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2 **Empirical H/V spectral ratios at the InSight landing site and implications for**  
3 **the martian subsurface structure**

4  
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27       **Abstract**

28

29       The H/V spectral ratio inversion is a traditional technique for deriving the local subsurface  
30 structure on Earth. We calculated the H/V from the ambient vibrations at different wind levels at  
31 the InSight landing site, on Mars, and also computed the H/V from the S-wave coda of the martian  
32 seismic events (marsquakes). Different H/V curves were obtained for different wind periods and  
33 from the marsquakes. From the ambient vibrations, the recordings during low-wind periods are  
34 close to the instrument self-noise level. During high-wind periods, the seismic recordings are  
35 highly contaminated by the interaction of the lander with the wind and the martian ground.  
36 Therefore, these recordings are less favorable for traditional H/V analysis. Instead, the recordings  
37 of the S-wave coda of marsquakes were preferred to derive the characteristic H/V curve of this site  
38 between 0.4 and 10 Hz. The final H/V curve presents a characteristic trough at 2.4 Hz and a strong  
39 peak at 8 Hz. Using a full diffuse wavefield approach as the forward computation and the  
40 Neighbourhood Algorithm as the sampling technique, we invert for the 1D shear-wave velocity  
41 structure at the InSight landing site. Based on our inversion results, we propose a strong site effect  
42 at the InSight site to be due to the presence of a shallow high-velocity layer (SHVL) over low-  
43 velocity units. The SHVL is likely placed below a layer of coarse blocky ejecta and can be  
44 associated with Early Amazonian basaltic lava flows. The units below the SHVL have lower  
45 velocities, possibly related to a Late Hesperian or Early Amazonian epoch with a different  
46 magmatic regime and/or a greater impact rate and more extensive weathering. An extremely weak  
47 buried low velocity layer (bLVL) between these lava flows explains the data around the 2.4 Hz  
48 trough, whereas a more competent bLVL would not generate this latter feature. These subsurface  
49 models are in good agreement with results from hammering experiment and compliance  
50 measurements at the InSight landing site. Finally, this site effect is revealed only by seismic events  
51 data and explains the larger horizontal than vertical ground-motion recorded for certain type of  
52 marsquakes.

53

54

55       **Key words:** Seismic noise, Site effects, Coda waves, Martian seismology, Marsquakes

## 56 **1 Introduction**

57 On November 26th, 2018, NASA's InSight mission landed on Elysium Planitia, Mars, and  
58 deployed a set of geophysical instrumentation aimed at investigating the planet's inner structure  
59 and dynamics. Along with other instruments, SEIS (Seismic Experiment for Interior Structure,  
60 [Lognonné et al., 2019](#)) monitors the martian ground motion using one six-channels seismological  
61 station, which was deployed on the ground, around of 2 m away from the InSight lander.

62  
63 The InSight landing site is located at 4.5024N/135.6234E inside a degraded impact crater, the  
64 so-called Homestead hollow, in Elysium Planitia ([Golombek et al., 2017, 2020c](#)). The surficial  
65 geology of this site was studied before the mission ([Warner et al., 2017](#)), using mainly orbital  
66 imagery and analysis of rocky ejecta craters, and also assessed after landing ([Golombek et al.,](#)  
67 [2020b; Warner et al., 2022](#)). According to the pre-landing observations, a model proposed for the  
68 shallow subsurface structure at the InSight landing site consists of a shallow fine regolith layer, a  
69 second layer of coarse ejecta, a deeper layer of fractured basalt followed by a layer of more pristine  
70 basalt and, finally, a deep layer of possible weakly-bonded sediments located at ~200 m depth  
71 below the lander ([Knapmeyer-Endrun et al., 2017; Pan et al., 2020](#)). Knowing the shallow  
72 subsurface layers of a site and their elastic properties is relevant for understanding the recorded  
73 ground-motion amplitudes. In this regard, the amplification of the ground motion in a specific  
74 frequency range is affected by the waves propagating through soil and soft rock layers, commonly  
75 referred to as a site effect ([Borcherdt, 1970; Anderson et al., 1986](#)). The analysis of analog samples  
76 has allowed studying the mechanical properties of the martian regolith at the InSight landing site,  
77 suggesting that the top layer is made of soft material ([Delage et al., 2017; Morgan et al., 2018](#)).  
78 Therefore, ground-motion amplification due to a site effect might be expected at the InSight landing  
79 site.

80  
81 On Earth, a classic technique used to evaluate ground-motion amplification is the horizontal-to-  
82 vertical spectral ratio (H/V or HVSR), which is defined as the ratio between the Fourier amplitude  
83 spectra of the horizontal and the vertical components of the seismic recordings. This technique,  
84 first introduced by [Nogoshi \(1971\)](#) and popularized by [Nakamura \(1989\)](#), allows the estimation of  
85 the fundamental resonance frequency and ground-motion amplification using seismic recordings  
86 of either ambient vibrations or earthquake motions. Even though this method has become popular

87 in recent decades, the discussion on its strengths and limitations is still due to the absence of a  
88 clear theoretical basis (Bonnefoy-Claudet et al., 2008). In this context, Sánchez-Sesma et al. (2011)  
89 have proposed that the ambient vibrations can be represented as a diffuse wavefield containing all  
90 types of body (P and S) and surface waves (Love and Rayleigh). This diffuse field approach (DFA)  
91 has a strong theoretical background based on the principle of equipartition of energy (Weaver,  
92 1982; Margerin, 2017). Under this assumption, the autocorrelation in the frequency domain is  
93 proportional to the imaginary part of the Green's function, so the latter can be directly linked to  
94 the H/V curve. Several studies have applied this theory to explain the features observed on the  
95 H/V curve and have demonstrated it to be a robust approach (e.g. Lontsi et al., 2015; Piña-Flores et  
96 al., 2016; Spica et al., 2018; Bora et al., 2020).

97  
98 The diffuse field regime can also be extended to the seismic event recordings, as shown by  
99 Margerin et al. (2009). Recently, Kawase et al. (2018) obtained similar H/V curves from ambient  
100 vibrations, the S-wave window and the late coda window, especially up to their first peak frequency.  
101 Thus, assuming the wavefield in the coda is equipartitioned, the DFA can be applied to model the  
102 H/V curve from this data window.

103  
104 Since the landing, some attempts have been made to reveal the subsurface structure at the  
105 InSight landing site. First, the SEIS recordings of the hammering sessions of the HP<sup>3</sup> (Heat Flow  
106 and Physical Properties Package) experiment were used to derive the seismic wave velocities in  
107 the first tens of centimeters below the ground surface (Brinkman et al., 2019; Lognonné et al.,  
108 2020). A re-evaluation of this data has determined the P-wave velocity to be  $119 \pm 29$  m/s and the  
109 S-wave velocity to be  $61 \pm 20$  m/s in the first ~40 cm of the shallowest layer (Brinkman et al.,  
110 2022). Kenda et al. (2020) derived a subsurface model based on ground-motion compliance (the  
111 surface response to atmospheric pressure loading) measurements, which was extended by Onodera  
112 (2022), who proposed a model with a single discontinuity at ~1 m depth in the first ~75 m of the  
113 subsurface below the lander, corresponding to the martian regolith over a layer of coarse blocky  
114 material. In addition, Hobiger et al. (2021) proposed a subsurface model to explain the surface  
115 wave ellipticity features that they observed between 1 and 5 Hz. They propose a buried low  
116 velocity layer (bLVL) sandwiched between older and younger lava flows to explain a trough in  
117 the ellipticity curve. The proposed model spans down to ~200 m depth but it lacks resolution in

118 the first 20 meters below the surface. A model with better resolution at shallow depths can be  
119 obtained by evaluating the H/V curve over a broader range of frequencies, so in this study we used  
120 the frequencies between 0.4 and 10 Hz.

121  
122 After more than two years of operation, SEIS has recorded persistent ambient vibrations during  
123 different periods of time. In addition, more than 900 martian seismic events (hereafter,  
124 Marsquakes) have been identified by the Marsquakes Service (MQS, [Clinton et al., 2018](#)). In this  
125 work, we compute and compare the H/V ratios from both ambient vibrations and the coda waves of  
126 marsquakes. Then, based on the DFA, we invert the H/V curve to find the most representative  
127 shallow subsurface models.

128

## 129 **2 The InSight data**

### 130 **2.1 Characteristics of the InSight data**

131 The SEIS instrument records the martian ground motion at the InSight landing site with two sensors:  
132 a tri-axial Very Broad Band (VBB) seismometer, with a higher sensitivity in the low frequency  
133 range (especially 0.01 to 5 Hz), and a tri-axial Short Period (SP) seismometer, more sensitive to  
134 higher frequencies (>5 Hz), which together cover the frequency range between 0.01 to 50 Hz  
135 ([Lognonné et al., 2019](#)). Also, the TWINS (Temperature and Winds for InSight) provide wind and  
136 air temperature measurements at the InSight landing site to help in understanding the seismic  
137 recordings ([Banfield et al., 2019](#); [Spiga et al., 2018](#)). All these sensors transmit data at different  
138 sampling rates depending on the requirements of the team and operational restrictions. In this sense,  
139 the most continuously available seismic data has been recorded by VBB at 20 sps (channel 02.BH).  
140 The availability of seismic data at 100 sps, either from VBB (00.HH) or SP (65.EH), is sparse and  
141 less continuous, mainly due to operational restrictions.

142

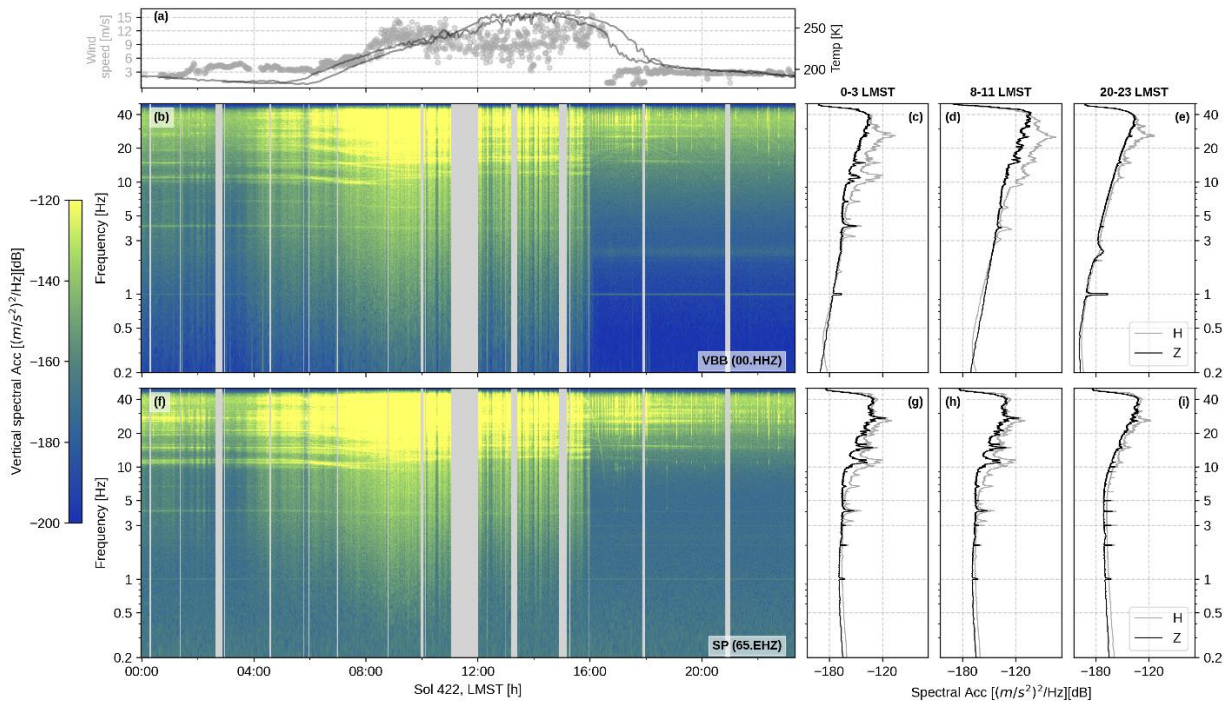
#### 143 **2.1.1 The ambient vibrations**

144 Even though the 20 sps data would be enough to retrieve the H/V curve for the desired frequency  
145 range, the 100 sps data yields a clearer perspective of the whole spectral curve. Throughout the  
146 mission, simultaneous recordings by both VBB and SP at 100 sps spanning longer than one martian  
147 Sol are available only for two time periods: from Sol 422 to Sol 423, during the summer on the  
148 northern hemisphere, and from Sol 762 to Sol 763, during the northern winter. We analyzed the

149 seismic data recorded by both VBB and SP at 100 sps on Sol 422 (Fig. 1), which is a good  
 150 representation of the period between spring and fall on the northern hemisphere, the least noisy time  
 151 of the martian year. In contrast, data recorded on Sol 762 is representative of the period between  
 152 northern fall and spring (including winter), when strong winds generate high noise levels  
 153 throughout the Sol (Dahmen et al., 2021b).

154  
 155 For each instrument, we pre-processed the data by correcting for the instrument response, high-  
 156 pass filtering at 0.01 Hz and rotating from the sensor orientations (U, V, W) to the geographic  
 157 coordinate system (Z, N, E). When both VBB and SP data are simultaneously available, the spectral  
 158 acceleration from a 120 s time window with 50% overlap was computed for each component. The  
 159 spectrograms of the vertical component of both VBB and SP are shown in Figures 1b and 1f along  
 160 with the wind speed and atmospheric temperature data provided by TWINS (Fig. 1a).

161



162  
 163 **Figure 1.** Spectrogram of martian ground motion recorded by VBB and SP at 100 sps on Sol  
 164 422. (a) Wind speed (gray circles) and air temperature (black lines) as a function of time. Data  
 165 from Sols 422 and 423 are used to cover TWINS data gaps. (b) spectrogram of the vertical  
 166 component of VBB acceleration at 100 sps. The median of horizontal (gray) and vertical (black)  
 167 PSDs of VBB 100 sps data are computed between (c) 00:00-03:00 LMST, (d) 08:00-11:00 LMST  
 168 and (e) 20:00-23:00 LMST. Plots (f), (g), (h) and (i) are analogous figures for SP 100 sps data.  
 169



170 The main characteristics of the ambient vibrations can be observed on Figure 1. As shown by  
171 [Giardini et al. \(2020\)](#), the background noise level is highly affected by the wind and temperature  
172 conditions at the InSight landing site. The noisiest period corresponds with the highest wind  
173 speeds, which are recorded roughly between 08:00 LMST (Local Mean Solar Time) and 16:00  
174 LMST. In contrast, the evening (between 16:00 - 24:00 LMST) is the quietest period of the day,  
175 where the lowest wind speeds are recorded ( $< 3$  m/s). The very narrow peaks observed at frequencies  
176 below 10 Hz, especially during the evening and night, correspond to the so-called tick noise at 1 Hz  
177 and its overtones, which is an artifact generated by cross-talk in the measurement system. Further  
178 details are provided by [Ceylan et al. \(2021\)](#) and [Zweifel et al. \(2021\)](#).

179  
180 Special attention must also be paid to the lander-related resonances, a set of major distinctive  
181 spectral peaks whose origin can be attributed to the lander system ([Dahmen et al., 2021b](#); [Schimmel  
182 et al., 2021](#)). They have been studied in detail in the frequency range between 1 and 9 Hz, where  
183 they are characterized by a temperature-dependent peak frequency, a wind-sensitive amplitude, a  
184 predominantly horizontal polarization and are clearly excited at 1.6, 3.3, 4.1, 6.8 and 8.6 Hz  
185 ([Ceylan et al., 2021](#); [Dahmen et al., 2021b](#)). Similar patterns are observed at higher frequencies  
186 ( $>10$  Hz), so additional lander-related resonances are likely also present in this spectral range.  
187 Furthermore, [Hurst et al. \(2021\)](#) showed there are a number of resonances at about 2.86, 5.3, 9.5,  
188 12, 14 and 23-28 Hz related to the Load Shunt Assembly (LSA), which provides mechanical  
189 separation between SEIS and the tether connecting to the lander in order to reduce the effect of  
190 lander perturbations on the seismometer.

191  
192 Another remarkable feature of the ambient vibrations is the strong resonance at 2.4 Hz, which is  
193 more visible during the quiet times of the northern summer, roughly between 16:00-24:00 LMST.  
194 [Dahmen et al. \(2021b\)](#) investigated this mode and have shown its behavior is contrary to the lander-  
195 related modes, as it is not excited by the steady winds during the mornings and it never disappears  
196 during quiet conditions (Fig. 1). [Hobiger et al. \(2021\)](#) proposed this mode is due to the response of  
197 a buried low velocity layer excited by Rayleigh waves generated by sources located at regional  
198 distances.

199  
200



201 Besides the lander resonances, other features such as one-sided long-period pulses, termed  
202 glitches, can be observed in the data (Scholz et al., 2020). The description of other particular  
203 features in the seismic data recorded by SEIS are provided by Ceylan et al. (2021) and Kim et al.  
204 (2021).

205

### 206 **2.1.2 The seismic events**

207 As of September 30th 2021, the MQS has reported more than 900 potential seismic events (Clinton  
208 et al. (2021), see [Data availability](#)), whose origin and nature are under investigation, but a  
209 classification based on their spectral content can be made. These events are classified into two  
210 main groups: the low frequency family, characterized by long-period energy below 1 Hz, and the  
211 high frequency family, characterized by the excitation of frequencies mainly above 1 Hz. The low-  
212 frequency family events can be divided into the Low Frequency (LF) events, which do not excite  
213 the 2.4 Hz mode, and the Broadband (BB) events, which do excite this mode (Clinton et al., 2021).  
214 On the other hand, in the high-frequency family, we can distinguish three different groups of  
215 events: (1) the 2.4 Hz events, which excite the 2.4 Hz mode and frequencies up to 4 Hz; (2) the  
216 High Frequency (HF) events, exciting the 2.4 Hz mode and higher frequencies up to 10 Hz; and (3)  
217 the Very High Frequency (VF) events, which show a strong excitation of the horizontal components  
218 at frequencies above 5 Hz, up to as high as 35 Hz (Clinton et al., 2021).

219

220 Along with this classification based on the spectral energy content, the seismic events also have  
221 assigned a quality index based on the signal strength and the ability to identify and interpret the  
222 phase arrivals (Clinton et al., 2021). Therefore, the quality index can be either A (*high*), B  
223 (*medium*), C (*low*) or D (*suspicious*). As we make use of the coda of the marsquakes to compute  
224 the H/V curve, only events with quality A and B were used. In total, 139 marsquakes were used  
225 to compute the H/V curve, from which the 2.4 Hz events are the most abundant, as shown in Table  
226 1. In the same way, the 100 sps channels were preferred whenever they were available, otherwise  
227 the 20 sps channels were used. Further details on the events used for this analysis, including the  
228 time windows for the H/V computation, can be found in the Supplementary Material.

229

230

231

232 **Table 1.** Summary of martian seismic events recorded by SEIS and used in the H/V analysis, as  
 233 reported by MQS through September 30th, 2021. The marsquakes are differentiated by event type  
 234 as classified by MQS: LF (Low Frequency), BB (Broad band), 2.4HZ, HF (High Frequency) and  
 235 VF (Very High Frequency). The two main columns indicate: the number of events identified by  
 236 the MQS per quality (A or B), and the number of events recorded either by VBB or SP at 20 or  
 237 100 sps.  
 238

	<i>Events</i>			<i>Recordings</i>			
	QA	QB	<b>Total</b>	VBB@20sps	VBB@100sps	SP@20sps	SP@100sps
<i>LF</i>	4	9	<b>13</b>	13	2	3	5
<i>BB</i>	2	6	<b>8</b>	8	2	2	2
<i>2.4HZ</i>	0	46	<b>46</b>	46	7	27	20
<i>HF</i>	0	51	<b>51</b>	51	12	27	22
<i>VF</i>	0	21	<b>21</b>	21	10	7	9
<b>Total</b>	6	133	<b>139</b>	139	33	66	58

239  
 240  
 241 The VF events are of special interest for this study as they contain energy well above 5 Hz, which  
 242 allows mapping of shallower depths at the InSight site. Even though quality A VF events have not  
 243 been reported by the MQS, there are 21 VF events with quality B (see Table 1). As shown in Table  
 244 1, VBB data at 100 sps are available for ten VF events whereas SP data at 100 sps are available  
 245 for nine events, with just one of them being recorded simultaneously by both SP and VBB.

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 253  
 254

### 255 3 H/V curves at the InSight landing site

#### 256 3.1 H/V analysis

##### 257 3.1.1 The diffuse field approach (DFA)

258 Based on [Sánchez-Sesma et al. \(2011\)](#), assuming a diffuse wavefield, the imaginary part of the  
 259 Green's function between two sites is proportional to the average cross correlations of the  
 260 corresponding displacements:

$$261 \langle u_i(\mathbf{x}_A, \omega) u_j^*(\mathbf{x}_B, \omega) \rangle \propto \text{Im}[G_{ij}(\mathbf{x}_B, \mathbf{x}_A; \omega)], \quad (1)$$

262 with  $\omega = 2\pi f$  the angular frequency,  $u_i(\mathbf{x}_A, \omega)$  is the displacement field component in  $i$  direction  
 263 at point  $\mathbf{x}_A$ , the Green's function  $G_{ij}(\mathbf{x}_B, \mathbf{x}_A; \omega)$  is defined as the displacement in the direction  $i$  at  
 264 point  $\mathbf{x}_B$  due to the application of a unit harmonic point force in the direction  $j$  at point  $\mathbf{x}_A$ . The  
 265 asterisk (\*) corresponds to the complex conjugate. If the sites  $\mathbf{x}_A$  and  $\mathbf{x}_B$  are the same, as well  
 266 as the components  $i$  and  $j$ , then the average of the autocorrelation corresponds to the directional  
 267 energy density  $E_i(\mathbf{x}, \omega)$  at point  $\mathbf{x}$  ([Sánchez-Sesma et al., 2008](#); [Perton et al., 2009](#)), such that:

$$268 E_i(\mathbf{x}, \omega) = \rho \omega^2 \langle \|u_i(\mathbf{x}, \omega)\|^2 \rangle \propto \text{Im}[G_{ii}(\mathbf{x}, \mathbf{x}; \omega)], \quad (2)$$

270 where  $\rho$  is the mass density. Thus, the H/V spectral ratio in a diffuse field, defined as the square  
 271 root of the ratio between the horizontal and the vertical energies ([Arai and Tokimatsu, 2004](#)), is  
 272 equivalent to the square root of the ratio between the imaginary parts of the corresponding Green's  
 273 functions, i.e:

$$HVSR = \frac{H}{V}(\mathbf{x}, \omega) = \sqrt{\frac{\langle \|u_1(\mathbf{x}, \omega)\|^2 \rangle + \langle \|u_2(\mathbf{x}, \omega)\|^2 \rangle}{\langle \|u_3(\mathbf{x}, \omega)\|^2 \rangle}}, \quad (3)$$

$$= \sqrt{\frac{\text{Im}[G_{11}(\mathbf{x}, \mathbf{x}; \omega)] + \text{Im}[G_{22}(\mathbf{x}, \mathbf{x}; \omega)]}{\text{Im}[G_{33}(\mathbf{x}, \mathbf{x}; \omega)]}}, \quad (4)$$

274 where  $i = 1, 2$  correspond to the horizontal components and  $i = 3$  is the vertical component.

275  
 276 We computed the H/V spectral ratios for both the ambient seismic noise data ( $nHV$ ) and the  
 277 seismic events ( $eHV$ ) following equation (3), thus adhering to the diffuse field approach. Our  
 278 methodology is slightly different from the classical average of H/V spectral curves as we compute

279 the final H/V from the average spectrum of each component. Because of this, to have the same  
280 spectral contribution from each time window, we normalized the vertical and horizontal spectra by  
281 the total power of the respective time window. The normalized ground motion corresponds to:

$$282 \quad \hat{u}_i(\mathbf{x}, \omega) = \frac{u_i(\mathbf{x}, \omega)}{\sqrt{\sum_{i=1}^3 |u_i(\mathbf{x}, \Delta\omega)|^2}}, \quad (5)$$

283 where the denominator is the normalization term, given by the total power in a certain bandwidth  
284  $\Delta\omega$ . For simplicity, we used  $\Delta\omega = 50$  Hz to normalize by the power of the total spectrum. This  
285 way, the final H/V is computed as in equation (3) but replacing  $u_i$  by the normalized ground motion  
286  $\hat{u}_i$ .

287  
288 For the computation of  $nHV$ , we used the data recorded during Sol 422 and Sol 423, which were  
289 divided into three different groups of data representing three different periods of time along a  
290 typical summer-time Sol (Fig. 1). These are a high-noise period (between 08:00-11:00 LMST), a  
291 low-noise period (20:00-23:00 LMST) and a moderate-noise period (00:00-03:00 LMST). For each  
292 instrument, SP and VBB, the H/V was computed using time windows of 120 s length with an  
293 overlap of 50%. In order to compare the performance of VBB against SP, we used the same 120 s  
294 data windows such that the segment is skipped when there is no data available for one of the  
295 sensors.

296  
297 The H/V of the marsquakes data was obtained in a similar way but based on the phase picks  
298 provided by the MQS. For events with quality A and B, the MQS provides the times of the P and S-  
299 wave onsets and also includes the times of the characteristic background seismic noise before the  
300 event (Clinton et al., 2021). According to this catalog, we computed the H/V of the S-wave coda,  
301 which has been shown to be depolarized and the energy to be equipartitioned (van Driel et al.,  
302 2021; Menina et al., 2021). The duration of this coda window is variable and is provided by the  
303 MQS such that it is a good representation of the S-wave coda and free of non-seismic perturbations  
304 (e.g., glitches). The H/V computation was performed in a similar way as for the noise data but using  
305 consecutive 20 s data windows with an overlap of 50%.

306  
307 For each event and sensor, the vertical spectral signal-to-noise ratio ( $SNR_z$ ) was computed using

308 the median power of the vertical component of the coda and the pre-event noise windows. For  
309 each sensor, a single *eHV* curve is derived as the median of all the segments with  $SNR_Z$  larger  
310 than 2 dB. The DFA-HV curve is expected to be less smoothed than the classical H/V approach,  
311 which typically implements a Konno-Ohmachi smoothing window (Konno and Ohmachi, 1998).  
312 Because of this, a visual inspection and manual smoothing following the median of the final *eHV*  
313 is performed in order to also discard any contamination due to lander resonances.

314

### 315 **3.1.2 Polarization attributes**

316 In order to have a better assessment of the spectral features of the H/V curves, we also computed  
317 the polarization attributes of both the seismic noise and the seismic events using a similar approach  
318 as presented by Park et al. (1987), which is based on the work of Samson (1983). For each data  
319 window, the calculation of the polarization features relies on the eigen-decomposition of the  
320 spectral covariance matrix ( $\mathbf{S}$ ) of the three-component ground motion data. The largest eigenvalue  
321 and the corresponding eigenvector of  $\mathbf{S}$  represent the polarization of the seismic signal (either noise  
322 or event coda) during the given time window for each frequency. The directional attributes of this  
323 polarization are of particular interest: the horizontal incidence angle  $\theta_H$ , measured in degrees  
324 clockwise from North, and the vertical incidence angle  $\theta_V$ , restricted to lie between  $0^\circ$  (vertical)  
325 and  $90^\circ$  (horizontal).

326

327 We also computed the degree of polarization (*dop*), as proposed by Samson and Olson (1980),  
328 which is a measure of how well the seismic signal can be described by fewer than three degrees  
329 of freedom. For a three-component ground motion record, the degree of polarization is defined as

$$dop = \frac{3\text{tr}(\mathbf{S}^2) - [\text{tr}(\mathbf{S})]^2}{2[\text{tr}(\mathbf{S})]^2}, \quad (6)$$

330 where  $\text{tr}$  is the trace and  $\mathbf{S}$  is the spectral covariance matrix of the ground motion record. This  
331 parameter ranges from 0, when the signal is depolarized, to 1, when a single non-zero eigenvalue  
332 exists and the signal is completely polarized in the direction of the corresponding eigenvector.  
333 High values of *dop* correspond to a polarized signal with a particle motion that can be either linear  
334 or elliptical. As lander resonances have been observed to be highly polarized (e.g., Dahmen et al.,  
335 2021b; Schimmel et al., 2021), the polarization attributes will be used for a better assessment and  
336 understanding of the resulting H/V features.

337

### 338 **3.2 Ambient noise H/V (nHV)**

339 From the seismic data simultaneously recorded by VBB and SP during Sols 422 and 423, a total  
340 of 1576 segments of 120 s length were used for our analysis. From these data, 215 segments  
341 correspond to the low-noise period (between 20:00 and 23:00 LMST), 202 segments to the  
342 moderate-noise period (00:00 - 03:00 LMST) and 216 segments to the high-noise period (08:00 -  
343 11:00 LMST). The spectral (vertical, horizontal and H/V spectra) and polarization features ( $dop$ ,  
344  $\theta_H$  and  $\theta_V$ ) are illustrated in Figure 2.

345

346 The spectral curves from both VBB and SP data (Fig. 2) reveal clear amplitude differences in  
347 the vertical components, at different noise periods, but an overall good match between the VBB and  
348 SP horizontal components.

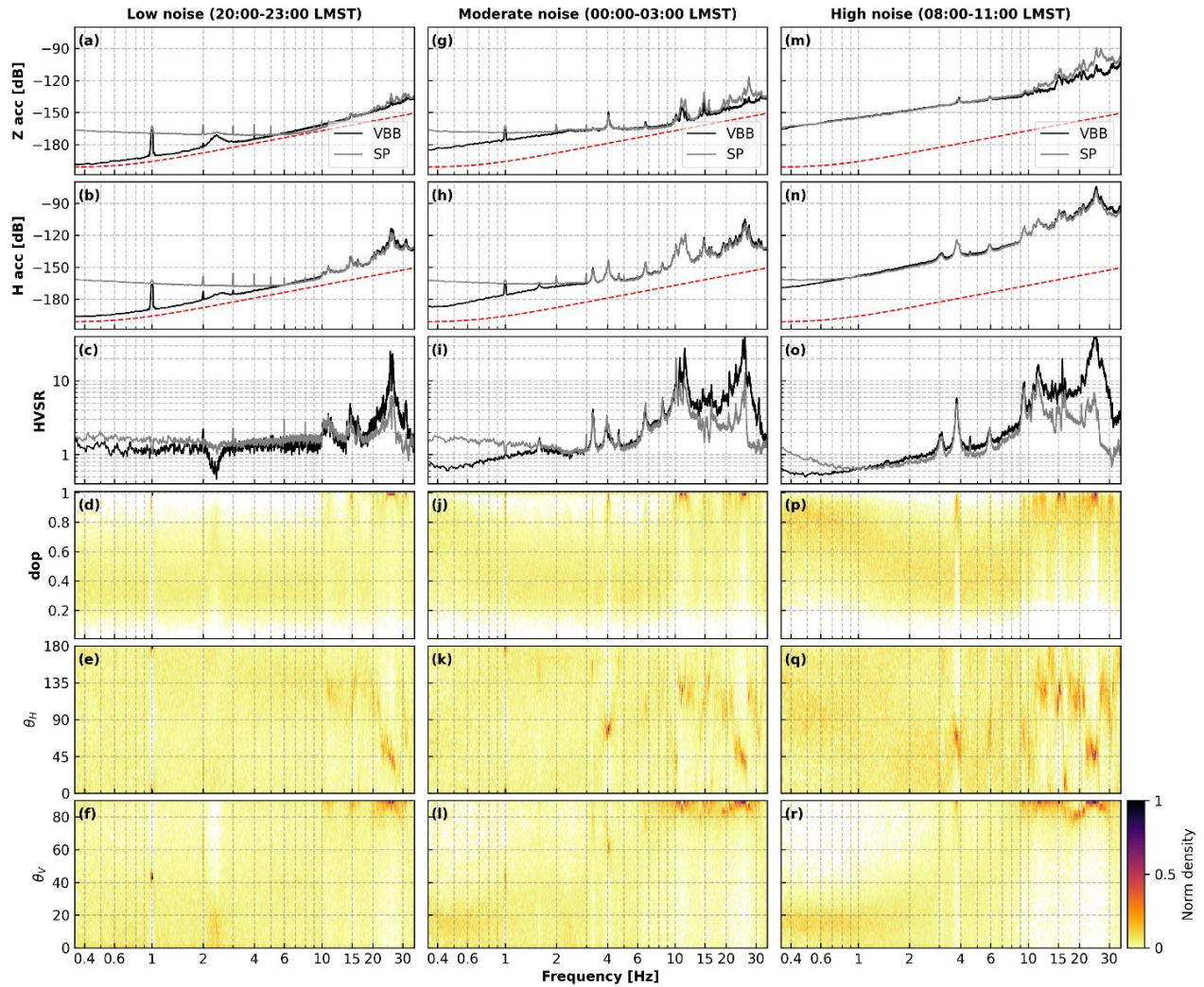
349

#### 350 **3.2.1 Low-noise period**

351 During the low-noise period (2a-f), the tick noise is a set of clear and narrow peaks observed at  
352 frequencies below 10 Hz, especially in the SP data. When no smoothing is applied, their presence  
353 in the H/V curve can be clearly identified and discarded. There is an overall good match between  
354 the SP and VBB horizontal components for frequencies above 6 Hz up to 21 Hz, which, in the  
355 vertical component is only observed between 14 and 20 Hz. Between 6 and 14 Hz, the amplitudes  
356 recorded by SP are slightly lower than those recorded by VBB, while below 6 Hz, the VBB  
357 recordings have lower amplitudes than SP. These amplitude differences below 14 Hz have been  
358 previously observed by Dahmen et al. (2021b), who interpreted the VBB spectral amplitudes  
359 between 6 and 14 Hz as its spectral noise floor, close to the theoretical instrument noise (Lognonné  
360 et al., 2019; Stutzmann et al., 2021), as shown in Fig. 2a. The same is observed for the SP  
361 amplitudes below 6 Hz, where the instrument noise level is reached. Besides the 2.4 Hz trough  
362 clearly visible from the VBB data, the resulting H/V curves are flat for frequencies below 10 Hz.

363





364  
 365 **Figure 2.** Spectral acceleration and polarization features during three different time periods of  
 366 Sols 422 and 423 (northern summer). (a)-(f) correspond to the vertical spectral acceleration, the  
 367 horizontal spectral acceleration, the HVSR, the degree of polarization ( $dop$ ) computed from VBB  
 368 data, the horizontal ( $\theta_H$ ) and vertical ( $\theta_V$ ) incidence angle, respectively, of the time period between  
 369 20:00 and 23:00 LMST. Analogously, plots (g)-(l) correspond to the time period between 00:00  
 370 and 03:00 LMST (moderate noise) whereas plots (m)-(r) are the respective features during the time  
 371 period between 08:00 and 11:00 LMST (high noise). The plots (a)-(c), (g)-(i) and (m)-(o) show  
 372 the median of the VBB (black) and SP (gray) data. Dashed red curve corresponds to the theoretical  
 373 self-noise of VBB.

374  
 375 Above 20 Hz, the recorded VBB horizontal amplitudes (VBBH) are slightly higher than those  
 376 from the SP (SPH), whereas the opposite is true for the vertical components (VBBZ and SPZ). As  
 377 the horizontal amplitudes are higher than the vertical ones for both sensors (see Fig. 1), a broad  
 378 peak in the H/V curve is observed, with higher amplitudes for the VBB sensor, particularly in the  
 379 frequency range between 20 and 30 Hz. In this frequency range, singular H/V peaks related to



380 highly polarized ground motion ( $dop > 0.7$ ) are revealed (Fig. 1d). The same is observed for other  
381 peaks at 10-12 Hz and around 15 Hz. All these peaks have a nearly horizontal incidence ( $\theta_V >$   
382  $60^\circ$ ), with different incidence angles  $\theta_H$ . Although the low-noise period is related to mainly low  
383 wind velocities, high wind bursts may also occur, which would explain the high polarization and  
384 horizontal incidence of the peaks observed at high frequencies ( $> 10$  Hz).

385

### 386 **3.2.2 Moderate and high-noise period**

387 During the moderate and high-noise period (Fig. 2g-l and 2m-r), the ambient vibrations level  
388 increases due to stronger winds and the aforementioned high-frequency peaks become even more  
389 distinguishable from the background noise. The overall spectral amplitudes are higher than in the  
390 low-noise period and, above 10 Hz, VBBZ has a persistent lower amplitude than SPZ. A variety  
391 of singular peaks are clearly observed on the H/V curve, including the lander modes in the ranges  
392 3-3.3 Hz, 3.8-4.1 Hz and around 6.8 Hz, which reveal a characteristic high and nearly horizontal  
393 polarization. All the singular peaks at higher frequencies (e.g.  $\sim 11$  Hz,  $\sim 15$  Hz,  $\sim 20$  Hz, and  $\sim 25$   
394 Hz) are even more polarized than in the low-noise period, with a predominantly horizontal rather  
395 than vertical incidence angle  $\theta_V$ , similar to the 4.1 Hz resonance, a well-known lander resonance  
396 (Dahmen et al., 2021b). Even more noticeable than in the low-noise period, striking differences  
397 between VBB and SP are observed for the H/V curves at frequencies above 10 Hz.

398

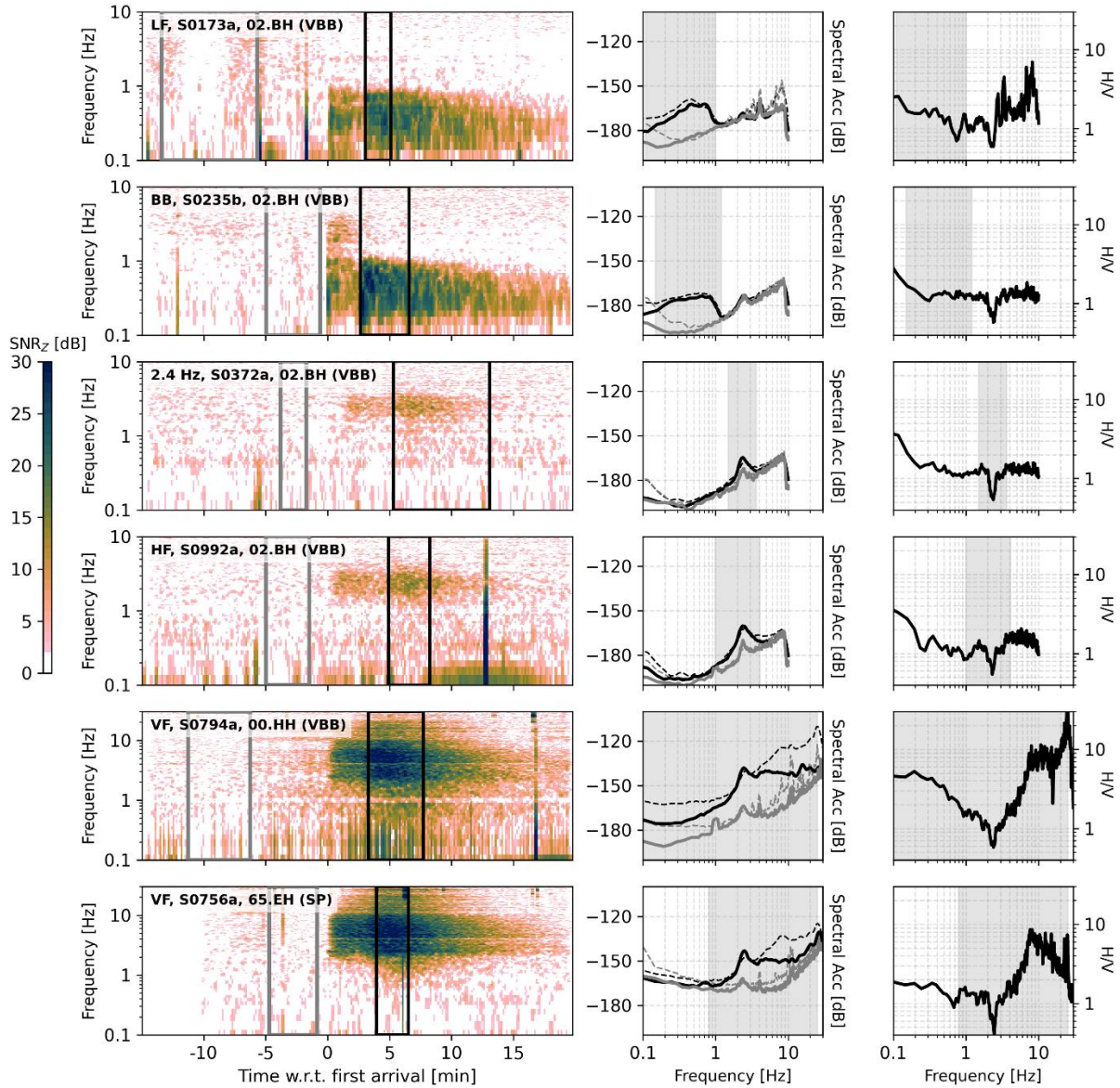
### 399 **3.3 Marsquakes H/V (eHV)**

400 The *eHV* curve was computed from the coda of 139 marsquakes. As we are interested in the  
401 computation of the H/V for actual seismic coda signal, we used the corresponding  $SNR_Z$  to choose  
402 the spectral segments with seismic energy above the pre-event seismic noise. Each type of  
403 marsquake excites different frequencies (Fig. 3), so using a pre-defined frequency range for  
404 different event types is meaningless, because there might be frequencies that are not excited by  
405 some seismic events. Thus, we combine all the H/V curves sections with  $SNR_Z > 2$  dB.

406

407 In order to check the SP and VBB differences revealed by the noise data, we also show two  
408 strong VF events independently recorded by VBB (event S0794a) and SP (event S0756a). Both  
409 events carry seismic energy above 1 Hz, but especially above 10 Hz (Fig. 3). They share H/V  
410 similarities between 1 and 10 Hz, but there are striking differences above 10 Hz. The H/V obtained

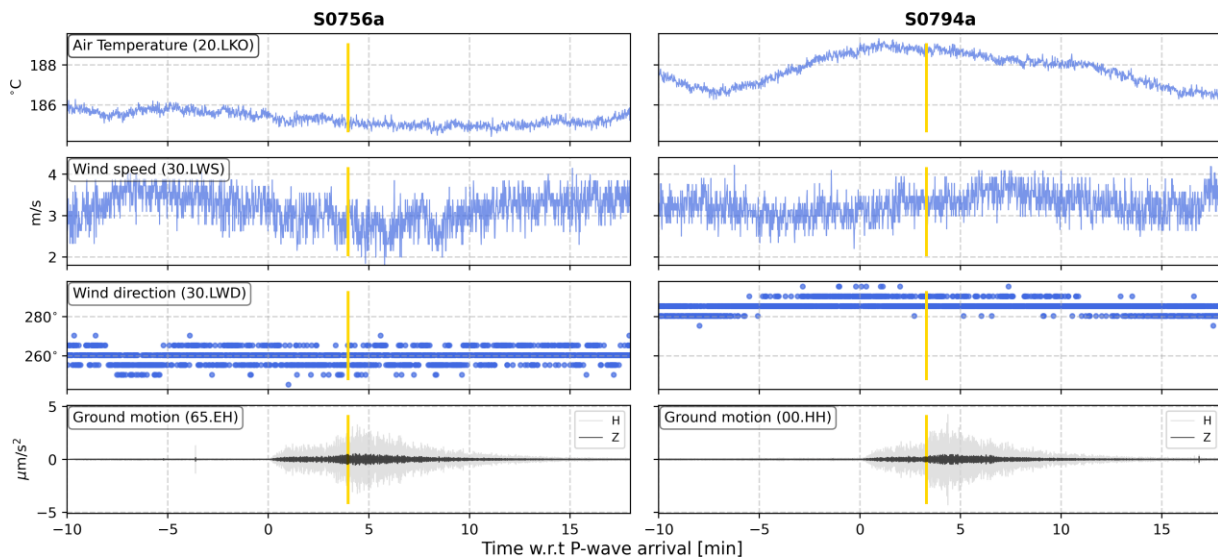
411 from the VBB recording presents a plateau-like shape followed by a strong peak at around 25 Hz,  
 412 whereas the SP recording reveal a decay towards higher frequencies.  
 413



414  
 415 **Figure 3.** Spectral features of different classes of marsquakes. From top to bottom: LF (S0173a),  
 416 BB (S0235b), 2.4 Hz (S0372a), HF (S0992a) and VF (S0794a and S0756a) class. Data from VBB  
 417 at 20 sps (02.BH) illustrate the characteristics of the LF, BB, 2.4 Hz and HF classes. The VF class  
 418 is represented by two events independently recorded by VBB (00.HH) and SP (65.EH) at 100 sps.  
 419 For each event, the  $SNR_z$  is plotted as a function of time, where a characteristic noise and S-wave  
 420 coda window are indicated as gray and black boxes, respectively. In the second column, the  
 421 vertical (solid) and horizontal (dashed) spectral power of the S-wave coda signal is compared to  
 422 the characteristic noise window. The H/V spectral ratio computed under the DFA approach is  
 423 represented by the black solid line. The shaded rectangular areas indicate the frequencies covered  
 424 by the different types of events.

425 The origin of the VF events, which shape the H/V curve above 5 Hz, remains unknown, so the  
 426 observed waveforms and different H/V curves might be influenced by the environmental  
 427 conditions. Nevertheless, during the occurrence of both VF events, no major environmental  
 428 changes related to the first arrival of the seismic energy or to the proposed S-wave arrival are  
 429 observed (Fig. 4). We thus conclude that the H/V curves of the VF events are unrelated to the  
 430 environmental conditions. Also, as we are using the seismic coda recorded at great distances, we  
 431 exclude the source as a determining feature.

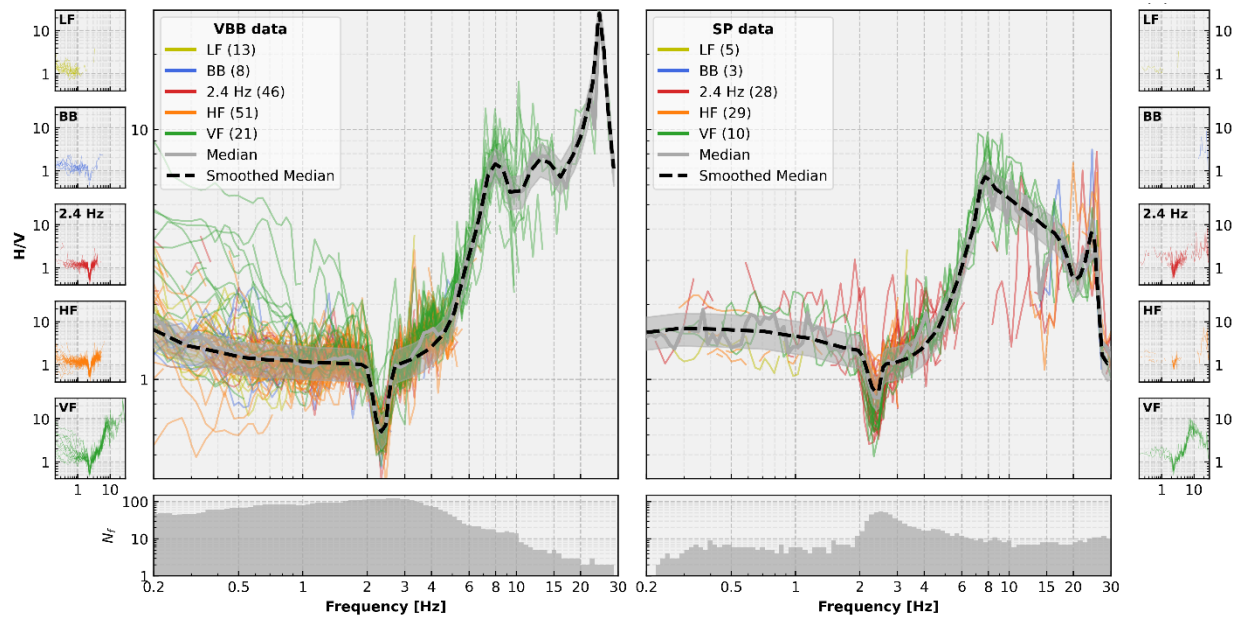
432



433 **Figure 4.** Environmental conditions during two large VF events: S0756a (left) and S0794a (right).  
 434 From top to bottom: air temperature, wind speed, wind direction, vertical acceleration and  
 435 horizontal acceleration. The vertical (black) and horizontal (gray) ground-motion recordings are  
 436 band-pass filtered between 6 and 9 Hz. The vertical yellow line indicates the S-wave arrival time  
 437 for each event.

438

439 We computed the median H/V curve for both SP and VBB sensors, separately (Fig. 5). As the  
 440 DFA-HV computation leads to unsmoothed curves, we applied a manual smoothing by following  
 441 the resulting median H/V curve, as shown in Fig. 5, which allowed us to mitigate the effect of lander  
 442 resonances such as the 4.1 Hz. Due to the lack of events with enough energy above the noise, the  
 443 *eHV* curve for the SP sensor is unreliable for frequencies below 2 Hz. Therefore, given the target  
 444 frequency range between 0.4 and 10 Hz, the preferred *eHV* curve is obtained from the VBB  
 445 recordings.



447 **Figure 5.** H/V curves derived from marsquakes recorded by VBB (left) and SP (right) with vertical  
 448 SNR larger than 2 dB. The curves are colored corresponding to different types of marsquakes. The  
 449 median and smoothed median H/V are denoted by the continuous gray and dashed black lines. The  
 450 gray areas illustrate the smoothed median  $\pm 15\%$  uncertainty range. The bottom plots indicate the  
 451 amount of marsquakes with  $\text{SNR}_z > 2$  dB per frequency ( $N_f$ ). Separate H/V curves for each type  
 452 of marsquakes are also plotted with the corresponding color.  
 453

454 Although there are only a few events with energy well above the ambient noise for frequencies  
 455 above 10 Hz, the H/V differences between SP and VBB are still noticeable, similarly to what was  
 456 derived from the noise data. Thus, we infer this phenomenon is most likely related to the  
 457 instruments themselves. The reason behind this SP-VBB difference is still unclear but seems to be  
 458 related to the amplification of the vertical components above 10 Hz. When compared to the  
 459 horizontals, the VBBZ seems to deamplify the ground motion in the frequency range roughly  
 460 between 10-35 Hz (see Fig. 1), whereas the SP sensor reveals similar amplitudes between SPZ and  
 461 SPH, especially for frequencies above 5 Hz, where the instrument response is flat (Lognonné et  
 462 al., 2019). The SP sensor was designed to record ground motion at high frequencies, so it would  
 463 be preferable here. Nevertheless, as the VBB and SP sensors are placed in different spots on the  
 464 SEIS Leveling system (LVL, Lognonné et al., 2019), a possible reason for the SP recording larger  
 465 vertical ground motions is that it could be exposed to larger vertical motions due to rotation of SEIS  
 466 (Fayon et al., 2018). Due to the persistent incompatibility of VBB and SP recordings at high  
 467 frequencies ( $>10$  Hz), both from noise or marsquakes data, we dismissed using the H/V curves  
 468 at high frequencies for any further analysis.



469

470 Finally, for frequencies below 10 Hz, the VBB H/V curve is chosen to be the representative  
471 *eHV* curve for the InSight landing site, which has a characteristic trough around 2.4 Hz and a  
472 strong peak around 8 Hz.

473

### 474 **3.4 nHV versus eHV**

475 Clear differences are observed between the VBB *nHV* and *eHV* curves, as shown in Fig. 6. On  
476 Earth, despite some differences, a generally good agreement between the *nHV* and *eHV* curves is  
477 typically observed (e.g., [Parolai et al., 2004](#); [Pilz et al., 2009](#); [Rivet et al., 2015](#)). [Napolitano et al.](#)  
478 [\(2018\)](#) suggest the differences between *nHV* and *eHV* curves can be related to an effect of the  
479 local topography, however, the InSight landing site is mostly flat without complex topography in  
480 the surrounding. Hence, the difference between the recorded *eHV* and *nHV* curves can be hardly  
481 related to a topographical effect. Rather, the reason for the difference between *nHV* and *eHV* is  
482 different for the quiet and noisy periods.

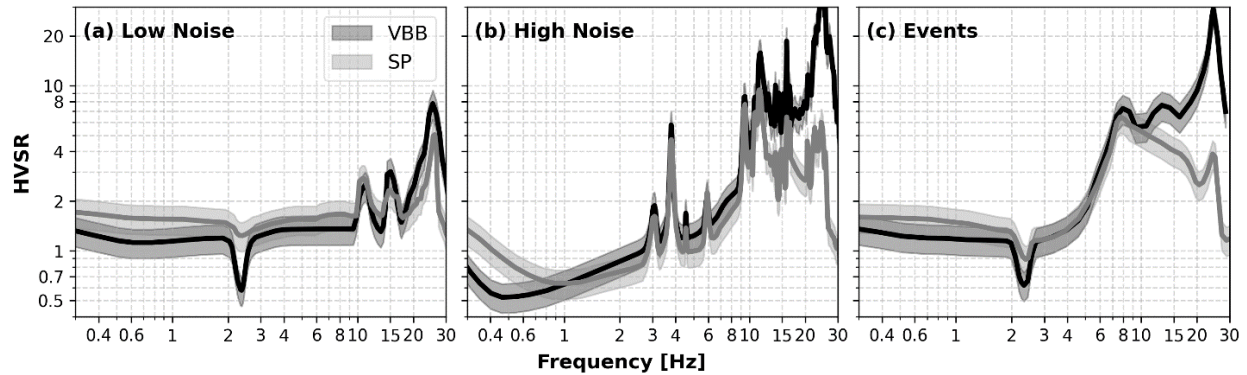
483

484 In the low-noise period, the *nHV* curve is similar to the *eHV* curve at frequencies below ~4  
485 Hz, including the trough around 2.4 Hz. Above 4 Hz, the *eHV* presents a strong peak around 8 Hz  
486 that is not visible on the low-noise *nHV* curve. We consider this difference might be caused by  
487 VBB most likely recording the instrumental self-noise at frequencies between 4 and 14 Hz. These  
488 observations suggest that, at least during the quietest period of a martian Sol, there is either an  
489 absence of energy coming from seismic waves propagating through the InSight landing site or the  
490 corresponding seismic energy is lower than the instrument self-noise of the SEIS instruments.  
491 Thus, due to the proximity and shape similarity of VBBZ to the theoretical self-noise, we suspect  
492 there is a risk during this time period of measuring the corresponding self-noises and thus the  
493 obtained H/V curve might be not representative of the subsurface structure, as has been  
494 experienced in some Earth cases (e.g., [van Ginkel et al., 2020](#)).

495

496

497



**Figure 6.** H/V curves for three different contexts at the InSight landing site as recorded by VBB (black) and SP (gray). **(a) Low noise:** mainly recorded during the martian evening and night, with wind speeds lower than  $\sim 2.8$  m/s, **(b) High noise:** typically recorded during the martian day-time, when high wind speeds ( $> 5$  m/s) are recorded, **(c) Events:** collection of early S-wave coda of the best recorded marsquakes.

During the quietest period of a martian Sol, the potential sources of noise at the InSight landing site are minimized due to the low wind speeds (Mimoun et al., 2017; Murdoch et al., 2017), so the instrument self-noise is likely recorded either on the horizontal or vertical components. Velocity variations in the frequency range between 6 and 9 Hz have been observed especially during the quiet periods. These variations are evidenced only on the horizontal (north and east) but not on the vertical component and can be understood as the thermo-elastic perturbation of the martian regolith sensed by a seismic wavefield (Compaire et al., 2022). Consequently, even if the horizontal ground-motion recorded during the quiet period is generated by the propagating seismic wavefield, it is unreliable to retrieve any information related to the subsurface structure from the H/V curve, because the vertical component is likely dominated by the instrument self-noise.

During moderate and high-noise periods, the differences between the  $eHV$  and the  $nHV$  curves are caused by different factors. The high-frequency signals recorded during these windy times, especially in the high-noise period, are above the instrumental noise, so they can be interpreted as actual ground-motion signals. The strong winds excite frequencies around 3.3, 4.1 and 6.9 Hz, which coincide with the lander resonances investigated by Dahmen et al. (2021b). Stronger excitation of frequencies around 11, 15, 20 and 25 Hz, which likely have a mechanical origin due to the interaction between the wind and the lander, are also observed. In the high-noise period, many of the narrow peaks are also related to the lander resonances, e.g. 3.0, 3.8, 5.8 Hz. These are the same lander resonances observed during the moderate-noise period, but their

525 eigenfrequencies are shifted because of the daily variation due to temperature changes (Dahmen et  
526 al., 2021b). A similar behavior is observed at higher frequencies, where the frequencies around 11,  
527 15, 20 and 25 Hz are strongly excited and shifted.

528  
529 The excitation of these non-natural resonances contaminates the H/V curves due to their  
530 mechanical origin, and thus do not represent the local subsurface structure. In addition, the  
531 broadband shape of the moderate and high-noise *nHV* curves can be understood as the mechanical  
532 noise generated by the interaction of strong martian winds with the InSight lander and the WTS, as  
533 proposed by Murdoch et al. (2017). In this case, even at high frequencies, the horizontal ground  
534 response to the wind is expected to be greater than the vertical one due to propagation of shear stress  
535 (Naderyan et al., 2016; Lott et al., 2017). This broadband *nHV* shape is not directly related to the  
536 subsurface structure. Indeed, Mucciarelli et al. (2005) showed that high wind speeds enhance the  
537 horizontal components, likely explained by flow rotation near the soil and the instrument, leading  
538 to unreliable H/V peaks at high frequencies.

539  
540 In general, the influence of the lander is highly visible on the *nHV* curves during moderate and  
541 high-noise periods. Between 1 and 10 Hz, even though these *nHV* curves also show an increasing  
542 towards higher frequencies (Fig. 6b), its shape is different (less steep) than the preferred *eHV* curve  
543 (Fig. 6c). For example, the H/V amplitude at 8 Hz is lower on the high-noise *nHV* (~2) than the  
544 *eHV* (~8). Also, the effect of Sorrels propagative pressure waves is identifiable as a broad trough  
545 below 1 Hz (Kenda et al., 2020; Stutzmann et al., 2021). Because of this high contamination by  
546 external factors, we discarded these noisy periods from the H/V analysis.

547  
548 Thus, the VBB *eHV* curve is preferred for the inversion for the subsurface structure instead of  
549 any of the *nHV* curves. In particular, the VBB *eHV* is suitable for the H/V inversion under the DFA  
550 because of the high diffusivity and strong multiple-scattering revealed for the martian crust  
551 (Lognonné et al., 2020; van Driel et al., 2021; Menina et al., 2021). These phenomena lead to a  
552 diffuse seismic coda, where a combination of scattered body and surface waves is expected and  
553 therefore the full wavefield DFA is a good representation.

554  
555



## 556 **4 H/V inversion**

### 557 **4.1 H/V inversion using DFA**

558 The *eHV* curve (hereafter, the final H/V and defined as *fHV*) is chosen to be a good representation  
559 of the H/V response of the subsurface structure at the InSight landing site. We inverted this *fHV*  
560 curve for a 1-D shear wave velocity model ( $V_s$ ) using the diffuse wavefield approach. The  
561 inversion scheme can be divided into two parts: the theoretical H/V forward modelling and the  
562 non-linear inversion procedure.

563

#### 564 **4.1.1 Forward modelling of H/V**

565 Given a 1-D layered subsurface model (including P-wave velocity, S-wave velocity, density and  
566 thickness of each layer), the theoretical H/V spectral curve under the DFA can be computed from  
567 the corresponding Green's function (GF), following equation (4). In this work, the GFs are  
568 calculated using the technique developed by [Margerin \(2009\)](#), which consists on the summation  
569 of the generalized eigenfunctions of the layered elastic medium. This technique is implemented  
570 via an open-source code that has been already successfully applied to terrestrial data (e.g. [Margerin](#)  
571 [et al., 2009](#); [Galluzzo et al., 2015](#)).

572

573 The code calculates the vertical and horizontal spectral ground-motion for each P-, S-, Love- and  
574 Rayleigh-waves individually, so the contribution of body and surface waves can be separately  
575 derived. The H/V curve for the full wavefield, including the contribution of all the types of waves,  
576 can be also obtained. Given the diffuse nature of the seismic coda used for the *eHV* curve, instead  
577 of using one type of wave propagation mode such as fundamental mode Rayleigh waves as in  
578 [Hobiger et al. \(2021\)](#), we make use of the full wavefield H/V curve as the forward theoretical  
579 prediction to explain the interpreted signal of the *eHV* curve at the InSight landing site.

580

#### 581 **4.1.2 Inversion algorithm and parameterization**

582 In order to find the best subsurface models explaining the observed *fHV* curve, we employed the  
583 Neighbourhood Algorithm (NA), which was developed by [Sambridge \(1999\)](#) and adjusted for this  
584 case by [Wathelet \(2008\)](#). This technique was implemented via the *dinver* toolbox included in the  
585 Geopsy package ([Wathelet et al., 2020](#)). The NA is suitable for this type of inversion due to the  
586 intrinsic non-uniqueness problem of the H/V curves, i.e. without further information or constraints,

587 the same H/V curve can be explained by many different subsurface models (e.g., Piña-Flores et al.,  
588 2016). The NA provides an efficient exploration of the parameters space to retrieve different  
589 subsurface models fitting the H/V curve.

590  
591 The NA makes use of the misfit between observed and theoretical H/V curves to explore the  
592 area of the parameter space where the models with low misfit are expected. The misfit function is  
593 defined as follows:

$$\phi_{hv}(\mathbf{m}) = \sqrt{\frac{1}{N} \sum_{i=1}^N \frac{\left( \log\left(\frac{H}{V_{mi}}\right) - \log\left(\frac{H}{V_{di}}\right) \right)^2}{\sigma_{di}^2}} \quad (7)$$

595 where  $\mathbf{m}$  is the evaluated model,  $N$  is the number of frequency points of the observed  $\left(\frac{H}{V_d}\right)$  and  
596 full-wavefield modelled  $\left(\frac{H}{V_m}\right)$  curves.  $\sigma_{di}$  is the standard deviation of the  $\frac{H}{V_d}$  curve at a given  
597 frequency. Following Lontsi et al. (2015), we implemented a logarithmic misfit to avoid  
598 overweighting strong peaks in the H/V curve. After the parameters space is explored with the NA,  
599 for a given parameters setting, several best models with the misfit around the global minimum are  
600 selected as the possible models explaining the observed  $fHV$  curve.

601  
602 We inverted for the shear wave velocity structure only, including the corresponding layer  
603 thickness, as it has been demonstrated to be the main parameter affecting the H/V curve (e.g.,  
604 Malischewsky and Scherbaum, 2004; Bonnefoy-Claudet et al., 2006). For the inversion, the  
605 parameters space explored by the NA is bounded by the prior knowledge based on the pre-landing  
606 model. This pre-landing model, based on the size range of rocky ejecta craters and exposures in  
607 nearby fracture zones, suggests a transition from the shallow regolith to a coarse ejecta layer,  
608 followed by a fractured basaltic layer and a deeper pristine basaltic unit (Knapmeyer-Endrun et  
609 al., 2017; Golombek et al., 2017; Warner et al., 2017). Based on the size range of the rocky-ejecta  
610 craters and ghost craters, previous mapping suggests that the basalt layer has a thickness of  $\sim 170$  m  
611 thick near the landing area (Warner et al., 2017; Golombek et al., 2018; Pan et al., 2020) and are  
612 underlain by sedimentary rocks likely of Noachian age (Pan et al., 2020).

613

614 Thus, based on the pre-landing model for the first 50 meters, the parameters space is defined for  
 615 a model with four layers over a half-space (4LOH). The results of the inversion are affected by this  
 616 constraint such that a different number of layers will likely lead to different solutions. Table 2  
 617 presents the value ranges of the parameter spaces explored in the different inversion runs. Further  
 618 details on these values are explained in the following.

619  
 620 **Table 2.** Range of values defining the parameter spaces to be explored during the inversion of the  
 621 *fHV* curve. The values in parenthesis correspond to the maximum shear-wave velocity for the  
 622 small (S) and medium (M) parameter spaces, respectively. Density and  $V_p/V_s$  are fixed for each  
 623 layer.

	Bottom depth [m]	$V_s$ [m/s]	Density [ $\text{kg/m}^3$ ]	$V_p/V_s$
<b>Layer 1</b>	0-10	Top: 40-80 Bottom: 70-300	1350	1.87
<b>Layer 2</b>	3-30	100-2000 (1000, 1500)	2000	1.73
<b>Layer 3</b>	5-60	100-2000 (1000, 1500)	2900	1.73
<b>Layer 4</b>	10-100	100-2000 (1000, 1500)	2900	1.73
<b>Half-space</b>	-	200-2000 (1000, 1500)	3300	1.73

624  
 625 The inversion of the H/V curve alone, without further observations, has been demonstrated to be  
 626 heavily affected by the non-uniqueness phenomenon (e.g., Piña-Flores et al., 2016). Therefore,  
 627 constraining the parameters space is relevant for obtaining the proper model. So far, the best new  
 628 constraints of the inversion are the shear-wave velocities obtained from the hammering experiment  
 629 (Lognonné et al., 2020; Brinkman et al., 2022), determined to be lower than 80 m/s at the surface,  
 630 and the thickness of the shallow regolith layer, expected to be no deeper than 10 m (Golombek et  
 631 al., 2020b,a). Due to the expected compaction, the S-wave velocity of the first layer is modelled  
 632 as a power law increase. Because the H/V inversion is not very sensitive to variations in density,  
 633 this parameter is fixed for each layer, as well as the  $V_p/V_s$  ratio. This way, the P-wave velocity  
 634 is derived from the inverted S-wave velocity. In particular, for the shallowest layer, we used  $V_p/V_s$   
 635 = 1.87, as reported by Brinkman et al. (2022), and  $\rho = 1350 \text{ kg/m}^3$ , following the pre-landing  
 636 assessment of this site (Morgan et al., 2018). This  $V_p/V_s$  lies in the range 1.68 – 2.56 for dry  
 637 unconsolidated material, as shown by investigations on Earth samples and also derived for the  
 638 Lunar regolith (e.g., Uyanik, 2010; Dal Moro, 2015). The density and  $V_p/V_s$  of the deeper layers  
 639 are set to standard values of volcanic regions on Earth (e.g., Lesage et al., 2018).

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Regarding the deeper layers, in volcanic areas on Earth, the shear-wave velocities of basaltic layers have been shown to range from 500 m/s to 2000 m/s at shallow depths (Delage et al., 2017). On the other hand, an unexpected low velocity layer should be placed at larger depths to explain the 2.4 Hz resonance (Hobiger et al., 2021). We explored a large parameters space with shear-wave velocities between 100 and 2000 m/s extending down to 100 m. In particular, we performed different inversion runs with different maximum shear-wave velocities of 1000 (small), 1500 (medium) and 2000 m/s (large model).

As shown in figure 6, our target  $fHV$  has a narrow trough around 2.4 Hz and a steep left flank leading to a strong peak at around 8 Hz. No clear peaks or troughs are observed at low frequencies between 0.4 and 2 Hz. For each frequency, a common uncertainty range of 15% of the H/V amplitude was set.

For each 4LOH parameters space presented in Table 2 (S1, M1, L1), a total of ~45000 models were explored using the NA, for which three different inversion runs were performed in order to have a better search of the models fitting the  $fHV$  curve. For each parameters space, the best fitting models with a misfit lower than 0.3 were chosen, from which 200 random models are plotted in Figure 7. This way, three different subsets of models that fit the  $fHV$  curve well can be identified. The best misfit of these models is obtained from the M1 inversion runs (~0.242). However, an overall good fitting of the  $fHV$  curve is obtained for models with misfit values lower than 0.3 and thus all these models can be a good representation of the subsurface structure.

671 **5 Discussion**

672 **5.1 Implications for the subsurface structure**

673 **5.1.1 Models from *fHV* inversion**

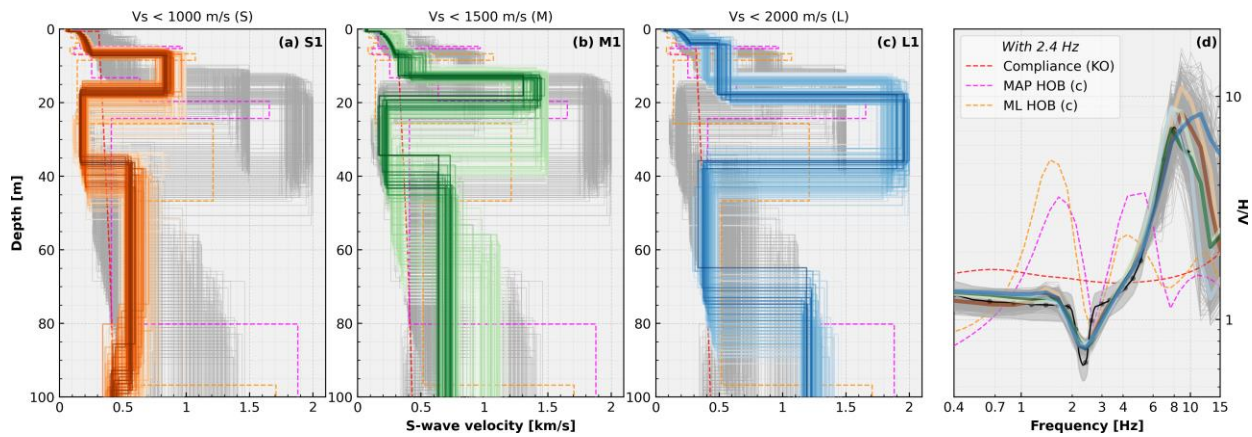
674 Some similarities and differences can be highlighted from the comparison of the S1, M1 and L1  
675 models (the SML1 models). They all present a characteristic shallow high velocity layer (SHVL)  
676 followed by a buried low velocity layer (bLVL) with a sharp contrast between the SHVL and the  
677 bLVL. The latter bLVL has been proposed to be the cause of the 2.4 Hz resonance due to seismic  
678 waves trapped in this low-velocity layer (Hobiger et al., 2021). Against the pre-landing subsurface  
679 models, the bLVL in the resulting models of this work, as well as Hobiger et al. (2021), is an  
680 unexpected feature of the subsurface structure. A similar sharp contrast is expected between the  
681 SHVL and the subsurface structure above, which can be understood as the mechanism to generate  
682 the 8 Hz peak on the *eHV* curve. The bLVL is followed by a faster half-space, which has lower  
683 velocities than the SHVL and therefore represents a less sharp discontinuity.

684  
685 The bLVL of the L1 models is in good agreement with the bLVL proposed by Hobiger et al.  
686 (2021) (hereafter, HOB) to explain the 2.4 Hz trough. Nevertheless, in our case, the units below  
687 the bLVL have relative lower velocities than the SHVL whereas, in the HOB models, the bLVL  
688 is followed by a layer with velocities even higher than the SHVL, which generates an H/V peak  
689 between 1 and 2 Hz that is not observed from the SEIS data, as shown in Fig. 7d.

690  
691 The models arrive at different velocities and thicknesses of each layer, which is a demonstration  
692 of the non-uniqueness problem of the H/V inversion. In general, depending on the thickness and  
693 velocity of the SHVL, the bLVL will be placed at shallower or larger depths with a thickness  
694 between 15 and 25 m and a velocity ranging between 100 and 500 m/s. In any case, a generic  
695 subsurface pattern of a bLVL below a SHVL is required to simultaneously generate a H/V peak  
696 around 8 Hz and trough around 2.4 Hz.

697  
698 Our results suggest the features of the *fHV* curve can be explained by the full wavefield rather  
699 than by a single type of waves. In particular, the 2.4 Hz resonance is hardly derived from the  
700 Fundamental Rayleigh mode as computed under the DFA (see Fig. S1). Instead, this resonance is  
701 closely coinciding with a P-wave resonance and modelled as a resonance of the full wavefield.

## Empirical $H/V$ from martian seismic noise and marsquakes



702  
703

704 **Figure 7.** Sets of models obtained from the inversion of the  $fHV$  curve, between 0.4 and 10 Hz,  
705 using different parameter spaces. 200 best random models are plotted for each of the three  
706 parameters space explored: **(a)** S1 (small, orange), **(b)** M1 (medium, green) and **(c)** L1 (large,  
707 blue). For each parameters space, the models with darkest colors indicate a best (lower) misfit. **(d)**  
708 Synthetic full wavefield  $H/V$  response of the different models drawn in subfigures (a)-(c). Two  
709 representative models from each parameters space are plotted following the corresponding color  
710 pattern. Besides, the constrained MAP and ML models from [Hobiger et al. \(2021\)](#) and the model  
711 derived from ground compliance measurements ([Onodera, 2022](#)), together with their  
712 corresponding synthetic full-wavefield  $H/V$  response, are plotted as magenta, yellow and red  
713 dashed lines, respectively.

714

715 For the L1 models, the bLVL coincides with what has been proposed to be a geological unit  
716 sandwiched between Early Hesperian to Early Amazonian basalt flows, which may have a  
717 sedimentary origin ([Hobiger et al., 2021](#)). The shallow high velocity layer then corresponds to the  
718 Early Amazonian basaltic lava flows (~1.7 Ga, [Warner et al., 2017](#); [Wilson et al., 2019](#)).  
719 Meanwhile, the half-space below the bLVL must be either a layer within the Early Amazonian or  
720 the Early Hesperian basalt lava flows ([Warner et al., 2017](#); [Hobiger et al., 2021](#)).

721

722 Crater statistics suggest significant erosion and landscape degradation between an Early  
723 Hesperian volcanic surface (3.6 Ga) and the early Amazonian effusive volcanism (1.7 Ga), which  
724 is estimated to be ~140 m thick ([Warner et al., 2022](#)). Furthermore, throughout the dichotomy  
725 boundary between the southern Noachian highlands and the northern plains, there are Noachian  
726 through Hesperian transition units that indicate active erosion and deposition of sedimentary  
727 materials ([Tanaka et al., 2014](#); [Pan et al., 2017, 2020](#)). To the south of InSight lander, some of the  
728 Amazonian-Hesperian transition units are sedimentary deposits ([Pan et al., 2020](#)) as well as the



729 Medusae Fossae Formation (Tanaka et al., 2014). In addition, alluvial activity has occurred further  
730 south in Gale crater during this period (Grant et al., 2014; Grant and Wilson, 2019). Given this  
731 evidence for aqueous activity in the geological record, it is possible that there was both erosion of  
732 the Early Hesperian surface and deposition of sedimentary deposits prior to the deposition of the  
733 Early Amazonian basalt flows.

734  
735 If Early Hesperian lava flows are beneath the bLVL, these rocks would be expected to be more  
736 fractured by impact cratering due to the higher cratering rate of the Hesperian (e.g., Hartmann and  
737 Neukum, 2001) or longer exposure to the surface; and to be more altered by aqueous activity than  
738 the Early Amazonian volcanics. The expected greater physical and chemical weathering of the basalt  
739 flows in Early Hesperian presents a reasonable explanation for the relatively lower seismic  
740 velocities of the half-space beneath bLVL compared to the SHVL.

741  
742 In the case of the S1 and M1 models, the bLVL is located at shallower depths (< 40 m) and the  
743 corresponding SHVL right above it is a thin and fast layer. Although we cannot completely discard  
744 these models, the thin SHVL and the extremely low velocities of the bLVL, considering the effects  
745 of the overburden pressure, seem to be unlikely and disfavor these models. Nevertheless, if the  
746 SHVL had higher velocities, its thickness would also increase and therefore the bLVL would be  
747 placed at larger depths. In any case, the thickness of the bLVL would range between 15-25 m,  
748 which is less than the ~50 m thickness proposed by Hobiger et al. (2021).

749  
750 There is a lack of resolution for the structure above the SHVL because the higher frequencies  
751 were excluded from the analysis. Nevertheless, the inversion of compliance measurements suggests  
752 the regolith layer is most likely about 1 m thick and everything below is associated with coarse  
753 blocky ejecta material (Onodera, 2022). This shallow interface would generate an H/V peak  
754 between 25 and 30 Hz, which is out of the frequency range here investigated. A H/V peak at these  
755 frequencies is hardly observed from the data due to the strong excitation of a highly polarized  
756 resonance at this frequency range (see Fig. 1 and 2), which might be related to the LSA (Hurst et  
757 al., 2021). Anyway, this shallow discontinuity between the regolith and the coarse ejecta layer  
758 cannot be discarded. Therefore, we can infer the top of the SHVL is likely below the coarse ejecta  
759 layer and does not correspond to the regolith interface.



760 **5.1.2 Alternative model without 2.4 Hz trough**

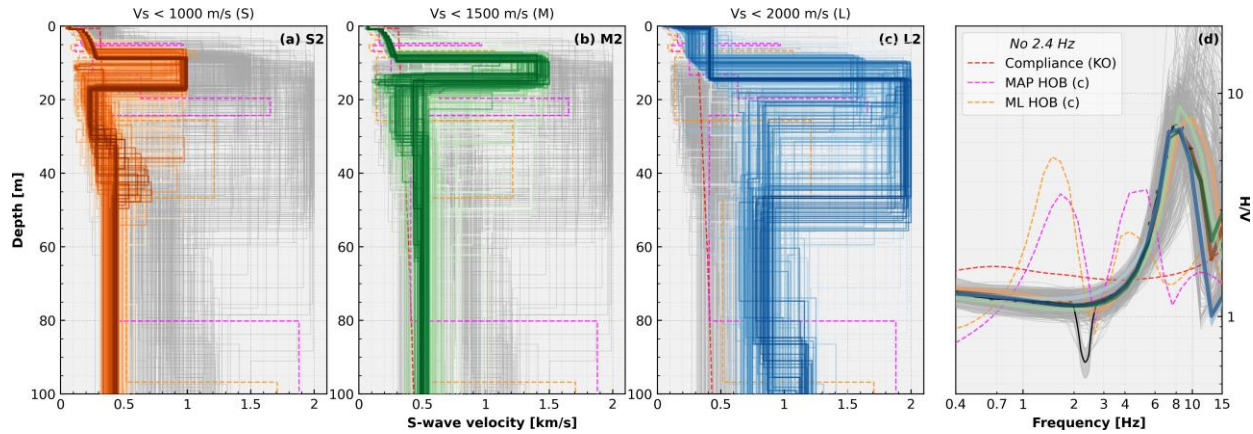
761 The inversions above were performed assuming the origin of the 2.4 Hz resonance is related to the  
762 subsurface structure. In fact, this has not yet been proven and the mechanism to generate this  
763 resonance remains unclear. An interesting observation is that this trough is clearly observed from  
764 seismic noise data and also from seismic events data, which is in contradiction to previous  
765 observations on Earth, where the effect of a bLVL on the H/V curve has been observed to be less  
766 visible in the noise data than the events (Di Giacomo et al., 2005; Panzera et al., 2015).

767  
768 Because of this, we performed a second round of *fHV* inversions using the same parametrization  
769 but simultaneously fitting the frequency ranges between 0.4-2 Hz and 3-10 Hz, so the 2.4 Hz is  
770 ignored. Once again, three parameter spaces are explored and are analogously referred as S2, M2  
771 and L2 models (SML2) and illustrated in Figure 8 in the same way as for the SML1 models (Fig. 7).

772  
773 From these new inversion runs, the non-uniqueness problem is still apparent, so it is difficult to  
774 provide one single model for the subsurface structure. One can see the S2, M2 and L2 models are  
775 analogous to the SML1 models. However, some interesting features can be highlighted. In both  
776 cases, ignoring the 2.4 Hz trough or not, the SHVL is required for modelling the strong 8 Hz peak  
777 and low velocities below it are needed. Nevertheless, in the SML2 models, the velocity contrast  
778 between the SHVL and the underlying bLVL is less sharp than those derived for the SML1 models.  
779 Thus, the presence of a bLVL is likely, even when the 2.4 Hz trough is ignored. The difference  
780 between generating a 2.4 Hz resonance or not will depend on the sharpness of the contrast between  
781 the SHVL and the bLVL.

782  
783 Consequently, the geological interpretation of the SML2 models is similar to the interpretation  
784 of the SML1 models. The main difference lies in the properties of the bLVL such that a weaker  
785 bLVL will generate the 2.4 Hz resonance, due to the sharp contrast with respect to the SHVL,  
786 whereas a more consolidated bLVL will properly model the *fHV* curve without the 2.4 Hz trough.

787



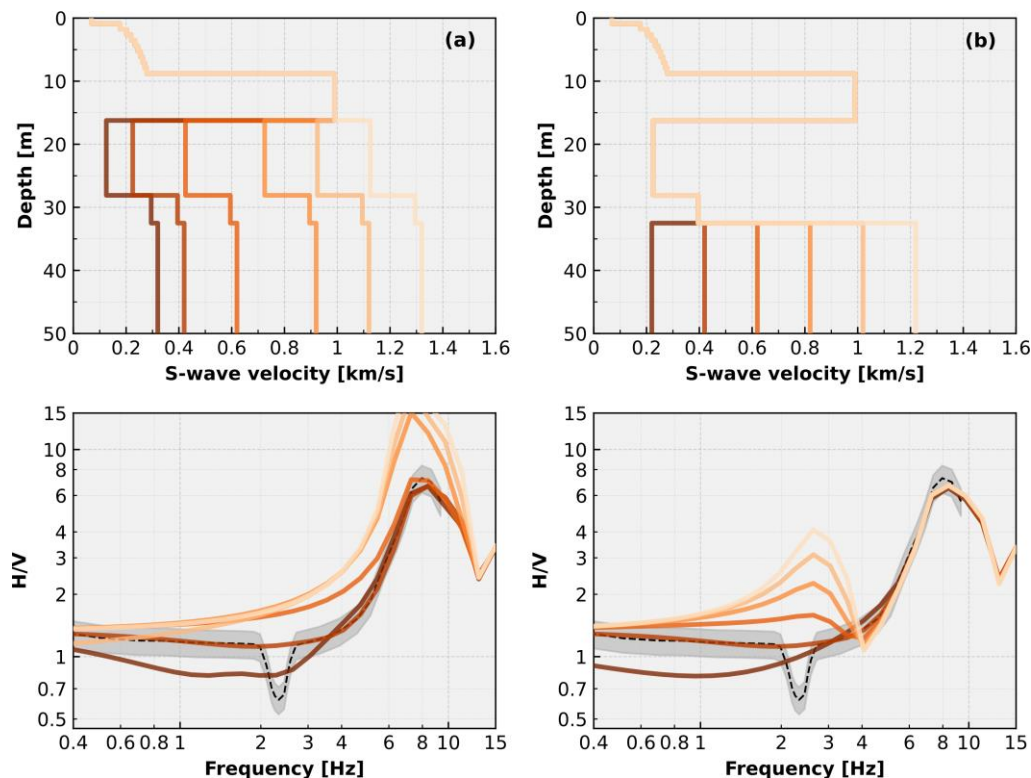
788  
 789 **Figure 8.** Sets of models obtained from the inversion of the  $fHV$  curve in two different frequency  
 790 ranges, between 0.4-2 Hz and 3-10 Hz, using different parameter spaces. 200 best random models  
 791 are plotted for each of the three parameters space explored. The color patterns and other features  
 792 are analogous to Fig. 7.

793  
 794 Lower velocities are required immediately below the SHVL to model the  $fHV$  curve, with or  
 795 without the 2.4 Hz trough. In this sense, Fig. 9a shows that models without a clear bLVL (lightest  
 796 colors) will also generate a H/V peak around 8 Hz, but with a larger amplitude and a poor fitting  
 797 of the left-flank decay. Thus, in order to fit both peak and decay, besides the SHVL, we require  
 798 the presence of a bLVL, which becomes an essential feature to explain the whole  $fHV$  curve.  
 799 Furthermore, as shown in Fig. 9b, if the layer below the bLVL has higher relative velocities, then a  
 800 secondary peak at lower frequencies, which is not observed from the data, would be generated.  
 801 Therefore, general low velocities are required below the SHVL.

802  
 803 The lower velocities below the SHVL can be explained by the presence of a sedimentary layer  
 804 and also differences in the physical weathering process between the Early Hesperian and Early  
 805 Amazonian lavas. This difference between the shallow Amazonian and deeper Hesperian layers is  
 806 always required, either for the SML1 or SML2 models, as it allows for the characteristic steep left  
 807 flank of the  $fHV$  curve.

808  
 809 Another relevant aspect is the different velocity ranges explored in the parameter spaces of the  
 810 SML1 and SML2 models. On Earth, Lesage et al. (2018) studied the velocity profiles for different  
 811 volcanic areas, including andesitic and basaltic deposits, and they found that shear-wave velocities  
 812 lower than 500 m/s are typically observed in the first 50 m depth. In a similar way, Panzera et al.

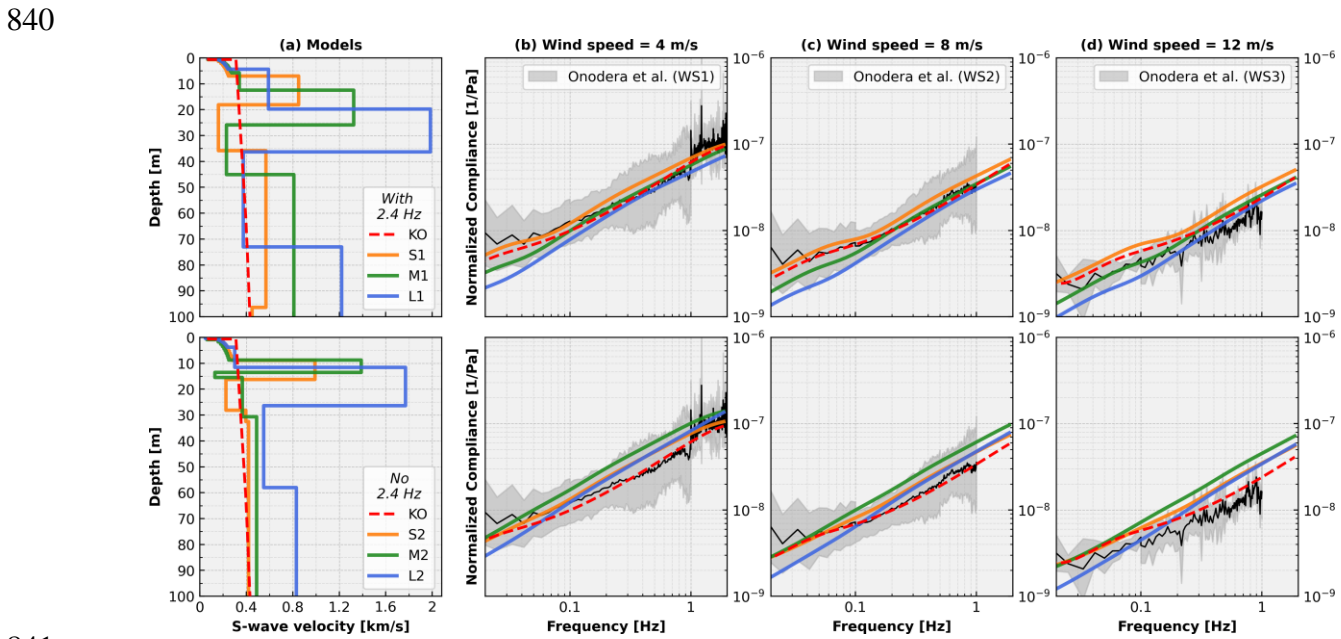
813 (2015) compared a stratigraphic sequence from borehole data with the velocity model derived from  
 814 H/V inversion for a site near Mt. Etna. They associated shear-wave velocities between 500-1000  
 815 m/s with the corresponding basaltic layer underneath. These regions on Earth share some  
 816 similarities with western Elysium Planitia (Golombek et al., 2017, 2020b). Under this context, the  
 817 velocities obtained for models S1 and S2 are well within the expected range of shallow velocities  
 818 in a volcanic region. Assuming these lower velocities, the thickness of the SHVL would be no  
 819 greater than 15 m, which falls in the reasonable range of basaltic lava flow thicknesses.  
 820 Nevertheless, shear-wave velocities around 2000 m/s have been obtained from laboratory  
 821 experiments for basaltic rock samples under the influence of confining pressure (e.g., Vinciguerra  
 822 et al., 2005). Also, differences between the shear-wave velocities derived from indirect seismic  
 823 and lab samples have been revealed (Lesage et al., 2018). Therefore, an SHVL with higher  
 824 velocities is still possible, which would be associated with a thicker layer.  
 825  
 826



827  
 828 **Figure 9.** Synthetic modelling of H/V using different velocity profiles below the shallow high  
 829 velocity layer (SHVL). (a) Different overall velocities below the SHVL. (b) Fixed bLVL velocity  
 830 and varying velocity of the half-space below.  
 831

832 **5.1.3 Compatibility with compliance observations**

833 Besides the H/V analysis, the ground compliance is an independent observation that can help to  
 834 understand the first tens of meters underneath the InSight landing site. In this regard, [Onodera](#)  
 835 ([2022](#)) computed the ground compliance using the SEIS and pressure data for a large set of  
 836 convective vortices occurring in the nearby region. The inversion under a Bayesian approach of  
 837 this data set allowed them to provide a most likely model consisting of a thin shallow regolith (~1  
 838 m thick) followed by a coarse ejecta layer without further discontinuities below (see Fig. 7, 8 and  
 839 10), at least down to ~75 m.



841

842 **Figure 10.** Characteristic models from set of models S1, M1, L1 (top) and S2, M2, L2 (bottom)  
 843 and their synthetic ground compliance. (a) Shear-wave velocity structure for characteristic models  
 844 from the SML1 (top) and SML2 models (bottom). The model proposed by [Onodera \(2022\)](#) is  
 845 plotted with dashed red line. The respective synthetic compliance response and the measured  
 846 ground compliance (black curve and dark gray area) are plotted for different wind levels: (b) 0 - 6  
 847 m/s, (c) 6 - 12 m/s, (d) 12 - 18 m/s.

848

849 Our proposed models differ from the models obtained from the inversion of compliance data as  
 850 we are unable to properly resolve the first few meters of the subsurface structure at the InSight  
 851 landing site, whereas the compliance inversion is highly sensitive to the shallow depths close to  
 852 the surface. Nevertheless, our models are constrained by the velocities derived from the  
 853 hammering experiment, which are in good agreement with those from the compliance inversion.

854

855 In order to assess the validity of our proposed models in terms of the observed ground  
856 compliance, among the best-fitting models, we chose one model representing each S1, M1, L1 and  
857 S2, M2, L2 model subsets, and computed their synthetic ground compliance response following  
858 the same approach as in [Onodera \(2022\)](#). The characteristic models and their synthetic compliance  
859 are plotted in Figure 10.

860  
861 The synthetic ground compliance modelling shows that our proposed models generate a  
862 compliance response that fits well within the error range of the measurements. Because of this,  
863 the rejection of models based on the compliance measurements can be hardly carried out.  
864 Particularly, the presence of the SHVL and the bLVL cannot be discarded. It is important to note  
865 that, given the Bayesian approach, the models obtained from the inversion of the compliance data  
866 are the most likely models given a set of *a priori* conditions. Nevertheless, models with unexpected  
867 rigidity such a high-velocity layer or a low-velocity layer can also explain the observations, as  
868 shown in Fig. 10 and S2 (see Supp Material).

869

## 870 **5.2 The relevance of the marsquakes data**

871 One of the advantages of using ambient vibrations data for the H/V analysis is certainly the  
872 abundance of recordings. On the contrary, using seismic events on Mars is less efficient not only  
873 due to the low seismic activity ([Giardini et al., 2020](#)) but also because the events are required to  
874 excite a wide frequency range.

875

876 Even though more than 900 events have been reported by the MQS, only the VF events have  
877 excited the resonance frequency at 8 Hz and just a few of them have been properly recorded by SEIS.  
878 The scarcity of these events is not a problem because we make use of their S-wave coda, which is  
879 produced by the multiple scattering of seismic waves. The multiple scattering phenomenon is  
880 expected to be the same for events occurring at different distances and/or azimuths, as long as they  
881 carry enough seismic energy above 5 Hz ([Aki and Chouet, 1975](#)). Thus, future events exciting the  
882 high-frequency part of the spectrum are expected to generate the same H/V curve from the S-wave  
883 coda, which can be interpreted as the interference of multiple reverberations due to local  
884 conversions in the subsurface structure underneath, which generates surface-wave like ground  
885 motion (rather than recording direct Rayleigh or Love waves). Therefore, the full wavefield



886 approach is an appropriate technique for modelling the corresponding H/V.

887

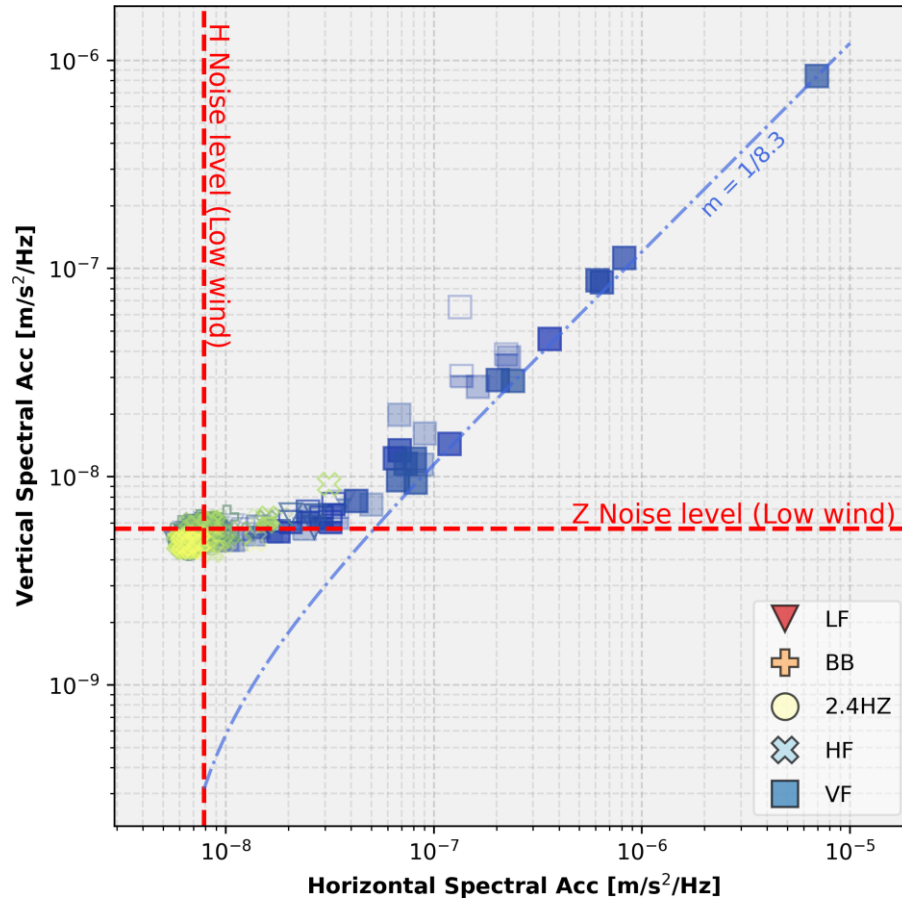
888 Although the hypocentral distance can be estimated by the  $S_g - P_g$  time, determining the back-  
889 azimuth of the VF events has been not possible yet due to the depolarization of the first arrival  
890 (van Driel et al., 2021). Therefore, the epicenter locations of these events have not been obtained  
891 yet and the high-frequency propagation mechanism is still unclear (van Driel et al., 2021; Clinton  
892 et al., 2021). At least, according to the meteorological data, these events seem to be unrelated to  
893 atmospheric or environmental perturbations. A possible mechanism explaining the propagation of  
894 such high frequencies for very long distances (i.e. large  $S_g - P_g$  time) might be similar to the  
895 propagation of T-phases on Earth through the SOFAR channel (Walker et al., 1992; Okal, 2008),  
896 but traveling through a thick waveguide with a really thin scattering layer inside so the energy is  
897 not leaked out. Further investigation of this mechanism is out of the scope of this work.

898

899 An interesting feature of the VF events is the almost negligible vertical ground-motion in the  
900 frequency range between 6 and 9 Hz. This observation can be explained by a strong local site effect  
901 at the InSight landing site due to the subsurface structure underneath. Given an input ground motion,  
902 the horizontal ground-motion is largely enhanced while the vertical one is weakly augmented. In  
903 fact, the horizontal ground-motion is about 7-8 times larger than the vertical one (see Figures 5 and  
904 6) due to the site effect and so the amplitudes may easily surpass the horizontal ambient noise. On  
905 the other hand, the apparent absence of vertical ground-motion can be understood as it having lower  
906 amplitudes than the ambient noise. This is also revealed by the analysis of the average ground  
907 acceleration around 8 Hz for all the events with quality A, B and C from the MQS catalog, as  
908 shown in Figure 11. In this case, the data shows that, given a horizontal ground-motion slightly  
909 above the noise level of the quietest period of the Sol, the expected vertical ground-motion lies  
910 below the median vertical noise level obtained from the same quiet period, when most of the  
911 marsquakes are recorded. Hence, as the vertical noise level is higher than the expected vertical  
912 ground-motion, there is no seismic signal on the vertical component associated with such event.

913

914



915  
 916 **Figure 11.** Vertical and horizontal ground acceleration around 8 Hz for all the marsquakes with  
 917 quality A, B and C reported by the MQS. The red dashed lines represent the median ground  
 918 acceleration recorded during the quietest period of Sols 422 and 423 for both vertical and horizontal  
 919 components. Different markers correspond to different type of marsquakes. The dot-dashed blue  
 920 line is a linear regression between the horizontal and the vertical acceleration, using events with  
 921  $SNR_z > 2$  dB (related to the H/V amplitude at 8 Hz). The filling pattern of the marker indicates  
 922  $SNR > 2$  dB for the horizontal (lower half), vertical (upper half) or both components (full filled).

923  
 924  
 925  
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 929  
 930  
 931  
 932



933 **6 Conclusions**

934 We used the VBB and SP seismic data recorded by SEIS instruments at the InSight landing site to  
935 investigate the horizontal-to-vertical spectral ratios (H/V), at frequencies between 0.4 and 10 Hz.  
936 The H/V was computed from both ambient vibrations (*nHV*) and seismic events data (*eHV*).

937  
938 The H/V curves obtained from VBB and SP data are similar for frequencies below 10 Hz  
939 whereas, above this frequency, the VBB H/V curves (both *nHV* and *eHV*) show higher  
940 amplification. This difference is related to a different amplification of the vertical component at high  
941 frequencies. However, the origin of this difference is still unclear, so we suggest ignoring the  
942 frequencies above 10 Hz for any further analysis of the H/V curve.

943  
944 Different *nHV* curves are observed during different periods of the martian day (Sol) due to the  
945 daily variation of the atmospheric conditions (mainly wind speed and temperature). These *nHV*  
946 curves are unreliable and do not represent the subsurface structure beneath InSight because the  
947 recorded seismic signals either (i) correspond to seismic signal close to the instrumental noise  
948 during the quietest period of the Sol, usually the martian evening when low wind velocities are  
949 recorded (< 3 m/s), or (ii) correspond to non-natural lander mechanical noise, including the strong  
950 excitation of lander resonances, during the noisier periods of the martian Sol, usually the daytime  
951 when high wind speeds are recorded. Unlike most places on Earth, using the ambient vibrations to  
952 reveal the shallow structure through the H/V technique is unfeasible at the InSight landing site on  
953 Mars.

954  
955 The *eHV* curves were obtained from the S-wave coda of all recorded martian seismic events with  
956 energy well above the background noise. The resulting *eHV* curve shares similarities and  
957 differences with the *nHV* curves, particularly during the low-noise period. They both present a  
958 trough at 2.4 Hz and similar shape for frequencies below ~4 Hz but a steep left flank leading to a  
959 peak at around 8 Hz is observed on the *eHV* curve. The inversion of the *fHV* (the *eHV* from VBB  
960 data) under the full diffuse field approach results in three different subsets of models, all of them  
961 suggesting the presence of a shallow high-velocity layer followed by a buried low-velocity layer.  
962 Because the origin of the 2.4 Hz resonance remains unclear, the *fHV* curve was also inverted in  
963 the frequency ranges between 0.4-2 and 3-10 Hz. The resulting models share the presence of a

964 high-velocity layer emplaced over layers with lower velocities and also a buried low-velocity layer  
965 (bLVL). In any case, the features of the H/V curve can be properly explained by the effect of the  
966 full wavefield and not only one type of waves.

967

968 We propose the emplacement of a high velocity layer at shallow depths (SHVL), likely an  
969 effusive Early Amazonian basaltic lava flow, to explain the strong excitation of the 8 Hz resonance  
970 during the VF events. We are unable to resolve the subsurface structure above the SHVL, but the  
971 pre-landing models and inversion of compliance data suggest the presence of a thin regolith  
972 followed by a coarse ejecta layer, which overlay the SHVL and are compatible with the *fHV*. Lower  
973 velocities below the SHVL are required to obtain the observed steep left flank of the 8 Hz peak.  
974 These deeper low velocities may be related to a more physically and chemically weathered Early  
975 Hesperian or Early Amazonian basaltic unit. A buried low-velocity layer, likely corresponding to  
976 a sedimentary layer interrupting these two basaltic units, is needed to explain the *fHV* curve with or  
977 without the 2.4 Hz trough. The 2.4 Hz resonance is generated as long as there is a sharp contrast  
978 between the bLVL and the SHVL.

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992

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1009

1010 **8 Data availability**

1011 The Interior Exploration using Seismic Investigations, Geodesy and Heat Transport (InSight)  
1012 seismic event catalog version 9 ([InSight Marsquake Service, 2022](#)), the waveform data and station  
1013 metadata are available from the Institut du Physique du Globe de Paris (IPGP) Datacenter and  
1014 Incorporated Research Institutions for Seismology Data Management Center (IRIS-DMC, [InSight  
1015 Mars SEIS Data Service, 2019b](#)). Seismic waveforms are also available from the National  
1016 Aeronautics and Space Administration Planetary Data System (NASA PDS), available at  
1017 <https://pds.nasa.gov/> (last accessed April 2022, [InSight Mars SEIS Data Service, 2019a](#)). The  
1018 channel location and codes follow an adapted version of the Standard for the Exchange of  
1019 Earthquake Data (SEED) naming convention. The seismic catalog ([InSight Marsquake Service,  
1020 2022](#)) provides information on all detected events, including the event classification based on  
1021 frequency content, phase picks, back-azimuth estimates, and event quality estimates. The code for  
1022 the computation of the theoretical H/V under the diffuse field approach is available upon request  
1023 from L. Margerin. Data processing and plotting has been done with Obspy ([Beyreuther et al.,](#)

1024 2010), Numpy (Harris et al., 2020) and Matplotlib (Hunter, 2007).

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