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BULLKID: Monolithic array of particle absorbers sensed by kinetic inductance detectors

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ABSTRACT

We introduce BULLKID, a phonon detector consisting of an array of dices acting as particle absorbers sensed by multiplexed Kinetic Inductance Detectors (KIDs). The dices are carved in a thick crystalline wafer and form a monolithic structure. The carvings leave a thin common disk intact in the wafer, acting both as holder for the dices and as substrate for the KID lithography. The prototype presented consists of an array of 64 dices of $5.4 \times 5.4 \times 5 \text{ mm}^3$ carved in a 3"diameter, 5 mm thick silicon wafer, with a common disk of 0.5 mm thick, hosting a 60 nm patterned aluminum layer. The resulting array is highly segmented but avoids the use of dedicated holding structures for each unit. Despite the fact that the uniformity of the KID electrical response across the array needs optimization, the operation of eight units with similar features shows, on average, a baseline energy resolution of $26 \pm 7 \text{ eV}$. This makes it a suitable detector for low-energy processes such as direct interactions of dark matter and coherent elastic neutrino-nucleus scattering.

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The low energy threshold and the high energy resolution that cryogenic phonon detectors can achieve make them a competitive choice in particle-physics experiments searching for weak or rare signals, such as the interaction of dark matter particles with ordinary matter^{1–3} or the neutrino coherent and elastic scattering of atomic nuclei.^{4,5} In these experiments, the detector unit consists of a target crystal acting as particle absorber, where the energy released is converted to phonons. By using semiconducting⁶ or superconducting^{7,8} thermometers as phonon sensors, energy resolutions from few electron volts to tens of electron volts have been achieved recently using crystals of mass between fraction of grams to tens of grams.

Several experiments are aiming at target masses of kilograms, but, at the same time, a high detector segmentation should be maintained for the identification of background processes. With absorber masses of grams or fraction of grams, arrays of hundreds or thousands of detector units will be needed, representing one of the main challenges in the field. Phonon sensors, indeed, require the operation in dilution refrigerators, and this is a complication for the readout and for the assembly of large arrays. Nonetheless, the structure holding the crystals is usually inert, and this can be an issue in terms of background events due to radioactive contaminations.⁹

We propose an array of phonon detectors, dubbed BULLKID, which is, at the same time, highly segmented, fully active, and can be easily fabricated. The concept consists in carving a square grid in one of the two surfaces of a "thick" wafer. The carvings stop near the opposite surface in order to create volumes with the shape of a dice acting as particle absorbers. The opposite surface of the wafer is left intact, and it forms a disk common to all dices and hosts the sensors, each

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coupled to a dice. We choose Kinetic Inductance Detectors (KIDs) as sensors because of their built-in multiplexing capability and relatively easy fabrication.

KIDs¹⁰ are superconducting resonators sensitive to the variation of the Cooper pair density. When energy is absorbed in the superconductor, it can break the pairs and vary their kinetic inductance, giving rise to measurable changes in the frequency of the resonator. KIDs are used as direct radiation absorbers in millimeter wavelength astronomy¹¹ and in single photon low-resolution spectrometers at visible to near-infrared wavelengths.¹²

The detection with KIDs of thermal phonons generated by interactions in an absorber was proposed a decade ago in order to increase the active volume,^{13,14} and today is the object of R&D.^{15,16} So far the best energy resolutions have been obtained by the CALDER project,¹⁷ which created devices consisting of a single KID of $2 \times 2 \text{ mm}^2$ active area deposited on a silicon absorber 380 μ m thick and $2 \times 2 \text{ cm}^2$ wide. The energy resolution is 80 or 26 eV, using as superconductors aluminum¹⁸ or an aluminum–titanium–aluminum tri-layer,¹⁹ respectively. The energy conversion efficiency, which is driven by the fraction of phonons reaching the KID and breaking Cooper pairs, is key to reach good energy resolutions in these devices. The value obtained in CALDER, which we use as reference for this work, is $\eta \sim 10\%$.^{18,20}

In this Letter, we present the first BULLKID prototype that demonstrates the feasibility and the potential of the approach. We describe the production, the operation, and the performance with focus on the phonon signal characterization and on the energy resolution measurement.

The prototype is created starting from a 3" diameter, 5 mm thick, (100) intrinsic and high-resistivity silicon wafer. The substrate is coated with a silicon nitride layer through low chemical vapor deposition. The carvings, performed with a circular saw dicing machine, are 0.6 mm wide and 4.5 mm deep. The common disk is 0.5 mm thick. The grid has 8×8 elements and a pitch of 6 mm, so that 64 dices of $5.4 \times 5.4 \times 5 \text{ mm}^3$ (0.34 g) are obtained [Fig. 1(a)]. In order to obtain a robust structure, the orientation of the grid is chosen to let the carvings run in directions away from the crystal defects created by the carvings, the wafer is etched in an acid solution.²¹ In this step, the silicon nitride layer acts as protective agent against the chemical etching.²² In the end, the silicon nitride layer is removed via hydrofluoric acid wet etching.

The wafer surface opposite to the carvings is instrumented with a multiplexed array of 60 aluminum KIDs, with each KID coupled to a dice. At the border, a corona \sim 1 cm wide is not instrumented to allow handling, thus leaving four dices at the grid corners not sensed [Fig. 1(b)]. The KIDs have an active area of 4 mm² each, the same of CALDER¹⁸ sensors for an easier comparison of the performances. The layout consists of a meandered inductor (L) 20 cm long and 20 μ m wide, made of 106 segments 1.88 mm long interleaved by 8 μ m. The inductor is closed on a interdigitated capacitor (C) with four fingers, whose length is adjusted to tune the resonator frequency $f_0 = 1/2\pi\sqrt{LC}$ between 0.77 and 0.88 GHz [Fig. 1(c)]. Each KID is inductively coupled to a single coplanar waveguide (CPW) running through the entire array. The lithography of the KID is made out of an aluminum film 60 nm thick and is performed in a single step. The wafer is then clamped at the border by Teflon supports in a 3Dprinted copper holder and bonded to SMA connectors for the readout.

The wafer holder is anchored to the coldest point of a dry ${}^{3}\text{He}/{}^{4}\text{He}$ dilution refrigerator with the base temperature $T_0 = 20$ mK.





FIG. 1. (a) Carved silicon wafer of 3" diameter and 5 mm thickness. Carvings are 4.5 mm deep and create 64 dices of $5.4 \times 5.4 \times 5 \text{ mm}^3$ each, leaving intact a 0.5 mm thick common disk. (b) Front side of the wafer with the multiplexed array of 60 aluminum KIDs fabricated on the common disk, with each KID sensing phonons from a single dice. (c) Layout of a KID. A meandered inductor *L* is closed on a capacitor *C* and coupled to a coplanar waveguide (CPW) that runs through the array. The resonant frequency of each KID is set by adjusting individually the length of the capacitor's fingers.

In order to protect the KIDs from thermal radiation and from magnetic fields, the detector is placed inside a shielding pot consisting of three layers of aluminum, copper, and Cryophy[®].²³ For the energy calibration, eight optical fibers individually excited at room temperature by a controlled 400 nm LED lamp face selected dices in the array, shining light on the side opposite to the KIDs. The RF bias of the KIDs is generated at room temperature with an Ettus X310 board²⁴ and fed in the cryostat where it is attenuated by 55 dB before reaching the array. The output of the array is fed into a HEMT low-noise amplifier placed at the 4 K stage of the cryostat and then routed outside, back in the same board for the downconversion of the RF waves. For the data processing, an opensource firmware for the board is used,²⁵ customized in order to trigger and acquire impulsive signals.

The RF transmission past the device as a function of frequency, $S_{21}(f)$, is shown in Fig. 2(a). 58 out of 60 (97%) resonators are identified. In order to extract the electrical features of each resonator, the data are corrected offline for impedance mismatches and line losses²⁶ and then fitted with the model,²⁷

$$S_{21}(f) = 1 - \frac{Q}{Q_c} \frac{1}{1 + j2Q \frac{f - f_0}{f_0}},$$
(1)

where $Q^{-1} = Q_c^{-1} + Q_i^{-1}$ is the total quality factor and Q_c and Q_i are the coupling and internal quality factors, respectively [Fig. 2(b)]. By fitting all the resonators, we find f_0 in good agreement with the design and $Q_i \gg Q_c$, revealing the good quality of the film. The distribution of $Q \simeq Q_c$ is, however, quite widespread around the design value of $1.5 \cdot 10^5$, with some resonator Q below 10^4 and some exceeding $5 \cdot 10^5$ [Fig. 2(c)]. In principle, Q_c is determined by design via the distance



FIG. 2. (a) Transmission S_{21} as a function of the readout frequency spanning across the array. Each dip corresponds to a KID, and 58/60 of them are identified. The broader dip at 0.81 GHz is attributed to a resonance mode of the feedline. (b) Fit for Eq. (1) on KID-40 (lines), using transmission data corrected for line losses and impedance mismatches (dots). (c) Total quality factor *Q* of all KIDs evaluated from the resonance fitting. The KIDs in the red-dashed contour are used for the analysis of the phonon signal and of the energy resolution.

between resonator and feed-line, which is precisely fixed by the lithography. However, the propagation in the CPW of the slot mode alters the coupling at different positions along the line. Ways to correct for this issue consist in performing several bondings along the feedline between the two ground planes, in order to fix their potential and to prevent the occurrence of the slot mode.

When an amount of energy *E* is released in a dice, changes of the Cooper pair density are detected by monitoring the time variation of S_{21} with the RF bias set at $f = f_0$. Changes in both the magnitude and phase of S_{21} can be used, even though the latter usually feature a better signal to noise ratio.²⁷ Restricting the analysis to the phase readout, its variation with energy can be expressed in terms of the device parameters as

$$\frac{d\phi}{dE} = \eta \cdot \frac{\alpha S_2(f_0, T_0)Q}{N_0 \Delta_0^2 V},\tag{2}$$

where $N_0 = 1.72 \cdot 10^{10} \text{ eV}^{-1} \mu \text{m}^{-3}$ is the single spin density of states in aluminum, $V = 2.4 \cdot 10^5 \mu \text{m}^3$ is the inductor volume, $S_2(f_0, T_0)$ = 4.9 is a dimensionless factor given by the Mattis–Bardeen theory related to the imaginary part of the conductivity,²⁷ α is the fraction of kinetic inductance with respect to the total inductance, and Δ_0 is the superconducting gap of the film. The values of α and Δ_0 are estimated from the measured shift of the resonant frequency of each KID with temperature.²⁸ By performing a scan from 20 to 350 mK, we find values averaged over all KIDs of $\alpha = (5.0 \pm 0.1)\%$ and $\Delta_0 = 189 \pm 2 \mu \text{eV}$, where the errors are the standard deviations of the distributions. The expected amplitude of the phase signal for $Q = 1.5 \cdot 10^5$ is then $d\phi/dE \simeq 26 \cdot \frac{\eta}{[0.1]}$ mrad/keV. This value is a factor 4 larger than in CALDER,¹⁸ a factor 2 from the value of S_2 at $f_0 \sim 0.8$ GHz in place of 2.7 GHz, and another factor 2 from the increase in α , achieved with a modified design of the inductor, which is made of narrower segments. The actual value of η is derived from the study of the response to optical pulses, as detailed in the following.

We choose to face the eight optical fibers available to the KIDs marked in Fig. 2(c), forming a compact cluster with Q value rather homogeneous and close to the design. We restrict the data analysis only to them. Figure 3 shows a typical phase pulse following an energy release of ~1 keV in the dice of KID-40. The rise time, computed as the time span between the 10% and the 90% of the rising edge, amounts to 170 μ s, similar to the value expected from the resonator ring time log (9) $\cdot Q/\pi f_0 = 140 \ \mu$ s. The decay time, computed as the difference between the 90% and the 30% of the trailing edge, amounts to 3.9 ms. By monitoring the decay time at increasing cryostat temperatures, we observe a significant decrease, down to 0.2 ms at 300 mK, indicating that it is generated by the recombination of quasiparticles after the pair breaking.²⁹

For the estimation of $d\phi/dE$, we exploit the statistics of the number of photons *N* absorbed by the dices, exploiting the technique already proved in Refs. 19 and 23. We shine hundreds of fast ($\sim \mu s$) photon bursts at increasing LED powers and acquire the pulses triggered from the KID data stream, which are processed offline with a matched filter in order to maximize the energy resolution.³⁰ For each set of bursts, the measured pulse amplitude is expected to be distributed as a Gaussian with mean $\mu = d\phi/dE \cdot \epsilon N$, where $\epsilon = 3.1$ eV is the (fixed) energy of a 400 nm photon, and variance due to Poisson fluctuations equal to $d\phi/dE \cdot \epsilon \mu$. Considering also the resolution at zero energy σ_0 due to the KID noise, the total variance can be written as

$$\sigma^2(\mu) = \sigma_0^2 + \frac{d\phi}{dE}\epsilon\mu.$$
(3)

The above equation is used to fit the data for $d\phi/dE$ in order to perform the energy calibration.

We perform the photon calibration at different powers of the KID bias. Indeed, when the power is increased, the signal to noise ratio improves until the KID enters in a non-linear regime.³¹ In this regime, however, the detector response is complicated by the non-linearity, and $d\phi/dE$ cannot be related anymore to η through Eq. (2). Therefore, for best energy resolutions, we set the power at the



FIG. 3. Raw phase pulse of KID-40 following an energy release of around 1 keV in the corresponding dice. The rise and decay times are 170 μs and 3.9 ms, respectively.

beginning of the non-linear regime, which corresponds to $P_H = -74$ to -68 dBm depending on the KID, while for the estimation of η , we lower the power to the minimum of the electronics, $P_L = -86$ dBm, which is well below the non-linear region.

Figure 4(a) shows the amplitude of the phase pulses of KID-40 with the bias set at P_H for different light intensities, along with Gaussian fits to extract σ and μ of the distributions. The point at zero amplitude is obtained from traces not containing pulses. From the fit to Eq. (3) of the σ^2 vs μ scattering, we estimate a responsivity $d\phi/dE|_H = 54 \pm 2 \text{ mrad/keV}$ [Fig. 4(b)]. Figure 4(c) shows the distribution of the calibrated noise, from which we can estimate a resolution at zero energy of $\sigma_0 = 24.1 \pm 0.4 \text{ eV}$. By performing the same operation on the other KIDs, we obtain similar results, with average values over the eight selected KIDs of $d\phi/dE|_H = 43 \pm 9 \text{ mrad/keV}$ and $\sigma_0 = 26 \pm 7 \text{ eV}$. It has to be noticed that decoupling the detector from vibrations is sometimes needed in order to reach the best noise conditions of phonon sensors. However, our results are obtained without a decoupling system and do not change when switching the pulse tube cryocooler on and off.



FIG. 4. (a) Measured amplitude of the phase pulses at increasing light burst intensity on the dice of KID-40. The lines show the best fits for Gaussian distributions; (b) variance σ^2 as a function of mean value μ of the Gaussians. The line is the best fit for Eq. (3); (c) distribution of the calibrated noise fluctuations fitted with a Gaussian (line).

When switching the power to P_L , we measure on average $d\phi/dE|_L = 57 \pm 7 \text{ mrad/keV}$. For cross-check, we replaced the LED lamp with one providing photons of 255 nm instead of 400 nm, and we obtained consistent results. By inverting Eq. (2), we derive $\eta = (24 \pm 4)\%$, a factor 2 larger value than in the devices of CALDER.

The high value of the energy conversion efficiency was predicted by the phonon simulations²⁰ we performed to design the device. Indeed, the volume of a BULLKID dice and of a CALDER substrate are similar, 146 vs 152 mm³; however, in a cubic shape, the average distance of a point in the volume from the sensor on a face is significantly smaller, thus enhancing the phonon capture. Simulations indicate also that the efficiency in a dice is limited by the thickness of the common disk, which acts as a channel with adjacent dices where phonons can leak. We evaluate this leak by shining light on a dice and by measuring the energy detected in nearby dices. With respect to the energy measured in the dice of origin, we measure on average $(14 \pm 3)\%$ of energy in each of the first neighbors lying on the same line (top-bottom and left-right), and (5 ± 1) % of energy in first neighbors in the diagonal direction. These values agree with the simulations, which predict also that the efficiency could be increased and the leak lowered by reducing the 0.5 mm thickness of the common disk.

In conclusion, our results demonstrate the feasibility of a phonon detector consisting of a monolithic and segmented array of 60 dices of 0.34 g each sensed by multiplexed kinetic inductance detectors. In particular, the phonon energy conversion efficiency in the KID outweighs the values achieved in other detectors and pushes the energy resolution down to a few tens of eV. The uniformity of the electrical response needs improvement, which will be achieved by improving the grounding of the feedline of the array. Further significant improvements of the energy resolution are feasible, either by replacing the KIDs superconductor with aluminum-titanium multilayers, which already proved a factor 3 improvement with respect to aluminum, or by improving the phonon focusing in the KID with deeper carvings. Finally, once the structure of a single array is defined, tens of identical arrays could be readily produced and piled-up, giving the opportunity to create a kg-scale, low-threshold, and low-background Dark Matter or neutrino scattering experiment.

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AUTHOR DECLARATIONS Conflict of Interest

The authors have no conflicts to disclose.

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Author Contributions

Angelo Cruciani: Funding acquisition (equal); Investigation (equal); Methodology (equal); Project administration (equal); Resources (equal); Supervision (equal); Writing - review & editing (equal). Vincenzo Guidi: Resources (lead). Johannes Goupy: Investigation (equal). Valerio Pettinacci: Methodology (equal). Giorgio Pettinari: Investigation (equal); Resources (equal). Marco Romagnoni: Investigation (equal); Writing - review & editing (equal). Melissa Tamisari: Investigation (supporting). Andrea Mazzolari: Funding acquisition (equal); Investigation (equal); Methodology (equal); Project administration (equal); Resources (lead); Writing - review & editing (equal). Alessandro Monfardini: Investigation (equal); Methodology (equal); Project administration (equal); Resources (lead). Marco Vignati: Data curation (equal); Funding acquisition (lead); Investigation (equal); Methodology (lead); Project administration (equal); Resources (lead); Writing - original draft (lead); Writing review & editing (lead). Laura Bandiera: Investigation (equal); Resources (equal). Martino Calvo: Investigation (equal); Resources (equal). Nicola Casali: Investigation (supporting). Ivan Colantoni: Investigation (supporting). Giorgio Del Castello: Software (lead); Writing - review & editing (equal). Matteo del Gallo Roccagiovine: Investigation (supporting); Software (supporting). Daniele Delicato: Investigation (equal); Methodology (equal); Software (equal); Validation (equal). Marco Giammei: Data curation (lead); Formal analysis (equal); Software (equal); Writing - original draft (equal).

DATA AVAILABILITY

The data that support the findings of this study are available from the corresponding author upon reasonable request.

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