

#### WAVES 2019

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#### DE LA RECHERCHE À L'INDUSTRIE

A high order impedance boundary condition with unique solution for the time harmonic Maxwell's equations

August 27, 2019

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## **Cea** Summary of the talk

- ► The industrial context
- High Order Impedance Boundary Condition (HOIBC)
- Sufficient Uniqueness Conditions (SUC)
- Constrained optimisation problem
- Integrals Equations (IE) with HOIBC
- Numerical results
- Outlooks & conclusion

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- $\blacktriangleright \vec{u}$  is a vector of  $\mathbb{R}^2$  or  $\mathbb{R}^3$
- ► A, B (capital) are matrices
- $\blacktriangleright$  Vectorial product is denoted by  $\times$
- Let  $\vec{\mathcal{H}} = \sqrt{\mu_0/\epsilon_0} \vec{H}$
- Time harmonic Maxwell ( $e^{i\omega t}$ ) equations read ( $k_0 = \omega \sqrt{\mu_0 \epsilon_0}$ )

$$\begin{cases} \vec{\nabla} \times \vec{E} + ik_0 \mu_r \, \vec{\mathcal{H}} = \mathbf{0} \\ \vec{\nabla} \times \vec{\mathcal{H}} - ik_0 \epsilon_r \, \vec{E} = \mathbf{0} \end{cases}$$

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# The industrial context

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### Cea The industrial context

**Object : a coating of arbitrary materials over a smooth perfect electric conductor (PEC)** 



Goal: compute accurately the Radar Cross Section (RCS) of the coated object

- For any incidence angle
- For various materials
- For the high frequency spectrum and microwaves



 $\operatorname{RCS} = \lim_{R \to \infty} 4\pi R^2 \left( \frac{\left| \vec{E}_s \right|^2}{\left| \vec{E}_{smax} \right|^2} \right)$ 

## Cea The chosen method

This talk :

- Integral Equation + Impedance Boundary Condition (IBC)
  - Need to mesh only the exterior surface of the object
  - Accuracy depends essentially on the impedance boundary condition
  - Once integral equation solutions are obtained, RCS can be deduced

Another talk :

High order transmission conditions for a Domain Decomposition Method applied to an efficient and accurate solution of EM scattering problems.
 B. Stupfel, <u>M. Lecouvez</u>, CEA, WAVES, Vienna, 29/08/19



# **High Order Impedance Boundary Condition**

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# Cea The impedance operator

From **M. Cessenat**, *Mathematical Methods in Electromagnetism: Linear Theory and Applications*, vol. 41. WORLD SCIENTIFIC, 1996, it is known that



There are few cases where this operator can be used numerically

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## C22 The symbol of the impedance operator

Under the following hypothesis

- Simple geometry: infinite plane, infinite cylinder, sphere
- Each layer has spatially uniform parameters (  $\epsilon_r$ ,  $\mu_r$ , thickness )

One can deduce the expression of the Fourier multiplier  $\hat{Z}$ .

- **D. J. Hoppe and Y. Rahmat-Samii**, Impedance boundary conditions in electromagnetics. Taylor & Francis, 1995.
- D. Cheng, Y. Zhao, and W. Lin, Spectral impedance boundary condition (SIBC) method for a spherical perfect electric conductor (PEC) with an uniform biisotropic coating, J. Phys. III France, vol. 3, no. 9, pp. 1861–1870, 1993.



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#### High Order Impedance Boundary Condition (HOIBC)

- An impedance boundary condition (IBC) is an approximation of the impedance operator.
- The Leontovich IBC has a constant symbol  $(\hat{Z}(\vec{k}, \omega) \simeq a_0)$ 
  - Exact for normal incidence
- HOIBC is defined as a polynomial fraction

$$(I + b_1 \mathcal{L}_D - b_2 \mathcal{L}_R)\vec{E_t} = (a_0 I + a_1 \mathcal{L}_D - a_2 \mathcal{L}_R)(\vec{n} \times \vec{\mathcal{H}})$$

**A. Aubakirov.** Electromagnetic scattering problem with higher order impedance boundary conditions and integral methods. General Mathematics. Université de Cergy Pontoise, 2014.

The following properties are used

- $\mathcal{L}_D \vec{U} = \overrightarrow{\nabla_t} \overrightarrow{\nabla_t} \cdot \vec{U} \Rightarrow \int_{\Gamma} \mathcal{L}_D \vec{U} \cdot \vec{\vec{U}} \le 0$   $\mathcal{L}_R \vec{U} = \overrightarrow{\nabla_t} \times (\overrightarrow{\nabla_t} \times \vec{U}) \Rightarrow \int_{\Gamma} \mathcal{L}_R \vec{U} \cdot \vec{\vec{U}} \ge 0$
- $\mathcal{L}_D \mathcal{L}_R = \mathcal{L}_R \mathcal{L}_D = 0$

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#### Cea High Order Impedance Boundary Condition (HOIBC)

The HOIBC gives the following Fourier multiplier

$$\widehat{Z} = \left(I + b_1 \widehat{L_D} - b_2 \widehat{L_R}\right)^{-1} \left(a_0 I + a_1 \widehat{L_D} - a_2 \widehat{L_R}\right)$$

Where

$$\widehat{L_D} = -\begin{bmatrix} k_x^2 & 0\\ 0 & 0 \end{bmatrix} \qquad \widehat{L_R} = \begin{bmatrix} 0 & 0\\ 0 & k_x^2 \end{bmatrix}$$

#### Our goal is to

Compute HOIBC coefficients that best fit  $\hat{Z}$  for any  $\vec{k}$ 

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#### Cea High Order Impedance Boundary Condition (HOIBC)

Methods to compute HOIBC coefficients

- ► Taylor/Pade
  - O. Marceaux & B. Stupfel. High-order impedance boundary conditions for multilayer coated 3-D objects. Antennas and Propagation, IEEE Transactions on. 48. 429 - 436. 2000.
- Collocation
  - A. Aubakirov. Electromagnetic scattering problem with higher order impedance boundary conditions and integral methods. General Mathematics. Université de Cergy Pontoise, 2014.

#### Least square minimisation

B. Stupfel, Implementation of High-Order Impedance Boundary Conditions in Some Integral Equation Formulations. IEEE Transactions on Antennas and Propagation. (2015).



# **Sufficient Uniqueness Conditions**

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#### **Cea** The General Sufficient Uniqueness Condition (GSUC)

From Cessenat, we recall the General Sufficient Uniqueness Condition

$$\Re\left(\int_{\Gamma} \underbrace{\left(n(\vec{x}) \times \vec{\mathcal{H}}(\vec{x})\right)}_{\vec{j}} \cdot \overline{\vec{E_t}}(\vec{x}) ds(\vec{x})\right) \ge 0$$

This condition enforce uniqueness of Maxwell solution.

Using the HOIBC with the properties of  $\mathcal{L}_D$ ,  $\mathcal{L}_R$  operators, we will find SUC that enforce the GSUC.

#### **Cea** Sufficient Uniqueness Conditions (SUC)

The HOIBC reads  $(I + b_1 \mathcal{L}_D - b_2 \mathcal{L}_R) \overrightarrow{E_t} = (a_0 I + a_1 \mathcal{L}_D - a_2 \mathcal{L}_R) \overrightarrow{I}$ ▶ HOIBC with  $a_1 = a_2 = b_1 = b_2 = 0$  (Leontovich)  $\Re(a_0) \geq 0$ • HOIBC with  $b_1 = b_2 = 0$  $\Re(a_0) \ge 0$ •  $\Re(a_1) \leq 0$ •  $\Re(a_2) \leq 0$ HOIBC  $-\Re(\overline{a_0}z) \le 0$  $\Re(\overline{a_1}z) \le 0$ •  $-\Re(b_1\overline{a_1}) \le 0$ •  $\Re(b_1 a_0 \overline{a_1 a_2}) \le 0$ •  $-\Re(b_2\overline{a_2}) \le 0$ •  $\Re(b_2 a_0 \overline{a_1 a_2}) \leq 0$  $\Re(\overline{a_2}z) \le 0$ •  $\Re(a_2) \leq 0$ •  $\Re(a_1) \leq 0$ Where  $z = |a_1| |a_2|^2 - b_1 a_0 \overline{a_1} |a_2|^2 - b_2 a_0 \overline{a_2} |a_2|^2$ 

Other SUC exist

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Find 
$$x = (a_0, a_1, a_2, b_1, b_2) \in \mathbb{C}^5$$
 that minimises  

$$F(x) = \frac{1}{2} ||Ax - b||_2^2 \quad \forall x \in \underbrace{\mathbb{C}}_{SUC}$$

Where

$$b_{i} = \hat{Z}(\overrightarrow{k_{i}})_{11}$$

$$b_{i+1} = \hat{Z}(\overrightarrow{k_{i}})_{12}$$

$$b_{i+2} = \hat{Z}(\overrightarrow{k_{i}})_{21}$$

$$b_{i+3} = \hat{Z}(\overrightarrow{k_{i}})_{22}$$

$$\begin{aligned} A_{i,:} &= \begin{bmatrix} 1 & L_D(\vec{k}_i)_{11} & -L_R(\vec{k}_i)_{11} & -(\hat{Z}(\vec{k}_i)L_D(\vec{k}_i))_{11} & (\hat{Z}(\vec{k}_i)L_R(\vec{k}_i))_{11} \end{bmatrix} \\ A_{i+1,:} &= \begin{bmatrix} 0 & L_D(\vec{k}_i)_{12} & -L_R(\vec{k}_i)_{12} & -(\hat{Z}(\vec{k}_i)L_D(\vec{k}_i))_{12} & (\hat{Z}(\vec{k}_i)L_R(\vec{k}_i))_{12} \end{bmatrix} \\ A_{i+2,:} &= \begin{bmatrix} 0 & L_D(\vec{k}_i)_{21} & -L_R(\vec{k}_i)_{21} & -(\hat{Z}(\vec{k}_i)L_D(\vec{k}_i))_{21} & (\hat{Z}(\vec{k}_i)L_R(\vec{k}_i))_{21} \end{bmatrix} \\ A_{i+3,:} &= \begin{bmatrix} 1 & L_D(\vec{k}_i)_{22} & -L_R(\vec{k}_i)_{22} & -(\hat{Z}(\vec{k}_i)L_D(\vec{k}_i))_{22} & (\hat{Z}(\vec{k}_i)L_R(\vec{k}_i))_{22} \end{bmatrix} \end{aligned}$$

Gradient based method (SLSQP)

#### Calderon multiplier of an infinite plane

 $\epsilon_r = 1 - i, \mu_r = 1, d = 5 \text{ cm}, f = 200 \text{ MHz}$ 



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## Cea The case of one layer of a lossless material

One layered lossless materials ( $\Im(\epsilon_r) = \Im(\mu_r) = 0$ ) are such that there exists  $s_{\infty} \in \mathbb{R}$  where  $\hat{Z}(k_0 s_{\infty}, 0) = \infty$ 

E.g.,  $\exists n \in \mathbb{N}$ 

$$s_{\infty} = \sqrt{\epsilon_r \mu_r - \left(\frac{\pi/2 + n\pi}{k_0 d}\right)^2}$$

It is mandatory to force  $b_1 = b_2 = (k_0 s_{\infty})^{-2}$  and remove them from the optimisation

# Calderon multiplier of an infinite plane coated with a lossless material

P. Soudais, ICEAA Conference, Verona, 2017  $\epsilon_r = 4, \mu_r = 1, d = 3.5 \text{ mm}, f = 12 \text{ GHz}$ 



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#### **RCS of a sphere (R=1m) coated with a lossless material**

 $\epsilon_r = 4, \mu_r = 1, d = 3.5 \text{ mm}, f = 12 \text{GHz}, \theta_{inc} = 0^{\circ}$ 



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# **Integral Equations with HOIBC**

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From J.-C. Nédélec, Acoustic and Electromagnetic Equations: Integral Representations for Harmonic Problems. Springer Science & Business Media, 2001



The standard EI are the Electric Field Integral Equation (EFIE) and the Magnetic Field Integral Equation (MFIE).

Unknowns are

$$\vec{J} = \vec{n} \times \vec{\mathcal{H}}, \vec{M} = \vec{n} \times \vec{E} \quad \in H_{div}(\Gamma)$$

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#### **Ceal** Expression of the HOIBC in Integral Equations

► EFIE  

$$\int_{\Gamma} \overline{E_t^{inc}}(\vec{x}) \cdot \vec{\phi}(\vec{x}) ds(\vec{x}) (\vec{x})$$

$$= ik_0 \int_{\Gamma} \left( \int_{\Gamma} G(\vec{x} - \vec{y}) \vec{f}(\vec{y}) ds(\vec{y}) \right) \cdot \vec{\phi}(\vec{x}) ds(\vec{x})$$

$$- \frac{i}{k_0} \int_{\Gamma} \left( \int_{\Gamma} G(\vec{x} - \vec{y}) \vec{\nabla} \cdot \vec{f}(\vec{y}) ds(\vec{y}) \right) \vec{\nabla} \cdot \vec{\phi}(\vec{x}) ds(\vec{x})$$

$$- \int_{\Gamma} \left( \int_{\Gamma} \vec{\nabla} G(\vec{x} - \vec{y}) \times \vec{M}(\vec{y}) ds(\vec{y}) \right) \cdot \vec{\phi}(\vec{x}) ds(\vec{x}) + \frac{1}{2} \int_{\Gamma} \overline{E_t}(\vec{x}) \cdot \vec{\phi}(\vec{x}) ds(\vec{x})$$

$$= -ik_0 \int_{\Gamma} \left( \int_{\Gamma} G(\vec{x} - \vec{y}) \vec{M}(\vec{y}) ds(\vec{y}) \right) \cdot \vec{\phi}(\vec{x}) ds(\vec{x})$$

$$+ \frac{i}{k_0} \int_{\Gamma} \left( \int_{\Gamma} G(\vec{x} - \vec{y}) \vec{\nabla} \cdot \vec{M}(\vec{y}) ds(\vec{y}) \right) \vec{\nabla} \cdot \vec{\phi}(\vec{x}) ds(\vec{x})$$

$$- \int_{\Gamma} \left( \int_{\Gamma} \vec{\nabla} G(\vec{x} - \vec{y}) \times \vec{f}(\vec{y}) ds(\vec{y}) \right) \cdot \vec{\phi}(\vec{x}) ds(\vec{x}) + \frac{1}{2} \int_{\Gamma} \overline{\mathcal{H}_t}(\vec{x}) \cdot \vec{\phi}(\vec{x}) ds(\vec{x})$$

**Ceal** Integration of HOIBC in Integral Equations

$$\frac{1}{2} \int_{\Gamma} \vec{E}_t \cdot \vec{\phi} = \frac{1}{2} \int_{\Gamma} \left( (a_0 + a_1 \mathcal{L}_D - a_2 \mathcal{L}_R) \vec{J} - (b_1 \mathcal{L}_D - b_2 \mathcal{L}_R) \vec{E}_t \right) \cdot \vec{\phi}$$

$$\frac{1}{2} \int_{\Gamma} \vec{\mathcal{H}}_t \cdot \vec{\phi} = \frac{1}{2} \int_{\Gamma} \vec{J} \cdot (\vec{n} \times \vec{\phi})$$

$$= \frac{1}{2a_0} \int_{\Gamma} \left( (I + b_1 \mathcal{L}_D - b_2 \mathcal{L}_R) \vec{E}_t - (a_1 \mathcal{L}_D - a_2 \mathcal{L}_R) \vec{J} \right) \cdot (\vec{n} \times \vec{\phi})$$

$$= \frac{1}{2a_0} \int_{\Gamma} \left( -(I - b_1 \mathcal{L}_R + b_2 \mathcal{L}_D) \vec{M} - (-a_1 \mathcal{L}_R + a_2 \mathcal{L}_D) (\vec{\mathcal{H}}_t) \cdot \vec{\phi} \right)$$

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## Cea The functional space Hdiv

FEM method: Let  $\Gamma_h$  be a triangular meshing of  $\Gamma$ Raviart-Thomas function : let  $(\overrightarrow{\phi_i})_i$  be the basis of  $H_{div}(\Gamma_h)$ 



$$\vec{J} \Rightarrow \sum_{j=1}^{N} I_j \vec{\phi_j}, \vec{M} \Rightarrow \sum_{j=1}^{N} m_j \vec{\phi_j}$$

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#### **Ceal** Representation of LD and LR operators

By definition

$$\int_{\Gamma_h} \mathcal{L}_D(\overrightarrow{\phi_i}) \cdot \overrightarrow{\phi_j} = -\int_{\Gamma_h} \vec{\nabla} \cdot (\overrightarrow{\phi_i}) \vec{\nabla} \cdot (\overrightarrow{\phi_j}) \coloneqq L_{D_{ij}}$$
$$\int_{\Gamma_h} \mathcal{L}_R(\vec{n} \times \overrightarrow{\phi_i}) \cdot (\vec{n} \times \overrightarrow{\phi_j}) = -\int_{\Gamma_h} \mathcal{L}_D(\overrightarrow{\phi_i}) \cdot \overrightarrow{\phi_j}$$

Problems arise with

$$\int_{\Gamma_h} \underbrace{\mathcal{L}_R}_{rot} \left( \overrightarrow{\phi_i} \right) \cdot \overrightarrow{\phi_j} = - \int_{\Gamma_h} \mathcal{L}_D \left( \overrightarrow{n} \times \overrightarrow{\phi_i} \right) \cdot \left( \overrightarrow{n} \times \overrightarrow{\phi_j} \right)$$



 B. Stupfel, Implementation of High-Order Impedance Boundary Conditions in Some Integral Equation Formulations. IEEE Transactions on Antennas and Propagation. (2015).

Let  $\Pi$  be the projection  $\Pi(\overrightarrow{\phi_i}) = \sum_{j=1}^{N} P_{ji} \overrightarrow{p_j}$  $\int_{\Gamma_h} \Pi(\overrightarrow{\phi_i}) \cdot \mathcal{L}_R(\Pi(\overrightarrow{\phi_j})) = \sum_{l=1}^{N} \sum_{m=1}^{N} P_{li} P_{mj} \int_{\Gamma_h} \left(\overrightarrow{p_l} \cdot \mathcal{L}_R(\overrightarrow{p_m})\right)$   $= -\sum_{l=1}^{N} \sum_{m=1}^{N} P_{li} P_{mj} \int_{\Gamma_h} \left(\overrightarrow{\phi_l} \cdot \mathcal{L}_D(\overrightarrow{\phi_m})\right)$   $= -(P^t L_D P)_{ij}$ 

• We define  $L_R$  as  $-P^t L_D P$ 

-  $L_{R_{ij}}$  is an approximate of  $\int_{\Gamma_h} (\overrightarrow{\phi_i}) \cdot \mathcal{L}_R(\overrightarrow{\phi_j})$ 

Which projection ???

## Cea The projection

A. Bendali *et al*, *A boundary-element solution of the Leontovich problem*, IEEE Transactions on Antennas and Propagation, vol. 47, no. 10, pp. 1597–1605, 1999
 They are written (q<sub>i</sub>)<sub>i</sub>



# Cea Dealing with Et

We still need to approximate

$$\int_{\Gamma_{h}} (b_{1}\mathcal{L}_{D} - b_{2}\mathcal{L}_{R})\overrightarrow{E_{t}} \cdot \overrightarrow{\phi_{i}}$$
  
Since by definition,  $\overrightarrow{E_{t}} = -\overrightarrow{n} \times \overrightarrow{M}$ 
$$\int_{\Gamma_{h}} (b_{1}\mathcal{L}_{D} - b_{2}\mathcal{L}_{R})\overrightarrow{E_{t}} \cdot \overrightarrow{\phi_{i}} = \sum_{j=1}^{N} m_{j} \int_{\Gamma_{h}} (b_{1}\mathcal{L}_{D} - b_{2}\mathcal{L}_{R})\overrightarrow{p_{j}} \cdot \overrightarrow{\phi_{i}}$$
$$\simeq \sum_{j=1}^{N} \sum_{l=1}^{N} m_{j}P_{lj} \int_{\Gamma_{h}} (b_{1}\mathcal{L}_{D} - b_{2}\mathcal{L}_{R})\overrightarrow{\phi_{l}} \cdot \overrightarrow{\phi_{i}}$$
$$\simeq \left( (b_{1}L_{D} - b_{2}L_{R})P \underline{m} \right)_{i}$$

Cealing with Ht

► Same goes for

$$\begin{split} &\int_{\Gamma_h} (a_1 \mathcal{L}_D - a_2 \mathcal{L}_R) (\vec{n} \times \overrightarrow{\mathcal{H}_t}) \cdot (\vec{n} \times \overrightarrow{\phi_i}) \\ &= -\int_{\Gamma_h} (a_1 \mathcal{L}_R - a_2 \mathcal{L}_D) \overrightarrow{\mathcal{H}_t} \cdot \overrightarrow{\phi_i} \\ &\simeq -\sum_{j=1}^N I_j \int_{\Gamma_h} (a_1 \mathcal{L}_R - a_2 \mathcal{L}_D) \overrightarrow{p_j} \cdot \overrightarrow{\phi_i} \\ &\simeq -\sum_{j=1}^N \sum_{l=1}^N I_j P_{lj} \int_{\Gamma_h} (a_1 \mathcal{L}_R - a_2 \mathcal{L}_D) \overrightarrow{\phi_l} \cdot \overrightarrow{\phi_i} \\ &\simeq -\left( (a_1 \mathcal{L}_R - a_2 \mathcal{L}_D) P \underline{I} \right)_i \end{split}$$

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Let  $M = G^{\phi\phi}$ 

The IBC0 gives

$$\left( \begin{bmatrix} A & B \\ B & -A \end{bmatrix} + \frac{1}{2} \begin{bmatrix} a_0 M & 0 \\ 0 & -\frac{M}{a_0} \end{bmatrix} \right) \begin{bmatrix} \underline{I} \\ \underline{m} \end{bmatrix} = \begin{bmatrix} \underline{b}_E \\ \underline{b}_H \end{bmatrix}$$

The HOIBC gives

$$\begin{pmatrix} \begin{bmatrix} A & B \\ B & -A \end{bmatrix} + \frac{1}{2} \begin{bmatrix} a_0 M + a_1 L_D - a_2 L_R & -(b_1 L_D - b_2 L_R)P \\ -\frac{(a_1 L_R - a_2 L_D)}{a_0}P & -\frac{(M - b_1 L_R + b_2 L_D)}{a_0} \end{bmatrix} \end{pmatrix} \begin{bmatrix} \underline{I} \\ \underline{m} \end{bmatrix} = \begin{bmatrix} \underline{b_E} \\ \underline{b_H} \end{bmatrix}$$

Full (2N x 2N) matrix
Sparse (2N x 2N) matrix

#### **CCO** RCS of a sphere (R=1m) with 4240 triangles

 $\varepsilon = 1 - i, \mu = 1, d = 0.05 \text{m}, f = 0.2 \text{ GHz} \text{ (meshed } \lambda_0 / 18 \text{)}, \theta_{inc} = 0^{\circ}$ 



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#### **RCS of a cone-sphere (** $\alpha$ = 8°, L=2m) with 11352 triangles

 $\varepsilon = 1 - i, \mu = 1, d = 5$  cm, f = 200 MHz (meshed  $\lambda_0/55$ ),  $\theta_{obs} = \theta_{inc}$ 



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## Cea Conclusion & outlooks

#### Conclusion

- HOIBC outperforms Leontovich
- SUC can be applied
- Computational time of HOIBC coefficients is negligible
- Easily interfaced with BEM codes

Outlooks

More HOIBC and corresponding SUC



# Thanks for your attention

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