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Are Buckminsterfullerenes “Molecular Ball Bearings”?

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1 Abstract

2 Buckminsterfullerenes (C₆₀) are near-spherical
3 molecules which freely rotate at room temper-
4 ature in the solid state and when dissolved in
5 solution. An intriguing question arises as to
6 whether C₆₀ molecules can act as “molecular
7 ball bearings”, i.e. preventing direct contact
8 between two solid surfaces whilst simultane-
9 ously dissipating shear stress through fast ro-
10 tation. To explore this, we performed measure-
11 ments of friction across a solution of C₆₀ in the
12 boundary lubrication regime. High resolution
13 shear and normal force measurements between
14 mica sheets separated by the C₆₀ solution were
15 made using a Surface Force Balance to provide a
16 single-asperity contact and sub-nanometer res-
17 olution in film thickness. We find that, even
18 at small volume fraction, C₆₀ forms a solid-like
19 amorphous boundary film sustaining high nor-
20 mal load, suggesting that this system undergoes
21 a glass transition under confinement. The C₆₀
22 film gives rise to a low friction coefficient up
23 to moderate applied loads, and we discuss the
24 possible relevance of the ball bearing effect at
25 the molecular scale.

26 Introduction

27 Human activity has always required the mo-
28 tion of objects, from the building of edifices in

29 prehistorical ages to the harvesting of energy
30 with wind turbines in present times. The ques-
31 tion of whether logs were used as “rollers” to
32 move megaliths has been debated,¹ nonetheless
33 it is clear that the idea of using wheels to re-
34 place sliding by rolling was early found to be
35 an efficient way to reduce energy dissipation
36 during motion, i.e. friction. While formulat-
37 ing the first fundamental laws of solid friction,
38 Da Vinci conceived of many ingenious machines
39 involving rotary parts where the friction is lim-
40 ited to the axis.² Ball bearings, consisting of
41 balls running along a groove (e.g. in an axle
42 assembly), are designed to reduce the friction
43 further by transforming sliding into rolling. It
44 is also known, since ancient times,³ that lu-
45 bricating the contact, i.e. inserting a liquid
46 between the moving solids, is an efficient way
47 to reduce wear and produce a moderate, or
48 at least stable friction. However, finding good
49 lubricants is complex because the appropriate
50 mixture has to remain effective in harsh condi-
51 tions (high loads/shear stresses/temperatures,
52 humidity etc.), and the field of tribology has
53 been active over the past century and until to-
54 day.⁴⁻⁶ Detailed, mechanistic interpretations of
55 friction are often complicated by processes act-
56 ing over multiple length-scales and timescales
57 simultaneously. For example a fluid may lu-
58 bricate motion as a thick film (hydrodynamic
59 regime) or in molecular confinement between
60 close asperities (boundary regime), either at dif-

61 ferent regions of a rough contact or under dif- 110
62 ferent shearing conditions. 111

63 Buckminsterfullerene (C_{60}) is a molecule of 112
64 almost ideal spherical shape⁷ (structure in Fig- 113
65 ure 1(a)). In its pure form under ambient con- 114
66 ditions C_{60} forms a solid in which the molecules 115
67 are able to rotate freely; inspection of the tem- 116
68 perature dependence of the heat capacity shows 117
69 that the energy associated with rotation of C_{60} 118
70 in the crystal is smaller than the ambient ther- 119
71 mal energy.⁸ This interesting property, com- 120
72 bined with relative chemical stability, led to 121
73 the early proposal that C_{60} could act as an 122
74 effective boundary lubricant: it might be ex- 123
75 pected that even when confined between two 124
76 surfaces it could rotate to dissipate stress, the 125
77 molecules effectively performing as “molecular 126
78 ball bearings”. Direct observations have shown 127
79 that spherical nanoparticles can rotate between 128
80 sheared surfaces, in a manner which is remi- 129
81 niscent of the rolling without slipping motion 130
82 of macroscopic ball bearings.⁹ By analogy to 131
83 the macroscopic mechanism of ball bearings, a 132
84 molecular ball bearing system should sustain 133
85 normal load (i.e. keeping the shearing solid 134
86 surfaces apart) yet without hindering molec-
87 ular rotations (which serve to dissipate shear
88 stress and so reduce friction). Although this
89 provides a useful motivating concept to con-
90 sider the effect of rotations in modifying fric-
91 tion at the nanoscale, we note that the macro-
92 scopic mechanism of ball bearings does not map
93 perfectly onto molecular systems under ambient
94 conditions: the molecular rotation rate will typ-
95 ically be much higher than the imposed shear
96 under ambient conditions. To differentiate be-
97 tween these two situations, we call the molec-
98 ular mechanism the “molecular ball bearing ef-
99 fect”. In this work we measure and appraise
100 whether C_{60} might satisfy these criteria. 134

101 Previous studies have investigated lubrication 147
102 by C_{60} or fullerene-like molecules in dif- 148
103 ferent ways. On one hand, they have been 149
104 used as a solid lubricant in dry conditions 150
105 (from simply dispersed powder to carefully 151
106 sublimated thin film), but they didn’t pro- 152
107 vide particularly exceptional frictional proper- 153
108 ties.^{10–14} C_{60} have been used as wheels for single- 154
109 molecule “nanocars”, and the displacement of 155

such nanocars was found to be indeed due to
the rotation of the C_{60} on the Au-(111) sur-
face at ~ 200 °C.¹⁵ Experimental and numer-
ical studies investigated the frictional behavior
on a C_{60} single crystal around an orientational
order-disorder phase transition at ~ 260 K, but
no significant change of friction coefficient was
found.^{16,17} On the other hand, when C_{60} or
fullerene-like molecules have been used as an
additive in a liquid, they formed a protective
boundary film that prevents wear and induces
a stable frictional response.^{18–20} In particular,
Campbell et al. confined a dispersion of C_{60}
in toluene between atomically-smooth mica sur-
faces in a Surface Force Apparatus, and studied
the hydrodynamic lubrication regime by look-
ing at the viscous response to a normal oscilla-
tion. They showed that this system exhibits a
full slip boundary condition, suggesting a par-
ticular “fluidity” of the C_{60} that are adsorbed
on the surfaces.¹⁸ In the present paper, we re-
port the first measurements of friction across a
dispersion of C_{60} in the boundary lubrication
regime.

Methods

Materials. C_{60} was synthesised via the arc
discharge method according to the procedure
first published by Krätschmer et al.²¹ and
was further isolated by high performance liq-
uid chromatography (HPLC) to a purity of
99.5%. Tetralin, 1,2,3,4-tetrahydronaphthalene
(Sigma-Aldrich, anhydrous, 99%), was used
as solvent (chemical structure in Figure 1(a)).
Tetralin was chosen as a good solvent for C_{60}
(solubility of C_{60} in tetralin is 16 mg/mL
at 25 °C²²) with low volatility (vapor pres-
sure of 0.05 kPa at 25 °C²³) and a mod-
erate viscosity (2.015 mPa.s at 25 °C²⁴).
The tetralin was dried with molecular sieves
(0.4 nm pore size, from Fisher Chemical)
for a week, and filtered before use (Ultra-
Cruz Syringe Filter, PTFE, 0.22 μ m). C_{60}
molecules were dispersed at a concentration of
5.60 \pm 0.01 mg/mL, corresponding to a mo-
lar fraction of 0.1065 \pm 0.0002% (given the
tetralin density of 0.9645 g/mL at 25 °C²³), or

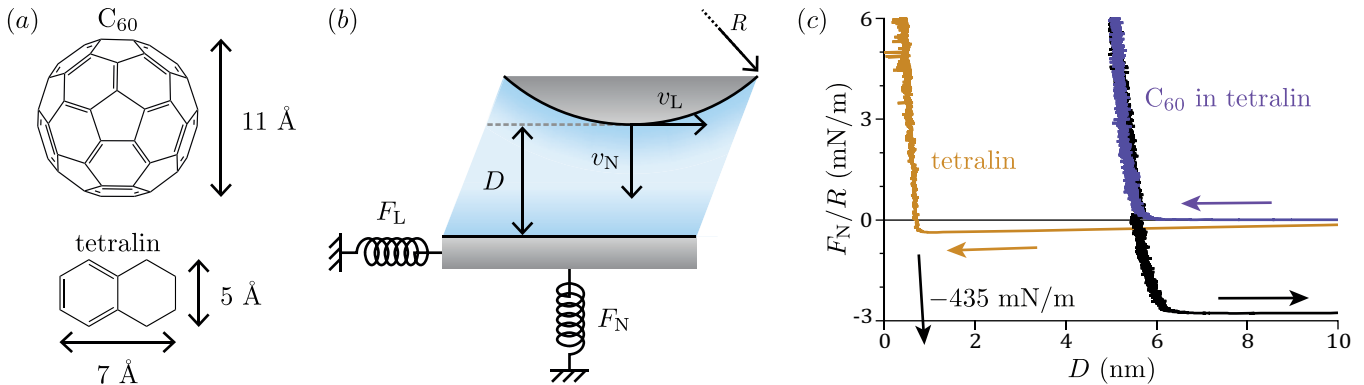


Figure 1: (a) Chemical structures and sizes of buckminsterfullerene (C_{60}) and tetralin. (b) Schematic of the SFB experiment, that allows to determine the interaction and friction forces between two mica surfaces separated by a liquid film of controlled thickness. (c) Normal force F_N rescaled by the radius of curvature R of the surfaces as a function of the separation D obtained at approach velocities $v_N \sim 1$ nm/s, for tetralin (approach in brown, pull-off force measured on retraction indicated by the black arrow) and the solution of C60 in tetralin (approach in purple, retraction in black).

156 a mean distance between the C_{60} molecules of 185
 157 5.979 ± 0.004 nm $\sim 5 \times$ (C_{60} diameter). 186

158 **Force measurements.** The measurements 187
 159 were performed with a Surface Force Balance 188
 160 (SFB), which is a method ideal for the study 189
 161 of normal and lateral forces transmitted across 190
 162 fluid and soft films with high resolution. A 191
 163 schematic diagram of the key aspects is in Fig- 192
 164 ure 1(b). The liquid film is held between two 193
 165 optical lenses, hemi-cylindrical in shape (ra- 194
 166 dius of curvature $R \sim 1$ cm) and arranged in 195
 167 crossed-cylinder configuration. This geometry 196
 168 provides a point of closest approach between 197
 169 the two surfaces, which is model experiment for 198
 170 study of a single-asperity contact. The optical 199
 171 lenses are coated with single crystal sheets of 200
 172 mica, so that the roughness is sub-molecular 201
 173 (roughness arising only from the atomic cor- 202
 174 rugation of the crystalline surfaces). The pre- 203
 175 cise geometry and liquid thickness are measured 204
 176 directly in-situ using white light interferome- 205
 177 try; so-called Fringes of Equal Chromatic Or- 206
 178 der (FECO). The surfaces (lenses) can be trans- 207
 179 lated in both normal and lateral directions rel- 208
 180 ative to one another, and the resulting forces 209
 181 between them are detected via the deflection 210
 182 of normal and lateral springs. These measure- 211
 183 ments can be performed simultaneously, so that 212
 184 information about film thickness, normal force, 213

and shear force can be measured in parallel (e.g. during approach of the surface from large distances to contact). The details of the procedure have explained elsewhere;²⁵⁻²⁸ in the following we note the quantities and details particular to the present experiments.

Muscovite mica is cleaved, backsilvered and glued on glass cylindrical lenses using dextrose, D-(+)-glucose (Sigma-Aldrich, 99.5%, chosen for its insolubility in tetralin). Two surfaces are mounted in a crossed-cylinder geometry to make a single contact between atomically smooth surfaces, and the liquid is injected in between to form a capillary bridge. The chamber is dried with P_2O_5 , phosphorus pentoxide (Sigma-Aldrich, 99%) and the room is regulated to 25°C. FECO are analyzed to measure the radius of curvature R of the surfaces and the liquid thickness, D . D is measured with a precision of 0.02 nm (RMS noise) and accuracy of 1 nm and $D = 0$ is defined as the mica-mica contact position measured in dry air before liquid injection. The refractive indices of 1.5413 at 20°C for tetralin²³ and 1.5417 at 22°C for the mixture were measured with a Bellingham+Stanley Abbe 60 ED refractometer.²⁹ A stepper motor is used to approach or retract the top surface at a normal velocity v_N and a sector piezo-electric tube allows application of

214 a shearing motion at lateral velocity v_L . Nor-260
215 mal force F_N and lateral force F_L are then mea-261
216 sured using springs, with respective stiffness of 262
217 133.8 ± 3.0 N/m and 441 ± 4 N/m. 263

218 Results

219 **Normal force.** The normal force profiles ob-267
220 tained are shown in Figure 1(c). For pure 268
221 tetralin, the surfaces experience a (van der 269
222 Waals) attractive interaction on approach of 270
223 the surfaces to ~ 10 nm causing a jump-in 271
224 to contact. The surface separation just after 272
225 the jump-in is close to the direct mica-mica 273
226 contact value (within the systematic experi-274
227 mental error). The finite gradient of this soft 275
228 wall is due to the compression of the mica, 276
229 the single material remaining in the optical 277
230 interferometer. On retraction the two sur-278
231 faces jump-out when reaching a pull-off force 279
232 of $F_{adh}/R = -435$ mN/m, which according to 280
233 the JKR theory corresponds to an adhesion en-281
234 ergy of $W = 2F_{adh}/(3\pi R) = -92$ mN/m.²⁵ 282
235 This value is comparable with the adhesion en-283
236 ergy between -160 mN/m and -108 mN/m 284
237 measured previously for mica-mica contact in 285
238 dry nitrogen.³⁰ It is not clear why a structural 286
239 force is not observed in this case, as might be 287
240 expected by comparison with similar measure-288
241 ments with apolar liquids like cyclohexane, ben-289
242 zene or toluene which do each give rise oscilla-290
243 tory structural surface forces.^{26,31-35} However, 291
244 a similarly strong adhesion minimum has also 292
245 been observed for these liquids, and attributed 293
246 to the presence of traces of water that wets the 294
247 mica surfaces. Particular care was taken to use 295
248 tetralin in dry conditions (storage in molecular 296
249 sieves, measurements with P_2O_5 in the cham-297
250 ber), however it is still possible that traces of 298
251 water may remain giving rise to an adsorbed 299
252 layer or part-layer on the mica. In the sub-300
253 sequent experiments we take this control mea-301
254 surement with pure tetralin as the reference sit-302
255 uation in order to investigate the effect of the 303
256 addition of small quantities of C_{60} under the 304
257 same conditions. 305

258 When 0.1 mol % C_{60} is added to the tetralin 306
259 the normal force between the surfaces is mod-307
308

ified significantly, as clear in Figure 1(c). On
approach of the surfaces a repulsive soft wall
is reached at ~ 6 nm, compressing by several
nm with increased load (appearing even more
clearly in Figure 3(b)). The onset of repul-
sion corresponds to the thickness of approxi-
mately 5 C_{60} molecules, and the soft wall holds
for loads up to 80 μ N, corresponding to a pres-
sure of ~ 6 MPa (given the contact radius of
 ~ 2 μ m), and on retraction an adhesive min-
imum of $F_{adh}/R = -2.7$ mN/m is obtained.
This value is comparable with what Campbell
et al. measured for C_{60} in toluene between
mica.¹⁸

In summary of the normal force profiles, we
find that very small volume fractions of C_{60}
lead to substantial modification to the inter-
action force between confining surfaces, giving
rise to a monotonic repulsive force extending to
 ~ 5 molecular diameters. This insight allows
us subsequently to interpret the direct friction
measurements, as follows.

Lateral force. Having characterised the nor-
mal interaction between the surfaces, we next
applied a lateral (shearing) motion of the top
surface relative to the bottom surface and de-
tected the resulting lateral force transmitted
across the liquid. In the SFB this can be per-
formed at the same time as approaching the sur-
faces and measuring the film thickness and nor-
mal force; in this section we present results of
the measured friction as a function of separation
and load. We compare the case of pure tetralin,
as control, to the tetralin with C_{60} . In Fig-
ure 2 we show the result of measurements with
pure tetralin (part (a)) and with C_{60} in tetralin
(part(b)). For the control experiment with pure
tetralin, we show the temporal evolution of the
liquid thickness D and the lateral force F_L when
the top surface is moved downward and then
upward at $v_N = 0.92 \pm 0.05$ nm/s and simultane-
ously oscillated laterally at $v_L = 287 \pm 1$ nm/s.
When the surfaces are separated by a finite
film of tetralin, before reaching surface con-
tact, no measurable lateral force is detected
(smaller than the sensitivity of ~ 1 μ N), mean-
ing there is no mechanical coupling between
the surfaces. At the point of jump-in to con-
tact the lateral force instantaneously increases

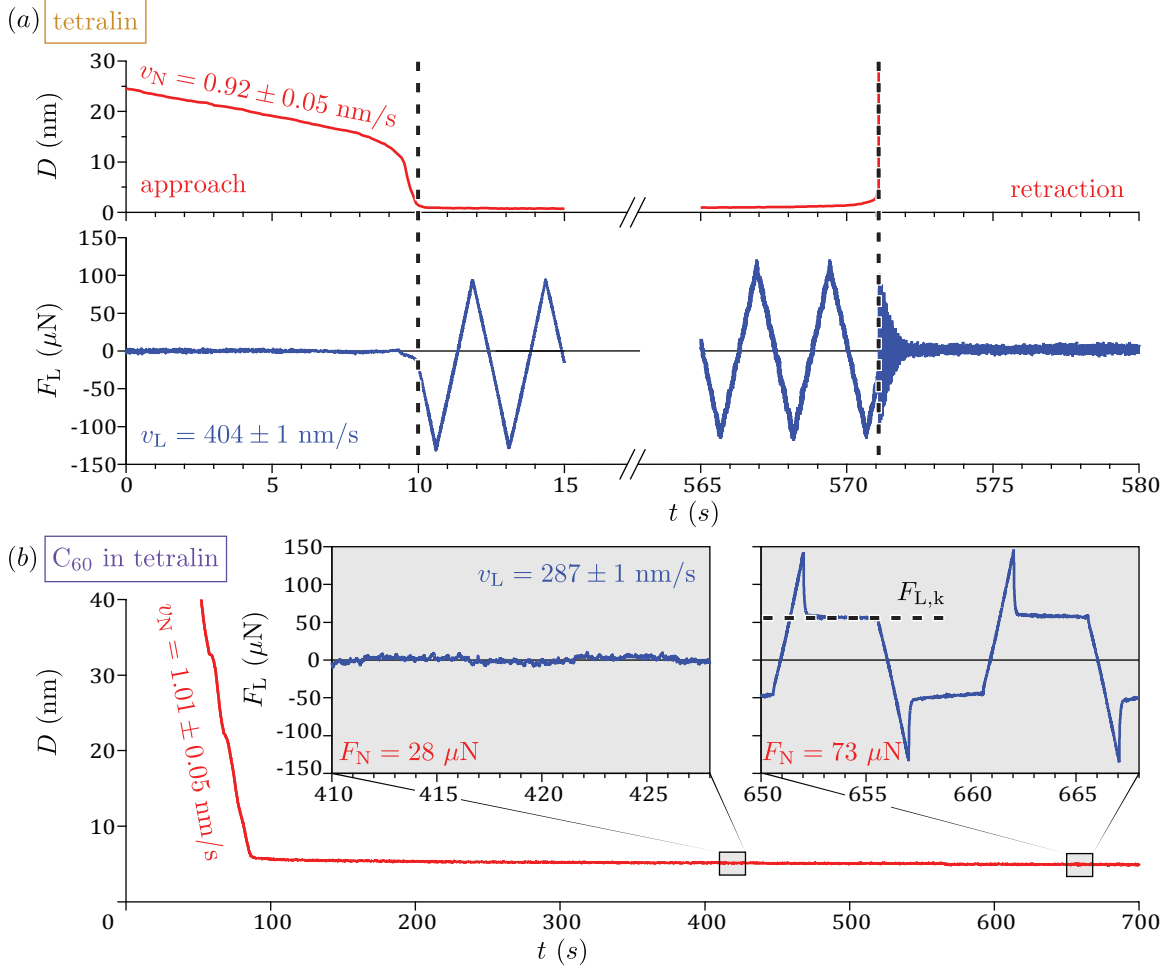


Figure 2: (a) Temporal evolutions of liquid thickness D (red traces) and lateral force F_L (blue traces) when approaching and retracting mica surfaces separated by tetralin with simultaneous constant-velocity shearing of one surface. The lateral force is below the experimental resolution until the surfaces reach direct contact, at which point they are rigidly coupled. (b) Temporal evolution of liquid thickness D when approaching the surfaces and simultaneously applying constant-velocity lateral motion to one surface across the solution of C_{60} in tetralin. The insets show the lateral force F_L at two time intervals (or equivalently two loads F_N as indicated), showing how the lateral force during shearing cycles evolves as the applied load is increased. At higher loads a clear yield spike followed by smooth sliding is observed; from this the kinetic friction $F_{L,k}$ is deduced.

309 in magnitude and varies directly with the ap- 358
 310 plied shearing amplitude; the saw-tooth shape 359
 311 is the signature that the surfaces are rigidly cou- 360
 312 pled, i.e with no relative motion throughout the 361
 313 cycle. Because of the strong adhesion between 362
 314 the surfaces, friction is controlled by adhesion³⁶ 363
 315 and is so high that the yield point of the con- 364
 316 tact is not reached within the range of lateral 365
 317 force explored. Thus we find that the yield force 366
 318 of the contact must be higher than 110 μN in 367
 319 this case. In experiments with higher shear- 368
 320 ing amplitudes, we found that the yield force 369
 321 was in fact higher than 330 μN ; corresponding 370
 322 to a lower limit for the contact shear stress of 371
 323 $\sigma_L \sim 26$ MPa. During retraction, a damped os- 372
 324 cillation at the resonance frequency of ~ 25 Hz 373
 325 is obtained when the surfaces jump-out, and 374
 326 then no lateral force is detected, consistently 375
 327 with the behavior on approach. In sum, we find 376
 328 that tetralin alone cannot support any applied 377
 329 load, and so squeezes out of a contact when fi- 378
 330 nite load is applied, giving rise to high friction 379
 331 in accordance with direct mica-mica contact. 380

332 Lateral forces measured across the solution of 381
 333 C_{60} in tetralin as a function of load - examples 382
 334 of which are in Figure 2(b) - show an entirely 383
 335 different behavior. When the surfaces approach 384
 336 to the distance corresponding to the repulsive 385
 337 wall the lateral force is still below the sensi- 386
 338 tivity limit. It was necessary to increase the 387
 339 load before any detectable lateral force could 388
 340 be recorded between the surfaces; the left-hand 389
 341 inset show the emergence of tiny lateral forces 390
 342 when the surfaces are being pushed together 391
 343 with a force of 28 μN . The amplitude of the 392
 344 lateral force then increases with the load, and 393
 345 the signal exhibit a strong stiction spike fol- 394
 346 lowed by a plateau (right-hand side inset). The 395
 347 clear yield point followed by sliding behavior is
 348 typical of a solid-like response to lateral applied
 349 stress. We systematically extracted the ampli- 396
 350 tude of the plateau, which we identified as the
 351 kinetic friction force $F_{L,k}$. In Figure 3(b) we 397
 352 compare the normal force and kinetic friction 398
 353 force profiles as a function of surface separation, 399
 354 D . In this representation, we clearly see that 400
 355 the range of the friction force is much smaller 401
 356 than the range of the normal force, becoming 402
 357 measurable only at separations of ~ 4 nm at 403

which point the layer is already substantially
 compressed and the load is high, qualitatively
 similar to what has been observed for lubrication
 by polymer brushes.³⁷ As shown in Figure
 3(a), the relationship between the kinetic
 friction force and the load is not linear, instead
 it has a strongly convex shape. At small loads,
 kinetic friction is proportional to the load, with
 no significant contribution from adhesion (zero
 friction at zero imposed load) and a coefficient
 of proportionality $\mu = 0.072 \pm 0.002$ (with
 the coefficient of friction defined as the local
 slope $\mu = dF_{L,k}/dF_N$). This quantity increases
 with the load, and reaches $\mu = 4.1 \pm 1.6$ at the
 maximum imposed load. Thus the friction coef-
 ficient evolves from a very low value, indicating
 efficient lubrication at moderate load, up to a
 high value under strong compression. To com-
 ment on these values, it is useful to compare
 them to the friction coefficient of different liq-
 uids between mica surfaces, all measured with
 a Surface Force Balance. Simple apolar liquids
 are generally characterized by a single friction
 coefficient: 1.1 for octamethylcyclotetrasiloxan
 (OMCTS), 2.2 for cyclohexane.³⁸ Ionic liquids
 exhibit quantized friction,³⁹ i.e. a friction co-
 efficient indexed by the number of ordered lay-
 ers of ions in the film, typically varying from
 0.007 to 0.5 for 1-decyl-1-methylpyrrolidinium
 bis[(trifluoromethane)sulfonyl]imide, $[\text{C}_{10}\text{C}_1\text{Pyrr}]$
 $[\text{NTf}_2]$.⁴⁰ Regarding the low-load friction coef-
 ficient, the C_{60} solution is thus between apolar
 liquids and ionic liquids, and is compara-
 ble with the 0.12 obtained for 2,6,10,15,19,23-
 hexamethyltetracosane (squalane), a branched
 hydrocarbon liquid that has been reported for
 exhibiting glassy behavior in certain confine-
 ment conditions.⁴¹

Discussion

A solid film. We now propose a simple qual-
 itative picture of what is happening at the
 molecular scale to interpret the observed behav-
 ior. The molecular forces governing the inter-
 action between C_{60} , tetralin and mica include
 van des Waals and steric forces. Mica is polar,
 and maybe covered with a (sub-)molecular

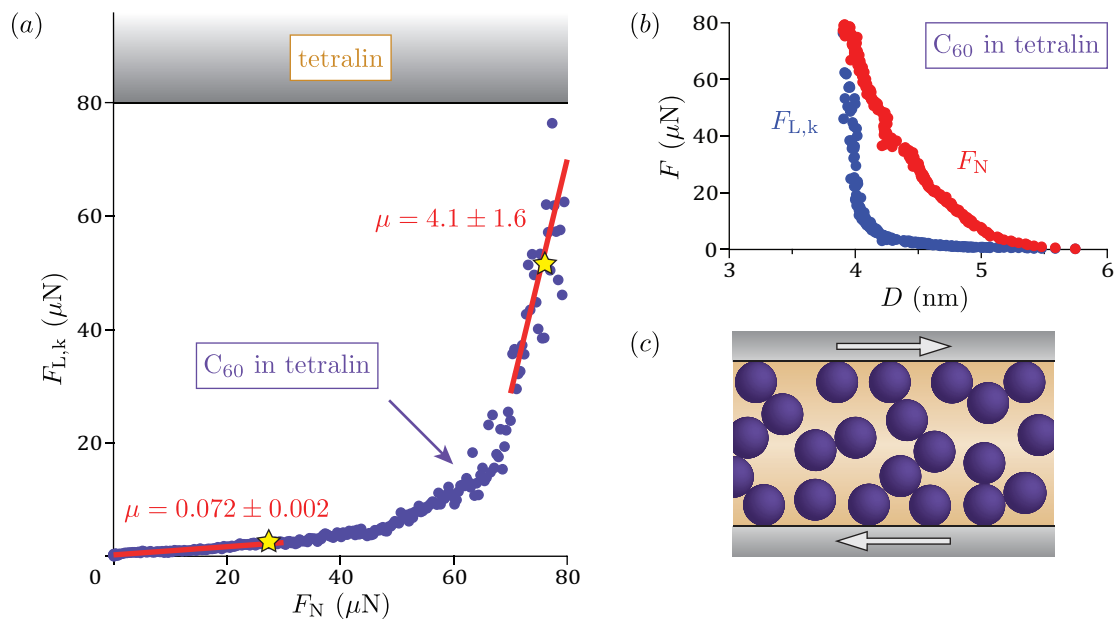


Figure 3: (a) Kinetic friction $F_{L,k}$ as a function of load F_N . Friction in pure tetralin was above the range limit of the experiment, as indicated by the shaded bar, whereas the solution of C_{60} in tetralin gave rise to measurable friction (in purple). The two stars correspond to the lateral force traces shown in insets of Figure 2(b), and the red lines are the linear fits used to deduce the local friction coefficient μ . (b) Normal (red) and kinetic friction (blue) force profiles, for the solution of C_{60} in tetralin. (c) Schematic representation of the system in confinement: the C_{60} molecules are randomly packed, steric interactions lead to a significant repulsion between the solid surfaces, but fast rearrangements induce a relatively small shearing resistance.

404 film of water. Tetralin is slightly polar and 453
 405 polarizable (calculated static polarizability of 454
 406 $1.8 \times 10^{-39} \text{ C} \cdot \text{m}^2/\text{V}$), whereas C_{60} is more 455
 407 polarizable because of the highly delocalized 456
 408 π electrons (measured static polarizability of 457
 409 $8.6 \times 10^{-39} \text{ C} \cdot \text{m}^2/\text{V}$ ⁴²). When the mica sur- 458
 410 faces are far apart, the C_{60} molecules in the 459
 411 bulk are separated by an average distance of 460
 412 about 5 times their diameter (deduced from the 461
 413 chosen concentration) and are attracted by a 462
 414 dispersion (London) interaction but the liquid 463
 415 dispersion is thermodynamically stable because 464
 416 the concentration is (just) below the saturation 465
 417 limit. A monolayer of C_{60} is probably initially 466
 418 adsorbed on each mica surface due to the induc- 467
 419 tion (Debye) interaction and the preference of 468
 420 mica for the more polar C_{60} rather than tetralin. 469
 421 When confining the liquid, tetralin tends to be 470
 422 squeezed-out, as shown by the reference mea- 471
 423 surement. The local concentration of C_{60} in 472
 424 the gap therefore increases as the surfaces ap- 473
 425 proach and the C_{60} molecules - which are al- 474
 426 ready close to the aggregation limit in the bulk 475
 427 solution - are expected to agglomerate, forming 476
 428 a strongly bound solid film (as shown by the 477
 429 soft wall in the normal force profile). The fact 478
 430 that this film holds for pressures up to $\sim 6 \text{ MPa}$ 479
 431 is remarkable, given that a yield stress of about 480
 432 $\sim 1 \text{ MPa}$ is measured when compressing a C_{60} 481
 433 single crystal along the $\langle 110 \rangle$ direction.⁴³ This 482
 434 is probably due to the fact that we are dealing 483
 435 with a nanometric film, the C_{60} having attrac- 484
 436 tive interactions with the confining surfaces and 485
 437 being packed in a disordered arrangement with 486
 438 no cleaving plane. 487

439 **A disordered film.** The absence of order 488
 440 in the film is revealed by the normal force pro- 489
 441 file showing a soft wall at distance of approx- 490
 442 imately 5 C_{60} diameters. This behavior was 491
 443 unexpected, because a structural force is usu- 492
 444 ally observed for apolar liquids between mica. 493
 445 When Campbell et al. studied a solution of 494
 446 C_{60} in toluene between mica, they observed 495
 447 a soft wall at $\sim 3.4 \text{ nm}$ at approach veloci- 496
 448 ties higher than 5 nm/s , or a structural force 497
 449 of period of 1.1 nm equal to the diameter of 498
 450 the C_{60} molecules at smaller velocities.¹⁸ They 499
 451 interpret this transition as C_{60} molecules be- 500
 452 ing kinetically trapped between the surfaces 501

and having no time to order. We never ob-
 served a structural force over the explored spots
 on the surfaces, experiments and velocities be-
 tween $\sim 1 \text{ nm/s}$ and $\sim 12 \text{ nm/s}$. This is most
 likely to be due to the different solvent and
 concentration chosen: Campbell et al. used
 a concentration of 0.095 mg/mL correspond-
 ing to a molar fraction of $\sim 0.001\%$ or $\sim 3\%$
 of the saturation limit in toluene (2.8 mg/mL
 at $25 \text{ }^\circ\text{C}$ ²²), whereas here we use a concentra-
 tion of 5.60 mg/mL corresponding to a molar
 fraction of $\sim 0.1\%$ or $\sim 35\%$ of the saturation
 limit in tetralin (16 mg/mL at $25 \text{ }^\circ\text{C}$ ²²). In our
 case, the C_{60} molecules in the bulk are much
 more concentrated and close to the agglomera-
 tion limit, and the order/disorder kinetic tran-
 sition may have been shifted to approach ve-
 locities much smaller than 1 nm/s . Combining
 the observations of no structural force and of
 a solid-like friction response, we conclude that
 under the experimental conditions used the C_{60}
 must form a disordered/amorphous solid, i.e. a
 glass, where the molecules are randomly packed
 in the gap (as illustrated in Figure 3(c)). The
 situation is thus related to the difficult prob-
 lem of glass transition in confinement, already
 investigated for various systems⁴⁴ like simple
 liquids,⁴⁵ polymers,⁴⁶ liquid crystals⁴⁷ or col-
 loids.⁴⁸ It is then tempting to interpret our mea-
 sured kinetic friction-load curve as a kind of
 Angell plot, that conventionally represents how
 the logarithm of the viscosity increases with the
 inverse temperature (for molecular liquids) or
 with the packing fraction (for colloidal liquids)
 when approaching the glass transition.^{49,50} Fol-
 lowing this scenario, it would be the increase
 of the C_{60} packing fraction with the load (as
 shown by the compression of the film) that leads
 to a dramatic slowing down of the dynamics,
 i.e. of the rearrangement timescale of the glassy
 film in the gap, as measured by the increase of
 the friction force.

Role of rotation. One can finally ask
 whether the rotation of C_{60} contributes to the
 frictional behavior. As shown by a 2D molecu-
 lar dynamics simulation of lubrication by cir-
 cular molecules, a high concentration in the
 gap can lead to jamming, which hinders the
 molecular rotation because the two sides of two

502 molecules in contact would have to rotate in 548
503 opposite directions.⁵¹ So if the rotation of C₆₀ 549
504 plays a role in our system, it is likely to happen 550
505 at small loads, for which we indeed measured a 551
506 small friction coefficient. Because of the rela- 552
507 tively strong adhesion of the C₆₀ on mica (De- 553
508 bye interaction), the lateral motion is probably 554
509 distributed in the middle of the gap and not 555
510 at the film/mica interfaces. The small resis- 556
511 tance to flow in the gap indicates that energy 557
512 is dissipated efficiently in the film; the mech- 558
513 anism for this could originate from (at least) 559
514 three modes. First, there is only small adhesion 560
515 between C₆₀ molecules (London interaction).¹⁸ 561
516 Second, there is room and time for rearrange- 562
517 ments, since C₆₀ molecules are randomly packed 563
518 with vacancies, at a packing fraction far enough 564
519 from the glass transition. Third, the C₆₀ may 565
520 rotate freely in the thin disordered film, like 566
521 they do in the bulk crystal, and this free ro-
522 tation could contribute to a dissipation mecha-
523 nism leading to low friction. In other words, a
524 “molecular ball bearing” effect may be occurring
525 and be partly responsible for the low friction
526 regime.

527 Conclusions

528 To summarize our findings, C₆₀ performs as 567
529 an excellent boundary lubricant additive in our 568
530 system; $\sim 0.1\%$ of C₆₀ is sufficient to form a 569
531 strong boundary film that reduces wear by pre- 570
532 venting direct contact between the sliding sur-
533 faces and gives rise to a small friction coefficient
534 at moderate loads. A key ingredient leading to 571
535 this useful outcome is that C₆₀ has a finite sol- 572
536 ubility and tends to solidify when the concen- 573
537 tration exceeds the saturation point locally in
538 confined contacts thus preventing squeeze-out 574
539 of the film. The fact that the C₆₀ appears to 575
540 form a disordered solid, evidenced by no regu- 576
541 lar oscillatory structural force despite solid-like 577
542 mechanical response, indicates that the convex 578
543 friction-load relationship may be the manifes- 579
544 tation of a glass transition under confinement. 580
545 The friction coefficient at moderate loads is re- 581
546 markably small, and so it is hypothesised that
547 the molecular rotations intrinsic to C₆₀ – the

“molecular ball bearing effect” – may be impor-
tant for reducing shear stress.

Future investigations should involve a sys-
tematic study of the effect of the concentra-
tion on kinetic trapping and on friction re-
sponse. To clarify the role of molecular rota-
tion, comparative Surface Force Balance mea-
surements with C₆₀ chemically grafted to the
surfaces and thus unable to rotate^{52,53} could be
performed. It would also be of interest to study
different surface materials such as graphene;⁵⁴
with only *sp*²-hybridized carbon materials ex-
ceptional properties can emerge.^{55–57}

Author Contributions

R.L. and C.D. performed the experiments. S.P.
and R.L. conceived of the project, interpreted
the data and wrote the paper. K.P. and S.S.
synthesised the fullerenes and contributed to
the experimental design.

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825 Graphical TOC Entry

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