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1 **Stable flexible transparent electrodes for localized heating of lab-on-a-chip devices**

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30 14 Keywords: transparent heaters, spatial atomic layer deposition, microfluidics, chip, selective
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32 15 heating, in situ, DNA

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35
36 17 Abstract

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38 18
39 19 *In situ* biological observations require stable, accurate and local temperature control of
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41 20 specimen. Several heating elements are coupled with microfluidic systems, but few of them are
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43 21 transparent to visible light and therefore compatible with microscopic observation. Traditional
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45 22 transparent electrodes such as indium tin oxide, still suffer from high fabrication cost and
46
47 23 brittleness, which is not fully compatible to emerging microfluidic devices. Here, we propose
48
49 24 a lightweight, low-cost, flexible transparent heater based on percolating silver nanowire
50
51 25 networks, protected with a transparent zinc oxide film, for the *in situ* monitoring of biological
52
53 26 experiments. Using the fluorescence of dyes bound to double-stranded DNA to monitor its
54
55 27 temperature *in situ*, we demonstrate that such nanocomposites allow rapid and reproducible
56
57 28 heating under low applied voltage. Furthermore, selective heating is achieved in different zones
58
59 29 of the same microchannel or for adjacent microchannels of the chip heating at different
60
61 30 temperatures, with a single transparent heater and bias.

1. Introduction

In situ microscopic observations of biological samples are often conducted in bulky environmental chambers to maintain the proper environment of the cells (temperature, oxygen, pH). Alternatively, several small size heating elements have been developed for lab-on-a-chip devices, but many of them are either complicated or difficult to be mounted, some could have potential water leaks or are not transparent.^[1-4] Temperatures of interest range from 30-42 °C for most cell cultures, to 50-95 °C cycles for DNA amplification by Polymerase Chain Reaction (PCR).^[3] A few transparent heaters (TH) compatible with biological microscopy observations have been presented in the literature. These studies report the design of PCR microfluidic chips using indium tin oxide (ITO) or graphene as heating elements.^[5-7] However, they did not monitor the temperature *in situ* and they do not offer localized and selective heating. In addition, ITO, which is so far the most commonly used transparent conductive material, apart from the limitations based on the indium scarcity and fabrication cost, is challenging to integrate and reuse into microfluidic devices due to its brittleness. Among alternative transparent electrodes investigated in the last decade, silver nanowire (AgNW) networks are one of the most promising emerging technologies.^[8-12] Combining low-cost, solution-based fabrication, flexibility, transparency, and high heating performances at low voltage supply, AgNW networks offer a clear asset for integration in TH applications.^[13-15] However, bare AgNW networks exhibit degradation of their properties with time or under thermal or electrical stress^[16-18]. This can be counteracted by covering them with a thin protective layer of metal oxide; the resulting composite electrode shows excellent electrical stability and durability.^[19-21] To the best of our knowledge, TH based on AgNW had not yet been coupled to microfluidic chips, for the *in situ* monitoring of biological observations.

Here we propose a lightweight, and up-scalable TH based on AgNW networks that can easily be integrated into a lab-on-a-chip in an optical microscope. We make use of the well-known denaturation-renaturation cycles of double-stranded DNA (dsDNA) to monitor the fluid temperature *in situ* using SYBR Green I fluorescence. We demonstrate the stable and reproducible heating performance of the TH by encapsulating the AgNW network with thin, protective zinc oxide (ZnO) layer using an open-air scalable ALD approach, namely, atmospheric-pressure spatial atomic layer deposition (AP-SALD), at rather low-temperature (≤ 200 °C).^[22-25] The electrical resistance of such AgNW/ZnO nanocomposite remains the same (10-15 Ω) after several bending cycles or hours of electrical or thermal stress. Following the appropriate calibration of the devices (based on the temperature measurements at several points

65 of the setup), the temperature inside the chip channels can be accurately controlled by supplying
66 a low voltage (<6.5 V) to drive the denaturation-renaturation processes. Furthermore, we
67 demonstrate that the localized heating of the lab-on-a-chip (i.e. heating of different sections of
68 a microchannel or of adjacent channels in a chip at different temperatures) is possible using a
69 single TH element and power source unit. In the present work, we used 3D-printed masks on
70 top of the AgNW networks, during spray-coating deposition, to create specific regions of
71 different network densities and thus local electrical resistivity. This constitutes a low-cost and
72 versatile approach that is compatible to scalable screen-printing techniques,^[26,27] and excludes
73 lithography, or other cleanroom patterning processes,^[28–30] or other more complex strategies
74 like laser-induced local heating.^[31]

76 2. Results & Discussion

77 2.1 Fabrication and integration of Transparent Heaters into lab-on-a-chip device

78
79 AgNW based flexible TH, encapsulated by a protective oxide thin coating, were fabricated by
80 scalable open-air and low-temperature processes, as schematically represented in **Figure 1a**.
81 First, AgNWs (Figure 1b) were deposited on glass or polymer substrates using a homebuilt
82 pneumatic spray system, with the targeted electrical resistance of 10-15 Ω/sq and optical
83 transparency of $\sim 85\%$ (including substrate contribution).^[32] In terms of the amount of silver
84 and considering the dimensions of the nanowires used in the present work, these properties
85 correspond to a network areal mass density (*amd*) of 70 ± 5 mg/m^2 .^[23] AgNW networks were
86 then coated with thin ZnO films deposited by AP-SALD.^[33] The thickness of ZnO was fixed at
87 30 ± 5 nm to ensure electrode stability (see previous reports and below for more details).^[16,21]
88 The temperature and duration of ZnO deposition (200°C for less than 1.5 min) are compatible
89 with the corresponding values of time-of-failure, as reported by Resende et al.,^[32] and respect
90 the stability of the AgNW network. Other recently published studies confirm that thermally-
91 sensitive materials are not affected by the oxide deposition by spatial ALD techniques, thanks
92 to their short processing times.^[34] Finally, silver paste contacts were applied on the two opposite
93 sides of the AgNW/ZnO specimen and copper wires (2 mm in diameter) were bonded to the
94 silver paste to connect the TH to the power supply. The fabrication process is compatible with
95 roll-to-roll (R2R) and other high throughput in-line processes, i.e. sheet-to-sheet. The
96 reproducibility can be statistically demonstrated on the optical properties of up to 130 spray-

97 deposited networks, showing a standard deviation of $\pm 1.1\%$ for the total transmittance (Figure
98 S1a).

99 TEM imaging of bare AgNWs is reported in Figure 1b, while Figure 1c demonstrates the
100 conformal ZnO coating around the AgNWs. At lower magnification, SEM imaging (Figure 1d)
101 exhibits the random distribution of the network. The final TH can be glued to the microfluidic
102 chip using double-sided tape allowing stable bonding with the entire device, as shown in Figure
103 1e. The lab-on-a-chip can then be placed on the stage of an optical microscope, as presented in
104 Figure 1f. Thanks to the tape, the TH can be easily removed from the chip and reused later, as
105 needed. The IR image shown in Figure 1f reveals the heat generated by the TH upon applying
106 a voltage across the AgNW network. Additional pictures and video of the lab-on-a-chip
107 fabrication steps and integration to the microscope set-up can be found in Figure S2. The
108 fluorescence of the SYBR Green I dye bound to the dsDNA in the solution filling the chip
109 channels could be recorded *in situ* while the TH was heating (i.e. subjected to a voltage). The
110 dye can be excited with blue light ($\lambda_{max} = 497 \text{ nm}$) and emits green light ($\lambda_{max} = 520 \text{ nm}$).
111 Figure 1g presents an example of the evolution of the recorded fluorescence during heating with
112 a voltage ramp (1 V/min) up to 4.5 V, as well as the extrapolated temperature inside the channel.
113 SYBR Green I exhibits an exceptional affinity for DNA that results in a large fluorescence
114 enhancement upon DNA binding.^[35] The dye binds to the minor groove of dsDNA and does
115 not bind to single-stranded DNA (ssDNA). Therefore, a sudden drop in fluorescent signal
116 during the ramp can thus be associated with the DNA melting inside the chip, occurring at 80-
117 81°C. Therefore, thanks to AgNW/ZnO based transparent heater, by applying only few volts,
118 we can reach the DNA denaturation and observe it *in situ*. Following this principle, we
119 performed several experiments that are discussed in the present article.

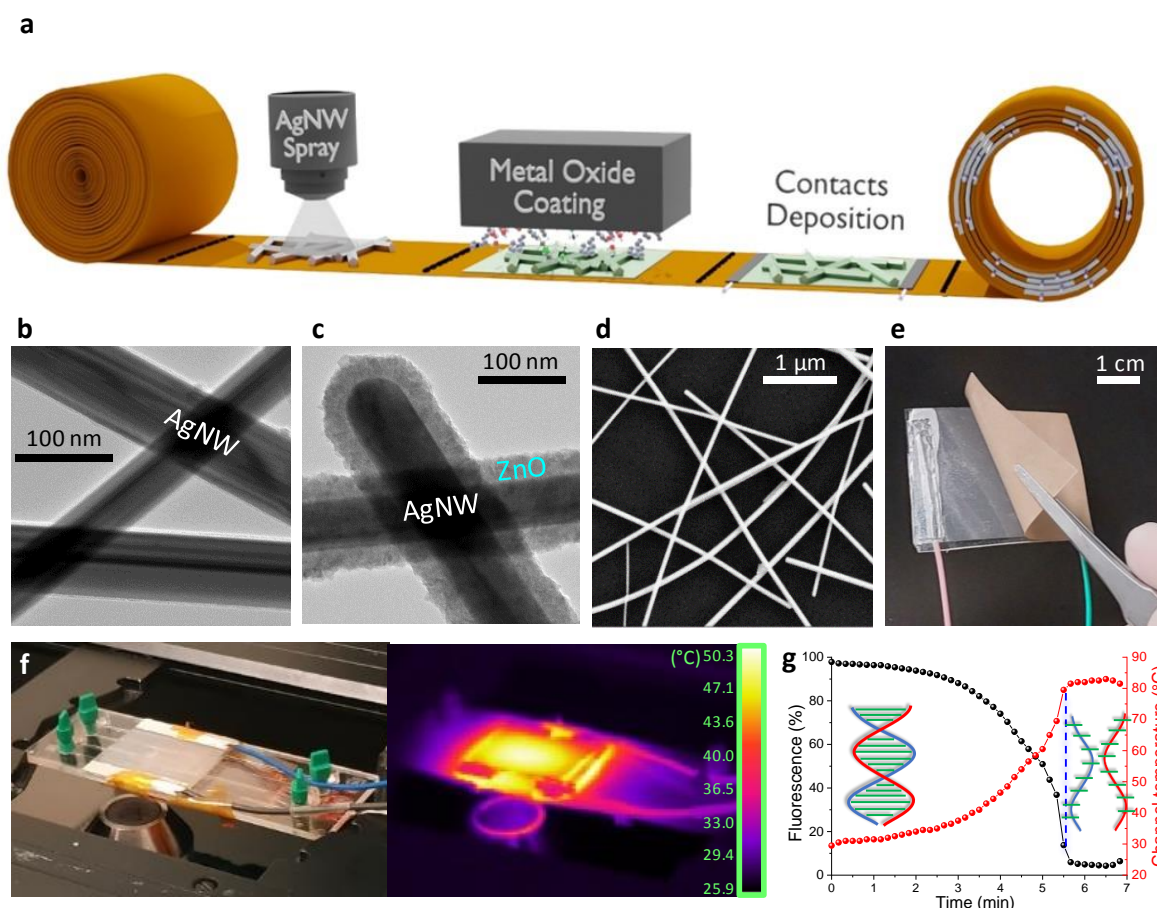


Figure 1. Fabrication of Transparent Heaters and integration into a microfluidic chip to realize a lab-on-a-chip for *in situ* fluorescence measurements. (a) Schematic representation of the fabrication of transparent heaters on flexible substrate, indicating its compatibility with roll-to-roll processes. First, silver nanowires (AgNW) in suspension are deposited by spray coating and then AgNWs are coated by a thin zinc oxide (ZnO) coating by open-air spatial atomic layer deposition. Finally, metallic contacts are deposited to supply the electric bias. (b) Transmission electron microscopy (TEM) image of bare AgNWs. (c) TEM image showing the conformal ZnO coating on the AgNW. The thickness of the coating is about 35 nm. (d) Scanning electron microscopy (SEM) image of a AgNW/ZnO network. (e) AgNW/ZnO based transparent heater (TH) with wires for the electrical connection, and one side stuck on a double-sided adhesive tape. By removing the protective light brown film of the tape, the TH is ready to be stuck to a chip. (f) Optical and infrared (IR) pictures of the lab-on-a-chip fabricated, placed on the stage of an optical microscope. By applying a low voltage, the TH heats the dsDNA in solution inside the chip microchannels. The fluorescence of the SYBR Green I dye, bound to the dsDNA, is recorded *in situ* during the heating. (g) Evolution of fluorescence (in black) during a voltage ramp up to 4.5 V and the extrapolated temperature (in red) inside the channel. The drastic drop

138 of the fluorescence occurs when the dsDNA reaches its melting point (dashed blue line). As
139 shown in the inset schema, the separation of the DNA strands during denaturation results in an
140 abrupt loss of fluorescence from the dye.

2.2 AgNW/ZnO based TH: properties, stability and reproducibility

143
144 **Figure 2a** exhibits the total transmittance of AgNW/ZnO network compared to bare AgNW
145 network, including the glass substrate contribution (i.e. without any substrate correction). Glass
146 transmittance is plotted as well for reference. The inset picture presents a typical AgNW/ZnO
147 TH specimen with silver paste electrodes. In the visible range (380-750 nm), there is a slight
148 decrease of the average transmittance from 82.0% to 80.1% due to the absorption/reflection of
149 the metal oxide coating (originated from plasmonic absorption). A slight increase was observed
150 for diffuse transmittance, from 5.5% to 6.2% while adding the ZnO coating (Figure S1b). This
151 increase can be explained by more diffuse scattering, this is associated with the light scattering
152 of the nanocomposite interfaces.^[36] Having a low fraction of diffuse transmission is essential
153 for the intended application since the larger the diffuse transmittance fraction, the hazier the
154 transparent heater, hindering somehow clear observations. In the NIR range (750-2500 nm),
155 there is also a slight influence of the ZnO coating, the average values of total transmittance are
156 (77.7±3.5)% and (76.8±3.7)% for bare and coated networks, respectively, while the diffuse
157 transmittance in NIR is (5.2±0.3)% and (5.6±0.3)%, respectively. These TH are therefore fully
158 compatible with microscope observations under transmitted illumination, i.e. phase-contrast
159 microscopy. Figure 2b demonstrates the good electro-mechanical properties of the transparent
160 heaters compared to ITO on PEN, commercially purchased from Sigma Aldrich, with an initial
161 sheet resistance of 55 Ω and film thickness of 300 nm. Both bare AgNW and AgNW/ZnO
162 networks show a very stable electrical resistance during 10000 bending cycles of 5 mm radius,
163 in the set-up shown in the inset of Figure 2b, while the ITO loses its high conductivity directly
164 after the first bending cycle.

165 The TH was subjected to 20 cycles of heating-cooling to investigate its stability, both for bare
166 and coated AgNW networks, between 50 and 120 °C with a ramp rate of ± 5 °C/min. As shown
167 in Figure 2c, the ZnO coated networks showed very stable electrical behaviour during 9 hours
168 of measurement, conversely to the bare AgNW networks, which already started degrading after
169 the second heating cycle. The resistance of the nanocomposites followed linearly the evolution
170 of the temperature and the final value after the 20 cycles was almost the same as the initial one

171 (increase of 0.65%) i.e. no network degradation took place. Furthermore, as reported in SI, the
172 stability of AgNW/ZnO based TH were evaluated also by 20 cycles of electrical stress with a
173 ramp of ± 0.5 V/min between 4 and 9 volts. The influence of the ZnO thickness in terms of
174 electrical stability during 20 voltage cycles is reported in the Figure S1c. Between the 10-100
175 nm range tested, the most stable was the 35 nm and thus it was fixed as optimum oxide thickness
176 value for the rest of the experiments involving the fabricated lab-on-a-chip presented here. The
177 fact that the optimal ZnO thickness appears to be 35 nm is slightly counterintuitive since one
178 could think that thicker coating could correspond to enhanced stability. However several
179 explanations can be proposed, and the prevailing one is the difference of thermal dilation
180 between the ZnO layer and the substrate which can induce structural defects in the layer and
181 leading to a weaker protection. A larger number of cracks in the ZnO layer can exist for thicker
182 ZnO coating.

183 Finally, the temperature of the sample was recorded during the voltage cycles by using a Pt100
184 thermocouple, to assess the generated Joule heating. Figure 2d, presents the temperature during
185 the 20 cycles, with a ramp rate of ± 0.5 V/min, along with the maximum value of relative change
186 of resistance in each cycle, for AgNW/ZnO TH with an initial resistance of 12.7Ω . The voltage
187 is varied between 4 and 9 V, which corresponds to a Joule heating of 70 and 140 °C,
188 respectively. It is important to note that these values were intentionally chosen as much higher
189 than the ones needed for the biological samples, in order to ensure a high durability of the THs.
190 Both the electrical resistance and the heating performance of the TH are very reproducible over
191 7 hours of applied electrical bias. In addition, during the present study, the AgNW/ZnO
192 specimens were used several times, i.e. 48 different biological experiments were carried out in
193 more than 6 months testing the same TH and the latter showed no electrical degradation.

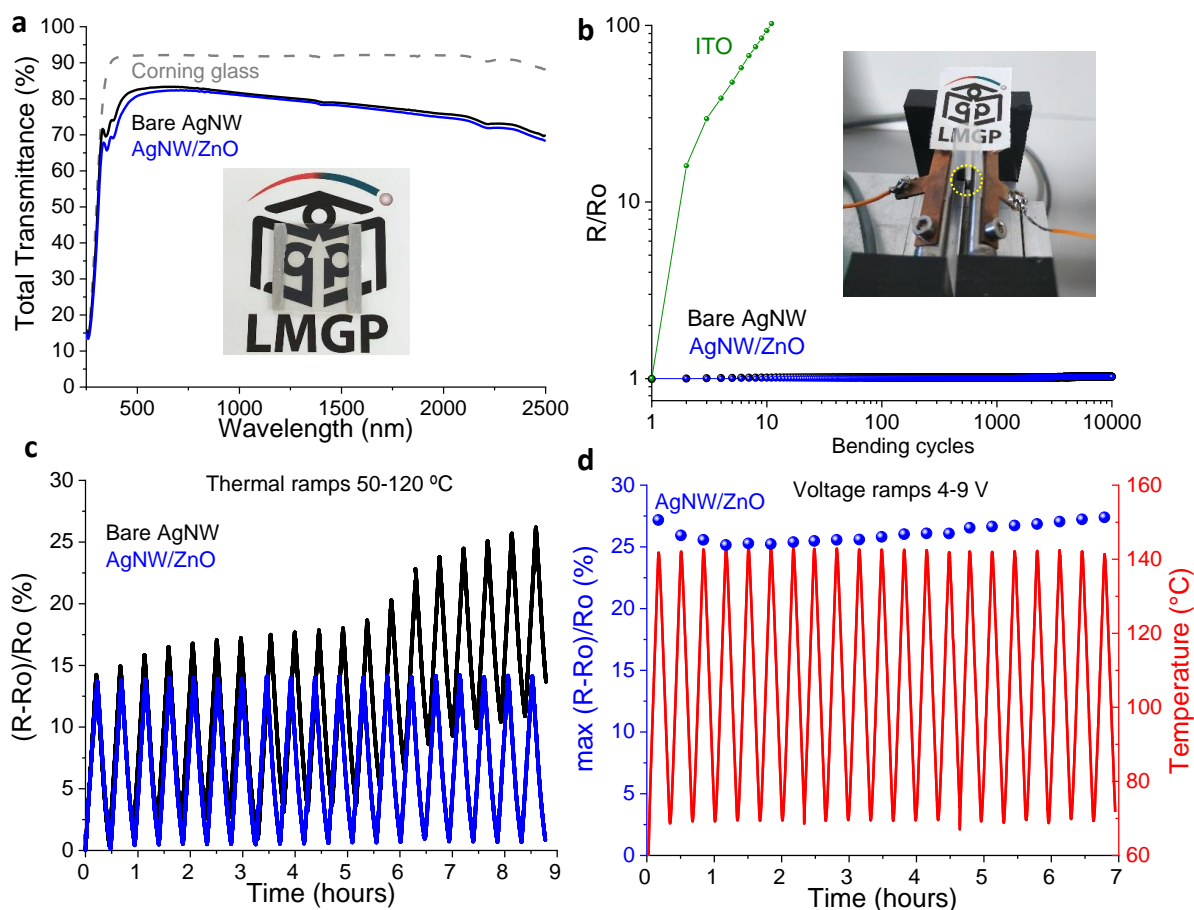


Figure 2. Physical properties and stability of AgNW-based TH; comparison between bare and 35 nm-ZnO coated networks. Bare AgNWs are represented in black and AgNW/ZnO in blue. (a) Total Transmittance in the UV-VIS-NIR spectrum, including the Corning glass substrate contribution, which is also plotted in grey dash line. (b) Relative electrical resistance change during 10000 bending cycles of 5 mm radius, compared to a commercial indium tin oxide (ITO, represented in green). (c) Relative electrical resistance change during 20 cycles of heating-cooling between 50 and 120 °C, with a rate of ± 5 °C/min. (d) Maximum relative electrical resistance change (blue dots) in each cycle of 20 consecutive voltage ramps of ± 0.5 V/min between 4 and 9 V, for ZnO coated AgNW networks. The red line corresponds to the Joule heating response during the voltage cycles.

2.3 Calibration of the lab-on-a-chip temperature

Once the fabrication and stability of the heating element were verified, the temperature of the liquid inside the microfluidic channels obtained for a particular bias applied to the TH had to be calibrated. The amount of heat released per unit of time is V^2/R (V is the bias while R is

210 the electrical resistance of the TH) and the power dissipated in the material is directly related
211 to the achieved steady-state temperature, through a balance between the Joule heating and the
212 heat losses.^[13] These losses are due to: i) the thermal conduction directly to the substrate and
213 then, indirectly, to the chip, ii) the convection to the surrounding air and iii) radiation emitted
214 from the hot surfaces. This leads to a difference between the temperatures on the surface of the
215 TH and the DNA solution inside the channels. The temperature of the device at different
216 positions was then measured independently by using a thermocouple and IR imaging (Figure
217 3a). The type of electrical bias (ramp, plateau, and cycles) was also varied, and the experiments
218 were repeated several times to verify the reproducibility with different AgNW/ZnO specimens
219 and with 3 different SYBR Green I preparations. As schematically presented in **Figure 3a**, we
220 measured and extrapolated the temperature in four different positions: a) T_1 : surface
221 temperature of TH by IR imaging, b) T_2 : temperature of TH deduced by the electrical resistance
222 measured by SMU (Source-Meter-Unit), c) T_3 : channel temperature deduced by the
223 fluorescence of SYBR Green inside the microchannel measured *in situ* by the microscope and
224 d) T_4 : temperature below the chip measured by conduction through a thermocouple (Pt100).
225 For the IR imaging, the parameter of emissivity, ε , can influence significantly the measurement
226 of T_1 . Based on a recent study, we considered in the present work the following emissivity value
227 for the AgNW network deposited on Corning glass: the value of $\varepsilon=0.75$.^[37] For the calculation
228 of T_2 , based on the metallic behavior of the AgNW network, the linear dependence of the
229 electrical resistance with the temperature is expressed by the following equation:

$$T_2 = T_0 + (R - R_0)/(\beta \cdot R_0)$$

230 where T_0 is the initial-room temperature, R is the measured resistance at the temperature T_2 ,
231 and R_0 is the initial resistance at room temperature. The temperature coefficient of electrical
232 resistance, β , was derived as $2.5 \cdot 10^{-3} \text{ K}^{-1}$, from the linear fitting of R versus T , as presented in
233 Figure S1d.

234
235 To estimate T_3 , we used the melting curve of a 448 bp-long DNA fragment, carried out in the
236 presence of the fluorescent intercalant SybrGreen, performed in a qPCR CFX 96 Bio-Rad
237 instrument (Figure S3). After background subtraction, fluorescence measurements were
238 normalized to the value obtained at 25 °C (room temperature). The $F(T)/F(25 \text{ °C})$ ratio is a
239 decreasing function of temperature, whose reciprocal curve was used to compute the local
240 temperature (see Methods section). In all recordings, when the local temperature extends up to
241 DNA melting (80-81°C), the transition is clearly visible as a sharp decline in fluorescence

242 signal. This transition temperature is therefore unambiguously reached *in situ* during the
243 recordings.

244 Figure 3b demonstrates the evolution of these temperatures during a voltage plateau of 3 V
245 applied for 10 minutes (ON state) followed by a zero-bias step for a few minutes back the room
246 temperature state (OFF state). During the OFF state, the electrical resistance was not measured
247 thus, neither the temperature of the AgNW/ZnO was estimated. T_1 (IR) is represented in green,
248 T_2 (from the AgNW resistance) is in blue, T_3 (channel, fluorescence) is in red while the T_4
249 (Pt100) is in gray. The temperatures follow the same evolution with a relatively constant
250 difference and $T_1 > T_2 > T_3 > T_4$. The IR temperature T_1 , which is related to the radiation losses is
251 close to the value of the temperature deduced from the electrical resistance of the specimen. As
252 expected from the heat conduction losses, the temperature of the AgNW/ZnO network T_2 is
253 higher than T_3 and T_4 . Due to the significant thickness of the glass substrate and plastic chip
254 (1.1 mm in both cases) and the lower thermal conductivity of these materials compared to
255 AgNWs, the difference between T_2 to T_4 can reach up to 20 °C in the explored temperature
256 range. Similarly, the temperature inside the channel, T_3 , deduced from the dye fluorescence,
257 was between T_2 and T_4 , and much closer to the TH temperature. This can be justified by the fact
258 that the channels in the microchip are designed closer to the upper surface of the chip and the
259 plastic has lower thermal conduction as well. In any case, the temperature gradient from T_1 to
260 T_4 showed reproducible behaviour during constant applied bias, for instance, when repeating
261 the same plateaus several times. This means that the electrical performance and the high
262 stability of the TH are reliable not only for heating, but also to estimate the temperature inside
263 the chip channels in a reproducible fashion. Additional experiments are provided in SI,
264 concerning the comparison between IR imaging and temperature measurements by Pt100
265 thermocouple during a voltage ramp (Figure S4a), the comparison of temperatures measured in
266 different positions of the thermocouple, i.e. under the chip or between the TH substrate and the
267 chip (Figure S4b). The electrical and heating performance of the TH is very reproducible as
268 demonstrated in Figure S4c, where 4 consecutive experiments (i to iv) of 3 V ON-OFF bias
269 applied to the same AgNW/ZnO specimen are plotted.

270 In general, some of the potential issues tackled during the calibration experiments should be
271 mentioned here, with the main one related to the chip's overheating. Reaching or passing 100
272 °C could lead sometimes to local melting of the channel and/or the evaporation of the DNA
273 solution leading to the formation of air bubbles disturbing the fluorescent signal. This could
274 also lead to the degradation of the biological sample, which is in any case very sensitive to long

275 air exposure, and high temperatures. Another issue could be the photo-bleaching of the
276 fluorescent dye and in order to avoid it, the sample was not constantly exposed to the blue light
277 but instead we used a shutter and recorded the fluorescent photos periodically, usually every 10
278 seconds.

279

280 **2.4 *In situ* biological observations during homogeneous heating**

281 Figure 3c demonstrates the evolution of the fluorescence of the SYBR Green I dye and the
282 channel temperature, T_3 , during 3 consecutive heating and cooling cycles between three voltage
283 plateaus of 2.5, 3.7, and 4.5 V. A voltage ramp of 1 V/min was used between these values. At
284 each cycle, the complete loss of fluorescence is obtained under a low applied bias of 4.5 V,
285 reaching the melting of the DNA, (T_m) as indicated by the deduced channel temperature T_3 as
286 well. These results prove the efficient and reproducible heating performance of the AgNW/ZnO
287 based TH, as well as its low thermal inertia, which allows the channel to heat and cool down
288 rapidly, with rates of 8.5 °C/min and -25 °C/min, respectively. Additional experiments of
289 consecutive cycles are provided in Figure S4d. All the TH samples fabricated and used
290 throughout our study were reusable and stable for more than 6 months.

291

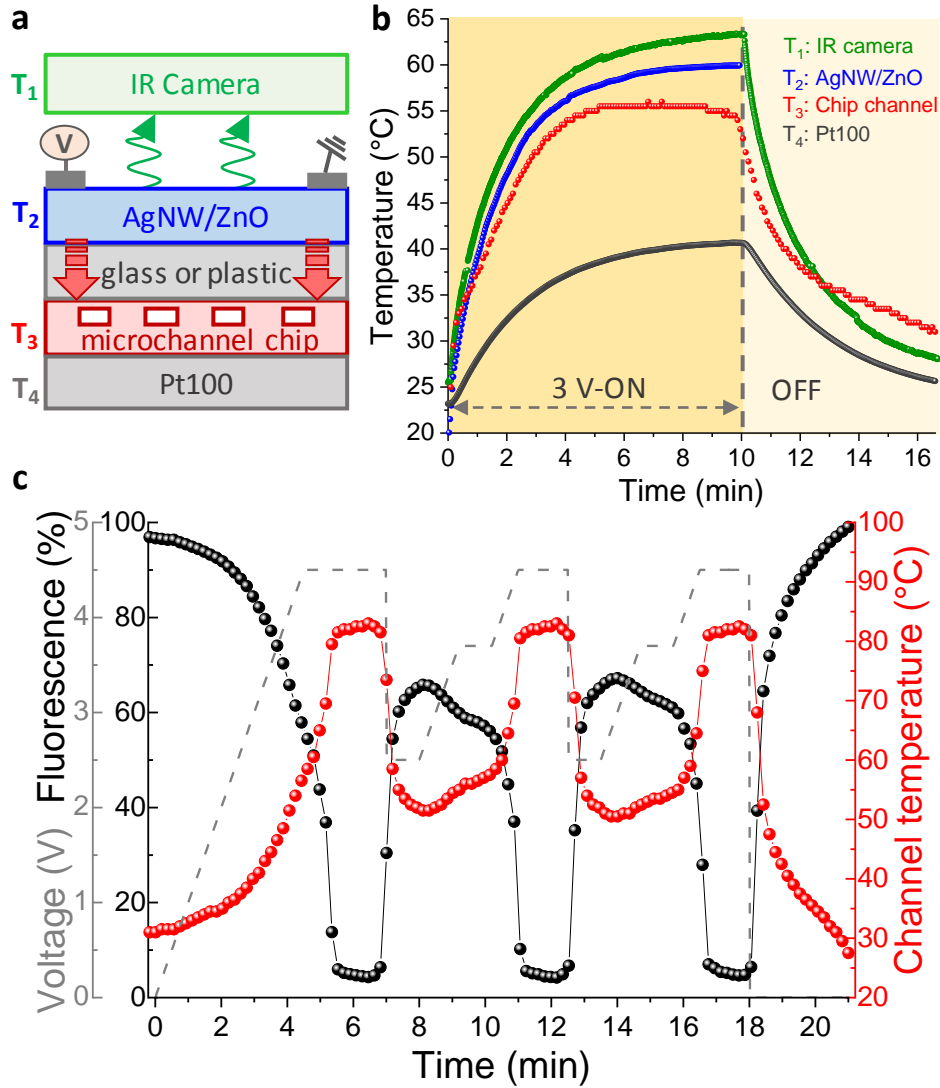


Figure 3. Temperature calibration of the lab-on-a-chip and *in situ* fluorescence measurements during voltage cycles applied to AgNW/ZnO based TH. (a) Schematic representation of the lab-on-a-chip cross-section. The layer thicknesses are not drawn at the same scale: the schema is simplified to highlight the different locations of temperature measurements. T_1 is measured by radiation-IR imaging (in green), T_2 is deduced from the electrical resistance of the AgNW-based TH (in blue), T_3 is deduced from the fluorescence of the dye inside the chip (in red) and T_4 is the temperature measured by conduction-thermocouple Pt100 (in gray). (b) Temperature versus time during a 3 V plateau applied for 10 minutes to AgNW/ZnO, followed by 0 V. (c) Normalized fluorescence of the SYBR Green I (in black dots) versus time measured *in situ* every 10 sec during 3 heating-cooling cycles with the deduced T_3 temperature inside the channel (red dots). The applied voltage (grey dash line) includes 3 plateaus, 2.5 and 3.7 V for 1 min and 4.5 V for 2.5 min initially and then 1.5 min. A ramp of 1 V/min is applied between the plateaus.

305 2.5 Fabrication and modelling of TH for localized heating

1
2 306 So far, we have demonstrated the pertinence of *in situ* observations of the fluorescence of the
3
4 307 SYBR-Green I dye bound to dsDNA in solution inside one channel of a microfluidic chip and
5
6 308 its evolution during heating-cooling cycles induced by a AgNW based TH. In this section, we
7
8 309 present the development of a versatile TH for localized heating, in order to investigate the
9
10 310 spatial or temporal distribution of the fluorescence either in different sections of a channel or
11
12 311 in two separate channels simultaneously. For this, AgNW networks that contain regions of
13
14 312 different network density, i.e. with different local electrical resistivity, were fabricated. Thus,
15
16 313 these regions undergo a different level of Joule heating when a certain voltage is applied to the
17
18 314 entire AgNW network. To achieve this, we have designed and fabricated 3D printed plastic
19
20 315 masks. The low temperature, at which the networks are deposited, allows the use of such a low-
21
22 316 cost, plastic masking technique. As represented schematically in **Figure 4a**, the masks were
23
24 317 placed on the substrate after an initial deposition of nanowires, to block further deposition of
25
26 318 nanowires in specific regions. All AgNW networks were finally coated with the same thickness
27
28 319 of ZnO coating as mentioned above, for enhanced stability. Several types of patterns were
29
30 320 developed during our studies; here we discuss the example of parallel bands, with sizes that fit
31
32 321 the channels of the microfluidic chip. The chip channel width is 1 mm and the distance between
33
34 322 the channels is 4.5 mm, thus we designed each band with a 7 mm width. During the spray
35
36 323 deposition, we started by covering the whole substrate with nanowires. When the resistance,
37
38 324 which is monitored *in situ* in a reference sample during the deposition of the nanowires, dropped
39
40 325 below 80 Ω in the reference sample, we placed the mask (picture in Figure 4b-i) on top of the
41
42 326 substrates and we continued the deposition until the reference sample reached a typical value
43
44 327 of 10-15 Ω . The resulting network has regions with different network densities, as shown by
45
46 328 the different optical contrast between them: the middle perpendicular band, which was masked,
47
48 329 has fewer nanowires and thus it looks less opaque (picture in Figure 4b-ii). The adjacent/non-
49
50 330 covered bands presented the typical *amd*, similar to the specimens discussed above. The
51
52 331 resulted resistance, of the specific specimen used for the experiments presented below, was 22
53
54 332 Ω . Since the bands are in series and not in parallel, the electrical current crossing the AgNW
55
56 333 network is supposed to be the same. This means that the region in the middle, which has a lower
57
58 334 amount of deposited nanowires and thus higher local electrical resistivity, is hotter (I^2R).
59
60 335 Furthermore, we have developed physical modelling by Comsol Multiphysics (the used
61
62 336 parameters are provided in Methods section) to predict the electrical properties and thermal
63
64 337 performance of Ag thin films. The films have bands of different electrical properties that
65

338 correspond to the local network density. This approximation allowed us to overcome the
1 339 computational limits and simulate specimens of the same size as the experimental ones. Figure
2 340 4c and d provide the spatial distribution of the temperature obtained by modelling and IR
3 341 imaging, respectively, for 5.3 V applied. The simulated electrical potential and surface current
4 342 density distribution are provided in Figure S4e-f. The simulated values are in good agreement
5 343 with the experimental ones, meaning that this approach can be used during the development of
6 344 transparent heaters serving the specific needs of lab-on-a-chip devices.

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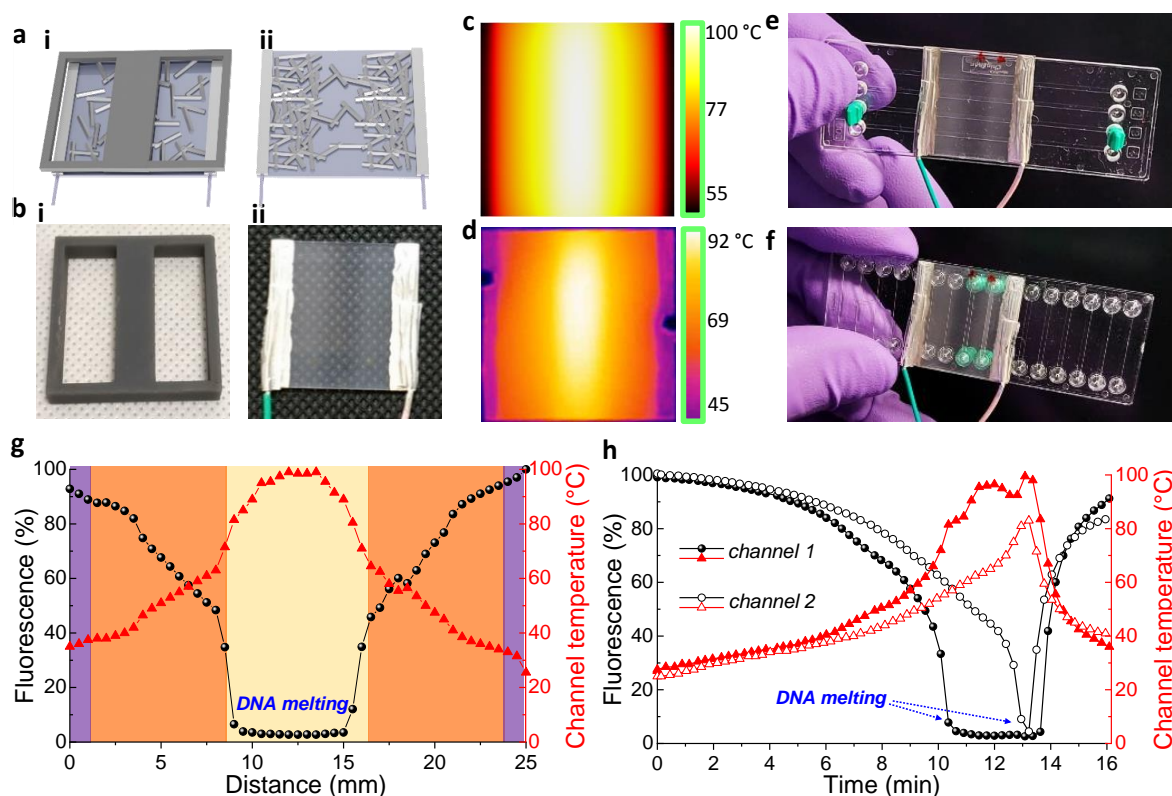
15 346 **2.5.1 *In situ* biological observations in a microfluidic chip during localized heating**

17 347

18 348 The patterned AgNW based TH was integrated into two different configurations of the
19 349 microfluidic chip channels and two types of experiments were performed. In the first case, we
20 350 used a chip containing channels parallel to the long edge of the chip, as in the experiments
21 351 presented so far, in order to investigate the heating of the biological sample at different
22 352 temperatures in the same channel under the same voltage. The patterned TH was placed as
23 353 shown in the picture in Figure 4e and the spatial distribution of the fluorescence of one channel
24 354 was monitored *in situ* during a voltage plateau. A bias of 5.3 V was applied and the monitoring
25 355 began after 9 minutes, when the T_m of the dsDNA and a steady-state regime for the TH were
26 356 reached. The spatial distribution of the fluorescence was monitored with a scanning along the
27 357 channel, with a 0.5 mm distance between two points of measurement. Normalized fluorescence
28 358 and channel temperature (T_3) at each point inside the channel are plotted in Figure 4g. This
29 359 temperature profile demonstrates clearly that there are three regions of different temperatures,
30 360 which spatially correspond to the bands of different AgNW network densities.

31 361 In the second case, we used a different chip in which the channels were perpendicular to the
32 362 long side of the chip, to investigate the evolution of the fluorescent dye simultaneously in two
33 363 adjacent channels that are heated at different temperatures under the same applied bias to the
34 364 TH. This time, the patterned TH was placed with the bands parallel to the microfluidic channels.
35 365 The first channel is covered with the sparser AgNW middle band, while the second channel is
36 366 exposed to the denser right band. More details about the chip dimensions are presented in the
37 367 Methods section. A voltage ramp of 0.5 V/min was applied up to 6.5 V, to ensure that the T_m
38 368 was reached. During this, the fluorescence of each channel was recorded consecutively *in situ*
39 369 every 10 seconds. The results showed clearly a different heating for each channel. As shown in
40 370 Figure 4h, channel 1, covered by the sparser band, reached higher temperature and in a faster

371 way, as expected given the different amd and thus local R value. Once the applied voltage was
 372 turned off and the TH started cooling down, the fluorescent signal of both channels recovered
 373 as well. However, back at room temperature, the average difference between the initial and final
 374 fluorescence, for three experiments performed consecutively, was +20% (channel 1) for the
 375 hotter channel and +5% for the colder one (channel 2). This increase in the fluorescence can be
 376 related to a local deformation of the plastic chip due to the high heating, mostly in the case of
 377 the hotter channel that reached 100 °C.



378
 379 **Figure 4.** Development of AgNW/ZnO based TH for localized heating and *in situ*
 380 measurements of fluorescence spatial distribution in one channel and time evolution in two
 381 channels simultaneously. (a) Schematic representation of the 3D printed mask placed during
 382 the AgNW spray deposition (i), once the network resistance has decreased to less than 100 Ω.
 383 Thus, the final AgNW network (ii) has a lower nanowire density in the middle band. (b) Optical
 384 pictures of the plastic 3D-printed mask (i) and the TH after ZnO and contacts deposition (ii).
 385 The network density is lower in the middle as also shown by the optical contrast-transparency.
 386 (c) Surface temperature distribution by physical modeling of the TH at 5.3 V applied bias. (d)
 387 Surface temperature distribution of TH at 5.3 V during an applied voltage ramp. (e) Optical
 388 picture of the lab-on-a-chip configuration for *in situ* study of spatial fluorescence distribution

389 in one channel in lengthwise orientation chip. The TH has three parallel bands, the one in the
390 middle with a lower AgNW density (associated with a larger resistance), and they are placed
391 perpendicular to the channels. (f) Optical picture of the lab-on-a-chip configuration for *in situ*
392 study of multiple channels fluorescence in crosswise orientation chip. The TH bands are placed
393 parallel to the adjacent channels, which have a 4.5 mm distance between them, so that each of
394 them heats homogeneously but at different temperatures. (g) Normalized fluorescence (black
395 dots) measured *in situ* with a step of 0.5 mm inside a channel during a plateau of 5.3 V applied
396 to the TH (e configuration). The deduced spatial distribution of the temperature is plotted as
397 well (red triangles). (h) Normalized fluorescence (dots) measured for two channels *in situ*
398 during a voltage ramp of 0.5 V/min until 6.5 V applied to the TH (f configuration) and the
399 deduced temperature is plotted as well (triangles). Every 10 seconds the fluorescence was
400 measured at each channel consecutively. The left channel (filled dots and triangles) was heated
401 by the more resistive, middle band and reached faster the DNA melting point compared to the
402 right channel (open dots and triangles).

3. Conclusions

406 In the present work, we demonstrated a proof-of-concept integration of transparent heaters (TH)
407 based on AgNW networks into *in situ* biological studies in an optical microscope. AgNW were
408 deposited and protected by a ZnO oxide layer, using open-air, low-temperature processes,
409 compatible with large-scale production (spray coating and spatial atomic layer deposition,
410 respectively). The fabricated TH are flexible and thus reusable, being easily placed and
411 removed from microfluidic chips and remained stable after several months of use. In addition,
412 selective heating can be achieved by easily patterning the TH thanks to conventional 3D printed
413 plastic masks. Using AgNW/ZnO based TH, presenting a typical electrical sheet resistance of
414 10-15 Ω/sq and 2.5x2.5 cm^2 size, temperatures up to 100 °C could be reached inside the chip
415 channels with less than 6.5 V applied bias, depending on the pattern of the AgNW network.

416 *In situ* biological observations were highly facilitated by the fabricated lightweight and low-
417 energy-consumption transparent heating elements, exhibiting robustness and reproducibility.
418 This is very important given the new challenges related to pandemic situations that require
419 effective means for the detection of biological and viral species in a fast, reliable and low-cost
420 way. The fluorescence of SYBR Green I dye, bound to dsDNA in solution inside the channels,
421 was recorded during consecutive heating-cooling cycles. DNA denaturation-renaturation was

422 observed in every cycle, and the derived temperature inside the channels followed the same
423 evolution as expected from the TH performance and physical modelling. Selective heating
424 thanks to simply patterned TH was demonstrated both, by the spatial gradient of the temperature
425 inside one channel and by the different temperatures inside two adjacent microchannels
426 observed in parallel. The versatile AgNW-based TH reported in this study can be readily
427 applicable to research studies and applications where localized heating and transparency are
428 needed, for instance, to perform crystallization studies in microfluidic reactors, for cell culture
429 and lab-on-a-chip systems or for transparent displays, among others.

4. Methods

4.1 AgNW synthesis and networks fabrication

434 AgNWs with an aspect ratio close to 100 (average diameter of 70 ± 10 nm and an average
435 length of 8 ± 3 μm) were kindly provided from the research team of Jean-Pierre Simonato from
436 CEA-LITEN in Grenoble, France, being produced as detailed in Mayousse et al.^[38] The AgNWs
437 were dispersed in methanol with an initial concentration of **3.9 g/L** and diluted afterwards 30
438 times to obtain a concentration of 0.1 g/L. Spray deposition was performed with an airbrush of
439 0.4 mm nozzle size (“Infinity” by Harder & Steenbeck) and a nitrogen inlet of 1.4 bar pressure.
440 The airbrush was fixed in a mechanical setup connected with a programmable automation
441 controller. During deposition, the airbrush was moving along a regular and periodic array in X
442 and Y directions, 7 cm above an aluminium plate set to 110 °C, for a direct evaporation of the
443 solvent. The substrates used, Alkaline earth boroaluminosilicate glass (Corning® 1737,
444 thickness 1.1 mm), were cut in squares of 25x25 mm², rinsed with acetone, sonicated for 15
445 min in isopropanol, rinsed with distilled water, and finally dried with N₂ gas. 0.1 mm thick
446 flexible, transparent polyimide substrates of the same size, were used as well (Neopulim®
447 kindly provided by Mitsubishi). To fabricate the patterned AgNW networks, masks made by a
448 3D printer with high temperature resin (version FLHTAM01 by Formlabs, Inc.) were placed
449 on the top of the substrate during spray deposition.

4.2 Oxide coating

452 ZnO thin films were deposited with the atmospheric-pressure spatial atomic layer deposition
453 (AP-SALD) home-made system of LMGP.^[33,39] Diethylzinc (DEZ, (C₂H₅)₂Zn, Aldrich), and
454 water vapor were used as precursors for zinc, and oxygen, respectively. The substrate

455 temperature was maintained at 200 °C. The gas injector was fixed at 150 μm from the substrate,
456 which oscillated at 10 cm/s between different precursor channels to produce 100 ALD cycles,
457 corresponding to 30±5 nm thick ZnO coating.

458

4.3 Microfluidic chip transparent heater set-up

460 Two types of Topas straight channel chips (purchased from microfluidic ChipShop®) were
461 used throughout the experiments. The dimensions of both chips are 75.5 mm x 25.5 mm x 1.5
462 mm and the fluidic interface in order to fill the channel by pipetting has the shape of mini luer.
463 The channel width and depth are 1 mm and 0.2 mm, respectively, and the distance between the
464 channels is 4.5 mm. One chip has four channels of 58.5 mm length and lengthwise channel
465 orientation, and the other sixteen channels of 18 mm length and crosswise channel orientation.
466 Silver paste contacts (L-200N purchased from CDS Electronique) were manually deposited at
467 two opposite sides of the AgNW/ZnO network and then thin, long copper wires were stuck to
468 the silver paste and were connected to the power supply. For the demonstration of the lab-on-
469 a-chip device, the AgNW/ZnO network on its polymeric substrate was attached with double
470 coated adhesive tape (3M™ 9629PC) on top of the microfluidic chip.

471

4.4 Experimental characterizations

473 AgNWs and film surface morphology were analyzed by field emission gun-scanning electron
474 microscopy (FEG-SEM Environmental FEI QUANTA 250 and SEM ZEISS-Gemini 300) and
475 transmission electron microscopy (JEOL JEM-2010 microscope). ImageJ software was used to
476 calculate the AgNW network density, expressed as the areal mass density *amd* (in mg/m²), by
477 a wire detection plug-in (Ridge detection), estimating the geometrical density in SEM images,
478 following the protocol described somewhere else.^[40] Optical properties were analyzed using a
479 Lambda 950 spectrophotometer from Perkin Elmer in the 250–2500 nm range. The electrical,
480 thermal, and mechanical properties of AgNW based transparent electrodes were investigated
481 by experimental homemade set-up. For the thermal ramp tests, the samples were placed on top
482 of a hotplate, whose temperature is controlled by temperature programmer/controller
483 (Eurotherm) connected to a LabVIEW software. For the bending tests, the samples were placed
484 between two jaws, whose position was moved using a motor, piloted by a LabVIEW. During
485 the thermal ramps and the bending tests, a voltage of 0.1 V was applied by two-point probes
486 and a source-measure-unit (SMU) (Keithley 2400) piloted by LabVIEW software as well, in

order to record the electrical resistance of the sample. The software allowed the recording of the temperature, voltage, current and resistance of the sample in real-time. The sourcemeter and the LabVIEW software were also used to control the voltage and measure the electrical resistance of the samples during the electrical tests and also for the heating of the microfluidic chip during the *in situ* optical microscope observations. The surface temperature spatial distribution of the specimens was measured by a FLIR T335 IR camera and by a resistance temperature detector (Pt100 RTD) embedded in a 120 μm thick PET layer. To monitor temperature *in situ*, SYBR Green I-DNA fluorescence in the microfluidic channels was observed with an Olympus IX71 inverted microscope equipped with a DP30DW camera, a 10x magnification objective and a 100 W Hg lamp. A motorized stage was used to switch channels during observations. The fluorescence was recorded and analyzed with Image Pro Plus 5 software.

4.5 Measurement of temperature inside the microfluidic channels

A pQE30 plasmid encoding *Dictyostelium discoideum* syntaxin 8 coding sequence (pQE30-Syn8) was used as a source of DNA.^[41] A 448 bp-long DNA fragment containing Syn8 coding sequence was amplified with the following 5' and 3' primers (5' : TTTTTTCGCATCACCATCACCA; 3' : GCTTGGCTGCAGGTCGACCCGGG, 8 pmoles each), using BioRad Sso1 SYBR Green I qPCR mix (20 μL assay). qPCR was performed in a CFX-96 instrument (2 min 94°C denaturation, 20 cycles at 94°C (30 s), 50°C (30 s), 72°C (1 min). After amplification, a melting curve was acquired from 25°C to 95°C by 0.5°C steps. As a control, a sample without template DNA was prepared in the same manner. The signal obtained in the absence of sample (blank) was subtracted to calculate specific fluorescence. Specific fluorescence measurements were normalized to the value obtained at 25°C. The F(T)/F(25°C) ratio is a decreasing function of temperature, which can be adjusted with the following empirical equation:

$$\frac{F(T^{\circ}C)}{F(25^{\circ}C)} (\%) = a - \frac{bT + c + dTe^{\frac{T_m-T}{w}}}{1 + e^{\frac{T_m-T}{w}}}$$

in the range 35-95°C, using the following parameters : a = 148, b = 0.081 °C⁻¹, c=138, d=1.60 °C⁻¹, T_m=80.2 °C, w=0.82 °C. Above 81°C, the fluorescence signals of sample with and without DNA matches, indicating that the residual fluorescence is due to free SYBR Green I. In the

517 range 25-35°C, the fitting was extended using a cubic polynomial defined by its value of 100
518 at 25°C and the value and slope of F(T)/F(25°C) at 35°C :

$$\frac{F(T^{\circ}C)}{F(25^{\circ}C)} (\%) = 100 - a'(T - 25) - b'(T - 25)^2 - c'(T - 25)^3$$

520 using the following parameters: $a' = 0.3313 \text{ }^{\circ}\text{C}^{-1}$, $b' = 0$ and $c' = 4.224 \cdot 10^{-3} \text{ }^{\circ}\text{C}^{-3}$. A calibration
521 curve relating the specific fluorescence ratio F(T)/F(25°C) as a function of T in the range 25-
522 95°C was therefore obtained with a precision of 0.5°C. The reciprocal curve was used to deduce
523 the local temperature from the F(T)/F(25°C) ratio. Practically, the blank signal was measured
524 outside the microchannel containing SYBR Green I-DNA sample and the initial specific
525 fluorescence was recorded before heating at room temperature F(25°C). The specific
526 fluorescence ratio F(T)/F(25°C) was compared to the calibration curve to compute the local
527 temperature with a precision of 0.5°C.

528

529 **4.6 Modeling**

530 Physical simulations of homogeneous and masked AgNW networks were performed using
531 Comsol Multiphysics® version 5.2 and the AC/DC Module. The software is based on finite
532 element analysis and the physics of “Electric Currents, Shell” and “Heat transfer in solids” were
533 used, coupling both electrical and thermal models and thus calculating the spatial distributions
534 of the electric potential, current density, and surface temperature. A thin Ag film on top of
535 Corning glass of 3 nm was simulated to represent the AgNW networks, as described in the
536 simulations performed in our previous work.^[16] Although AgNW constitute nanomaterials for
537 which sizes can be of the same order of magnitude of electrons mean free path, we considered
538 for the sake of simplicity through Comsol simulations heat transfer modeling within a
539 continuous medium. The thin film has three parallel bands of different electrical properties,
540 corresponding to the experimental patterned AgNW networks, fabricated with the help of the
541 3D printed masks. In the case of less dense band in the middle, the sheet resistance was set to
542 80 Ω/sq, while the rest of the specimen was set to 10 Ω/sq. The size of the simulated specimens
543 was the same as the experimentally fabricated ones (25x25 mm²) as well as the glass substrate
544 size (25x25x1.1 mm³). A work plane was added, where rectangular contacts with a width of 1.5
545 mm were added on the left and the right sides with the appropriate electric boundary conditions.
546 To perform thermal simulations, three main mechanisms of heat losses were taken into account:
547 convection, conduction, and radiation. In the model, the two layers were not physically

548 separated so the conduction between them is considered ideal and any external conduction
1 549 losses were neglected (for instance the conduction losses through the connecting wires were
2
3 550 not taken into account). The emissivity of Corning glass was considered for the radiation losses
4
5 551 and the value of 0.75 was considered for the Ag film, same as the AgNW network value set for
6
7 552 the IR imaging in the experiments. Concerning the convection losses, a heat transfer coefficient
8
9 553 of $h= 10 \text{ W}/(\text{m}^2\cdot\text{K})$ was applied for the glass substrate, $h= 50 \text{ W}/(\text{m}^2\cdot\text{K})$ for the silver layer and
10
11 554 $h= 40 \text{ W}/(\text{m}^2\cdot\text{K})$ for the less dense/conductive band.

13 555 **Supporting Information**

15 556 Supporting Information is available from the Wiley Online Library.

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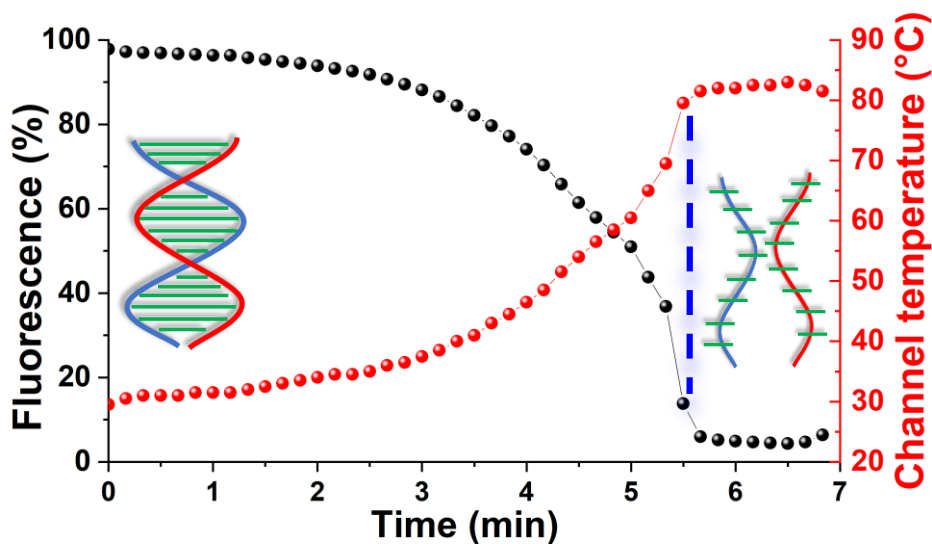
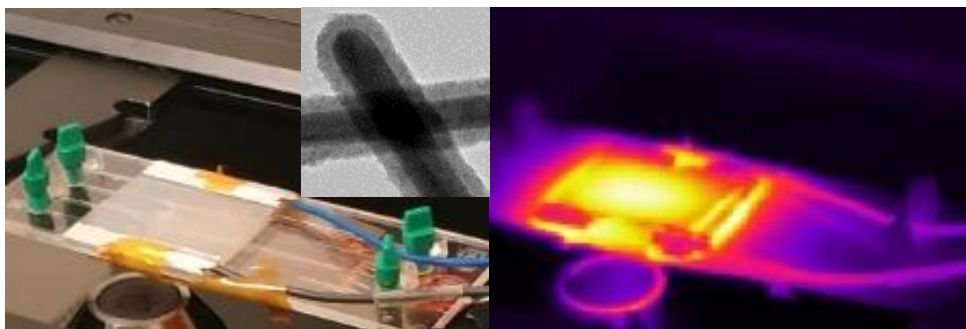
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2 647
3 648 Lightweight, flexible and highly stable transparent heaters based on silver nanowire networks,
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5 649 are integrated in lab-on-a-chip for *in situ* monitoring of biological processes. Localized heating
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7 650 using a single transparent heater and applied bias, is demonstrated inside one microchannel or
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9 651 for adjacent microchannels of the same chip heating at different temperatures.

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19 656 **Stable flexible transparent electrodes for localized heating of lab-on-a-chip devices**

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23 658 **ToC Figure**



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