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Evaluating European ECOSTRESS Hub Evapotranspiration Products Retrieved from Three Structurally Contrasting SEB Models over Europe

3 Tian Hu¹, Kaniska Mallick^{1,10}, Patrik Hitzelberger², Yoanne Didry², Gilles Boulet³, Zoltan

4 Szantoi^{4,8}, Benjamin Koetz⁴, Itziar Alonso⁴, Madeleine Pascolini-Campbell⁵, Gregory

5 Halverson⁵, Kerry Cawse-Nicholson⁵, Glynn C. Hulley⁵, Simon Hook⁵, Nishan Bhattarai⁶,

6 Albert Olioso⁷, Jean-Louis Roujean³, Philippe Gamet³, Bob Su⁹

¹Department of Environment Research and Innovation, Luxembourg Institute of Science and 7 Technology, Belvaux 4362, Luxembourg, ²Department of IT for Innovative Services, Luxembourg 8 Institute of Science and Technology, Belvaux 4362, Luxembourg, ³Centre d'Etudes Spatiales de 9 la Biosphère, CNES, CNRS, INRAE, IRD, UPS, Toulouse 31401, France, ⁴Science, Applications 10 & Climate Department, European Space Agency, Frascati 00044, Italy, ⁵Jet Propulsion 11 Laboratory, California Institute of Technology, Pasadena, California 91109, USA, ⁶Department of 12 Geography and Environmental Sustainability, University of Oklahoma, Norman, Oklahoma 13 73019, USA, ⁷Unité de Recherche écologie des Forêts Méditerranéennes, INRAE, Avignon, 14 France, ⁸Stellenbosch University, Stellenbosch 7602, South Africa, ⁹Department of Water 15 Resources, Faculty of Geo-Information Science and Earth Observation (ITC), University of 16 Twente, P.O. Box 217, Enschede, 7500 AE, The Netherlands, ¹⁰Department of Environmental 17 Science, Policy and Management, University of California, Berkeley, California 94720, USA 18

19 Corresponding author: Tian Hu (tian.hu@list.lu), Kaniska Mallick (kaniska.mallick@list.lu)

20 Key Points:

- Evaporation products over Europe and Africa were generated using 3 different models
 (STIC, SEBS, and TSEB) in the European ECOSTRESS Hub
- Comparison at 19 eddy covariance sites revealed noteworthy model divergence with increasing aridity and vegetation sparseness
- A substantial overestimation of the official NASA ECOSTRESS ET product was found under high water limitations
- 27

28 Abstract

The ECOsystem Spaceborne Thermal Radiometer Experiment on Space Station (ECOSTRESS) is 29 a scientific mission that collects high spatio-temporal resolution (~70 m, 1-5 days average revisit 30 time) thermal images since its launch on 29 June 2018. As a predecessor of future missions, one 31 of the main objectives of ECOSTRESS is to retrieve and understand the spatio-temporal variations 32 in terrestrial evapotranspiration (ET) and its responses to soil water availability. In the European 33 ECOSTRESS Hub (EEH), by taking advantage of land surface temperature retrievals, we 34 generated ECOSTRESS ET products over Europe and Africa using three structurally contrasting 35 models, namely Surface Energy Balance System (SEBS) and Two Source Energy Balance (TSEB) 36 parametric models, as well as the non-parametric Surface Temperature Initiated Closure (STIC) 37 model. A comprehensive evaluation of the EEH ET products was conducted with respect to flux 38 measurements from 19 eddy covariance sites over 6 different biomes with diverse aridity levels. 39 Results revealed comparable performances of STIC and SEBS (RMSE of ~70 W m⁻²). However, 40 the relatively complex TSEB model produced a higher RMSE of ~90 W m⁻². Comparison between 41 STIC ET estimate and the operational ECOSTRESS ET product from NASA PT-JPL model 42 showed a difference in RMSE between the two ET products around 50 W m⁻². Substantial 43 overestimation (>80 W m⁻²) was noted in PT-JPL ET estimates over shrublands and savannas 44 presumably due to the weak constraint of LST in the model. Overall, the EEH is promising to serve 45 46 as a support to the Land Surface Temperature Monitoring (LSTM) mission.

47 **1 Introduction**

Evapotranspiration (ET) is an intrinsic component of climate in the land-atmosphere system and 48 plays a critical role in affecting turbulence, cloud formation and convection at the local scale 49 (Chen and Liu 2020; Fisher et al. 2017). As an important component of the water cycle in the 50 terrestrial ecosystems, it quantifies the amount of water loss from the Earth surface to atmosphere 51 (Chen and Liu 2020; Jasechko et al. 2013). ET consists of evaporation from soil (or water bodies) 52 and wet vegetation and transpiration through pores in plant leaves. Through the stomatal 53 conductance, transpiration is closely related to CO₂ exchange between leaf and atmosphere 54 (Anderson et al. 2008). Thus, ET links the land surface water, energy, and carbon cycles (Anderson 55 et al. 2008; Fisher et al. 2017; Mallick et al. 2021), and is a keystone variable in terrestrial 56 ecosystem processes (Bai et al. 2022; Bayat et al. 2018; Kustas and Anderson 2009; Ryu et al. 57

58 2011).

Thermal infrared (TIR) remote sensing has been widely used to obtain ET at large scales 59 considering land surface temperature (LST) constrains the magnitude and variability of the surface 60 energy balance (SEB) components and is immensely sensitive to evaporative cooling (Crago and 61 Oualls 2014; Mallick et al. 2021; Mallick et al. 2014; Norman et al. 1995). ET products are 62 63 generated from TIR observations of different sensors, including Landsat (Anderson et al. 2012; Anderson et al. 2021; Jaafar et al. 2022), Moderate resolution Imaging Spectroradiometer 64 (MODIS) (Chen et al. 2019; Chen et al. 2021; Senay et al. 2013), Visible Infrared Imaging 65 Radiometer Suite (VIIRS) onboard polar-orbiting satellites (Jaafar et al. 2022), and Advanced 66 Baseline Imager (ABI) (Anderson et al. 2007; Fang et al. 2019) onboard Geostationary Operational 67 Environmental Satellite (GOES). These ET data are harnessed in a variety of applications such as 68 69 drought monitoring (Anderson et al. 2011; González-Dugo et al. 2021; Otkin et al. 2013), water resource management (Anderson et al. 2012), irrigation control (Allen et al. 2011), global change 70

studies (Dai et al. 2004; Mao et al. 2015), and biodiversity assessments (Fisher et al. 2011).

However, there remains a gap in retrieving ET with concurrently high spatial and temporal resolutions at the global scale. For the polar-orbiting satellites, the Landsat ET product has a high spatial resolution (30 m via thermal sharpening) but coarse temporal resolution (16 days). MODIS and VIIRS have a daily temporal resolution but coarse spatial resolution (\geq 500 m). For the geostationary satellites, the diurnal cycle can be captured by the sub-hourly observations, but the spatial resolution is above 1 km due to the orbit altitude and spatial coverage is limited to the continental scale. This constrains subsequent applications of ET products.

The ECOsystem Spaceborne Thermal Radiometer Experiment on Space Station (ECOSTRESS), 79 positioned on the International Space Station (ISS) on 29 June 2018, is a pathfinder for the next 80 generation TIR missions (Fisher et al. 2020; Hook et al. 2019; Hulley et al. 2021). It collects 81 thermal images in five bands between 8 and 12.5 µm with a high spatio-temporal resolution at 82 varying times of the day. The spatial coverage is between $\pm 52^{\circ}$ latitude over the globe. The pixel 83 size after resampling at the nadir is $\sim 70 \times 70$ m. The average revisit time is approximately 1-5 84 days, depending on the latitude (Xiao et al. 2021). Over high latitude regions where the ISS orbital 85 direction shifts, the observation frequency can reach several times in a single day. Therefore, the 86 ECOSTRESS data provides an unprecedented opportunity for monitoring terrestrial ecosystems 87 (Fisher et al. 2020; Liu et al. 2021; Xiao et al. 2021). 88

89 The European ECOSTRESS Hub (EEH) is a project funded by the European Space Agency (ESA),

targeted at generating high spatio-temporal resolution LST and ET products over Europe and Africa from ECOSTRESS observations. Three structurally contrasting SEB models were selected

- to produce ET estimates, i.e., one-source Surface Energy Balance System (SEBS) and Two Source
- 93 Energy Balance (TSEB) parametric models, and the one-source Surface Temperature Initiated
- 94 Closure (STIC) analytical model. The EEH LST estimates were used as the driving force for ET
- retrieval from the three models, with the support of ancillary meteorological data and variables
 describing the surface conditions (e.g., albedo, vegetation coverage). The uniform forcing data
- 97 describing the lower boundary conditions enables a fair comparison across a wide spectrum of 98 energy and water availability scenarios among the three models with different parameterization
- schemes. EEH LST and ET products between August 2018 and December 2021 can be downloaded from the Food Security-TEP portal (https://foodsecuritytep.net/). More information

101 about EEH can be found on the landing page (http://isp-projects.private.list.lu/eeh/public/).

In this paper, we aimed to evaluate the three ECOSTRESS ET products generated in EEH at the continental scale. A two-step evaluation strategy was adopted. First, the EEH ET products were

compared with flux measurements from 19 eddy covariance sites over Europe between 2018 and

105 2019. Then, the best performing EEH ET product was compared with the official National

- 106 Aeronautics and Space Administration (NASA) ECOSTRESS ET product retrieved using the PT-
- 107 JPL model. The purpose of this study is two-fold: 1) providing insights into ECOSTRESS ET

products generated using SEB models with different structures and parameterizations schemes, 2)

supporting ET retrieval for the future thermal missions like ESA's Land Surface Temperature

Monitoring (LSTM) (Koetz et al. 2019), the Franco-Indian joint Thermal infraRed Imaging Satellite for High-resolution Natural resource Assessment (TRISHNA) (Lagouarde et al. 2018)

and NASA's Surface Biology and Geology (SBG) (Cawse-Nicholson et al. 2021).

113 **2 ET models in EEH**

114 ET is intrinsically associated with the SEB equation, which is based on the partitioning of net

available energy into sensible and latent heat fluxes. The SEB equation is written as follows

$$R_N = \lambda E + H + G \tag{1}$$

116 where R_N is the net radiation, H and λE are sensible and latent heat fluxes (W m⁻²), respectively,

and G is the ground heat conduction flux. The segregation of net available energy $(R_N - G)$ into the

118 two different convective fluxes (H and λE) depends on the land surface moisture status,

atmospheric conditions in the lower boundary layer, and biophysical control of vegetation (Anderson et al. 2008; Kustas and Anderson 2009; Mallick et al. 2014; Mallick et al. 2018a;

121 Mallick et al. 2018b).

Most thermal-based ET models calculate ET as a residual of SEB after estimating H or estimate 122 evaporative fraction first and derive ET from the net available energy. These models can be broadly 123 characterized as one-source and two-source models based on the conceptualization of the land 124 surface. In the one-source models, the vegetated surface is regarded as a 'big leaf' and the 125 evaporating front is assumed to be at the source/sink height, which is in the immediate vicinity of 126 127 the surface level. Whereas the two-source models assume that the vegetated surface consists of the soil and vegetation components, and the energy fluxes are partitioned between these two 128 129 components.

130 2.1 STIC

The one-source STIC model was first proposed by Mallick et al. (2014). STIC is based on the 131 integration of radiometric temperature into the Penman-Monteith (PM) formulation to find the 132 analytical solution of the aerodynamic and surface conductances. To do so, STIC combines an 133 LST-driven water stress index with aerodynamic equations of H and λE and a modified 134 complementary relationship advection-aridity hypothesis (Mallick et al. 2015). The latest version 135 of STIC (Bhattarai et al. 2018; Mallick et al. 2016) combines the Shuttleworth-Wallace sparse 136 canopy formulation model with the PM big-leaf model to calculate the vapour pressure at the 137 source/sink height (Shuttleworth and Wallace 1985). 138

139 2.1.1 State equations of STIC

140 The four state equations are at the core of STIC, which describe aerodynamic and surface 141 conductances (g_A and g_C), aerodynamic temperature (T_0), and evaporative fraction (F_E):

$$g_A = \frac{\phi}{\rho c_p \left[(T_0 - T_A) + \frac{e_0 - e_A}{\gamma} \right]}$$
(2)

$$g_C = g_A \frac{e_0 - e_A}{e_0^* - e_0} \tag{3}$$

$$T_0 = T_A + \left(\frac{e_0 - e_A}{\gamma}\right) \left(\frac{1 - F_E}{F_E}\right) \tag{4}$$

$$F_E = \frac{2\alpha s}{2s + 2\gamma + \gamma \frac{g_A}{g_C}(1+M)}$$
(5)

where Φ is the net available energy, ρ is the density of air (kg m⁻³), c_p is the specific heat of air at constant pressure (MJ kg⁻¹ K⁻¹), γ is the psychrometric constant (hPa K⁻¹), T_A is air temperature at

144 the reference height, e_0 and e_0^* is the vapor pressure at the source/sink height, e_A is atmosphere

145 vapor pressure, α is the Priestley-Taylor (PT) coefficient, s is the slope of saturation vapour

146 pressure versus temperature curve estimated at T_A , M is the surface moisture availability (between

- 0 and 1), which is estimated from LST. Based on the four state equations, algebraic closure is not
 possible due to the involvement of additional unknowns. Therefore, an iterative solution is adopted
- possible due to the involvement of additional unknowns. Therefore, an iterative set to estimate the additional unknown variables (e_0^* , e_0 , α and *M*).
- 150 2.1.2 Iterative solution of e_0^* , e_0 , α and *M* in STIC
- 151 From the aerodynamic equation of λE , e_0^* can be expressed as

$$e_0^* = e_A + \frac{\gamma \lambda E(g_A + g_C)}{\rho c_p g_A g_C}$$
(6)

- Following Shuttleworth and Wallace (1985), the vapour pressure deficit ($D_0 = e_0^* e_0$) and vapour
- 153 pressure (e_0) at the source/sink height are expressed as follows:

$$D_0 = D_A + \frac{s\phi - (s+\gamma)\lambda E}{\rho c_p g_A} \tag{7}$$

$$e_0 = e_0^* - D_0. (8)$$

154 A physical equation of α is expressed as

$$\alpha = \frac{\left[2s + 2\gamma + \gamma \frac{g_A}{g_C}(1+M)\right]g_C(e_0^* - e_A)}{2s[\gamma(T_0 - T_A)(g_A + g_C) + g_C(e_0^* - e_A)]}.$$
(9)

155 *M* is expressed as the ratio of the vapour pressure difference to the vapour pressure deficit between 156 the surface and atmosphere as follows

$$M = \frac{e_0 - e_A}{e_0^* - e_A} = \frac{e_0 - e_A}{k(e_s^* - e_A)} = \frac{s_1(T_{0D} - T_D)}{ks_2(T_R - T_D)}$$
(10)

where T_{0D} is the dew-point temperature at source/sink height and T_D is the air dew-point temperature, T_R is the radiometric surface temperature, s_1 and s_2 are the psychrometric slopes of the saturation vapour pressure and temperature between the $(T_{0D} - T_D)$ vs. $(e_0 - e_A)$ and $(T_R - T_D)$ vs. $(e_s^* - e_A)$, and k is the ratio between $(e_0^* - e_A)$ and $(e_s^* - e_A)$, as shown in Figure 1. Despite T_0 driving the sensible heat flux, the comprehensive dry-wet signature of the underlying surface due to soil moisture variations is directly reflected in T_R . Thus, T_R in the denominator is directly related to the surface moisture availability (M). In Equation 10, T_{0D} can be calculated as

$$T_{0D} = T_D + \frac{\gamma \lambda E}{\rho c_p g_A s_1}.$$
(11)

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164

Figure 1. Schematic representation of the exponential relationship between saturation vapor 165 pressure versus temperature. 166

An iterative method is applied to solve the equations because the four state variables and e_0^* , e_0 , α 167 and *M* are entangled. 168

2.1.3 Initialization 169

An initial value of α is assigned as 1.26 and initial estimates of e_0^* , e_0 are obtained from T_R and M170 as

171

$$e_0^* = 6.13753 e^{\frac{17.27T_R}{T_R + 237.3}} \tag{12}$$

$$e_0 = e_A + M(e_0^* - e_A).$$
(13)

M is initialized by assuming $e_0^* = e_s^*$, i.e., k in Equation 10 equals 1, expressed as follows 172

$$M = \frac{s_1(T_{0D} - T_D)}{s_2(T_R - T_D)}.$$
(14)

 T_{0D} can be expressed as 173

$$T_{0D} = \frac{e_s^* - e_A - s_3 T_R + s_1 T_D}{s_1 - s_3}.$$
(15)

The slopes s_1 and s_3 can be expressed as 174

$$s = 4098 \frac{6.13753e^{\frac{17.27T}{T+237.3}}}{(T+237.3)^2}$$
(16)

- where T is set to T_D and T_R for s_1 and s_3 , respectively. With the initial estimates of e_0^* , e_0 , α , and 175 *M*, g_A , g_C and λE can be calculated. Then e_0^* , e_0 , α and *M* are updated, and λE is recalculated. The 176 iteration continues until the convergence of λE is achieved. 177
- 2.1.4 Hysteresis consideration 178
- By considering the hysteresis between T_R , D_A , and λE , the surface moisture availability M can be 179 expressed as 180

$$M = \frac{\gamma s_1 (T_{0D} - T_D)}{s_3 (T_R - T_{0D})s + \gamma s_4 (T_A - T_D)}.$$
(17)

Hysteresis occurs because the capacity of the soil and vegetation to supply moisture to the atmosphere is larger in the morning than in the afternoon (Boegh et al. 1999). As such, two equations are used for estimating M in STIC depending on the occurrence of hysteresis. It is assumed that Equation 10 is used to indicate surface wetness that controls the evapotranspiration from the upper few centimetres of the surface, whereas Equation 17 is used to indicate the rootzone wetness that controls the evapotranspiration under strong hysteretic conditions between λE , R_N , T_R and D_A .

188 2.1.5 Driving parameters for STIC

The input variables used for driving the STIC model are listed in Table 1. The LST and emissivity 189 are retrieved from the EEH L2 LST product. The land surface properties including albedo, and 190 191 land use land cover (LULC) data and fractional vegetation coverage (FVC) are obtained from the Copernicus Global Land Service (CGLS, https://land.copernicus.eu/global/index.html). The 192 meteorological 193 data are obtained from the ERA5 reanalysis data 194 (https://cds.climate.copernicus.eu/cdsapp#!/search?type=dataset). All these CGLS and ERA5 data are spatially (bilinearly) and temporally (linearly) interpolated to match the ECOSTRESS LST 195 196 data.

Table 1. Input parameters for STIC, SEBS, and TSEB

Data	Purpose	Model	Source	Spatial	Temporal
				resolution	resolution
LST	R_N, T_R	STIC, SEBS, TSEB	ECOSTRESS	~70 m	daily
Emissivity	R_N	STIC, SEBS, TSEB ECOSTRESS		~70 m	daily
Black sky and	R_N	STIC, SEBS	CGLS	1 km	10-day
white sky					
albedo					
(a_{bs}, a_{ws})					
FVC	surface	STIC, TSEB	CGLS	300 m	10-day
	condition				
NDVI	surface	SEBS	CGLS	300 m	10-day
	condition				
LAI	surface	TSEB	CGLS	300 m	10-day
	condition				
LULC	surface	STIC, SEBS, TSEB	CGLS	100 m	annual
	condition				
Shortwave	R_N	STIC, SEBS	ERA5	0.25°	1 hour
direct radiation					
(R_{Sdir})					
Shortwave	R_N	STIC, SEBS, TSEB	ERA5	0.25°	1 hour
global radiation					
(R_S)					
Air temperature	lower boundary	STIC, SEBS, TSEB	ERA5	0.25°	1 hour
(T_A)	condition (2 m)				

Atmosphere vapour pressure (e_A) or	lower boundary condition (2 m)	STIC, SEBS, TSEB	ERA5	0.25°	1 hour
Dewpoint temperature					
(T_D)					
Wind speed	lower boundary condition (10 m)	SEBS, TSEB	ERA5	0.25°	1 hour

198 2.2 SEBS

199 The one-source SEBS model was developed by Su (2002), which also includes sub-models for the

200 roughness length of heat as well as momentum transfer and a formulation for the determination of

201 the evaporative fraction on the basis of energy balance at limiting cases.

- 202 To derive the sensible and latent heat fluxes, the similarity theory is used. In the Atmospheric
- 203 Surface Layer (ASL) similarity relationship, the profiles of the mean wind speed *u* and the mean
- 204 temperature $\theta_0 \theta_a$ can be expressed as follows

$$u = \frac{u_*}{k} \left[ln \left(\frac{z - d_0}{z_{0m}} \right) - \Psi_m \left(\frac{z - d_0}{L} \right) + \Psi_m \left(\frac{z_{0m}}{L} \right) \right]$$
(18)

$$\theta_0 - \theta_a = \frac{H}{ku_*\rho c_p} \left[ln\left(\frac{z-d_0}{z_{0h}}\right) - \Psi_h\left(\frac{z-d_0}{L}\right) + \Psi_h\left(\frac{z_{0h}}{L}\right) \right]$$
(19)

where z is the height above the surface (m), $u^* = (\tau_0/\rho)^{1/2}$ is the friction velocity (m s⁻¹), τ_0 is the surface shear stress (kg m⁻¹ s⁻²), ρ is the density of air (kg m⁻³), k = 0.4 is von Karman's constant, d_0 is the zero plane displacement height (m), z_{0m} is the roughness height for momentum transfer (m), θ_0 is the potential temperature at the surface (°C), θ_a is the potential air temperature (°C)at height *z*, z_{0h} is the scalar roughness height for heat transfer (m), ψ_m and ψ_h are the stability correction functions for momentum and sensible heat transfer respectively. *L* is the Obukhov length, which is defined as follows.

$$L = -\frac{\rho c_p {u_*}^3 \theta_v}{kgH} \tag{20}$$

where *g* is the acceleration due to gravity (m s⁻²) and θ_v is the potential virtual temperature near the surface.

The friction velocity, the sensible heat flux and the Obukhov stability length are obtained by solving the system of non-linear Eqs. 18-20. Derivation of the sensible heat flux using the above equations requires only the wind speed and temperature at the reference height as well as the surface temperature and is independent of other SEB terms.

The input parameters used for the SEBS model are listed in Table 1. Most of the input parameters are the same as used for the STIC model, except for two additional parameters. The normalized differential vegetation index (NDVI) data from CGLS are used in the retrieval of leaf area index (LAI) and canopy height. The wind speed from the ERA5 data is used in the retrieval of aerodynamic resistance.

223 2.3 TSEB

The TSEB model was first proposed by Norman et al. (1995) who represented the surface by a combination of soil and vegetation components. Through the introduction of the TSEB model, the problem of defining the extra resistance (caused by using the radiometric temperature instead of

227 aerodynamic temperature) in the calculation of sensible heat is bypassed.

Component radiometric temperatures are used to compute the surface energy balance fluxes for the canopy and soil components of the combined land surface system:

$$R_{N,S} = H_S + \lambda E_S + G \tag{21}$$

$$R_{N,C} = H_C + \lambda E_C \tag{22}$$

- where H_S and H_C are soil and canopy sensible heat fluxes, respectively. λE_S and λE_C are the soil evaporation and canopy transpiration, respectively. *G* is the soil conduction heat flux, $R_{N,S}$ and $R_{N,C}$ are the net radiation for the soil and canopy components.
- By using the series resistance network to account for the interactions between the soil and
- vegetation canopy fluxes, the sensible heat fluxes can be expressed as follows:

$$H_S = \rho c_p \frac{T_S - T_{AC}}{R_S} \tag{23}$$

$$H_c = \rho c_p \frac{T_c - T_{AC}}{R_X} \tag{24}$$

where R_S and R_X are the aerodynamic resistance from soil surface and total boundary layer aerodynamic resistance of the complete canopy leaves, respectively, T_{AC} is the momentum aerodynamic temperature.

For the latent heat flux from the canopy, the Priestly-Taylor formula is used to initially estimate a potential rate for λE_C

$$\lambda E_C = \alpha_{PT} f_G \frac{s}{s+\gamma} R_{N,C} \tag{25}$$

240 where α_{PT} is the Priestly-Taylor constant, with the initial value set to 1.3 and a higher value (~2)

under well-watered partial canopy cover conditions in advective environments, f_G is the fraction of green vegetation, with the initial value set to 1. Based on λE_C , the initial canopy temperature T_C

243 can be obtained as follows

$$T_c = T_a + \frac{R_{N,C}R_A}{\rho c_p} \left[1 - \alpha_{PT} f_G \frac{s}{s+\gamma} \right]$$
(26)

where R_A is the aerodynamic resistance to heat transfer (s/m). The soil component temperature can be calculated based on the ensemble radiometric temperature T_R and T_C . Then the sensible and latent heat fluxes of soil are calculated based on the energy balance.

- Non-physical solutions, such as daytime condensation at the soil surface (i.e., $\lambda E_S < 0$), can be
- obtained under conditions of moisture deficiency. This occurs because the initial value of a_{PT} used
- for the initiation of λE_C can lead to an overestimation of transpiration in water deficit environments.
- 250 If this is encountered, α_{PT} is iteratively reduced until λE_S approaches 0.

The input parameters used for the TSEB model are listed in Table 1, which are almost the same as used for SEBS. The canopy height is calculated using the FVC and LULC data by linear scaling between a seasonal minimum and maximum canopy height value for each land surface type (Massman 1997). The uniform driving variables for the three models facilitate a fair and thorough comparison among the three different SEB models.

256 **3 Evaluation method**

257 To evaluate the three EEH ET products, 19 eddy covariance (EC) sites over Europe were selected (Table 2) from the Integrated Carbon Observations System (ICOS) and European Fluxes Database 258 Cluster (EFDC). These sites cover six different biomes, including forest (deciduous broadleaf 259 forest, evergreen needleleaf forest and mixed forest), cropland, grassland, shrubland, wetland and 260 savanna. The instantaneous clear-sky ET estimates (in the form of latent heat flux) were compared 261 against half-hourly latent heat flux measurements closest to the ECOSTRESS overpass times 262 263 between 2018 and 2019 at the selected sites. A Bowen ratio SEB closure correction was applied to the EC data before the comparison based on the measurements of four components in surface 264 radiation budget, λE , H, and G (Bhattarai et al. 2018). Some extracts were unbale to provide all 265 the seven measurements required for the SEB closure correction and thus discarded. Moreover, 266 the extracts were also discarded if any of these seven measurements did not have a good quality 267 (indicated by the quality control flag). Considering the average footprint of the EC sites (Fisher et 268 al. 2020), subsets of 3×3 pixels were extracted centred on the tower coordinates and the average 269 ET values were used in the comparison. To mitigate the uncertainties introduced due to cloud 270 271 contamination, only extracts surrounded by 15×15 (approximately 1 km) cloud-free pixels (based on the EEH cloud mask product) were considered for further evaluation. The evaluation was first 272 273 conducted over different land surface types, followed by an overall comparison by gathering the samples at all the sites. 274

Table 2. List of the selected eddy covariance flux sites. The biomes are according to the IGBP 275 classification, and climate is according to the Köppen climate type. Biomes covered in this study 276 include deciduous broadleaf forest (DBF), evergreen needleleaf forest (ENF), mixed forest (MF), 277 savanna (SAV), cropland (CRO), grassland (GRA), shrubland (SHR) and wetland (WET). Climate 278 types include humid subtropical (Cfa), temperate oceanic (Cfb), hot-summer Mediterranean (Csa), 279 hot-summer humid continental (Dfa), warm-summer humid continental (Dfb), and subarctic (Dfc). 280 Mean annual precipitation (MAP) and aridity index (AI) indicate the aridity level at the sites. AI 281 is calculated as the ratio between precipitation and potential ET for 30 years and indicates the local 282

climatology.

Site ID	Biome	Climate	Latitude (°)	Longitude (°)	MAP	AI	Source
					(mm)		
BE-Lcr	DBF	Cfb	51.11	3.85	861	0.93	ICOS
BE-Lon	CRO	Cfb	50.55	4.75	743	0.97	ICOS
BE-Maa	SHR	Cfb	50.98	5.63	839	0.93	ICOS
BE-Vie	MF	Cfb	50.31	6.00	1062	1.37	EFDC
CZ-Wet	WET	Dfa	49.03	14.77	604	0.74	EFDC
DE-Geb	CRO	Cfb	51.10	10.92	470	0.58	EFDC
DE-Gri	GRA	Dfb	50.95	13.51	872	0.91	ICOS
DE-Kli	CRO	Dfb	50.89	13.52	842	1.00	EFDC
DE-Rur	GRA	Cfb	50.62	6.30	1033	1.38	EFDC
DE-RuS	CRO	Dfb	50.87	6.45	698	0.82	ICOS
ES-LM1	SAV	Csa	39.94	-5.78	700	0.30	EFDC

ES-Abr	SAV	Csa	38.70	-6.79	400	0.32	EFDC
FR-Aur	CRO	Cfb	43.55	1.11	669	0.74	ICOS
FR-Bil	ENF	Cfb	44.49	-0.96	960	0.89	ICOS
FR-Hes	DBF	Cfb	48.67	7.07	820	0.89	EFDC
FR-LGt	WET	Cfb	47.32	2.28	700	0.73	ICOS
FR-Mej	GRA	Cfb	48.12	-1.80	722	0.79	ICOS
IT-Lsn	SHR	Cfa	45.74	12.75	1100	0.91	ICOS
IT-Tor	GRA	Dfc	45.84	7.58	945	1.42	ICOS

284 Three statistical metrics were used to assess the performances of ET products:

$$r = \frac{\sum_{i=1}^{n} (E_i - \bar{E}) (O_i - \bar{O})}{\sqrt{\sum_{i=1}^{n} (E_i - \bar{E})^2} \sqrt{\sum_{i=1}^{n} (O_i - \bar{O})^2}}$$
(27)

$$RMSE = \sqrt{\sum_{i=1}^{n} \frac{(E_i - O_i)^2}{n}}$$
(28)

$$bias = \sum_{i=1}^{n} \frac{E_i - O_i}{n}$$
⁽²⁹⁾

where *r* is the Pearson's correlation coefficient, *RMSE* is root-mean-square error, *bias* is the mean

bias, between the model and measurements, *n* is the total number of data pairs. E_i and O_i are the model estimated and measured latent heat fluxes and \overline{O} is the average of observed values and \overline{E} is

model estimated and measured latent heat fluxes and $\boldsymbol{0}$ is the average of observed values and \boldsymbol{E} is the average of estimated values. Additionally, the Kling-Gupta efficiency (KGE) is adopted to

the average of estimated values. Additionally, the Kling-Gupta efficiency (KGE) is adopted to provide a quantitative and objective assessment of the agreement between the measured latent heat

269 provide a quantitative and objective assessment of the agreement between the like

fluxes and ET estimates (Gupta et al. 2009). It is calculated as follows

$$KGE = 1 - \sqrt{(r-1)^2 + (\frac{\sigma_s}{\sigma_0} - 1)^2 + (\frac{u_s}{u_0} - 1)^2}$$
(30)

where *r* is the Pearson correlation coefficient, σ_0 and σ_s are the standard deviations of EC site measurements and EEH estimates, respectively, and u_0 and u_s are the averages of measurements and estimates, respectively. The closer KGE is to 1, the more consistent the ET estimates are with the flux measurements.

Furthermore, the best performing ET product among the three was compared with the operational NASA ECOSTRESS ET product generated using the PT-JPL model (Fisher et al. 2020) at the same EC sites. The three statistical metrics described in Equations 27-29 were also used in the comparison.

299 4 Results

300 4.1 Model intercomparison

301 Comparison among the three EEH ET products over six different biomes (Figure 2) for a wide

range of soil water content (SWC) reveals that the STIC ET estimates produce the least statistical

errors over forest, cropland, shrubland and savanna (RMSE between 57.21 and 78.90 W m⁻², bias 303 between -21.43 and 38.36 W m⁻²). While the SEBS ET estimates have the highest consistency with 304 respect to EC measurements over grassland and wetland, the performance of SEBS is poor in 305 semiarid shrubland and savanna. SEBS shows the highest RMSE (~135 W m⁻²) and bias (~119 W 306 m^{-2}) in these water-scare ecosystems among the three ET products. In contrast, TSEB ET estimates 307 have the maximum RMSE (between 68.39 and 132.37 W m⁻²) and bias (between 36.77 and 92.83 308 W m⁻²) over most of the land surface types except for shrubland and savanna (RMSE between 60 309 and 85 W m⁻², bias between 10 and 50 W m⁻²). The performances of STIC and TSEB are 310 comparable over shrubland and savanna, with differences of RMSE and bias within 10 W m⁻². 311 Overall, ET estimates from STIC have consistent performances across different biomes. The SEBS 312 313 ET estimates perform reasonably well in radiation-controlled ecosystems, which is on the contrary to the TSEB estimates. 314

All the models show relatively higher uncertainties in ET estimates over forest and wetland, where 315 RMSEs are approximately 80 W m⁻² and biases are above 30 W m⁻². The large error in ET 316 estimates over forest is probably partly caused by the inconsistency between the meteorological 317 variables from the ERA5 reanalysis data and the actual conditions at the reference height above 318 the forest. On the contrary, due to the low canopy height and uniform landscape, the atmospheric 319 conditions are better depicted by the meteorological data over grassland and cropland, which leads 320 to a better ET estimation accuracy in these biomes. For the wetland, the high ET errors under high 321 SWC condition could be due to the presence of background water, which does not match the 322 conceptualized surface (soil-vegetation-atmosphere continuum) in the three SEB models. Over 323 324 savanna, the overestimation by all the models reflects the challenges in estimating ET over semiarid complex landscapes with substantial water stress and low magnitude of ET. 325





Figure 2. Comparison between the observed ET at EC sites and instantaneous ET estimates from STIC, SEBS and TSEB for 6 biomes during the period 2018–2019. The colour bar represents the soil water content (SWC) measurements from the EC sites.

The time series of EEH ET estimates at six representative biomes is shown in Figure 3. Overall, the ET estimates capture the variation in EC flux measurements although the magnitude is different on some days. The diurnal variation of ET is reasonably represented by the estimates (Figure 3(a) and (c)). The lagged responses of ET to rainfall events are shown. In line with the better performances over grassland and cropland in Figure 2, the EEH ET estimates are also closer to the



(d) IT-Lsn

EC measurements over these two biomes as compared to the other four. The overestimation of the EEH ET products over savanna is clearly embodied (Figure 3(f)).



Figure 3. Time series of the observed ET and EEH ET estimates from STIC, SEBS and TSEB at six representative sites of different biomes (a) forest (BE-Vie), (b) cropland (DE-RuS), (c) grassland (DE-Rur), (d) shrubland (IT-Lsn), (e) wetland (FR-LGt), and (f) savanna (ES-LM1). The blue line represents the diurnal cycle of latent heat flux measurements at the EC sites. The bar represents the daily precipitation obtained by accumulating the half-hourly measurements from the EC sites.

Overall, the STIC ET estimates have the lowest statistical errors (Figure 4). The accuracy of SEBS is similar, with an RMSE around 70 W m⁻², bias of ~10 W m⁻², and correlation coefficient (*r*) around 0.8. ET estimates from TSEB have a relatively larger RMSE (92.90 W m⁻²) and bias (49.45

345 W m⁻²) although having a similar r (0.77) to the other two models.



Figure 4. Comparison between the observed ET and EEH ET estimates at all the eddy covariance

sites for (a) STIC, (b) SEBS and (c) TSEB during the period between 2018 and 2019. The colour

bar represents the SWC measurements from the EC sites.

To understand the model performance under different aridity conditions, the relationship between KGE and aridity index is shown in Figure 5. Aridity index is calculated as the ratio between

²⁵¹ receipitation and notantial ET for 20 years, which indicates the local elimateleasy. Here, the Clobal

precipitation and potential ET for 30 years, which indicates the local climatology. Here, the Global

Aridity Index and Potential Evapotranspiration Climate Database v3 (Zomer and Trabucco 2022) 352 (Global-AI_PET_v3) at 1 km pixel scale was used to obtain the aridity indices at the EC sites. The 353 KGE for STIC at most of the sites are close to 1, indicating a good agreement between the ET 354 estimates and EC measurements. Only the two sites over wetland and two sites over savanna are 355 below 0.5, which is consistent with the large biases in these two biomes as found in Figure 2. It is 356 also clear that the accuracy of ET estimates improves when the sites have a humid climate (aridity 357 index >0.65) as compared to those with a semiarid (0.2-0.5) or dry subhumid (0.5-0.65) climate. 358 The SEBS estimates have a similar performance when the aridity index is above 0.5. Whereas 359 KEG is notably lower for SEBS under a semiarid climate. The KGE samples for TSEB are more 360

scattered, and the magnitudes of KGE at most of the sites are lower than STIC and SEBS.



Figure 5. KGE at different aridity levels for various sites for (a) STIC, (b) SEBS and (c) TSEB during the period between 2018 and 2019. Sites over the same land surface type are represented using the same marker. The KEG at ES-Abr for SEBS (-5.07) and TSEB (-2.50) are not shown due to the excessively low values. The higher the aridity index is, the more humid conditions are.

366 4.2 Comparison between STIC and PT-JPL

Given that the ET estimates from STIC showed the best agreement with the EC measurements, 367 STIC ET was compared with the official ECOSTRESS ET that was generated using the PT-JPL 368 model (Figure 6). The performance of STIC is pronouncedly better as compared to PT-JPL over 369 all the biome types. The differences in RMSE are ~ 50 W m⁻² in all the cases except over cropland 370 where the difference is around 20 W m⁻². The PT-JPL ET estimates are scattered, with most 371 samples above the 1:1 line. This is reflected in the large positive biases of PT-JPL estimates. The 372 overestimation of PT-JPL as compared to STIC in dry conditions (with low EC ET) is clearly 373 shown. In particular over shrubland and savanna, all the estimates from PT-JPL are greater than 374 from STIC. We infer that this is caused by the weak LST constraint in the PT-JPL model, which 375 makes the model insensitive to surface water stress. In the PT-JPL model, LST is just used in the 376 calculation of surface net radiation. Whereas in the STIC model, LST is embedded in the 377 calculation of surface soil moisture availability and thus directly linked to evaporative fraction 378 379 (Equation 5).





- **Figure 6.** Comparison between the observed ET at EC sites and instantaneous ET estimates from STIC and PT-JPL over 6 land surface types during the period between 2018–2020. The colour bar
- represents the SWC measurements from the EC sites.
- Overall, the PT-JPL model has a RMSE of 123.55 W m⁻² and bias of 48.54 W m⁻², which are both
- $\sim 50 \text{ W m}^{-2}$ higher than those of STIC. The PT-JPL ET estimates are scattered, in contrast to the
- 385 STIC estimates that are tightly and evenly distributed around the 1:1 line (Figure 7(a) and (b)).
- 386 The Taylor diagram further clarifies the closeness of STIC ET estimates to the ground 'truth'
- although the standard deviation of PT-JPL ET estimates is closer to that of the observations.



- **Figure 7.** Comparison between the observed ET and instantaneous ET estimates at all the eddy
- covariance sites for (a) STIC and (b) PT-JPL and (c) Taylor diagram during the period between 2018 and 2020.

391 **5 Discussion**

392 5.1 Factors affecting model performances

Different impact factors influencing the model performances were investigated, including SWC (Figure 8), vapor pressure deficit (VPD, Figure 9), viewing zenith angle (VZA, Figure 10), and FVC (Figure 11), respectively.

For all the models, the variation of ET bias with SWC is exponential (Figure 8). A sharp increase 396 in ET bias with progressive surface drving (decreasing SWC) is evident when SWC is below 0.1 397 $m^3 m^{-3}$, which is also associated with low ET magnitude. This is particularly obvious for SEBS, 398 which showed a large overestimation under dry conditions. This reflects the challenges as well as 399 400 opportunities in enhancing the performances of ET models in water-scarce regions where the coupling between the land surface and atmosphere is strong and evaporation is mainly driven by 401 soil water induced stomatal control (Mallick et al. 2022; Mallick et al. 2016). In contrast, when 402 SWC is above 0.2 m² m⁻², the ET bias tends to diminish and approaches zero, although 403 underestimation is indicated when EC ET are high. Due to the scattered samples of TSEB 404

estimates, the relationship between ET bias and SWC is not so strong ($R^2 = 0.07$) as found in STIC and SEBS. However, the overall trends in ET bias versus SWC are similar in all the three models.



Figure 8. ET bias (ET estimate minus ground measurement) versus SWC for (a) STIC, (b) SEBS and (c) TSEB during the period between 2018 and 2019. Samples at all the sites except for the wetland sites are included. The wetland sites are excluded due to the high SWC and different pattern between ET bias and SWC from the other land surface types.

411 Compared with SWC, the relationship between ET bias and VPD is not so strong although the bias

412 is generally larger when VPD is above 20 hPa (Figure 9). The increase of ET bias with VPD is

413 more noticeable for SEBS. This is consistent with the large uncertainty of SEBS that could not

adequately capture the low ET magnitudes over shrubland and savanna.



Figure 9. ET bias (ET estimate minus ground measurement) versus VPD for (a) STIC, (b) SEBS and (c) TSEB during the period between 2018 and 2019.

417 No impact of VZA on ET bias is found for all the three models (Figure 10). The magnitude of ET

bias across different VZAs is close. We infer this is partly because the angular variation of thermal

radiation is not pronounced when VZA is below 30° (Ermida et al. 2018; Hu et al. 2019; Mwangi

420 et al. 2022). Moreover, the high spatial homogeneity at the EC sites (Fisher et al. 2020) is also an

421 important factor for the weak angular variation of thermal radiation.



Figure 10. ET bias (ET estimate minus ground measurement) versus VZA for (a) STIC, (b) SEBS and (c) TSEB during the period between 2018 and 2019.

The overestimation of ET over sparsely vegetated surfaces (FVC < 0.5) is notable for all the three 424 models (Figure 11). The ET bias of STIC is lower as compared to the other two models, with most 425 of the samples below 100 W m⁻². The ET bias of SEBS for FVC <0.2 is substantially higher than 426 STIC and TSEB, which is consistent with the high RMSE of SEBS ET estimates over shrubland 427 and savanna. This is also reported in previous studies (Bhattarai et al. 2018; Boulet et al. 2012; 428 Faivre et al. 2017), which is mostly associated with the underestimation of H due to uncertainties 429 in the estimation of kB^{-1} and z_{0M} when the difference between T_R and T_0 is substantial. Chen et al. 430 (2013) proposed an improved roughness height parameterization by updating kB^{-1} of bare soil, 431 which showed a better performance than the original SEBS model by correcting for the 432 underestimation of H. However, it is beyond the scope of this study to compare the revised SEBS 433 434 model with the others in detail. For densely vegetated surfaces (FVC >0.8), the ET bias is evenly distributed above and below the zero-bias line. However, the magnitude of bias is higher over 435 densely vegetated surfaces due to the relatively higher ET. For TSEB, high biases in ET are found 436 when FVC approaches unity. This high bias in TSEB is presumably due to the uncertainty in 437 fraction of green vegetation, which is also reflected in the large RMSE of TSEB ET over forests 438 in Figure 2. Given no attempt was made to change the pyTSEB version of Nieto et al. (2016), we 439 adopted the default value of fraction of green vegetation (=1) of pyTSEB in EEH. This can be 440 somehow problematic when vegetation senescence occurs. However, accurate retrievals of these 441 vegetation biophysical parameters are difficult to obtain at large spatial scales, especially for 442 ECOSTRESS that only has TIR observations, which could add additional challenges to TSEB. 443 Moreover, the PT-TSEB version with a single PT coefficient was used in the EEH. The PM-TSEB 444 version with tabulated minimum stomatal resistance might mitigate the large uncertainties of 445 TSEB over densely vegetated surfaces (Colaizzi et al. 2014). 446





- and (c) TSEB during the period between 2018 and 2019.
- 449 5.2 Contrasting performances of ECOSTRESS ET products

The STIC ET estimates showed consistent performances over different land surface types. This 450 could be attributed to the non-parameterized structure of this model. Different from the other 451 thermal based models, the aerodynamic and surface resistances in STIC are expressed through 452 physical equations without empirical parameterization of surface roughness and atmospheric 453 stability corrections. However, the calculation of aerodynamic resistance relies on wind speed in 454 455 SEBS and TSEB, which makes these models relatively more sensitive to uncertainties associated with wind velocity. Moreover, the aerodynamic temperature is directly retrieved in STIC instead 456 of utilizing the radiometric temperature as a proxy and involving subsequent empirical corrections 457 as commonly conducted in one-source models (Mallick et al. 2022). As a result, the dependence 458 of ET estimates on additional inputs (e.g., wind speed and canopy height) is also eliminated in 459 STIC. LST is mainly used for depicting surface water availability in STIC rather than directly 460

461 calculating sensible heat flux. Considering the current validation datasets, the STIC model is462 relatively robust across varying biomes.

The SEBS ET estimates showed similar accuracy to the STIC estimates in all cases except for over 463 sparsely vegetated surfaces (i.e., shrubland and savanna). This could be associated with empirical 464 parameterizations of resistances to accommodate the inequality between radiometric temperature 465 and aerodynamic temperature (Mallick et al. 2022; Trebs et al. 2021). Over sparse canopies, large 466 uncertainties exist in the parameterization scheme. Bhattarai et al. (2018) and Trebs et al. (2021) 467 reported that uncertainties in kB^{-1} greatly hindered the accuracy of ET estimates in the arid and 468 semiarid ecosystems. Moreover, there is no universal methodology for calculating the heat 469 roughness length, which varies with vegetation structure, surface water stress and climatic 470 conditions (Kustas and Anderson 2009; Mallick et al. 2022). As such, the SEBS model should be 471 used with caution in operational ET retrieval. 472

The TSEB ET estimates had larger uncertainties overall as compared to STIC and SEBS. Over 473 forests, the RMSE and bias reached 132.37 and 92.83 W m⁻², respectively. As reported by Yang 474 et al. (2015), a major factor is the uncertainty in determining the initial P-T coefficient, which 475 represents the aerodynamic forcing and vegetation controls on ET. We used the value of 1.26 in 476 the model implementation. However, the P-T coefficient has strong spatial variations with surface 477 dryness, VPD, wind speed and canopy biophysical properties. Thus, a deterministic P-T coefficient 478 479 can lead to uncertainties at large scales. An adjustment of the initial P-T coefficient based on land surface type may mitigate the uncertainty in ET estimates (Andreu et al. 2018; Cristóbal et al. 480 2020; Cristóbal et al. 2017; Guzinski et al. 2013). Also, the soil aerodynamic resistance 481 parameterization and the associated empirical coefficients could be another reason (Li et al. 2019). 482 Moreover, the determination of fraction of green vegetation was simplified in EEH and set to 1 483 directly. This could also contribute to the large uncertainties of TSEB ET estimates considering 484 the import role of canopy biophysical parameters in heat transfer (Kustas et al. 2016). A possible 485 solution could be estimating f_G based on the empirical approach proposed by Fisher et al. (2008). 486 In this case, additional input parameters are required such as fraction of absorbed 487 photosynthetically active radiation (fAPAR), which will bring extra complexity in operational ET 488 retrieval. Although the biophysical parameters (e.g., LAI and FVC) used in TSEB are the same as 489 in STIC and SEBS, the TSEB ET estimates seem to be more susceptible to uncertainties in these 490 biophysical inputs due to the model structure and partitioning of energy between soil and 491 vegetation. Due to the absence of visible and shortwave infrared (VSWIR) bands in the 492 ECOSTRESS observations, external biophysical parameters were used in the ET retrieval. 493 494 However, the temporal and spatial mismatches between these biophysical parameters and the instantaneous ECOSTRESS LST estimates could have introduced errors into the TSEB ET results 495 (Anderson et al. 2021). 496

The accuracy of PT-JPL ET estimates was substantially lower as compared to the STIC estimates 497 498 over all the land surface types. This could be attributed to the following reasons. First, the ECOSTRESS LST is only used for calculating surface net radiation in PT-JPL ET retrieval. Net 499 radiation has a weak dependence on LST and therefore the ET products generated using PT-JPL 500 does not take full advantage of surface water stress information embodied in LST. Second, PT-501 JPL relies on atmospheric vapor pressure deficit instead of LST for constraining the ET 502 components. Moreover, the determination of the P-T coefficient for different biomes is a challenge 503 504 as well as a major source of uncertainties. Thus, a physically based formula is needed to estimate

the P-T coefficient for better interpolation of the aerodynamic forcing and soil-vegetation controlin the SEB process.

507 5.3 Uncertainties and limitations in the current evaluation

Although we selected EC sites with good maintenance and only used good quality flux measurements, uncertainties could still exist in the measured fluxes, which may have influenced the evaluation results. Due to the unavailability of well-maintained EC sites over Africa, we only evaluated the EEH ET products over Europe. Also, sites in semiarid regions (e.g., over savanna) have limited sample numbers due to the sparse spatial coverage of ECOSTRESS over the Iberian Peninsula. Inclusion of more EC sites over Africa and semiarid regions in Europe would benefit a

514 more thorough and comprehensive evaluation of EEH ET products in the future.

In the ECOSTRESS observations, only five thermal bands (three since May 2019 due to the loss 515 of the two onboard Mass Storage Units) are available. Therefore, ancillary data related to land 516 surface biophysical properties can only be obtained from external sources. In the case of EEH, we 517 used the CGLS FVC, and albedo data generated from Sentinel-3/OLCI and PROBA-V. Therefore, 518 discrepancies in spatial resolution and satellite overpass times cannot be avoided, which could 519 impact the ET retrieval process. Moreover, cloud masking without the support of VSWIR bands 520 is challenging and problematic. Although strict cloud screening was exercised in the evaluation, 521 residuals from the cloud mask could still harm the accuracy of LST retrieval, thus impacting ET 522 estimation. Fortunately, in the future thermal missions such as TRISHNA and LSTM, these 523 problems will be minimized substantially with the measurement in VSWIR bands. 524 Correspondingly, the accuracy of ET estimates can be envisaged to further improve. 525

526 Due to the issue with the sensor's radiometric calibration in Collection 1 ECOSTRESS data, a cold 527 bias of ~1 K was found in the ECOSTRESS LST products (Hulley et al. 2021). This has been 528 addressed in Collection 2 that will be released in 2022. Accordingly, we will reprocess the 529 ECOSTRESS LST, and ET products based on the Collection 2 ECOSTRESS radiance data and 530 extend the temporal coverage of EEH products to September 2023 in the Phase-2 of EEH. The 5-531 year time series of high spatio-temporal resolution ECOSTRESS products with improved accuracy 532 is expected to greatly benefit the studies on terrestrial ecosystem processes.

533 6 Conclusion

TIR observations from ECOSTRESS onboard the ISS with high spatio-temporal resolution 534 provide a good opportunity for generating LST and ET products at the field scale over the globe. 535 In this study, we evaluated three ECOSTRESS ET products generated in the EEH project based 536 on three structurally contrasting thermal-based SEB models (i.e., STIC, SEBS, and TSEB). The 537 ET estimates were compared against latent heat flux measurements at 19 EC sites over Europe 538 between 2018 and 2019. Furthermore, the best performing STIC ET estimates were compared with 539 the NASA official ECOSTRESS ET products using the PT-JPL model at the same sites. Six 540 different land surface types were encompassed in the evaluation, including forest, grassland, 541 cropland, shrubland, wetland and savanna. 542

The results revealed that the STIC ET estimates had consistent performance over different land surface types with a relatively better accuracy as compared to the other two models, which is

directly linked to the analytical framework of STIC without resistance parameterizations. The 545 SEBS estimates had similar performances to STIC except over shrubland and savanna where the 546 uncertainties of SEBS ET were substantially higher than for the other two models. This is attributed 547 to the large uncertainties in empirical parameterizations of resistances to accommodate the 548 inequality between radiometric temperature and aerodynamic temperature in SEBS over sparsely 549 vegetated surfaces. The performance of TSEB was particularly good in water-scarce ecosystems. 550 However, large uncertainties were found in TSEB in radiation-controlled ecosystems. The setting 551 of P-T coefficient, soil aerodynamic resistance parameterization, fraction of green vegetation 552 values, and temporal and spatial mismatches between the input biophysical parameters and the 553 instantaneous ECOSTRESS LST retrievals could account for the high uncertainties to some extent. 554

Compared with the PT-JPL estimates, the performance of STIC was substantially better over all the land surface types. The overall RMSE and bias were both \sim 50 W m⁻² higher in the PT-JPL estimates than those of STIC. The serious overestimation of PT-JPL ET estimates could be explained by the weak LST constraint in the model.

We conclude that the high spatio-temporal resolution EEH ET products provide an unprecedented opportunity for environmental and agricultural applications. The comprehensive evaluation among the EEH ET estimates driven by uniform forcing data provides insights into SEB models with different structures and contrasting parameterization schemes. Overall, the EEH is promising to serve as a support for the future thermal missions such as TRISHNA jointly collaborated by France

and India, SBG from NASA and LSTM from ESA.

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