related to water loss as this weight loss happened around 100 °C. To tentatively minimize this effect in compounded materials, the lignin was dried prior to compounding. However, the molten polymer exiting the extruder was cooled in a water bath before pelletizing so that there was no control on the extent of moisture present in the lignin within the polymer. The weight loss during the temperature ramp-up of PE-lignin blends was negligible (< 0.5 wt%) at low lignin content (5 wt%), but starts to be significant, as shown for PCR-PE4, at 20 wt% lignin content. There, 1 wt% was already lost before starting the isothermal experiment. Results showed only minimal weight loss of the LDPE samples containing 5 wt% lignin after 2 h, which reflected a good thermal stability of the materials. In LDPE-6 (containing 30 wt% of lignin), an increased weight loss was observed (1.4 wt%), reflecting the presence of 6 times the amount of lignin in LDPE-1 material. PCR-PE materials containing 5 wt% lignin showed a slightly higher weight loss compared to LDPE based blends of similar lignin content, yet differences remain low and in the order of magnitude expected regarding the content of lignin. Regarding PCR-PE4, a lower weight loss was recorded with respect to the lignin content (9 wt% vs e.g 14 % for PCR-PE1 containing 5 wt% of lignin), however, considering the additional 1 wt% weight loss during the temperature ramp-up, the true weight loss would be in the same range (2.8 wt% would correspond to ~ 14 wt% based on the lignin content). Overall, besides some moisture related weight loss, the PElignin blends experienced only slight weight loss that would not be detrimental when subjecting them to a blow molding process.

#### Table 3. Weight loss of lignin, PE and PE-lignin blends measured by TGA

Sample	Weight loss (%) at	Weight loss (%) / wt% of lignin
	200 °C after 120 min	in PE at 200 °C after 120 min
FP101	8.2	-
LDPE-ref	0.2	-
LDPE-1	0.2	4
LDPE-2	0.3	6
LDPE-3	0.3	6
LDPE-4	0.7	7
LDPE-6	1.4	5
PCR-PE-ref	0.2	-
PCR-PE 1	0.7	14
PCR-PE 2	0.6	12
PCR-PE 3	0.8	16
PCR-PE 4	1.8	9



264265 Figure

Figure 2. TGA curves of LDPE materials in isothermal experiments at 200 °C

#### 3.2. Influence on crystallinity

DSC measurements were first performed to evaluate the impact of lignin onto PE's initial crystallinity (Xc = 50%) (Table 4, Figure S2). Increasing lignin content into PE led to a decrease of the material's crystallinity. However, taking into account the amorphous characteristic of lignin (Figure S3), a higher decrease would be expected based on the dilution factor due to lignin incorporation in the crystalline PE matrix. For instance, at 30 wt% lignin incorporation rate, a total material crystallinity of 35 % still remained (entry 7). This cannot be attributed to lignin particles acting as a nucleating agent for PE, as a true indication of nucleating ability for a nucleating agent is the increase of the crystallization point. In this case, there is basically no change. Instead, it is suspected that water

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which might be absorbed by lignin influences the melting enthalpy value measured. Enthalpy of vaporization of water is 2260 J/g, which is one order of magnitude higher than melting enthalpy of PE, and occurs within the melting range of PE. The incorporation of a compatibilizer in a PE-lignin system did not change the apparent PE crystallinity as for instance a similar crystallinity was observed between LDPE-1 and LDPE-2. DSC measurements were also performed on PCR materials and details are shown in supporting information (Table S2 and Figure S4 to S8). A similar statement as for LDPE can be made, as the addition of up to 20% did not significantly affect neither melting and crystallization temperatures, nor the degree of crystallinity compared to the PCR-PE reference. However, due to the presence of two different types of PE in PCR-PE, two peaks were observed for both melting and crystallization, with a relatively broad DSC curve which made the variations induced by the presence of lignin in the material insignificant.

Table 4. Thermal data and crystallinity of LDPE-lignin blends measured by DSC

Entry	Sample	Tc (°C)a	ΔHc (J/g) <sup>a</sup>	Tm (°C) a	ΔHm (J/g) a	Total Xc (%)b
1	LDPE-ref	99.5	192.9	100.2	143.6	50
2	LDPE-1	99.0	195.5	100.0	140.8	49
3	LDPE-2	98.9	192.0	101.0	138.5	48
4	LDPE-3	99.0	180.6	101.2	124.2	43
5	LDPE-4	98.7	176.2	100.0	130.7	46
6	LDPE-5	98.8	167.3	101.0	116.8	41
7	LDPE-6	98.6	149.8	100.0	101.0	35
8	PCR-PE-ref	110.2	130.2	112.3	131.0	46
9	PCR-PE-1	109.9	141.5	114.7	131.8	46
10	PCR-PE-2	110.0	167.2	114.8	142.8	50
11	PCR-PE-3	110.0	148.9	115.2	127.3	45
12	PCR-PE-4	109.4	129.1	108.9	117.8	41

a. Det. via DSC. For PCR-PE materials, onset Tc and Tm are reported. See supporting info for the full details; b. Degrees of crystallinity (Xc) were calculated dividing the melting enthalpy of 100 % crystalline PE (286.2 J·g $^{-1}$ ) according to ref.<sup>23</sup> The melting enthalpy was determined from the DSC second heating scan.

#### 3.3 Antioxidant properties

The antioxidant properties conferred to PE by lignins with high phenolic content were recently reported,<sup>10</sup> and this antioxidant effect of lignins has been established for a broad range of ligninpolyolefins blends.<sup>24</sup> In this study, the effect of compatibilizers on the antioxidant properties of the LDPE-lignin blends was determined using OIT measured by DSC on molten polymer (Figure 3). OIT has been shown to be a robust analytical method for determining antioxidant performances in polyolefins, where the concentration of phenolic antioxidants (above 100 ppm level) was found linearly correlated with measured induction times.<sup>25</sup> In agreement with the fact that LDPE was unstabilized, an immediate thermal oxidation occurred within a few seconds (entry 1). With 5 wt% of lignin, an antioxidant effect was observed with 91 min OIT (entry 2), which was of the same order but yet exceeded the 80 min OIT previously reported for the extract from annual plant soda lignin.<sup>10</sup> While the addition of 1 wt% PE-GMA did not increase OIT, PE-HEMA further enhanced the lignin antioxidant properties with an OIT of 100 min. Since compatibilizers do not possess any antioxidant properties by themselves, the increased OIT could be explained by a better dispersion of the lignin within the PE material, or by indirect contribution to radical stabilization through matrix effect. OIT was further increased when using higher lignin content, achieving for instance an over 3 h protection (no measure was performed for longer times) for lignin incorporation rate equal to or higher than 20 wt%. This result confirmed that lignin possessing high phenolic content can provide outstanding antioxidant properties and that, at high loading content with the use of a compatibilizer, a long lifetime protection could be achieved. As a matter of comparison, tetrakis-(methylene-3-(3,5-di-tertbutyl-4-hydroxyphenyl)-propionate methane ("Irganox 1010"), a phenolic antioxidant traditionally used in

polyolefins, led to an OIT of ~60 min at 0.25 wt% loading in HDPE (which is on the high range in commercial polyolefins). OIT being proportional to antioxidant concentrations, it means that at least 0.75 wt% of Irganox 1010 would be necessary to reach more than 3 h of OIT. Interestingly, the structure of the compatibilizer influenced the lignin properties in the matrix. The more beneficial effect of PE-HEMA compared to PE-GMA may be explained by different factors. First, the amount of HEMA was higher than the amount of GMA in the PE-copolymers. Secondly, HEMA did not alter the functionalities of the lignin as interacting only through H-bond while GMA could potentially react with the OH and CO<sub>2</sub>H groups of the lignin.

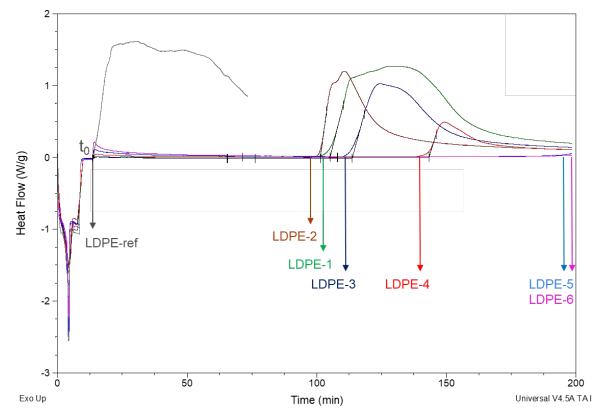


Figure 3. OIT Measurements of LDPE and LDPE-lignin blends

Table 5. OIT of LDPE and LDPE-lignin blends

Sample	OIT (min)
LDPE-ref.	<0.5
LDPE-1	91
LDPE-2	87
LDPE-3	100
LDPE-4	129
LDPE-5	> 180
LDPE-6	> 180

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#### 3.4 Optical properties

Haze and gloss measurements were performed to assess the effect of lignin on the films aspect and to infer any effect of compatibilizers (Table 6, Figure S11 and S12). The images of the film (Figure 4) indicated that more back particles were present in uncompatibilized films (LDPE-1 and PCR-PE1), with a more pronounced effect in the PCR-PE material. It could be deduced from the visual appearance of the films that PE-GMA was a more effective compatibilizer of the system than PE-HEMA, as the films appeared more homogeneous and with lower proportion of black particles, especially by comparison of LDPE-2 and LDPE-3. This was confirmed by a lower haze and higher gloss performance of such materials. However, haze and gloss are dominated by surface roughness. For instance, a higher gloss in LDPE-2 means that a less rough surface was obtained when compared to uncompatibilized LDPE-1. For PCR-PE4 containing 20 wt% of lignin, a high haze was obtained, which matches the visual appearance of the film, but also a higher gloss was noticed compared to all the other PCR-PE films. However, due to the size of the gloss-meter, only the middle part of the film could be measured which appears drastically different than the edges. Overall, the cast films produced show a different thickness at the edges (60 to 70  $\mu$ m) compared to the center of films (100 to 120  $\mu$ m). The addition of lignin leads to a bigger discrepancy between the thickness of the edges (which appear slightly darker) and the one in the center. It is the most pronounced in PCR-PE4 where up to 200 µm thickness was measured at the edges while only ~ 100 µm was measured in the center. Hence, the apparent film inhomogeneity only allows to draw conclusions on optical properties in the center of the film, which is not representative of the whole film.

Table 6. Haze and gloss measurements of the cast films

	LDPE-	-	LDPI	Ξ-	LDPE	<u> </u>	LDPI	Ξ-	PCR-		PCR-		PCR-		PCR-		PCR-	-
	ref		1		2		3		PE-re	ef	PE-1		PE-2		PE-3		PE-4	
Haze	28.6	±	59.0	±	50.0	±	73.1	±	50.0	±	75.4	±	80.0	±	80.2	±	87.6	H
[%]	0.5		0.3		0.9		0.9		0.3		0.6		0.5		0.5		0.7	
Gloss	4.3	±	13.5	±	16.5	±	11.7	±	7.8	±	6.5	±	6.0	±	7.4	±	14.2	H
[%]	1.1		3.1		3.1		2.8		2.7		1.2		0.7		1.4		0.5	





Figure 4. Images of cast films

#### 3.5 Photo-permeability (UV-Vis) results

Photo-permeability of the lignin-PE blends was measured (Figure 5) on films (Figure S18) relative to the transmittance of virgin LDPE and PCR. The transmittance of LDPE increased significantly at higher wavelengths going from ~50% at 250 nm to ~75% at 800 nm. The addition of 5 wt% of lignin (in the absence of any compatibilizer) not only retarded this phenomenon, but also lowered drastically the transmittance throughout the whole measurement range. For instance, the transmittance %T remained below 10% up to 380 nm to only climb up to 55% at 800 nm. While the extra addition of PE-GMA compatibilizer slightly increased the photopermeability of the film, PE-HEMA on the contrary resulted in an additional 10% decrease of

transmittance throughout the whole measurement range. Thus, an almost complete absorption was still observed up to 400 nm. Such result is similar to the performance of TiO<sub>2</sub> at 2 wt% loading which gives 0% transmission in the region of 200-350 nm.<sup>26</sup> The PCR-PE material (Figure 6), already absorbed more UV than virgin LDPE and had only 60% transmittance at 800 nm. Again, the addition of 5 wt% lignin decreased drastically UV transmittance which remained pretty flat up to 400 nm. The presence of compatibilizers (PE-GMA and PE-HEMA) did not affect spectrophotometric properties. Only through the increase of lignin content, an almost full UV absorption was observed with a transmittance lower than 5% throughout the whole measurement range when 20 wt% of lignin was used. Such a material would thus fulfill the requirements of mulching films in terms of photo-permeability while having outstanding antioxidant properties.

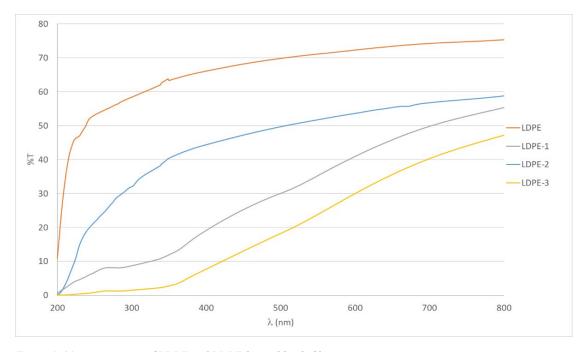


Figure 5. % transmittance of LDPE and LDPE-lignin blends films

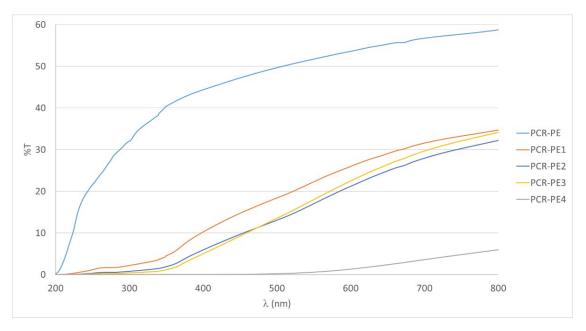


Figure 6. % transmittance of PCR and PCR-lignin blends films

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The effect of lignin on LDPE and PCR was assessed by measuring the yield stress, strain at break as well as the modulus on both injection molded bars and films (on machine direction MD and transverse direction TD, Figure S13 to Figure S24). Regarding LDPE films, the addition of 5 wt% lignin alone did not alter much the original material mechanical properties, enhancing them in some instances. Interestingly, the addition of PE-HEMA provided a little improvement. However, it appeared difficult to make films of good quality with the samples containing higher amounts of lignin. Regarding PCR films, the addition of 5 wt% lignin alone negatively affected the mechanical properties of the material. The addition of 1 wt% of PE-GMA restored values close to original levels. This result was consistent with the visual observation where PCR-PE films containing PE-GMA where of superior quality compared to uncompatibized PCR-PE and, to a lower extent, to the one containing PE-HEMA. Furthermore, PCR-PE2 film, which showed the best visual aspect, had the highest strain at break on both machine and transverse directions, due to the absence of stress concentrators in the films with better homogeneity (Figure 7). When using 20 wt% lignin content and PE-HEMA as compatibilizer, materials became harder and less deformable which was particularly noticed in TD as films broke at very low strain. With increased hardness (modulus) the materials also become more sensitive to stress concentration as the stress intensity increases with increasing modulus.

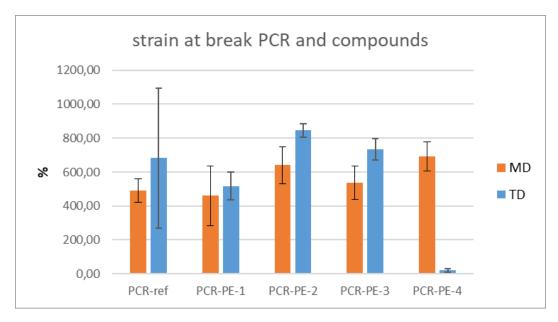


Figure 7. Tensile test on PCR films: strain at break

For studying materials with higher amount of lignin, injection molding of thick objects was necessary. A similar observation was made compared to the films, for both PCR and LDPE materials. The addition of lignin did make the material harder but more brittle as shown by the decreased strain at break. It was particularly noticeable with the highest amounts of lignin used. The compatibilizer did not induce major changes compared to the control (LDPE-1 vs LDPE-2). This behavior was further confirmed by the Izod impact test on notched specimen at -30 °C (Figure S30). Since mulching films experience a wide range of temperatures, the test was performed at low temperature to help gauge the impact resistance of the material in cold environments. Starting from a 75% ductile LDPE material, lignin addition led to a complete loss of ductility which was not mitigated by the compatibilizer (Table 7).

Table 7. Izod impact results on IM LDPE, Notched -30 °C

		LDPE	LDPE-1	LDPE-2	LDPE-4	LDPE-6
Ductility	%	75	0	0	0	0
Impact Strength-Avg	J/m	660	52,3	48.0	46.0	32,2
Impact Strength-Std	-	392	5,0	5,6	8,2	6,7
Impact Strength-Rsd	%	59,5	9,5	11,6	17,9	20,8

#### 408 3.6 Puncture resistance

The maximum force, the peak at force (Figure 8) and the energy at break (Figure S25) were calculated from the puncture resistance test. Due to thickness differences between the films, results were corrected for thickness variations. In all cases, the addition of 5 wt% lignin decreased the puncture resistance, as can be seen for LDPE-1 and PCR-PE1. PE-GMA boosted the performance of the LDPE blend, slightly surpassing the LDPE values while PE-HEMA did not provide any improvement. For PCR-PE, PE-GMA restored the performance back to the original values, but interestingly, in this case PE-HEMA was a slightly more effective compatibilizer. Again, at high loading content such as in PCR-PE4, the material showed a brittle elastic fracture at a relatively low force which was not mitigated by the presence of the compatibilizer.

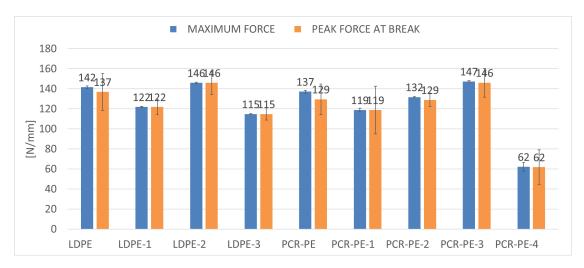


Figure 8. Puncture resistance measurement

#### 3.7 Antibacterial properties

Some LDPE-lignin films were subjected to the antibacterial test according to ISO22196 standard, using an LDPE film without any additive as control. To study the influence of the compatibilizer, we selected LDPE-1 (containing 5 wt% lignin), LDPE-2 (using additionally 1wt% PE-GMA) and LDPE-3 (using additionally 1wt% PE-HEMA), results are shown in Figure 9 (see Figure S26, Table S3 to S8 for additional details and analyses of variance). All LDPE films did not display any antibacterial activity towards *E. coli*. LDPE-1 showed a small bacterial reduction on *S. aureus* (log R = 1.2, i.e 94% reduction) which was only slightly enhanced in presence of PE-HEMA compatibilizer (LDPE-3: log R = 1.5, i.e 97% bacterial reduction). Interestingly the presence of PE-GMA compatibilizer in LDPE-2 provided a full bacterial reduction (log R > 4.3, i.e bacterial reduction >99.99%). A similar observation was made in our previous study on HDPE where films containing 5 wt% of a lignin extract with high phenolic content displayed antibacterial properties only towards the gram-positive bacteria *S. aureus*. This result was consistent with the fact that gram-positive bacteria are more sensitive towards antibacterial

substances than gram-negative bacteria because of their cell wall structure which is protected by an outer membrane.<sup>27</sup> These current results further showed that the antibacterial effect might not only be related to the homogeneity and compatibility of the composites, since PE-GMA led to lower performance in terms of mechanical resistance compared to PE-HEMA. The understanding on the bactericidal action of phenolic compounds remains vague.<sup>28</sup> In the present case, the lignin molecules being fully embedded in the matrix, a migrating phenomenon leading to lignin's penetration through the cytoplasmic membrane is unlikely. Additionally, it was recently shown that polyphenols exhibit different antibacterial activity on different type of bacteria.<sup>29</sup> They could be very active against one strain and completely ineffective against another and no clear correlation could be made with the class of polyphenols. However, the dominant hypothesis of mechanism of action of polyphenols is that of an accumulation on bacterial surface, <sup>30</sup> which would be linked to the polyphenol hydrophobicity.<sup>31</sup> Thus, it is possible that the effect of the compatibilizer on the antimicrobial activity of the film results from the interaction between the compatibilizer and lignin leading to the formation of a complex with higher hydrophobicity that lignin alone.

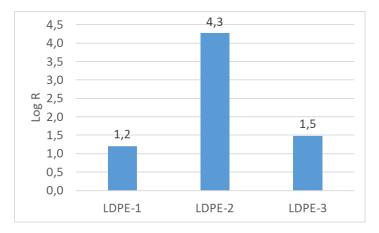


Figure 9. Bacterial reduction (in Log R) of S. Aureus of lignin containing films compared to a LDPE film

## Conclusion

The objective of this work was to assess the effect of two distinct compatibilizers on the performances of PE-lignin blends, with mulching as targeted application. LDPE and PCR-PE were successfully blended with a lignin sample containing a high phenolic content, allowing the production of composites as molded parts and films. The results showed that the effect depends both on the structure and content of the plasticizer. Depending on the test and the original PE resin, PE-HEMA and PE-GMA performed differently but overall, PE-GMA proved to be a more effective compatibilizer in terms of film quality and antimicrobial properties. The use of compatibilizers enhanced the antioxidant properties which reached more than 3 h OIT when lignin was present at 20 wt% and beyond. The photo-permeability of the materials was also decreased, reaching a transmittance lower than 5% throughout the whole measurement range (200 - 800 nm) when 20 wt% of lignin was used in PCR. Additionally, good antibacterial properties were obtained on Grampositive bacteria when using PE-GMA as compatibilizer. While higher lignin contents led to a more brittle material, processable films were achieved for both LDPE and PCR at 5 wt% lignin content. At higher lignin contents, the compatibilizer failed to maintain some key properties such as the strain at break in transversal direction, the puncture resistance and the overall processability of the material became more difficult. However, it was demonstrated that lignin contents up to 30 wt%) can be potentially used in LDPE with an improvement of some materials' properties (antioxidant, UV protection) beneficial for mulching film applications. Additionally, it was shown that it is possible to use PCR made from different PE samples, instead of virgin plastic, while achieving similar

472 473	properties. These materials are thus promising candidates for mulching film application where PCR, which still lacks proper high-volume market applications, is more and more used.
474	ASSOCIATED CONTENT
475 476	<b>Supporting information</b> . Experimental data, TGA, DSC, Haze, Gloss, mechanical properties (tensile, Izod impact, puncture resistance) and antibacterial tests of materials tested.
477	AUTHOR INFORMATION
478	Corresponding Authors
479	* (J.V.) E-mail: jerome.vachon@sabic.com
480	<b>Author Contributions</b>
481 482	The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.
483	Notes
484 485	The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.
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493	ABBREVIATIONS
494 495 496 497 498 499 500 501	HDPE: high density polyethylene; LDPE: low density polyethylene; LLDPE: linear low density polyethylene; PCR: Post-Consumer recycled; HEMA: 2-hydroxyethyl methyl acrylate; GMA: glycidyl methacrylate; RPM: Revolutions per minute; OIT: Oxidation Induction Time; NMR: Nuclear Magnetic Resonance; TGA: thermogravimetric analysis; DSC: differential scanning calorimetry; $\Delta$ Hm: enthalpy of melting; $\Delta$ Hc: enthalpy of crystallization; Tc: crystallization temperature; Tm: melting temperature; Xc: degree of crystallinity: TD: transverse direction; MD: machine direction

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