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Thermal Properties of Nanocrystalline Silicon Nanobeams

Jeremie Maire,* Emigdio Chávez-Ángel, Guillermo Arregui, Martin F. Colombano, Nestor E. Capuj, Amadeu Griol, Alejandro Martínez, Daniel Navarro-Urrios, Jouni Ahopelto, and Clivia M. Sotomayor-Torres

Controlling thermal energy transfer at the nanoscale and thermal properties has become critically important in many applications since it often limits device performance. In this work, the effects on thermal conductivity arising from the nanoscale structure of free-standing nanocrystalline silicon films and the increasing surface-to-volume ratio when fabricated into suspended optomechanical nanobeams are studied. Thermal transport in structures with different grain sizes is characterized and elucidated the relative impact of grain size distribution, from 10 to 400 nm, and geometrical dimensions on thermal conductivity. A micro-time-domain thermoreflectance method is used to study free-standing nanocrystalline silicon films and find a drastic reduction in the thermal conductivity, down to values below $10 \text{ W m}^{-1} \text{ K}^{-1}$. Decreasing the grain size further decreases the thermal conductivity. In optomechanical nanostructures, this effect is smaller than in membranes due to the competition of surface scattering in decreasing thermal conductivity. Finally, a novel versatile contactless characterization technique is introduced that can be adapted to any structure supporting a thermally shifted optical resonance and used to evaluate the thermal conductivity. The data agrees quantitatively with the thermoreflectance measurements. This work opens the way to a more generalized thermal characterization of optomechanical cavities and to create hot-spots with engineered shapes at desired positions in the structures as a means to study thermal transport in coupled photon-phonon structures.

1. Introduction

Depending on the application, materials with widely varying thermal properties may be required. While for thermoelectric applications ultra-low thermal conductivity is essential,^[1,2] high thermal dissipation rates are mandatory for thermal management in microelectronics.^[3] Therefore, it is crucial to understand thermal transport at the nanoscale to design structures with optimized thermal properties for a given application. Optomechanics (OM)^[4] is one such application for which one typically wants to avoid absorption and the resulting heating, either to operate the resonator in the quantum regime, which is why 2D structures are usually preferred over nanobeams, or even to induce amplification by dynamical back-action.^[5] However, other approaches use thermal properties to control the mechanical resonator, for example, self-pulsing-induced lasing^[6–8] or bolometric back-action. Therefore, the direction towards thermal management in OM depends on the targeted application, making it essential to

J. Maire^[†], E. Chávez-Ángel, G. Arregui, M. F. Colombano, D. Navarro-Urrios, C. M. Sotomayor-Torres
Catalan Institute of Nanoscience and Nanotechnology (ICN2)
CSIC and BIST
Campus UAB, Bellaterra, Barcelona 08193, Spain
E-mail: jeremie.maire@u-bordeaux.fr

G. Arregui, M. F. Colombano
Depto. Física
Universidad Autónoma de Barcelona
Bellaterra, Barcelona 08193, Spain

N. E. Capuj
Depto. Física
Universidad de La Laguna
San Cristóbal de La Laguna 38200, Spain

 The ORCID identification number(s) for the author(s) of this article can be found under <https://doi.org/10.1002/adfm.202105767>.

^[†] Present address: Institut de Mécanique et d'ingénierie (I2M) CNRS UMR5295, Talence 33405, France

N. E. Capuj
Instituto Universitario de Materiales y Nanotecnología
Universidad de La Laguna
Santa Cruz de Tenerife 38071, Spain

A. Griol, A. Martínez
Nanophotonics Technology Center
Universitat Politècnica de València
València 46022, Spain

D. Navarro-Urrios
MIND-IN2UB
Departament d'Enginyeria Electrònica i Biomèdica, Facultat de Física
Universitat de Barcelona
Martí i Franquès 1, Barcelona 08028, Spain

J. Ahopelto
VTT Technical Research Centre of Finland Ltd
P.O. Box 1000, Espoo FI-02044 VTT, Finland

C. M. Sotomayor-Torres
Catalan Institute for Research and Advances Studies ICREA
Barcelona 08010, Spain

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1 acquire direct information on thermal properties instead of
2 having them as free parameters in complex models.

3 In the context of micro- and nanoscale thermal transport,
4 single crystal silicon (c-Si) has been widely used as a platform
5 to study thermal engineering with structures like phononic
6 crystals. Si nanostructures exhibit strongly reduced thermal
7 conductivity,^[9–14] non-diffusive thermal transport,^[15] and tuning
8 of the thermal conductivity through the modified dispersion
9 relation in phononic crystals.^[16,17] In these structures, surface
10 phonon scattering is the main mechanism impacting thermal
11 properties when the dimensions are smaller than the mean free
12 path of phonons in the bulk material, that is, in the range of
13 100 nm to a few micrometers.^[18–22] Nanocrystalline Si (nc-Si)
14 is a specific type of polycrystalline Si in which the grain size
15 is well below 1 μm . Due to the relatively easy tuning of the
16 mechanical, optical, electrical, and thermal properties by tai-
17 loring the stress and grain-size,^[23] as well as controlled material
18 fabrication with conventional low-temperature amorphous Si
19 deposition techniques, nc-Si is widely used in MEMS offering
20 a cost-competitive alternative to crystalline silicon in many
21 practical scenarios such as 3D integration.^[24] In nc-Si, the scatter-
22 ing of phonons at grain boundaries adds to other phonon
23 scattering mechanisms. This kind of scattering further reduces
24 the thermal conductivity in nc-Si, cf. single c-Si, in nanostruc-
25 tures such as phononic crystals.^[25,26] In this work, we quantify
26 the relative effect of grain boundary scattering on thermal con-
27 ductivity in corrugated OM nanobeams. Recently, nc-Si was
28 shown to be an excellent, versatile, and cost-competitive alter-
29 native to its crystalline counterpart to exploit OM non-linear
30 dynamics under ambient conditions, with non-linear dynamic
31 functions such as mechanical lasing and chaos, over a much
32 larger frequency bandwidth compared to Silicon-on-Insulator
33 (SOI) devices.^[27] A complementary study of various properties
34 of nc-Si thin films realized at different annealing temperatures
35 focused on different grain sizes and tensile stress.^[23]

36 Here, we investigate the thermal properties of nc-Si mem-
37 branes and optomechanical nanobeam cavities with different
38 grain sizes, which are structurally characterized by image pro-
39 cessing of dark-field transmission electron microscope (TEM)
40 images. To access the thermal decay rates and conductivity,
41 we use two pump-probe techniques. For a direct assessment,
42 we use micro time-domain thermoreflectance ($\mu\text{-TDTR}$) as a
43 proven technique and extract the thermal conductivity by fitting
44 the experimental temperature rise with finite element mod-
45 eling (FEM). We demonstrate that the thermal conductivity of
46 the nanocrystalline membrane is at least 4 times lower than its
47 crystalline counterpart, with a further reduction by a factor of 2
48 when grain size decreases to an average of 163 nm. A similar
49 phenomenon occurs in the nanobeams studied here but its
50 relative impact is smaller than in membranes as it competes
51 with enhanced surface scattering stemming from the lower
52 dimensions of these nanobeams. We further introduce a new
53 two-laser measurement technique for direct measurements of
54 thermal properties of in operandi OM nanobeams, similar to
55 time-stretch spectroscopy used for microspheres.^[28] This tech-
56 nique is based on the cooling rate of an optical resonance to
57 measure the thermal decay rate of the cavity. We unveil the
58 potential of this technique, which can be readily applied in cur-
59 rent OM devices with an optical cavity, and compare the results

1 to those obtained by $\mu\text{-TDTR}$. We show how optical resonances
2 with different profiles can induce a thermal dissipation rate
3 variation of up to 20% in a single optical cavity. Our results
4 provide new insights on the thermal characteristics of nc-Si
5 devices, which may find application in optics, optomechanics,
6 and energy-harvesting devices.

2. Nanocrystalline Silicon Films and Structural Analysis

12 The membranes and nanobeams were fabricated on wafers
13 with a thick silicon dioxide film and a 220 nm thick nc-Si layer
14 on top of the oxide, resembling the SOI wafers typically used in
15 the fabrication of optomechanical devices. The wafers were pro-
16 duced by the following process. A thick SiO_2 layer is first grown
17 by wet oxidation at 1050 $^\circ\text{C}$ on a Si wafer, followed by a 220 nm
18 thick layer of amorphous Si (a-Si) deposited at 574 $^\circ\text{C}$ by low-
19 pressure chemical vapor deposition (LPCVD). Four wafers were
20 annealed at different temperatures: 650 (OMS1), 750 (OMS2),
21 850 (OMS3), and 950 $^\circ\text{C}$ (OMS4) for 60 min. The annealing
22 converts the amorphous Si to nc-Si, with the grain size distri-
23 bution ranging from a few nm to a few hundreds of nm. The
24 thickness of the nc-Si films after annealing was 211 nm meas-
25 ured by spectroscopic reflectometry.

26 Bright field planar TEM images of the nanocrystalline film
27 annealed at 950 $^\circ\text{C}$ (OMS4) and the corresponding selective area
28 diffraction pattern are shown in **Figure 1**. The crystallites do not
29 exhibit a preferential orientation. The image is representative of
30 all the samples used in this work with only the grain size distribu-
31 tion obtained by analyzing dark-field TEM images varying with
32 annealing temperature. In all samples, the crystallite size has a
33 log-normal distribution with the average crystallite size of 163
34 (OMS1), 171 (OMS2), 187 (OMS3), and 215 nm (OMS4). The a-Si
35 layer is under compressive stress after deposition and annealing
36 convert it to tensile, measured to be 290 (OMS1), 250 (OMS2), 170
37 (OMS3), and 90 MPa (OMS4). Further details of the nc-Si wafer
38 fabrication, grain size, and stress analysis can be found in Ref. ^[23]

39 To identify the effects arising from the nanocrystallinity of
40 the material, identical reference samples were fabricated on
41 commercial SOI wafers with a 220 nm thick single-crystalline
42 Si layer. Since measurements are performed in air, all struc-
43 tures possess a layer of native oxide on their free surfaces.
44 This layer has been shown to decrease thermal conductivity in
45 ultrathin membranes with thickness below 30 nm.^[9] However,
46 the intensity of the effect decreases for thicker membranes and
47 is thus expected to be small for the structures investigated in
48 this manuscript. Furthermore, since all structures possess this
49 native oxide layer, it does not impact the relative analysis of
50 their thermal properties. A summary of the structural charac-
51 teristics of all samples is given in **Table 1** and samples will be
52 designated by their average grain size from now on.

3. Thermal Conductivity Measurements by $\mu\text{-TDTR}$

57 The thermal properties of a device are affected by the structure
58 of the material itself, the processing steps, the operating condi-
59 tions, and the geometry of the device. It has been shown that

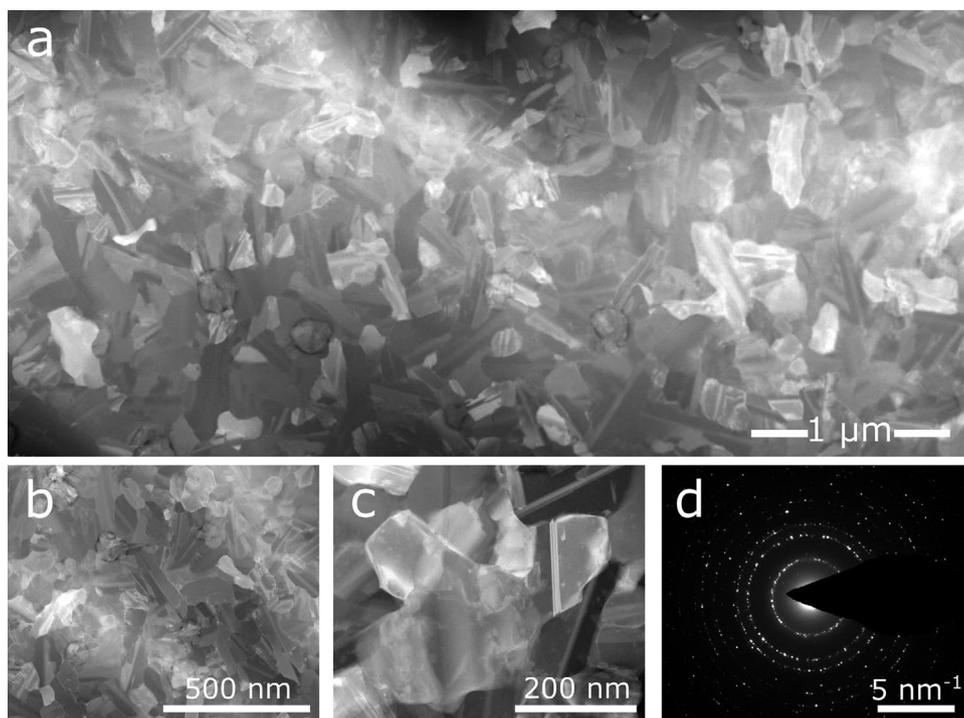


Figure 1. Structure of nanocrystalline silicon. a–c) Bright field planar TEM images of the nc-Si film with an average grain size of 215 nm and $T_a = 950\text{ }^\circ\text{C}$ with increasing zoom, showing the randomly oriented grains and their relatively large size distribution. d) Selective area electron diffraction image.

the surface can play a major role in thermal conductivity when the surface-to-volume ratio (S/V) is large.^[9] We use μ -TDTR technique to measure the thermal conductivity of the nanocrystalline films and the nanobeams. The thermal conductivity extracted with this technique corresponds to the ability of the material to conduct heat by accounting for the effects of nanopatterning, such as phonon boundary scattering and the reduction in the volume of material. μ -TDTR has been previously used to characterize the thermal properties of numerous nanostructures, including membranes, nanobeams,^[29,30] phononic crystals,^[31–35] or phonon lenses,^[36] and to demonstrate effects such as heat focusing,^[36] ballistic thermal transport,^[29,30,37] and to highlight the contribution of the wave nature of phonons to thermal transport at cryogenic temperatures.^[17] We use two different sample designs shown in **Figure 2**, one for investigation of the role of the nanocrystalline material and the other to investigate the role of surfaces. The gold pad in the middle of the samples acts as a transducer and as the detector. The temperature of this pad is directly related to its reflectivity, which is probed by a continuous-wave laser (532 nm). A 405 nm pulsed

laser periodically heats the metal and lets it cool down between pulses. The heating time is chosen to allow the system to reach a steady state. The temperature gradient across the structures then progressively disappears as the heat flows from the central pad to the heat bath. The characteristic time for the temperature gradient to vanish is measured and its inverse gives the heat dissipation rate. The cooling curve can be described with a single-parameter exponential decay in time, $\exp(-\gamma t)$, where γ is the heat dissipation rate of the system. Further details about the technique and a schematic of the setup are given elsewhere.^[17,36]

The nanobeams consist of an optomechanical cavity flanked on both sides by an OM Bragg mirror to prevent the leakage of the colocalized optical and mechanical modes. Each part of the OM nanobeam consists of a repetition of unit cells comprising a central beam with stubs on both sides and a cylindrical hole in the center. The OM nanobeam is shown in **Figure 2**. The OM cavity used to confine optical and GHz mechanical modes corresponds to the central region of 12 unit cells in which the pitch, hole diameter, and stub width along the beam axis progressively decrease towards the center by a factor Γ , which is typically around 0.8. On both sides of this region, the Bragg mirrors consist of 10 unit cells. The nominal values of the pitch, hole diameter, and stub width are 500, 300, and 250 nm, respectively. The dimensions perpendicular to the beam axis, which are nominally identical in the Bragg mirrors and in the cavity are the width of the central beam (500 nm) and the depth of the stub (500 nm). A detailed schematic is shown in **Figure S2**, Supporting Information, and the fabrication process of these OM nanobeams is detailed elsewhere.^[8] The fabrication process is explained in the Supporting Information.

Table 1. Summary of structural characteristics of fabricated samples.

	Thickness [nm] (monitor wafers)	T_a [$^\circ\text{C}$]	Average grain size [nm]	Tensile stress [MPa]
c-Si	220			-39
OMS4	211	950	215	90
OMS3		850	187	170
OMS2	211	750	171	250
OMS1		650	163	290

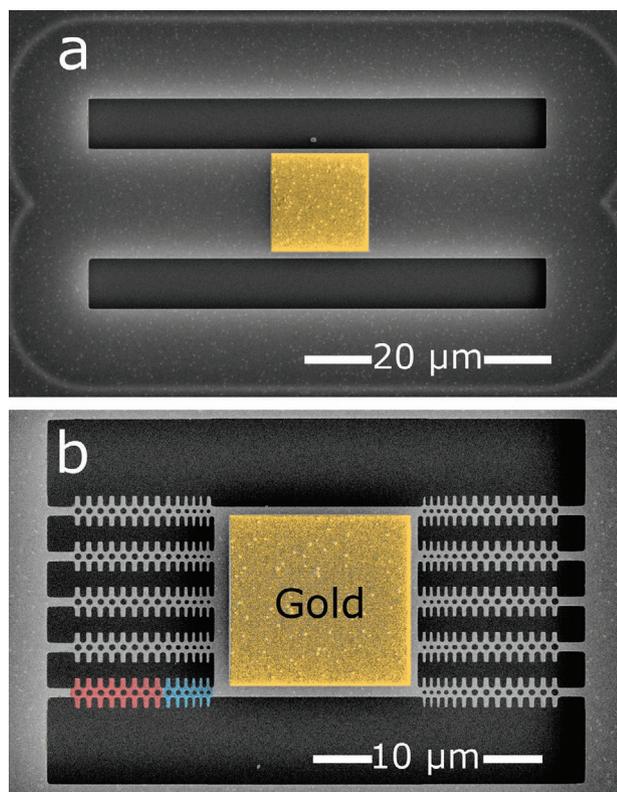


Figure 2. Structures for μ -TDTR measurements. a) SEM image of a suspended nc-Si membrane. b) SEM image of the nanobeams. The Bragg mirror of the bottom left beam is shown in red and half of the optomechanical cavity in blue. The central gold pad that is the transducer for μ -TDTR measurements is highlighted in yellow.

We first investigate the effect of nanocrystals on thermal transport by measuring nominally identical suspended membranes fabricated on the wafers with different annealing temperatures T_a . In these structures, the only phonon scattering mechanism that is not intrinsic to the material is surface scattering at the top and bottom surfaces of the membranes. As this scattering only depends on the spacing between the surfaces, which is identical for all samples, and the surface quality, the differences in heat dissipation rates solely stem from the crystallinity. For each of the nanocrystalline samples, we measure three nominally identical structures. We then calculate the average value of the heat dissipation rate γ and the standard deviation of the measurements gives the error bars. The results are shown in **Figure 3a**. It is clear in the figure that γ increases with annealing temperature and it is not an intrinsic feature instead directly depending on the geometry, as can be seen that the shorter membranes dissipate heat faster. The intrinsic thermal property is the thermal conductivity. Due to the geometry of the structure, neither the 1D nor the 2D heat equation can be used to analytically deduce the thermal conductivity. Hence, we use FEM simulations to virtually reproduce our μ -TDTR experiments, with a heating phase modeled by an inward heat flux in the metal pad, of the same duration as the experimental heating, and a cooling phase. The temperature is “probed” at the center of the metal pad. In this 3D FEM model, thermal conductivity is the only free parameter. The heat dis-

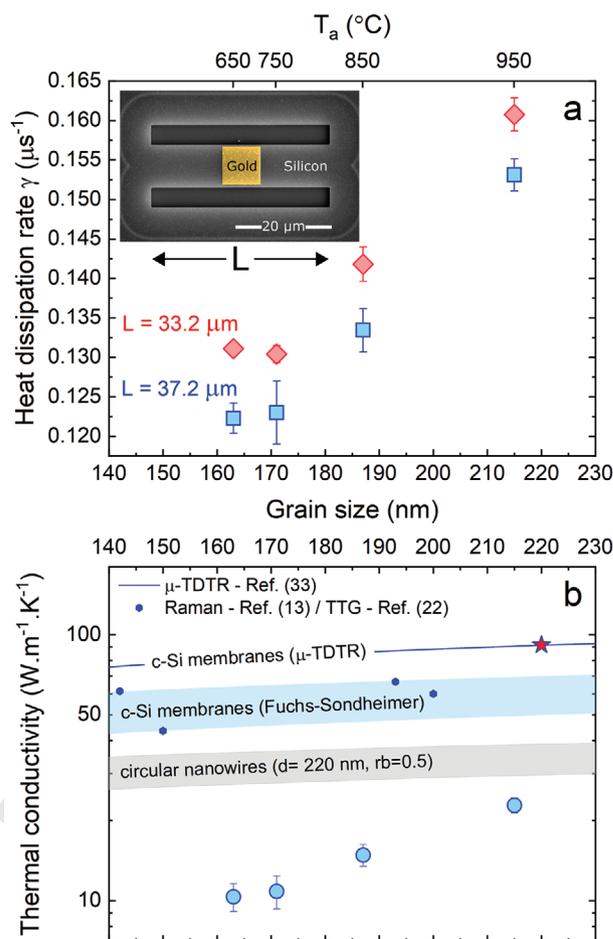


Figure 3. Thermal properties of nanocrystalline Si membranes. a) Heat dissipation rate γ measured as a function of the annealing temperature T_a and the corresponding average grain size for two membrane lengths L . b) Thermal conductivity of the same membranes as a function of T_a (light blue dots). The blue “c-Si membranes” line corresponds to a fit of the μ -TDTR data for crystalline silicon, adapted from Ref. [33]. The red star indicates the estimated thermal conductivity of a 220 nm thick c-Si membrane. The small blue dots and the blue stripe represent the thermal conductivity of c-Si membranes measured by Raman thermometry^[13] and the TTG technique.^[22] The stripes represent calculations for membranes based on the Fuchs–Sondheimer model (blue) and for circular nanowires (220 nm diameter and fixed carrier-reflection parameter $R_b=0.5$) using a Mayadas model.

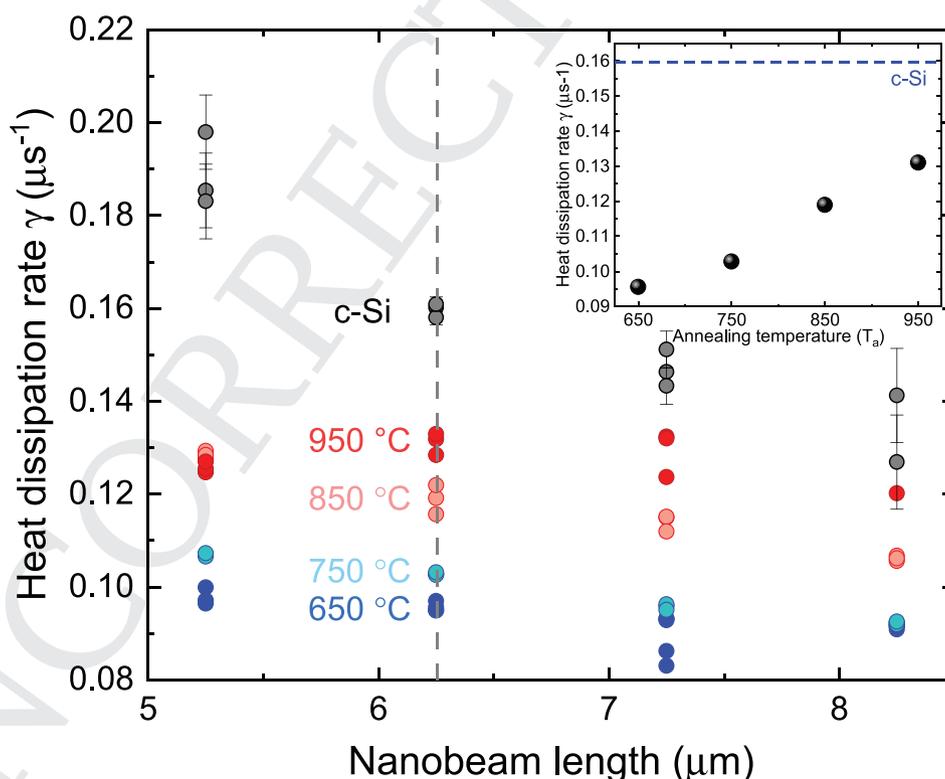
sipation rates obtained for different values of the thermal conductivity are then compared with the experimental dissipation rate to extract the experimental thermal conductivity. The uncertainty on the measurement of the structure dimensions (± 3 nm) results in an error in thermal conductivity of less than 5%. Further details of the measurement system and FEM simulations are provided in Refs. [17,36,38].

The results of that analysis as a function of the grain size are shown in **Figure 3b**. For comparison, the values for c-Si are given, with the x-axis representing the membrane thickness, which is the limiting dimension in that particular case. For each average grain size, the thermal conductivity value is a weighted average of the data displayed in **Figure 3a**. Data from c-Si membranes measured by μ -TDTR,^[33] Raman thermometry,^[13] and transient thermal gratings (TTG)^[22] yield thermal conductivity

1 between 40 and 90 W m⁻¹ K⁻¹ for the dimensions covered by
2 this study. Due to fabrication limitations related to buckling of
3 single c-Si membranes, we could not measure their thermal
4 conductivity. Nonetheless, the Fuchs–Sondheimer model
5 has been extensively used to describe that effect and it shows
6 extremely good agreement with the reported values in the liter-
7 ature.^[29] In such membranes, thermal transport stills occur
8 in two directions. Whereas membranes are 2D structures and
9 the dimension can be linked to thermal properties due to the
10 interfaces, we have introduced calculations about nanowires
11 as an example of one-dimensional structures to cover a wider
12 range of structures. We thus calculate the thermal conductivity
13 in nanowires of diameter 220 nm using a Mayadas model, in
14 which thermal transport is 1D. We also introduce grains in the
15 simulated nanowires, with a fixed carrier-reflection parameter
16 Rb = 0.5. In Figure 3b, we see that the expected thermal con-
17 ductivity is indeed lower in these nanowires than in the mem-
18 branes. Details of these calculations are given in Supporting
19 Information. In the nc-Si membranes studied in this work,
20 thermal transport is impeded in all three directions. We observe
21 that even when the average grain size of 215 nm ($T_a = 950$ °C)
22 of these membranes is similar to the thickness, the thermal
23 conductivity is reduced by 54% compared to the single crystal
24 case. This reduction increases to 77% in the sample with the
25 smallest average grain size of 163 nm. To explain these results,
26 it is important to note that although specular phonon scattering
27 events can occur at atomically flat surfaces at room tempera-
28 ture,^[39] thermal transport is considered diffusive overall.^[22] The

1 difference in thermal conductivity between crystalline and
2 nanocrystalline silicon membranes therefore mainly stems
3 from the scattering events at grain boundaries, whose frequency
4 of occurrence in nc-Si is directly linked to the grain size distri-
5 bution. Furthermore, a recent experimental study on 145 nm-
6 thick crystalline Si membranes^[40] shows that phonons with a
7 mean free path above 215 nm contribute nearly 20% to thermal
8 conductivity at room temperature. This proportion is expected
9 to be relatively higher in our membranes due to the increased
10 thickness and subsequent shift of the mean free path distri-
11 bution towards higher values. Anufriev et al.^[39] showed that
12 phonon mean free path smaller than 400 nm contributes sig-
13 nificantly to thermal conductivity in a 145 nm thick membrane.
14 This suggests that the grain size distribution in our samples
15 covers the range of mean free paths with the strongest contri-
16 bution to thermal conductivity. It explains the strong suppres-
17 sion of the thermal conductivity measured here. Furthermore,
18 we see that our experimental values of thermal conductivity lie
19 below the expected values for nanocrystalline nanowires from
20 the Mayadas model with a carrier reflection parameter of 0.5.
21 Although no direct quantitative comparison is possible between
22 these two sets of values, they suggest that the transmission at
23 grain boundaries in our samples might be lower than the value
24 input in the model. High spatial resolution measurements on
25 single grain boundaries might shed light on the transmission
26 at single grain interfaces.

27 The role of the S/V ratio using nc-Si optomechanical nano-
28 beams is shown in Figure 4 where the same trend observed
29



56 **Figure 4.** Impact of nanostructuring and grain size on the heat dissipation rate. Heat dissipation rate γ measured with the μ -TDTR technique as a
57 function of nanobeam length and annealing temperature T_a . The grey dots show the rate measured from geometrically identical single-crystalline
58 nanobeams. Inset. Average γ of 6.25 μm long nanobeams as a function of the annealing temperature. Errors bars are shown with the data from SOI
59 samples only for clarity and correspond to the standard deviation of the measurement in structures of identical length.

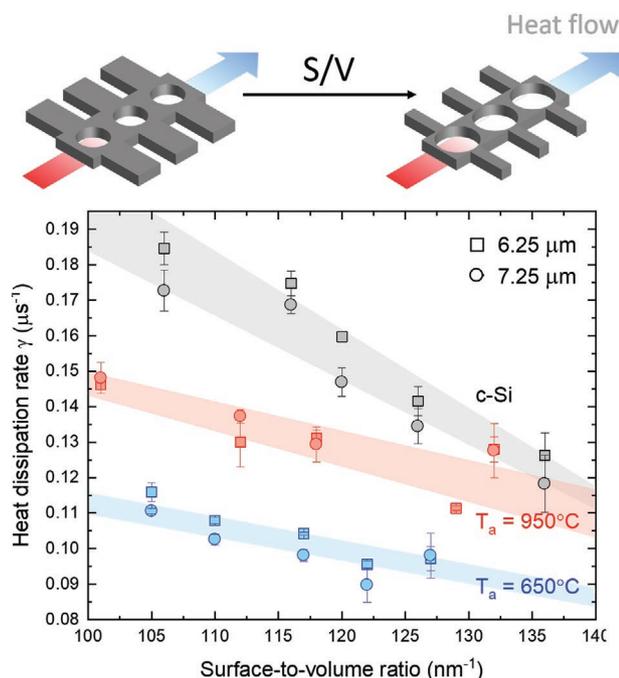


Figure 5. Impact of S/V ratio on heat dissipation rate. Heat dissipation rate γ as a function of the S/V ratio in nanobeams made of nc-Si with an average grain size of 163 ($T_a = 650$ °C, blue), 215 nm ($T_a = 950$ °C, red), and of single crystalline silicon c-Si (grey). Data is shown for two nanobeam lengths: 6.25 μm (squares) and 7.25 μm (circles). The colored stripes are guides to the eye.

in nc-Si membranes is qualitatively observed also for OM nanobeams, that is, the heat dissipation rate decreases with increasing length and with decreasing grain size. In the case of periodic nanobeams, Γ corresponds to the decrease of the geometrical parameters towards the central island of the OM structure (see Figure S1, Supporting Information). In our experiment, the measured values of heat dissipation rate γ are insufficiently sensitive to Γ . Therefore, no distinction is made in the rest of this work between structures with differing Γ values. The inset to Figure 4 shows that the grain size impacts heat dissipation in a similar way as in membranes, with an increase of the heat dissipation rate by more than 30% comparing samples made out of nc-Si annealed at $T_a = 650$ °C and $T_a = 950$ °C. However, the difference with c-Si is much smaller than in the suspended membranes since the heat dissipation is $\approx 19\%$ slower in nc-Si nanobeams with $T_a = 950$ °C than in identical

nanobeams made of c-Si. This phenomenon is attributed to the fact that the heat dissipation is already strongly suppressed in c-Si nanobeams due to surface phonon scattering.

Due to the multi-parameters involved, evaluating the impact of geometry on the thermal properties is not straightforward. Two main parameters have been extensively used in the literature as a way to encompass the effect of geometry in nanostructures and phononic crystals, namely, the neck size—the smallest width available for phonons to travel through—and the S/V ratio to highlight the importance of surface scattering. We varied the geometry for each sample by increasing the hole diameter and reducing the width of the central beam as well as the width and length of the stubs. These changes effectively increase the S/V ratio and are schematically shown in the upper part of Figure 5. The data confirms that for a given S/V ratio, that is, for a similar geometry, the heat dissipation rate increases with increasing grain size but remains lower than that of c-Si. It is interesting to note that for the highest S/V ratio, which corresponds to the smallest neck, heat is dissipated nearly as fast in c-Si as it is in the sample with $T_a = 950$ °C. This observation suggests that as surface scattering increases and the neck becomes small enough—below 75 nm in our samples—the impact of crystallinity becomes negligible for that sample. The second observation is highlighted by the colored areas in Figure 5. Note that these colored areas are visual guides and not fits the data. Given that heat is dissipated through the nanobeams but also through air, the slope of each area qualitatively indicates the relative impact of geometry on heat dissipation. We see in Figure 5 that nanocrystalline material has less dependence on the S/V ratio compared to single c-Si and the geometry seems to have a lower impact as the grains become smaller.

We summarize the μ -TDTR data in Table 2. The data obtained from membranes is compared to its crystalline counterpart estimated from μ -TDTR in the literature, whereas the data from nanobeams is normalized to that of the corresponding membrane and to that of the c-Si nanobeam of a similar S/V ratio. An increase of the S/V ratio corresponds to an overall decrease in the nanobeam neck, stub width and depth, and an increase in hole diameter. The data for nanobeams is obtained for a length of 6.25 μm as shown in the inset to Figure 4. We see that the thermal conductivity for the high S/V ratio structure with an average grain size of 187 nm has the lowest reported thermal conductivity. This specific value, lower than expected, is attributed to uncertainties, which are larger for structures with lower

Table 2. Summary of thermal characteristics of membranes and nanobeams.

	Membranes		Nanobeams					
	K [$\text{W m}^{-1} \text{K}^{-1}$]	K/ $K_{\text{c-Si}}$	$S/V = 116.4 \pm 0.8 \text{ nm}^{-1}$			$S/V = 127.9 \pm 1.2 \text{ nm}^{-1}$		
K [$\text{W m}^{-1} \text{K}^{-1}$]			K/ $K_{\text{c-Si}}$	K/ K_{membrane}	K [$\text{W m}^{-1} \text{K}^{-1}$]	K/ $K_{\text{c-Si}}$	K/ K_{membrane}	
c-Si	91.5	1	42.73	1	0.47	25.33	1	0.28
215 nm	22.8	0.249	16.06	0.38	0.70	8.71	0.34	0.38
187 nm	14.9	0.163	9.63	0.23	0.65	6.43	0.25	0.43
171 nm	10.9	0.119	5.95	0.14	0.55	2.09	0.08	0.19
163 nm	10.3	0.113	5.27	0.12	0.51	3.22	0.13	0.31

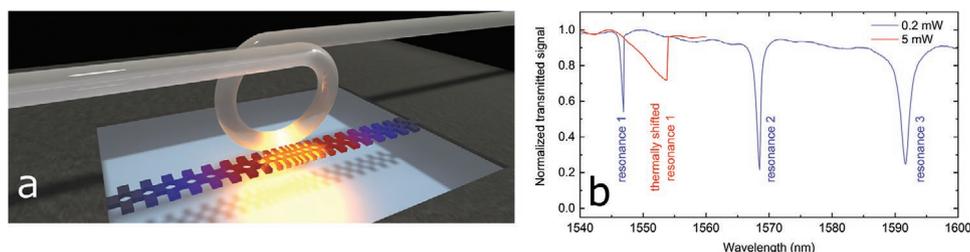


Figure 6. Principle of optical resonance cooling. a) Schematic of the experimental configuration involving the fiber loop and the nanobeam. The red to blue gradient along the beam represents the temperature distribution induced by the pump, whereas the probe laser is represented in yellow. b) Optical transmission spectra through the optical fiber in the sample with an average grain size of 187 nm. The transmission measured at low power, that is, without heating the cavity, is shown in the blue trace. Heating of the cavity at higher laser power (5 mW) is shown in the red trace, with the first optical resonance thermally shifted to a longer wavelength. The spectra are obtained by sweeping the pump laser from short to long wavelengths.

thermal conductivities. The thermal conductivity data for nanobeams with an average grain size of 187 nm is highlighted since it will be compared to values obtained by the optical resonance cooling technique.

4. Thermal Dynamics by Optical Resonance Cooling

The nanobeams studied here have been extensively used as a platform for OM experiments, including self-pulsing,^[6,8] chaotic behavior,^[7] injection locking,^[41] and synchronization,^[42] among others.^[23,27] In this context, non-linear dynamics involving self-pulsing limit cycle have played a key role. Such non-linear dynamics involve not only free carrier dispersion but also the temperature increase of the cavity, which directly depends on the thermal properties of the nanostructure. Of particular interest is the thermal decay rate Γ_{th} . This thermal decay rate is used in modeling to explain the dynamics of the system,^[6] but so far has only been estimated. Here, we demonstrate a way to directly measure Γ_{th} using the cooling rate of the optical resonance of an OM cavity, since the heat dissipation rate γ obtained by μ -TDTR is not strictly equivalent to Γ_{th} in optomechanical devices due to the added contribution of the suspended central section and gold pad and their heat capacity. Details of the method are given in the Supporting Information. Briefly, two tuneable laser beams, with wavelengths around 1.5 μ m and polarization states independently controlled, are multiplexed into a tapered fiber. The thinnest part of the taper is twisted into a loop, which is then positioned parallel to the nanobeam as shown schematically in **Figure 6a**. The distance between the fiber and the nanobeam is approximately 0.2 μ m so that the long tail of the evanescent field of the fiber mode locally excites the resonant optical modes of the cavity. The light traveling through the fiber from either laser can couple to the optical cavity modes if its wavelength corresponds to one such resonance. When measurements are performed in transmission, the light that was not coupled to the resonance continues its path through the optical fiber. The signal is then separated so that each branch is dedicated to one laser. The signal in each branch goes through an in-line bandpass filter adjusted to one of the two lasers and is then detected by a fast InGaAs photodetectors (12 GHz bandwidth). The signals from both detectors are then transmitted to and recorded by an oscil-

loscope. All measurements are performed in an anti-vibration cage at ambient temperature and atmospheric air pressure. More details of the measurement system to characterize optomechanical cavities are given in previous work^[42] and a schematic of the setup is shown in Supporting Information.

To obtain the thermal decay rate Γ_{th} we rely on a pump-probe technique. The first three cold resonances of the measured structure are shown in **Figure 6b** with the blue line. First, we turn on the pump laser in a blue-detuned position, at a shorter wavelength compared to the empty “cold” cavity resonance, that is, the position of the resonance without photons in the cavity, which corresponds to the 1st resonance at 1545.5 nm in **Figure 7**. The wavelength of the pump laser is then continuously increased, and as this pump laser couples to the resonance in the cavity, the transmission through the fiber exhibits a dip. At fixed laser power, we continue increasing the wavelength of the pump laser, thus continuously shifting the resonance until it is approximately 4.5 nm away from its “cold” position while verifying that the cavity remains below the self-pulsing limit. The spectrum of a thermally shifted resonance is shown in red in **Figure 6b**. The probe laser is then turned on at a wavelength between the initial position of the resonance measured at low laser power and the position thermally shifted by 4.5 nm by the high-power pump laser, and the wavelength-filter is adjusted to the probe laser. A waveform generator then gives an impulse to the pump laser, switching it off, which triggers the acquisition of the waveform of the probe laser on the oscilloscope. This cycle is repeated for each new wavelength of the probe laser, effectively mapping the spectrum between the cold and heated wavelengths of the optical resonance. The recorded curves, examples of which are displayed in **Figure 7b**, are then fitted with a Lorentzian function to identify the transmission minimum. It is interesting to note that as the resonance cools down, the dip in the signal gets broader and more asymmetric, which is a direct consequence of the slowing down of the cooling with increasing delay. The wavelength of the probe laser is converted to a temperature rise using the thermo-optic coefficient. This coefficient gives the shift of the optical resonance with temperature increase and was measured to be 0.09 nm K⁻¹ in our previous work.^[27] The temperature rise is then plotted against the time elapsed after switching off the pump laser, as shown in **Figure 7**, and fitted with an exponential decay function. The extracted decay rate then corresponds to the thermal decay rate Γ_{th} . To extract the thermal conductivity,

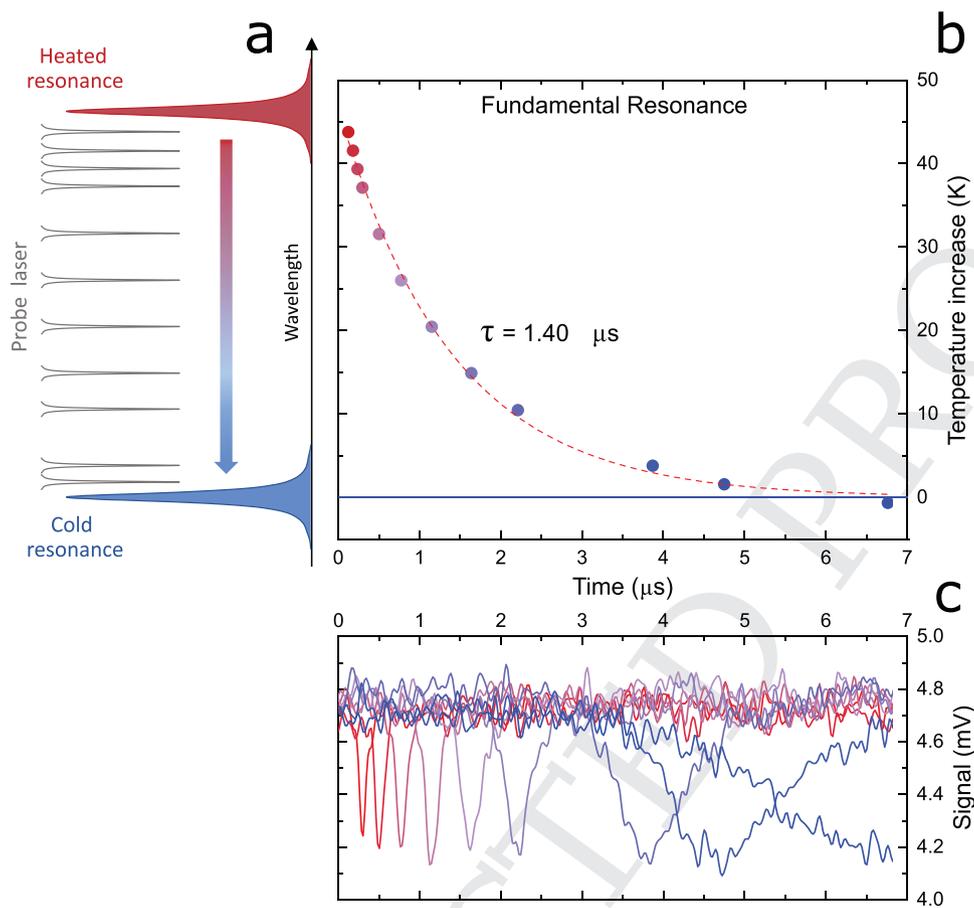


Figure 7. Thermal measurements using optical resonance cooling. a) Schematic of the different wavelengths of the probe laser in-between the cold and hot resonance. b) Temperature of the cavity measured at different wavelengths of the probe laser. The cooling speed, or decay rate, is extracted from the exponential decay curve (dotted line). c) Oscilloscope-recorded optical signal for different probe laser wavelengths. As the pump-probe wavelength difference increases, that is, as the resonance cools down, the dip in the signal gets broader and occurs at a later time.

we use finite element method (FEM) simulations by importing the nanobeam geometry from an SEM image and reproducing the experimental situation in a 3D FEM model. We first calculate the optical resonances of the optical cavity and use it as a heater. Once the temperature in the cavity has reached a steady-state, we turn off the heater and monitor the cooling rate of the nanobeam. The simulation is repeated for different values of the thermal conductivity of the nanobeam and the extracted decay rates are matched to the experimental value to identify the real thermal conductivity. Additional details about the setup and the thermal conductivity extraction are given in the Supporting Information.

Figure 7 shows the results of the measurements of the first optical resonance of an OM nanobeam made out of the nc-Si with an average grain size of 187 nm ($T_a = 850 \text{ }^\circ\text{C}$). The cavity and Bragg mirrors comprise 6 and 10 cells on each side, respectively, resulting in a nanobeam length of 16.5 μm . This measurement was repeated for the 2nd and 3rd optical resonance of the same cavity. The three resonances display thermal decay times of 1.40, 1.67, and 1.61 μs , respectively. The different decay times are attributed to differences in the spatial mode profile of each of the optical resonances, as shown in the Supporting Information. The extracted thermal conductivity for each of

the optical resonance is then 771, 704, and 756 $\text{W m}^{-1} \text{K}^{-1}$, respectively, giving an average thermal conductivity of $744 \pm 0.29 \text{ W m}^{-1} \text{K}^{-1}$. Although no direct quantitative comparison with μ -TDTR measurements is possible due to differences in geometry, namely, the absence of the central island and transducer, the thermal conductivity falls within the range obtained by the μ -TDTR method for similar geometries (see Table 2). Note that the extracted thermal conductivity considers the exact geometry, including the presence of the optical fiber next to the nanobeam. In optomechanics experiments, the optical fiber plays an important role in dissipating heat, which can be observed, for example, in the change of the self-pulsing frequency mentioned above. Indeed, the volume of the fiber being much larger than that of the nanobeam compensates for the low thermal conductivity of glass, at 1.4 $\text{W m}^{-1} \text{K}^{-1}$, especially when considering nc-Si nanobeams with low thermal conductivity. The optical fiber, therefore, constitutes one of the main factors limiting the sensitivity of the technique in extracting the thermal conductivity of the nanobeams. The measurements presented here nonetheless show the validity of this method to determine thermal conductivity but more importantly to obtain the thermal decay rate associated with OM cavities in real characterization configuration.

5. Discussion and Conclusions

In summary, we have used several different experimental techniques to investigate the structural and thermal properties of OM crystal cavities made of nanocrystalline silicon. Dark-field TEM analysis shows that different annealing temperatures result in different grain size distributions, which affect the thermal properties of the material. We used micro-time-domain thermoreflectance to measure heat dissipation rates in the nanocrystalline thin films and observe a strong reduction compared to the single-crystalline films. This is attributed to phonon scattering at the grain boundaries. A recent study on c-Si membranes^[40] suggests that the grain size distribution in our samples covers the range of mean free paths that contribute most to thermal conductivity, thus potentially explaining the low measured values of thermal conductivity. Measurements of the mean free path distribution in our nc-Si membranes should be the focus of a future study to quantify this aspect. We then investigated the thermal properties of released OM nanobeams. In such structures, the geometrical dimensions are small with respect to phonon mean free path, which means that surface scattering has a strong effect on thermal conductivity. We showed that the thermal conductivity is very low in nanocrystalline nanobeams, well below $10 \text{ W m}^{-1} \text{ K}^{-1}$, and depends on the grain size. However, the impact of the grain boundaries in nanobeams is lower than in membranes as the grain boundary scattering competes with the surface scattering stemming from nanostructuring. Finally, we have developed a novel technique to directly measure thermal decay in nanostructures with an optical cavity. The method can be readily adapted to existing OM structures. By using a pump-probe technique to measure the cooling rate of a localized optical resonance, we were able to extract thermal decay rates in nanobeams without any modification of the structure. The values obtained are consistent with those from the thermoreflectance technique and show the strong potential of this novel contactless method for all nanostructures with optical cavities. The results presented in this work clarify the impact of grain boundaries on thermal transport in silicon micro- and nano-structures, in a context in which crystalline state is a key parameter in NEMS and/or NOEMS. Moreover, the versatility of the new characterization technique paves the way to more standardized measurements of thermal properties and to potentially study the impact of strain on thermal and optomechanical properties.

Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

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Conflict of Interest

The authors declare no conflict of interest.

Data Availability Statement

The data that support the findings of this study are openly available in Zenodo at [http://doi.org/\[doi\]](http://doi.org/[doi]), reference number [reference number].

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