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**Facile coating of Co<sub>3</sub>O<sub>4</sub> on open-cell metallic foam for N<sub>2</sub>O catalytic decomposition** Phuoc Hoang Ho<sup>a,b,§,†,\*</sup>, Katarzyna Świrk<sup>c,§</sup>, Giancosimo Sanghez de Luna<sup>a,§</sup>, Magdalena Jabłońska<sup>b,d,e</sup>, Francesca Ospitali<sup>a</sup>, Francesco Di Renzo<sup>c</sup>, Gérard Delahay<sup>c,\*\*\*</sup>, Giuseppe Fornasari<sup>a</sup>, Angelo Vaccari<sup>a</sup>, Regina Palkovits<sup>b,d</sup>, Patricia Benito<sup>a\*\*\*</sup> <sup>a</sup> Dipartimento di Chimica Industriale “Toso Montanari”, Università di Bologna, Viale Risorgimento 4, 40136, Bologna, Italy <sup>b</sup> Institut für Technische und Makromolekulare Chemie, RWTH Aachen University, Worringerweg 2, 52074 Aachen, Germany <sup>c</sup> ICGM, Université de Montpellier, CNRS, ENSCM, Pôle Recherche Balard, 1919 Route de Mende, 34090 Montpellier, France <sup>d</sup> Center for Automotive Catalytic Systems Aachen, RWTH Aachen University, Schinkelstr. 8, 52062 Aachen, Germany <sup>e</sup> Institute of Chemical Technology, Universität Leipzig, Linnéstr. 3, 04103 Leipzig, Germany <sup>§</sup> Equal contribution

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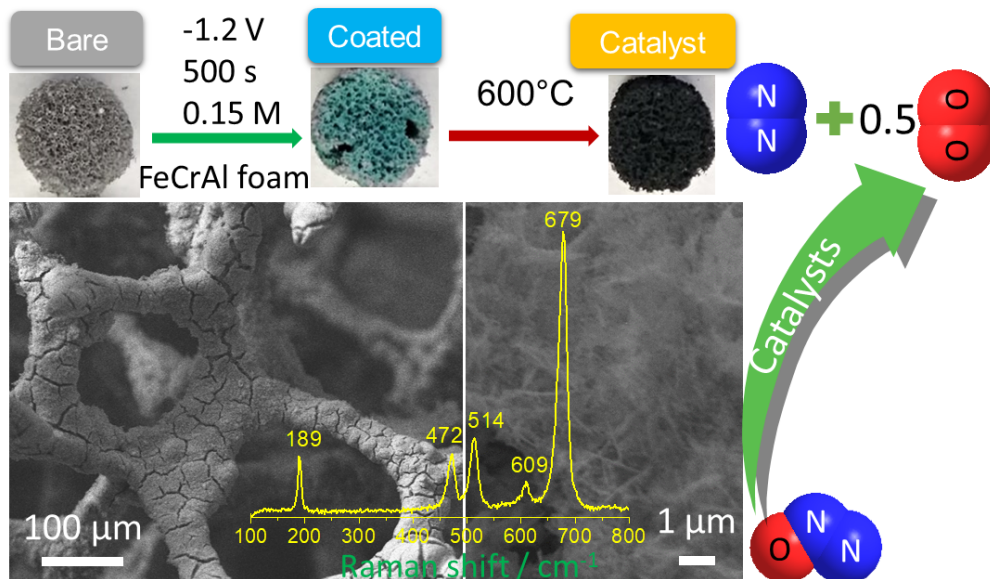
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## Abstract

Co<sub>3</sub>O<sub>4</sub> coated on open-cell metallic foams (, merging catalytic activity of Co<sub>3</sub>O<sub>4</sub> and advantages derived from the geometry of the support), are promising for environmental applications such as the decomposition of N<sub>2</sub>O (deN<sub>2</sub>O). This study demonstrates how ~~it is possible to~~ easily and reproducibly prepare a well-adhered layer of Co<sub>3</sub>O<sub>4</sub> by the electrosynthesis of Co(OH)<sub>2</sub> followed by thermal treatment (600 °C). with Aa similar specific surface area as the materials prepared with the precipitation method (~ 22 m<sup>2</sup> g<sup>-1</sup> coating), and controlled thickness on FeCrAlloy open-cell foams of different porosity and dimension are achieved. by the electrosynthesis of Co(OH)<sub>2</sub> followed by thermal treatment (600 °C). The obtained structured catalysts show stable performance activity after three cycles of catalytic decomposition of N<sub>2</sub>O between 250 and 550 °C. , with a The materials reached similar T<sub>50</sub> of approximately 460 °C, which is comparable to the combustion or precipitated catalysts but provides a lower pressure drop. Under the operating conditions with a sequential test, the presence of NO and/or O<sub>2</sub> inhibits partially the catalytic performance activity of the structured catalysts while the presence of H<sub>2</sub>O showed a slight enhancement in the N<sub>2</sub>O conversion at a temperature above 450 °C.

## Graphical abstract



## Highlights

- $\text{Co}(\text{OH})_2$  layer is easily coated on FeCrAlloy open-cell foam by electrodeposition.
- Calcination at 600 °C results in a stable coating of  $\text{Co}_3\text{O}_4$  with a high specific surface area.
- Catalyst loading can be tailored by synthesis time and electrolytic concentration.
- $T_{50}$  for  $\text{deN}_2\text{O}$  is in a range of 477 – 543 °C with in the presence of  $\text{O}_2$ ,  $\text{NO}$ , and  $\text{H}_2\text{O}$ .
- Promising use in other energy and environmental applications.

**Keywords:** Electrodeposition,  $\text{Co}(\text{OH})_2$ ,  $\text{Co}_3\text{O}_4$ , open-cell metallic foam,  $\text{N}_2\text{O}$  decomposition.

## 1. Introduction



Open-cell foams are a special member of the 3D structured support family with high porosity (void fraction 90-95%) and geometrical surface area (e.g.,  $7800 \text{ m}^2 \text{ m}^{-3}$  for  $450 \text{ }\mu\text{m}$  cell-size with 85% porosity); hence the structured catalysts based on open-cell foams offer many advantages in terms of mass and heat transfer together with a low-pressure drop [1]. Such advantages are promising for environmental applications in which the processes operate at high GHSV and are exothermic. Open-cell foams are now commercialized with various compositions, from ceramic- to metallic- or alloy-based materials. Metallic or alloy foams with high thermal or electrical conductivity offer additional advantages in mechanical strength and heat transfer for heterogeneous catalysis [2, 3]. A key point for those applications is the development of a technique to coat the structured supports with a stable layer of catalytic materials. Conventional wash coating or dip coatings are challenging because of significant differences in properties between the metallic foam and ceramic-coating layer as well as the pore blockage. The latter is important for foams with small pores, although spin coating has been reported to solve this issue [4]. Spin coating follows almost the same procedure as wash-coating/dip-coating for the preparation of the catalyst slurry, except the last step uses spinning to provide better distribution and to remove excess coating slurry [4]. Although this technique has been found to significantly improve the properties and hence the catalytic activity of the structured catalysts, it may still face the problem of modification of catalytic materials during the slurry preparation [5-7].

Besides spin coating, electrodeposition has been proposed by some of us to coat hydrotalcite- or ceria-derived materials for syngas production and environmental applications [8, 9]. Herein we extend the method to coat a cobalt-based material on small pore FeCrAlloy foams for the preparation of open-cell foam structured catalysts carrying a  $\text{Co}_3\text{O}_4$  material. Structured supports carrying on cobalt-based materials have found application in both electrocatalysis [10-13] and heterogeneous catalysis [14-17]. A few studies have reported the preparation of  $\text{Co}_3\text{O}_4$  or  $\text{Co}(\text{OH})_2$  on Ni foams but only as a rather thin film for water oxidation or supercapacitors [10, 13]. Such thin coating, few microns, lacks the mass loading required for heterogeneous catalysis purposes. In addition,  $\text{Co}_3\text{O}_4$ -coated ceramic honeycomb monoliths and foams have been used for  $\text{N}_2\text{O}$  abatement [14, 17-19], partial oxidation of ethanol [15], combustion of volatile organic compounds [16], methane oxidation [20], and Fischer–Tropsch synthesis [21-24]. Our previous study reported that structured catalysts containing an Rh-based coating were promising for the catalytic decomposition of  $\text{N}_2\text{O}$  [25]. However, moving from noble metals toward transition metals, the development of catalysts has gained more interest due to the higher cost of the former than the latter. To the best of our knowledge, the use of  $\text{Co}_3\text{O}_4$  coated on open-cell metallic foams is rare, especially for the important process of  $\text{N}_2\text{O}$  decomposition. Nitrous oxide is a strong greenhouse gas, from plants producing nitric acid or adipic acid, the emissions of which must be reduced to meet the  $2 \text{ }^\circ\text{C}$  limit of global temperature increase [26].

This study introduces the electrodeposition of a relatively thick layer of  $\text{Co}(\text{OH})_2$  up to  $15\text{-}18 \text{ }\mu\text{m}$  on FeCrAlloy open-cell foam of high pore density (80 PPI), which is then transformed into  $\text{Co}_3\text{O}_4$  by calcination at  $600 \text{ }^\circ\text{C}$ . The coating layer and the final structured catalysts are characterized to study morphology, specific surface area, and redox properties in comparison

with precipitated  $\text{Co}_3\text{O}_4$ . A selected application of the structured catalyst for  $\text{N}_2\text{O}$  decomposition has been tested.

## 2. Experimental

### 2.1 Catalyst preparation

Cylindrical pieces of FeCrAlloy open-cell foam (diameter 8 mm x height 7 mm, supplied by Poivair, denoted as foam type I) were cut from a commercial panel (nominal 80 pores per inch (PPI), panel thickness 7 mm). Cobalt hydroxides were in situ coated on the foam in short times by one-step electrodeposition using a double compartment electrochemical cell, flushing the electrolyte with a flow rate of  $2 \text{ mL min}^{-1}$ . Detailed information on the instrument can be found elsewhere [27]. The samples were prepared at a cathodic potential of  $-1.2 \text{ V}$  vs SCE using different concentrations of  $\text{Co}(\text{NO}_3)_2$  aqueous solutions ( $0.06 - 0.15 \text{ M}$ ) and synthesis times ( $500 - 1500 \text{ s}$ ). As a general trend in electrosynthesis, either synthesis time or electrolytic concentration can influence the loading and crystallinity of the coated materials [28]. Herein, to demonstrate how the coating loading can be controlled by the electrosynthesis, three selected samples prepared at  $0.06 \text{ M} - 1500 \text{ s}$ ,  $0.10 \text{ M} - 1000 \text{ s}$ , and  $0.15 \text{ M} - 500 \text{ s}$  were shown. The electrodeposited samples were washed thoroughly with distilled water before drying at  $40 \text{ }^\circ\text{C}$  for 24 h. The samples were eventually calcined at  $600 \text{ }^\circ\text{C}$  for 6 h in static air with a ramp rate of  $10 \text{ }^\circ\text{C min}^{-1}$  and denoted as Co-0.15, Co-0.10, and Co-0.06, wherein the number referred to the concentration of the electrolytes. To check if the method can work on different types of metallic foams, some samples were also synthesized using another FeCrAlloy support (1.6 mm thickness x 9 mm diameter, nominal cell size  $450 \text{ }\mu\text{m}$  (approximately 120 PPI), supplied by Alantum, denoted as foam type II) at  $-1.2 \text{ V}$ ,  $0.15 \text{ M}$ , and  $250 \text{ s}$ .

For comparison purposes, the  $\text{Co}_3\text{O}_4$  powder catalyst was also prepared by precipitation. A  $1.0 \text{ M}$  nitrate solution of  $\text{Co}(\text{NO}_3)_2$  was dropwise introduced into a beaker containing  $100 \text{ mL}$  of  $1.0 \text{ M}$   $\text{Na}_2\text{CO}_3$  solution. The pH was adjusted at  $10 \pm 0.1$  by  $1.0 \text{ M}$   $\text{NaOH}$  solution. The resulting slurry was aged for  $0.5 \text{ h}$  at  $60 \text{ }^\circ\text{C}$ , filtered, and washed thoroughly with warm distilled water ( $60 \text{ }^\circ\text{C}$ ). The final products were dried at room temperature for 24 h and subsequently calcined at  $600 \text{ }^\circ\text{C}$  for 6 h. The powder catalyst was then pelletized and sieved to collect a fraction of particle size from  $0.25$  to  $0.50 \text{ mm}$  for the catalytic test.

### 2.2 Characterization techniques

X-ray diffraction (XRD) measurement was performed using a PANalytical X'Pert diffractometer equipped with a copper anode ( $\lambda = 1.5418 \text{ \AA}$ ) and a fast X'Celerator detector. The pattern was recorded from  $10$  to  $80^\circ$  of  $2\theta$  with a step size of  $0.067^\circ$  and a counting time of  $60 \text{ s}$ .

Scanning electron microscopy (SEM) coupled to energy dispersive spectrometry (EDS) was performed by using an EP EVO 50 Series Instrument (EVO ZEISS) equipped with an INCA X-act Penta FET® Precision EDS microanalysis and INCA Microanalysis Suite Software (Oxford

Instruments Analytical) to provide images of the spatial variation of elements in a sample. The accelerating voltage was 20 kV and the spectra were collected for 60 s.

The specific surface area of the catalysts was determined by N<sub>2</sub> adsorption/desorption at -196 °C. The measurements were carried out using a Micromeritics ASAP 2020 instrument. Two coated foams containing approximately 30 mg of the coating were used for each measurement. Samples were degassed under vacuum < 30 µm Hg, heated up to 150 °C, and maintained for 30 min before performing the measurement. The specific surface area (S<sub>BET</sub>) was calculated using the Brunauer-Emmett-Teller (BET) multiple-point method in the relative pressure range p/p<sup>0</sup> from 0.05 to 0.3.

Micro-Raman measurements were performed in a Renishaw Raman Invia configured with a Leica DMLM microscope. The available sources are an Ar<sup>+</sup> laser (514.5 nm, P<sub>max</sub> = 30 mW) and a diode-laser (780.0 nm, P<sub>max</sub> = 300 mW). The system was equipped with edge filters to cut Rayleigh scattering, monochromators (1800 lines/mm for Ar<sup>+</sup> laser, and 1200 lines/mm for diode laser) and a Charge-Coupled Device (CCD) thermoelectrically cooled (203 K) detector. Measurements were performed with the Ar<sup>+</sup> Laser (514.5 nm) at power level P<sub>out</sub> = 3 mW (10% power). Each spectrum was recorded by four accumulations (30 s for each).

Hydrogen temperature-programmed reduction (H<sub>2</sub>-TPR) was performed in an AutoChem II (Chemisorption analyzer, Micromeritics). The catalyst (two coated foams) was firstly outgassed at 150 °C under 30 mL min<sup>-1</sup> of He for 30 min. After cooling to 30 °C under He gas, the carrier gas was switched to 5% H<sub>2</sub>/Ar (v/v) at 30 mL min<sup>-1</sup>. When the baseline was stable, the temperature was increased to 900 °C with a ramp of 10 °C min<sup>-1</sup>. The amount of H<sub>2</sub> consumed was measured using a thermal conductivity detector (TCD). Water vapor was removed from effluent gas by the means of a cold trap placed in an ice-water bath.

### 2.3 Catalytic test

The catalytic tests for the decomposition of N<sub>2</sub>O (deN<sub>2</sub>O) were performed in a quartz reactor (ID 8 mm) containing two foams of catalyst (diameter 8 mm and height 7 mm). Prior to each experiment, the structured catalysts were outgassed at 500 °C for 0.5 h under 80 mL min<sup>-1</sup> of N<sub>2</sub> and then cooled down to 50 °C. After that, 80 mL min<sup>-1</sup> of a gas mixture containing 1000 ppm N<sub>2</sub>O in N<sub>2</sub> as balance was switched on to pass through the catalyst bed with GHSV = 6800 h<sup>-1</sup> (or WHSV = 160,000 L kg<sup>-1</sup> h<sup>-1</sup> calculated based on 30 mg coating materials). The reaction was carried out at atmospheric pressure and in a range of temperatures from 50 °C to 500 °C (in absence of inhibitor) or 600 °C (in presence of inhibitors) with an interval of 50 °C. At each temperature, the reaction was stabilized for 0.5 h before being sent for quantification of N<sub>2</sub>O concentration. The gas composition in the outlet stream was analyzed by infrared spectroscopy using an Agilent Cary 660 equipped with a Pike 2 m heated gas cell.

For type II foam activity testing, five foam discs containing a total of about 24 mg of the coating were loaded into a quartz reactor (inner diameter 9 mm). The catalyst was pretreated at 550 °C for 1 h under a flow of He (30 mL min<sup>-1</sup>) and then cooled to 250 °C. Different gas compositions

(balance with He) were used for the tests including: I)  $[\text{N}_2\text{O}] = 2500 \text{ ppm}$ , ii)  $[\text{N}_2\text{O}] = 2500 \text{ ppm} + [\text{O}_2] = 2\%$ ; iii)  $[\text{N}_2\text{O}] = 2500 \text{ ppm} + [\text{NO}] = 500 \text{ ppm}$ ; iv)  $[\text{N}_2\text{O}] = 2500 \text{ ppm} + [\text{NO}] = 500 \text{ ppm} + [\text{O}_2] = 2\%$ , and v)  $[\text{N}_2\text{O}] = 2500 \text{ ppm} + [\text{H}_2\text{O}] = 3.6\% + [\text{O}_2] = 2\%$ . Water was added before being mixed with the  $\text{N}_2\text{O}/\text{He}$  gas flow. The by passing the  $\text{O}_2/\text{He}$  gas flow passed through a temperature-controlled saturator, containing water liquid, before being mixed with the  $\text{N}_2\text{O}/\text{He}$  gas flow. A series of tests were performed in sequential order as shown in Figure S1. The gas compositions were analyzed by a quadruple mass spectrometer (Pfeiffer Omnistar) equipped with Channeltron and Faraday detectors (0–200 amu).

The conversion of  $\text{N}_2\text{O}$  ( $X(\text{N}_2\text{O})$ ) was determined according to  $X(\text{N}_2\text{O}) = ([c(\text{N}_2\text{O})_{\text{in}} - c(\text{N}_2\text{O})_{\text{out}}]/c(\text{N}_2\text{O})_{\text{in}}) \times 100\%$ , where:  $c(\text{N}_2\text{O})_{\text{in}}$  and  $c(\text{N}_2\text{O})_{\text{out}}$  – concentration of  $\text{N}_2\text{O}$  in the inlet gas, and concentration of  $\text{N}_2\text{O}$  in the outlet gas.

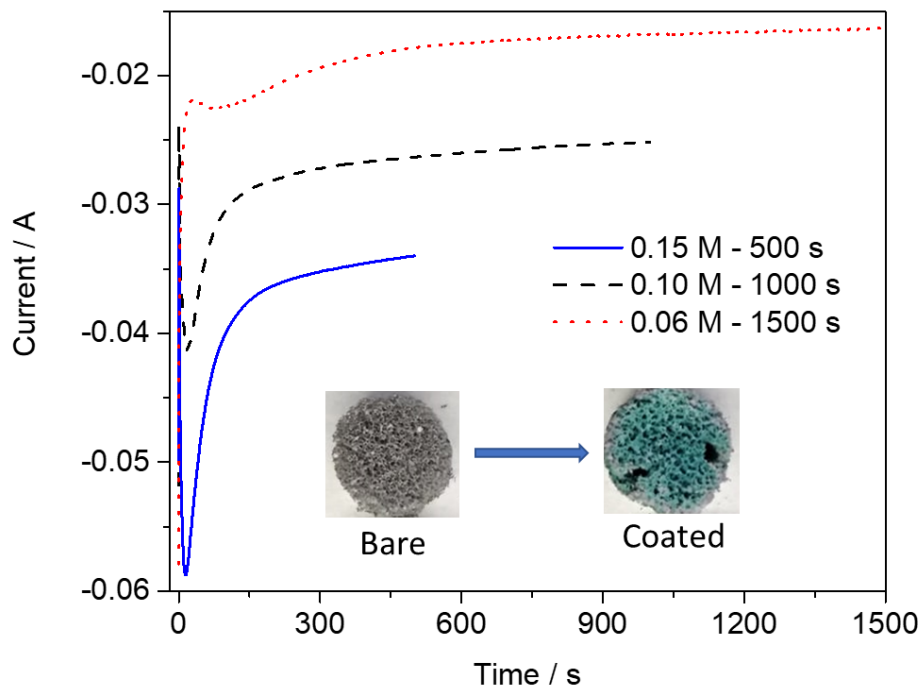
The reaction rate (in term of a number of  $\text{N}_2\text{O}$  molecules converted on a defined surface area (1  $\text{m}^2$ ) of the catalyst during a given time (1 s)) was calculated by the following equation:  $r$  ( $\text{mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ ) =  $n \cdot (X/100)/(m \cdot S_{\text{BET}})$ , where  $n$  – molar flow rate of  $\text{N}_2\text{O}$  [ $\text{mol} \cdot \text{s}^{-1}$ ],  $m$  – catalyst weight [g],  $S_{\text{BET}}$  – specific surface area [ $\text{m}^2 \cdot \text{g}^{-1}$ ] and  $X$  –  $\text{N}_2\text{O}$  conversion [%] [29].

The apparent activation energy was calculated from the slope of linear regression derived from the Arrhenius equation  $k = A \cdot e^{-(E_a/RT)}$ , where  $k$  was calculated from the kinetic model for the flow reactor with an assumption of the first-order reaction  $k\tau = X_{\text{N}_2\text{O}}/(100 - X_{\text{N}_2\text{O}})$  [30]. In which  $k$  ( $\text{s}^{-1}$ ) is the kinetic rate constant,  $A$  is the pre-exponential factor and it has the unit of  $\text{s}^{-1}$  for the first-order reaction,  $E_a$  ( $\text{J mol}^{-1}$ ) is the apparent activation energy,  $R$  ( $\text{J} \cdot \text{mol}^{-1} \text{K}^{-1}$ ) is the ideal gas law constant,  $T$  (K) is temperature,  $\tau$  (s) is space-time (approximate 0.38 s) which is determined from the ratio between the volume of the catalytic bed (about  $0.5 \text{ cm}^3$ ) and total flow of  $1.33 \text{ cm}^3 \text{ s}^{-1}$ .

### 3. Results and Discussion

#### 3.1 Catalyst physico-chemical characterizations

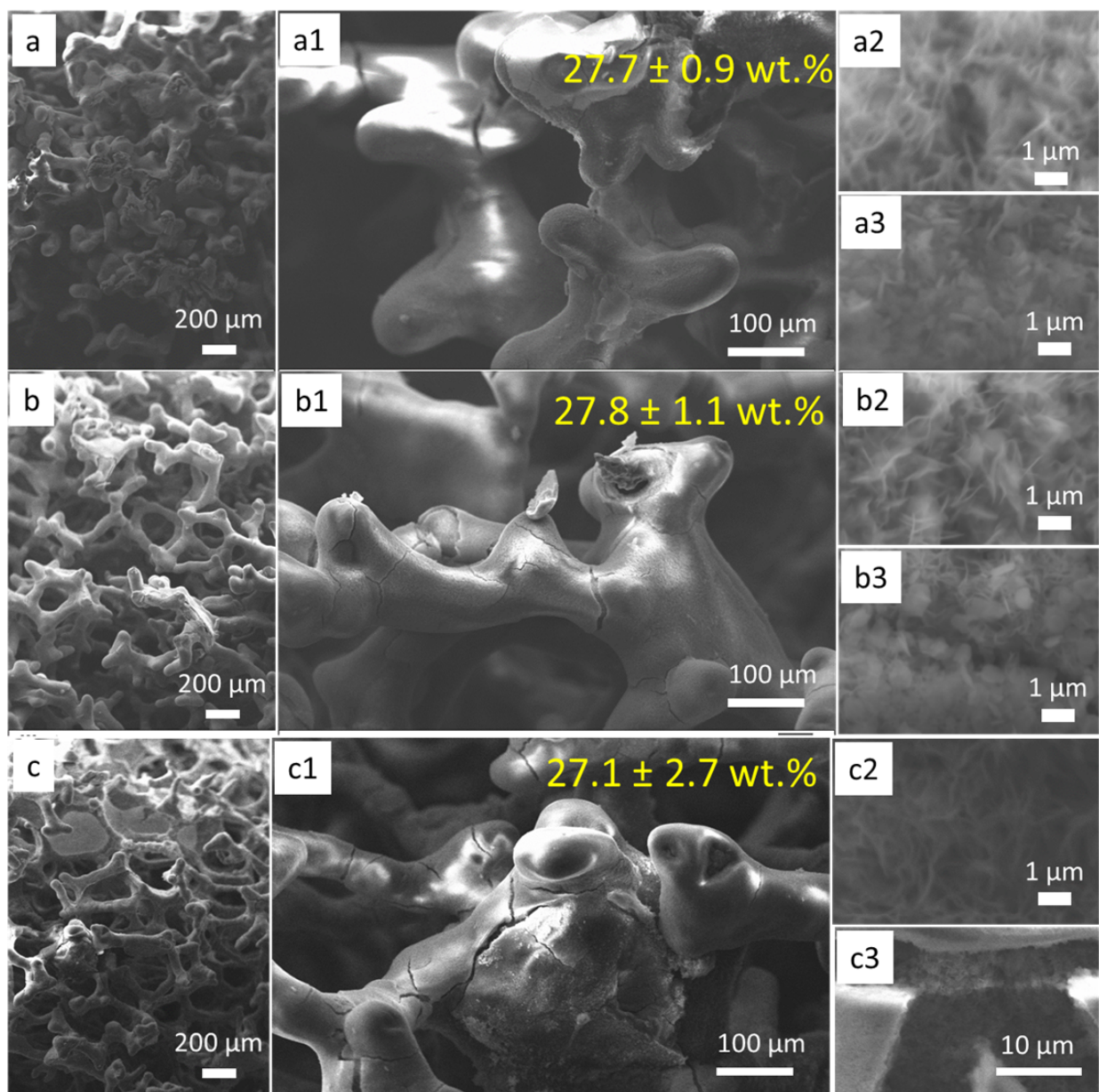
The electrodeposition of hydroxides on the surface of a metallic foam is based on the generation of  $\text{OH}^-$ , mainly from the reduction of nitrate and/or water at the interface of cathode-electrolyte, by applying a cathodic potential and then consumption of those  $\text{OH}^-$  by chemical precipitation with available cations at the cathode vicinity [31]. Such reduction processes consume electrons and the consumption rate is represented by the current transient curves as shown in Figure 1.



**Figure 1.** Transient current curves recorded during the electrodeposition of  $\text{Co(OH)}_2$  on foam type I at  $-1.2 \text{ V vs SCE}$ . The insets show optical images of bare foam and the coated foam prepared in  $0.15 \text{ M Co(NO}_3)_2$  electrolytes for  $500 \text{ s}$ .

Increasing the concentration of electrolyte from  $0.06$  to  $0.15 \text{ M}$  led to higher nitrate reduction and hence resulted in an increase of current from  $18$  to  $34 \text{ mA}$  (Figure 1). This trend is in agreement with our previous work on the electrodeposition of Mg-Al hydrotalcite compounds [28]. An important question is whether such nitrate (and also water) reduction currents generate a pH high enough for the precipitation of  $\text{Co(OH)}_2$ . This pH value is around  $7.3 - 7.5$  for concentrations  $0.15 - 0.06 \text{ M}$  of  $\text{Co(NO}_3)_2$ , respectively (calculated from equilibrium solubility constant  $K_s = 6.93 \cdot 10^{-15}$  [32]). Although the electrosynthesis on the foam could favor heterogeneous precipitation instead of homogeneous one inducing the deposition of uniform and small particles due to the fast and uniform increase of pH near the foam surface [33]. It should be noted that pH measured near the cathode is a balance of generation and consumption of  $\text{OH}^-$  and, after an initial pH increase from the acidic value of the electrolyte, it stabilizes to equilibrium values for precipitation of the hydroxides. For instance, pH values around  $8.5 - 9.0$  were measured during the electrodeposition of Mg/Al hydrotalcite-like compounds at  $-1.2 \text{ V vs SCE}$  in the bath containing electrolytes with a concentration of  $0.03 - 0.1 \text{ M}$ . Thus, it is expected that the synthesis conditions in this work ( $-1.2 \text{ V vs SCE}$ , electrolytic concentration  $0.06 - 0.15 \text{ M}$ ) generated a pH high enough for precipitation of  $\text{Co(OH)}_2$ . Indeed a blue coating, a typical color for  $\text{Co(OH)}_2$ , was observed on the electrodeposited samples after drying at  $40 \text{ }^\circ\text{C}$  (Inset of

Figure 1). In addition, it should be emphasized that the applied potential and synthesis time in this study were optimized on the basis of some of our previous works on the electrodeposition of hydrotalcite-like compounds and  $\text{CeO}_2$  [8, 9, 27, 34]. Applied potential at  $-1.2 \text{ V}$  vs SCE could reduce the contribution of hydrogen evolution reaction, which decreased the stability of the coating. While the synthesis duration was adjusted to avoid excessive precipitation of the coating materials causing pore blockage in the foam., it was observed that, as the concentration of the electrolyte increased, the precipitation was promoted. Therefore, the time of precipitation was reduced to 500, 1000, and 1500 s for 0.15, 0.10, and 0.06 M electrolytes, respectively. Hence the most challenging issue of conventional dip-coating (removal of excess liquid-like by withdrawal) on small pore foams could be overcome by adjusting the synthesis time during the electrosynthesis even when thick coatings are prepared (*vide infra*).

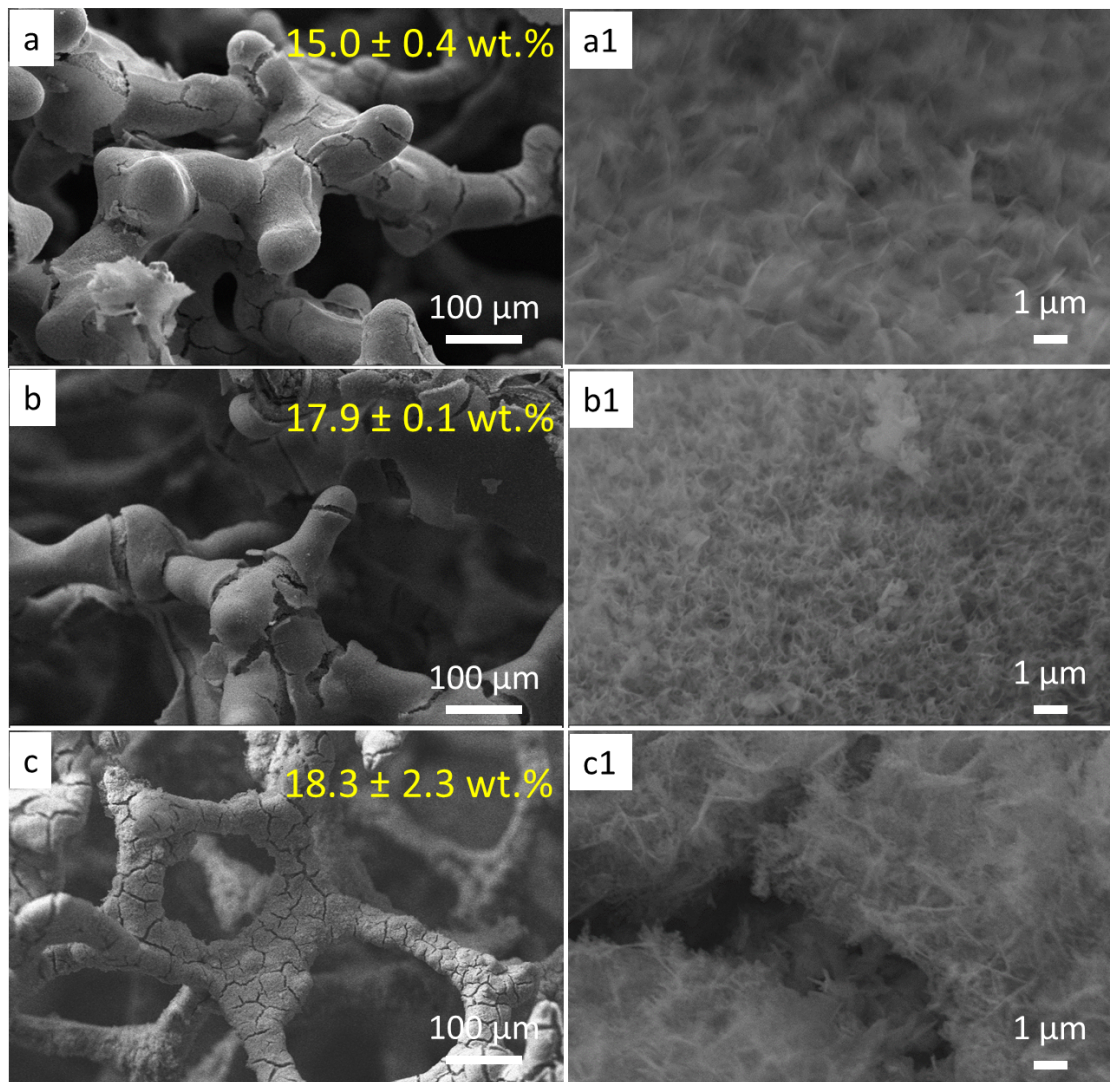


**Figure 2.** SEM images of electrodeposited samples (foam type I) prepared at  $-1.2 V$  vs  $SCE$  in different concentration of  $Co(NO_3)_2$  electrolytes and synthesis duration: 0.06 M, 1500 s (a, a1, a2, a3); 0.10 M, 1000 s (b, b1, b2, b3); and 0.15 M, 500 s (c, c1, c2, c3). Figures a2, b2, and c2 showed the morphology of the second layer (top layer) while Figures a3 and b3 showed that of the first layer (bottom layer near foam surface). Figure c3 showed a crack with two different morphologies. Values of loadings were taken on an average of four replicated experiments.

To investigate the morphology of the coating, SEM analyses were carried out and the images at different magnifications of the foams electrodeposited in the three electrolytes were displayed in Figure 2. The concentration of electrolyte can influence the morphology of the hydroxide particles and thus of the coating [28]. The foam surfaces were fully covered by compact and almost crack-free blue layers with solid loadings, regardless of the synthesis conditions studied, of approximately 27 – 28 wt.% (Figure 2a1, b1, and c1). In some locations, cracks allowed to estimate the layer thickness to be about 15-18  $\mu m$ , which was much thicker than those around 4-5  $\mu m$  previously reported for electrodeposited  $Co(OH)_2$  [12, 13]. These coatings were composed of 100 to 300 nm nanoparticles with a needle-like morphology (Fig. 2A2, b2, and c2) typical of  $\alpha-Co(OH)_2$  electrodeposited on Ni foam [13] or stainless steel plate [12]. Analyzing the zones where cracks developed, regardless of the electrodeposition conditions, it was observed that a layer near the foam surface showed larger particle size (Fig. 2A3, 2b3, and 2c3) than that of the top layer (Fig. 2A2, 2b2, and 2c2). This behavior suggests that the synthesis conditions used in this work did result in similar values of loading and morphology of the coating.

After calcination at 600 °C for 6 h, the loading decreased to 15 – 18 wt.% due to water and  $NO_x$  removal. During thermal treatment, some narrow cracks developed, though the coating was still stable, Figure 3a-c. The needle-like morphology was maintained, but larger particle sizes (about 200 – 400 nm) were observed in the layers (Figure 3a1-c1) in comparison to the as-synthesized sample (Figure 2). This is the normal sintering of particles under thermal treatment conditions [35].



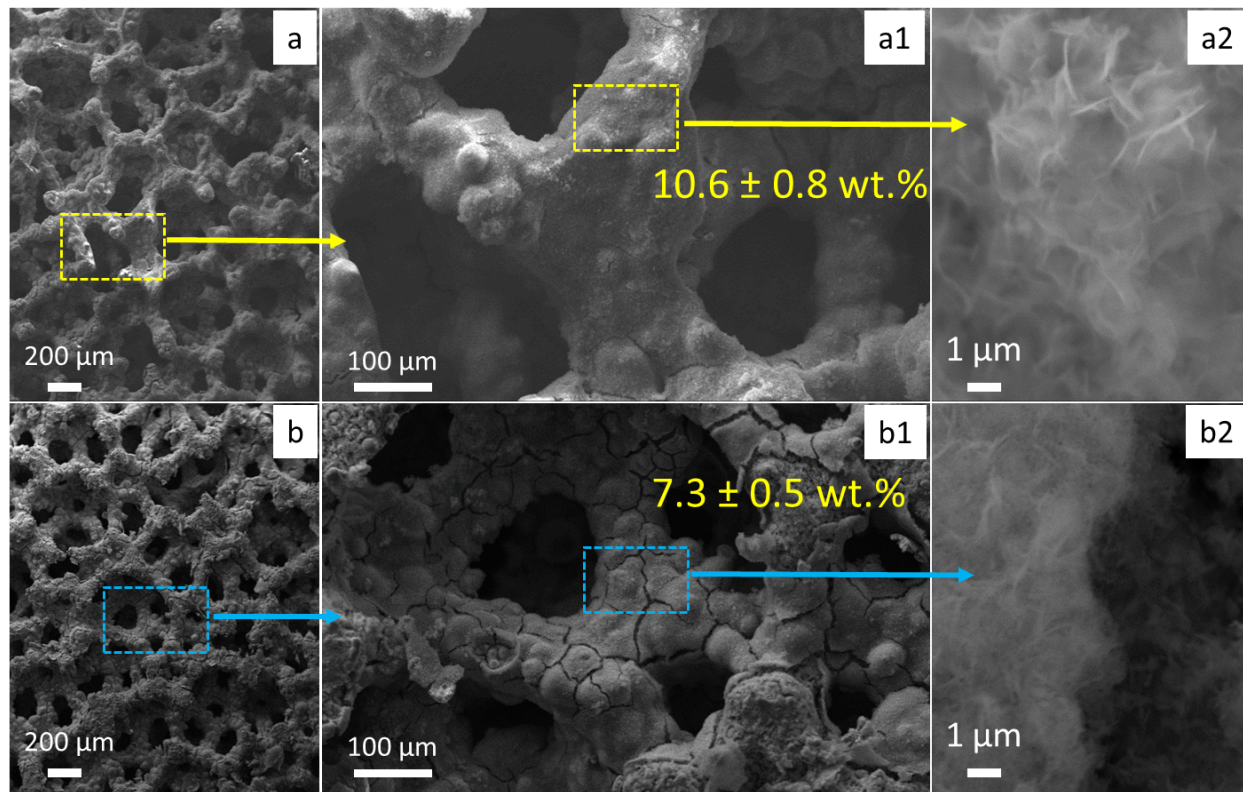


**Figure 3.** SEM images of  $\text{Co}_3\text{O}_4$  structured catalysts (foam type I) prepared at  $-1.2 V$  vs SCE in different concentration of  $\text{Co}(\text{NO}_3)_2$  electrolytes: 0.06 M-1500 s (a, a1); 0.10 M-1000 s (b, b1); and 0.15 M-500 s (c, c1). Calcination at  $600^\circ\text{C}$  for 6 h, temperature ramp  $10^\circ\text{C min}^{-1}$ . Values of loadings were taken on an average of four replicated experiments.

The electrosynthesis is also applied to coat  $\text{Co}_3\text{O}_4$  on another type of FeCrAlloy foam (type II) with different dimensions (1.6 mm thickness x 9 mm diameter) and pore sizes (nominal cell size  $450\ \mu\text{m}$ ), and the SEM images of the samples after electrosynthesis and after calcination are shown in Figure 4. It should be noted that the difference in dimension of the foam substrate requires an adjustment in the synthesis parameters to avoid the deposition of excess materials causing the blockage of the foam substrate. For example, the synthesis time was 250 s for this small foam type II. This was only half compared to that for foam type I while keeping the same concentration of the electrolyte (0.15 M) and applied potential ( $-1.2 V$  vs SCE). Both as-synthesized samples and calcined samples showed very similar morphology to those prepared on foam type I. The loading of the washcoat layer on the foam type II was approximately 10.6 and



7.3 wt.% for the as-synthesized and calcined samples, respectively. A lower loading on foam type II than foam type I was due to a shorter synthesis time.

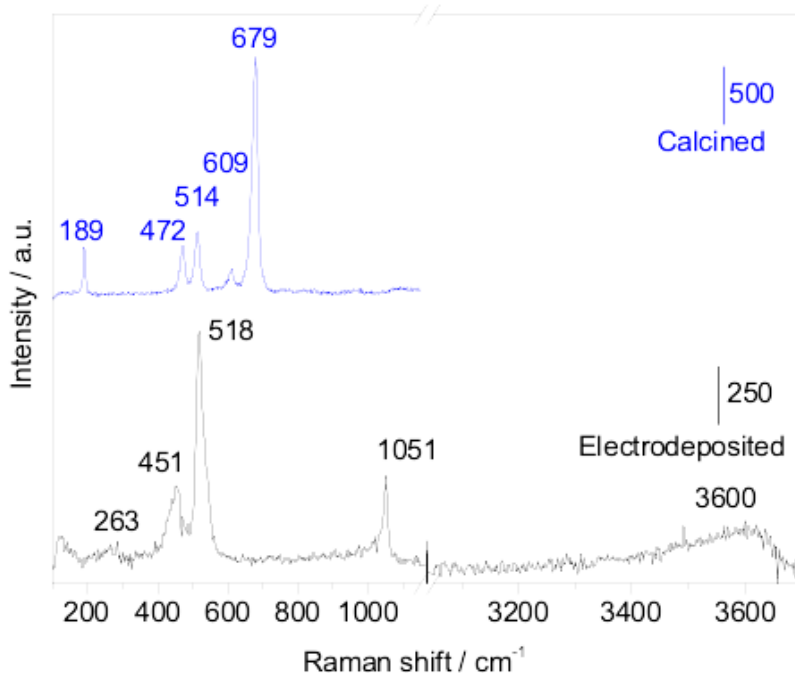


**Figure 4.** SEM images of  $\text{Co}_3\text{O}_4$  coated on foam type II by the electrodeposition at  $-1.2 V$  vs SCE for 250 s in 0.15 M of  $\text{Co}(\text{NO}_3)_2$  electrolyte: after electrodeposition (a, a1, a2) and after calcination at  $600^\circ\text{C}$  for 6 h (b, b1, b2). Values of loadings were taken on an average of 12 replicated experiments.

The formation of a single cobalt hydroxide phase was expected [12], but despite several attempts, we were unable to record diffraction patterns in which the coating reflections were observed. This may be due to the poor crystallinity of the deposited phase rather than to a low amount of material, as we were able to record patterns for other coated foams ( $\text{CeO}_2$ , MgAl hydrotalcite-like compounds?) containing lower solid loadings [27, 34]. To obtain information about the crystalline nature of the solid deposited, the sample Co-0.15 was analyzed by micro-Raman, Figure 5. The two representative peaks of  $\text{Co}(\text{OH})_2$  were recorded at  $518$  and  $451\text{ cm}^{-1}$ , which were associated with  $\text{CoO}$  ( $A_g$ ) symmetric stretching and O-Co-O bending modes, respectively [36]. It was noted that from Raman spectra, two types of structures, namely,  $\alpha$ - $\text{Co}(\text{OH})_2$  and  $\beta$ - $\text{Co}(\text{OH})_2$  could be identified by an intense band at  $518$  and  $502\text{ cm}^{-1}$  Raman shift,

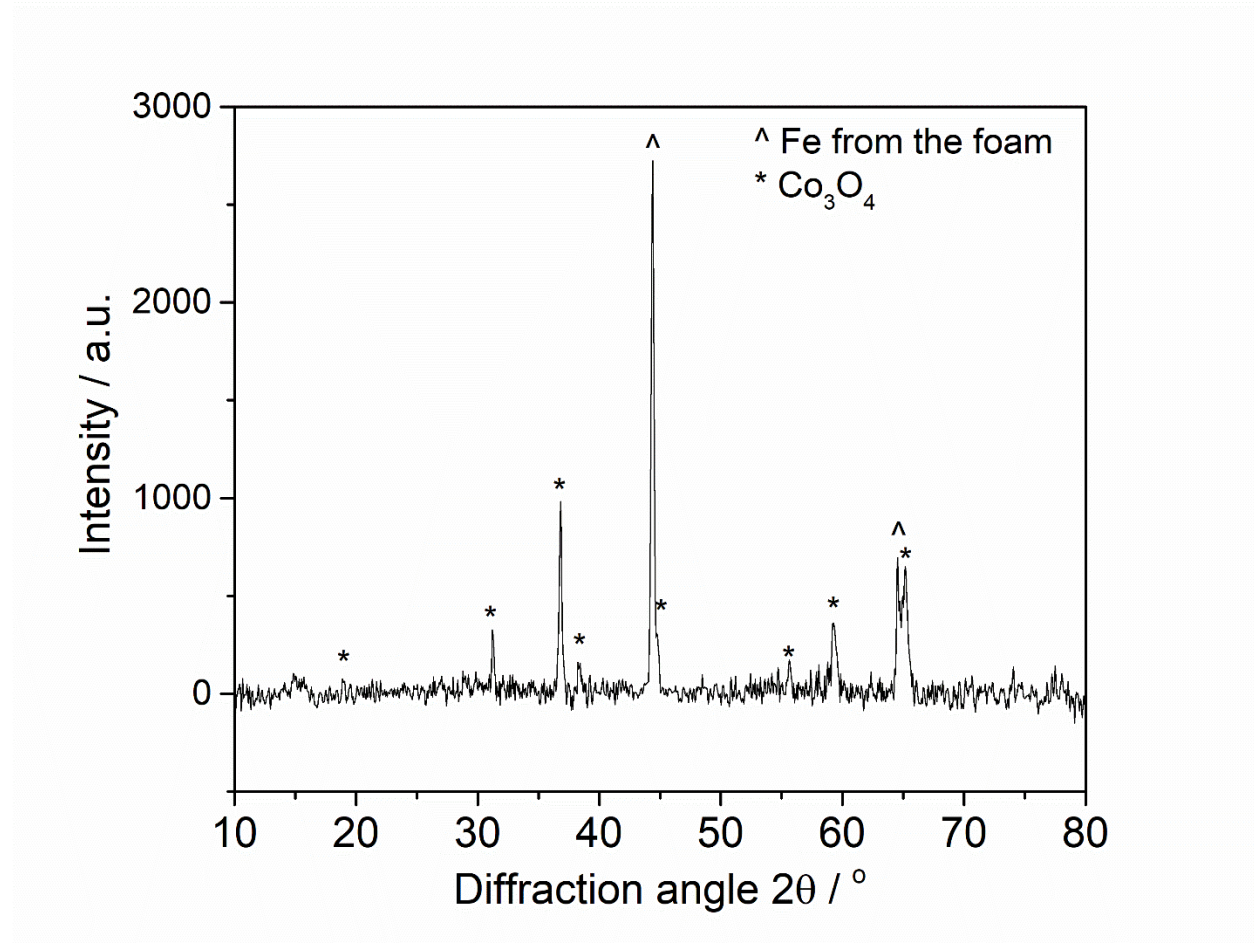
respectively. Therefore, the only presence of an intense band at  $518\text{ cm}^{-1}$  without a band at  $502\text{ cm}^{-1}$  in the Raman spectrum confirmed the  $\alpha\text{-Co(OH)}_2$  but not  $\beta\text{-Co(OH)}_2$  structure in the as-electrodeposited sample [37]. In addition, the broad band centered at around  $3600\text{ cm}^{-1}$  was attributed to the  $\nu_{\text{OH}}$  of water and hydroxyl in the layer of  $\text{Co(OH)}_2$  [38]. The sharp peak at  $1051\text{ cm}^{-1}$  was assigned to the  $\nu_1$  symmetric stretching mode of  $\text{NO}_3^-$  species which could be both adsorbed or intercalated in  $\text{Co(OH)}_2$  [39].

Raman spectra of the calcined catalyst showed five peaks assigned to the  $\text{Co}_3\text{O}_4$  spinel structure. The most intense band at  $679\text{ cm}^{-1}$  was related to the  $A_{1g}$  mode. The three peaks at  $189$ ,  $514$ , and  $609\text{ cm}^{-1}$  were associated with the  $F_{2g}$  mode, while the last one at  $472\text{ cm}^{-1}$  was related to the  $E_g$  mode [40]. The absence of bands at  $3600$  and  $1051\text{ cm}^{-1}$  confirmed that all hydroxides and nitrate were decomposed. The catalyst synthesized by precipitation also presented five peaks in the Raman spectrum, but only one peak at  $188\text{ cm}^{-1}$  had the same Raman shift of Co structured catalyst, the other four peaks were shifted to lower values (Figure S2a). This indicated that there may be differences in the structure of Co spinel obtained from the two methods.

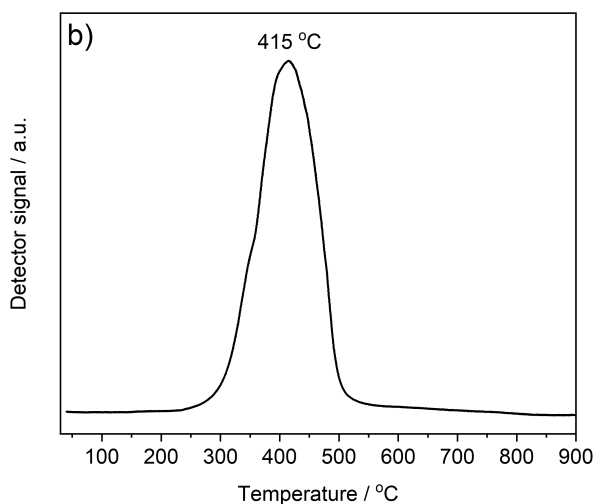
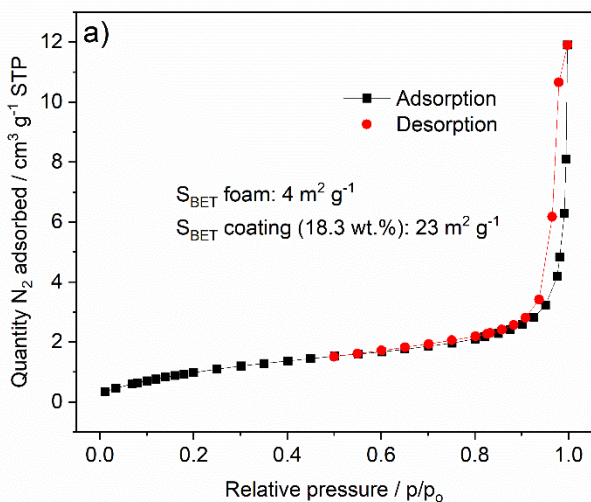


**Figure 5.** Raman spectra of Co-based structured catalysts (foam type I) prepared at  $-1.2\text{ V}$  vs  $\text{SCE}$  in  $0.15\text{ M Co(NO}_3)_2$  electrolytes for  $500\text{ s}$ .

XRD patterns of the coated foams after calcination instead showed the reflections of the  $\text{Co}_3\text{O}_4$  structure and the Fe of the foam (Figure 6). The crystallite size of  $\text{Co}_3\text{O}_4$  calculated for the main reflection (plane (311) at  $2\theta$  of approximately  $36.8^\circ$ ) using Scherrer's equation was about 35 nm.



**Figure 6.** XRD pattern of  $\text{Co}_3\text{O}_4$  coated on foam (type II) after calcination at  $600^\circ\text{C}$ .



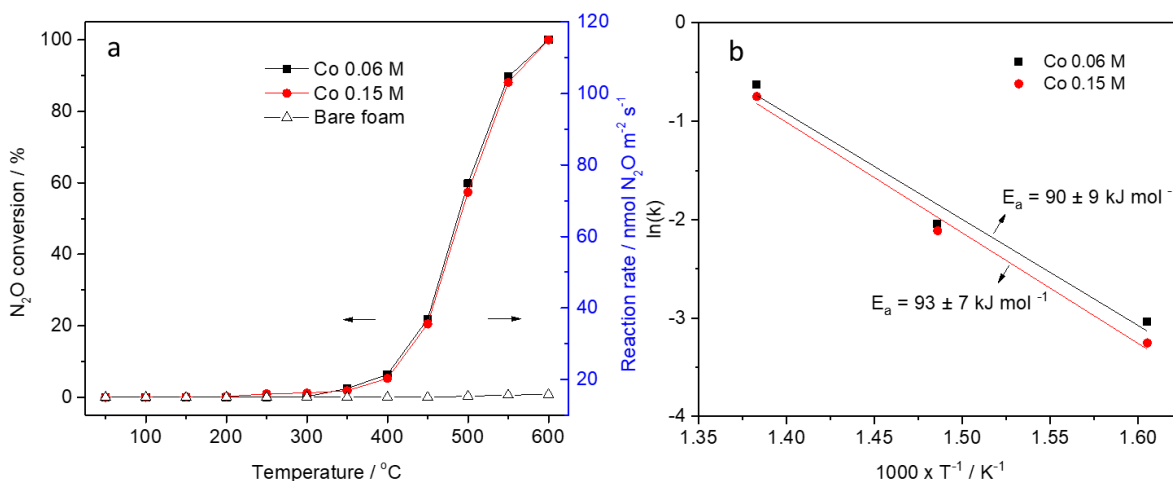
**Figure 7.** Characterization of Co-based structured catalysts (foam type I) prepared at  $-1.2 V$  vs  $SCE$  in  $0.15 M Co(NO_3)_2$  electrolytes for 500 s, and calcined at  $600\text{ }^\circ C$  for 6 h: a) isotherm nitrogen adsorption-desorption and b)  $H_2$ -TPR.

Figure 7a showed typical type IIb of  $N_2$  adsorption-desorption isotherm on sample Co-0.15. This is characteristic of non-microporous materials with interparticle pores. The specific surface area determined by the BET method was about  $4\text{ m}^2\text{ g}^{-1}$ , corresponding to  $23\text{ m}^2\text{ g}^{-1}_{\text{coating}}$ . It is noted that the bare foam showed a negligible specific surface area. A similar specific surface area,  $22\text{ m}^2\text{ g}^{-1}_{\text{coating}}$  was measured for the Co-0.06 catalyst, suggesting that the synthesis conditions did not largely modify the textural properties of the resulting  $Co_3O_4$  catalysts, in agreement with SEM images. It should be noted that these specific surface area values were significantly higher than for the  $Co_3O_4$  powder catalyst prepared by thermal decomposition ( $4\text{ m}^2\text{ g}^{-1}$ ) [41] or precipitation ( $10\text{ m}^2\text{ g}^{-1}$ , using  $(NH_4)_2CO_3$  as precipitation agent and calcined at  $700\text{ }^\circ C$  for 3h) [42], as well as

than a commercial catalyst (Fluka  $16 \text{ m}^2 \text{ g}^{-1}$ ) [43]. Otherwise it was but lower than a precipitated sample calcined at  $600 \text{ }^\circ\text{C}$  prepared by us in this work ( $25 \text{ m}^2 \text{ g}^{-1}$ , using NaOH) or from literature ( $30 \text{ m}^2 \text{ g}^{-1}$ , using  $(\text{NH}_4)_2\text{CO}_3$ ) [44].

The reducibility of  $\text{Co}_3\text{O}_4$  in Co-0.15 was analyzed by  $\text{H}_2$ -TPR and presented in Figure 7b.  $\text{H}_2$  was consumed mainly in the range from  $300$  to  $500 \text{ }^\circ\text{C}$ . The low-intensity shoulder at  $350 \text{ }^\circ\text{C}$  could be associated with the reduction of  $\text{Co}_3\text{O}_4$  to  $\text{CoO}$ , while the major peak at ca.  $415 \text{ }^\circ\text{C}$  may be attributed to the reduction of bulk  $\text{CoO}$  to  $\text{Co}$ . The shape of the curves was similar to  $\text{H}_2$ -TPR profiles of  $\text{Co}_3\text{O}_4$  prepared by combustion method [41] or of a commercial product [43] although the maximum temperature ( $T_{\text{max}}$ ) again depended on the preparation method. Indeed, the  $T_{\text{max}}$  of the electrodeposited Co catalyst was lower (around  $60 \text{ }^\circ\text{C}$ ) than that of the combustion catalyst but higher than that of the commercial one. Compared to the precipitated catalyst, the electrosynthesis structured catalyst was easier to be reduced since the peaks were shifted to lower temperatures. The  $\text{H}_2$ -TPR profile of precipitated catalyst showed two distinct peaks around  $406$  and  $520$  which were significantly higher than those of electrosynthesis catalyst (Figure S2b). This may be probably related to particle size because the small crystallite sizes are easier to be reduced than the big ones [45]. It was noted that the reducibility of the catalyst may influence its activity because the reduction of  $\text{Co}^{3+}$  to  $\text{Co}^{2+}$  by the desorption of oxygen is the determining step of the overall reaction rate [45]. The order of  $T_{\text{max}}$  was the same as the activity order during  $\text{deN}_2\text{O}$ .

### 3.2 $\text{N}_2\text{O}$ catalytic decomposition



**Figure 8.**  $\text{N}_2\text{O}$  catalytic decomposition on Co structured catalysts (foam type I): a)  $\text{N}_2\text{O}$  conversion (left Y-axis) and reaction rate (right Y-axis); and b) Arrhenius plots for apparent activation energy calculation. Reaction conditions: two coated foams, GHSV =  $6,800 \text{ h}^{-1}$ , under  $80 \text{ mL min}^{-1}$  of  $1000 \text{ ppm N}_2\text{O/N}_2$ . Arrhenius plots used data points with conversion lower than  $25\%$   $\text{N}_2\text{O}$  conversion. The error of the activation energy was calculated from the standard deviation value of the slope of the fitting curve.



For the N<sub>2</sub>O decomposition, a pair of coated foams (type I, diameter 8 mm and height 7 mm) was loaded inside the quartz reactor. N<sub>2</sub>O conversion and reaction rate of 0.1 vol.% N<sub>2</sub>O/N<sub>2</sub> over Co-0.06 and Co-0.15 catalysts at temperatures 50 – 600 °C were presented in Figure 8a. A pair of bare foams calcined at 600 °C was also tested under the same reaction conditions for comparison purposes. The bare foam was inactive for N<sub>2</sub>O decomposition up to 600 °C (conversion < 1%) as reported in our previous work [25]. Both Co-0.06 and Co-0.15 catalysts were active for deN<sub>2</sub>O and their performance activity was almost identical. In both cases, N<sub>2</sub>O started to be decomposed at 350 °C and converted completely at 600 °C. Klegova and co-workers reported the N<sub>2</sub>O decomposition over Co<sub>3</sub>O<sub>4</sub>/open-cell SiC foam at the same N<sub>2</sub>O concentration (1000 ppm) but lower GHSV (3000 h<sup>-1</sup> vs 6800 h<sup>-1</sup> in this work) [18]. Interestingly, comparable catalytic performances activity were obtained with their optimized sample, prepared by a suspension coating method, and our sample prepared by electrosynthesis: for example, at 450 °C almost the same 20% conversion of N<sub>2</sub>O was measured, although a double GHSV was used in our study. However, it should be noted that both foam size (14 cm<sup>3</sup>, diameter x length = 3 cm x 2 cm) and total flow rate (700 mL min<sup>-1</sup>) were different from this study.

It is very challenging to compare N<sub>2</sub>O decomposition performances activity of the structured and pelletized catalysts reported in the literature, due to dissimilarity in the reaction conditions. N<sub>2</sub>O decomposition rate (*r*, also called turnover reaction rate TOR, nmol N<sub>2</sub>O m<sup>-2</sup> s<sup>-1</sup>) may be an accurate assessment for such purpose [25]. The results of TOR for the structured catalysts used in this work are displayed in Figure 8a (right Y-axis). TOR of Co-based catalyst was 39 (nmol N<sub>2</sub>O m<sup>-2</sup> s<sup>-1</sup>, at 490 °C), which was higher than the one of Co<sub>3</sub>O<sub>4</sub> pelletized catalyst (less than 30 nmol N<sub>2</sub>O m<sup>-2</sup> s<sup>-1</sup>, at 500 °C) reported by Kaczmarczyk et al. [42]. However, this value was lower than for a Co<sub>3</sub>O<sub>4</sub> commercial powder catalyst (about 135 nmol N<sub>2</sub>O m<sup>-2</sup> s<sup>-1</sup>, at 400 °C) reported by Maniak and coworkers [43]. It was worth noting that these results were performed under different reaction conditions. In a work with more similar reaction conditions (0.3 g catalyst, 90 mL min<sup>-1</sup> of 1000 ppm N<sub>2</sub>O/N<sub>2</sub>) performed on Co<sub>3</sub>O<sub>4</sub> pelletized catalyst prepared by combustion method, Franken et al. [41] presented a TOR of 24.3 nmol N<sub>2</sub>O m<sup>-2</sup> s<sup>-1</sup> (calculated at T<sub>50</sub> around 550 °C).

To make a better comparison with pelletized catalysts, the Co<sub>3</sub>O<sub>4</sub> catalyst prepared by precipitation was tested under the same concentration of N<sub>2</sub>O (1000 ppm) and total flow rate (80 mL min<sup>-1</sup>), but with 300 mg of catalyst. The N<sub>2</sub>O conversion and reaction rate are shown in Figure S3. TOR at 490 °C was around 7.3 nmol N<sub>2</sub>O m<sup>-2</sup> s<sup>-1</sup>. It can be therefore highlighted that a Co-based structured catalyst exhibited better TOR in comparison to Co<sub>3</sub>O<sub>4</sub> pelletized catalyst prepared by combustion or precipitation method. This could be related to the high specific surface area, particle size, or reducibility, as reported for the effect of the preparation method of cobalt spinels on their N<sub>2</sub>O decomposition activity [46, 47]. It should be noted that the internal diffusion limitation is also an important factor that needs to be considered for the comparison between the pelletized and structured catalysts. The coating layer of the structured catalyst (15-18 μm) is significantly thinner than the grain size of the pelletized catalyst (0.25-0.50 mm) and therefore it is expected the mass transfer limitation is lesser for the former than the latter. The

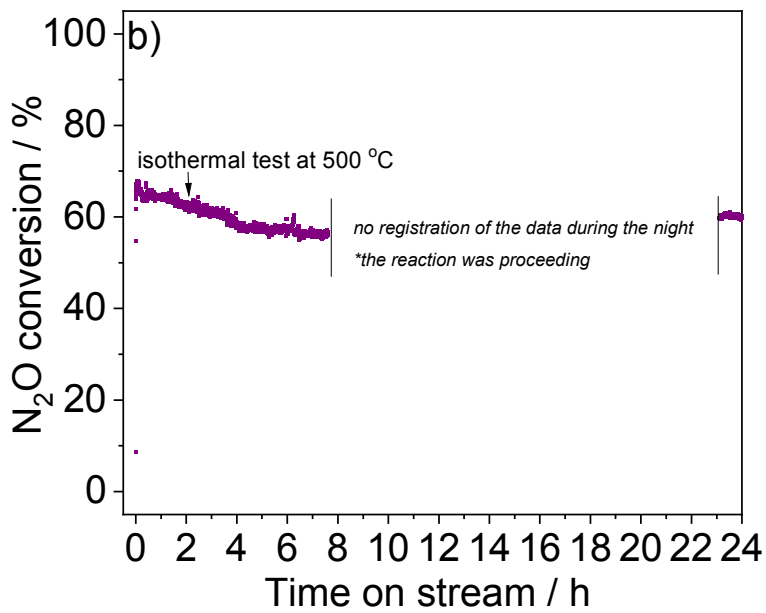
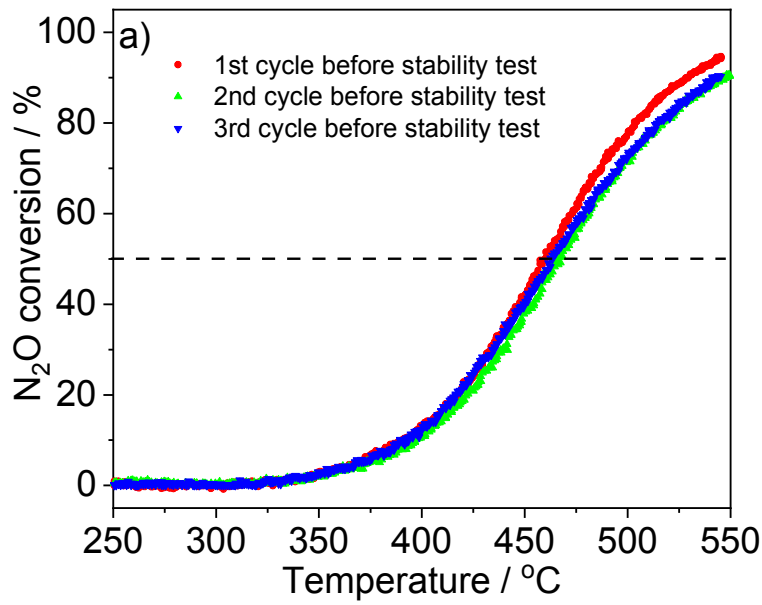
comparison of TOR of Co-based structured catalysts and other Co-containing catalysts in literature was summarized in Table 1.

**Table 1.** Comparison of turnover reaction rate between Co-based structured catalysts and Co-containing catalysts reported in literature.

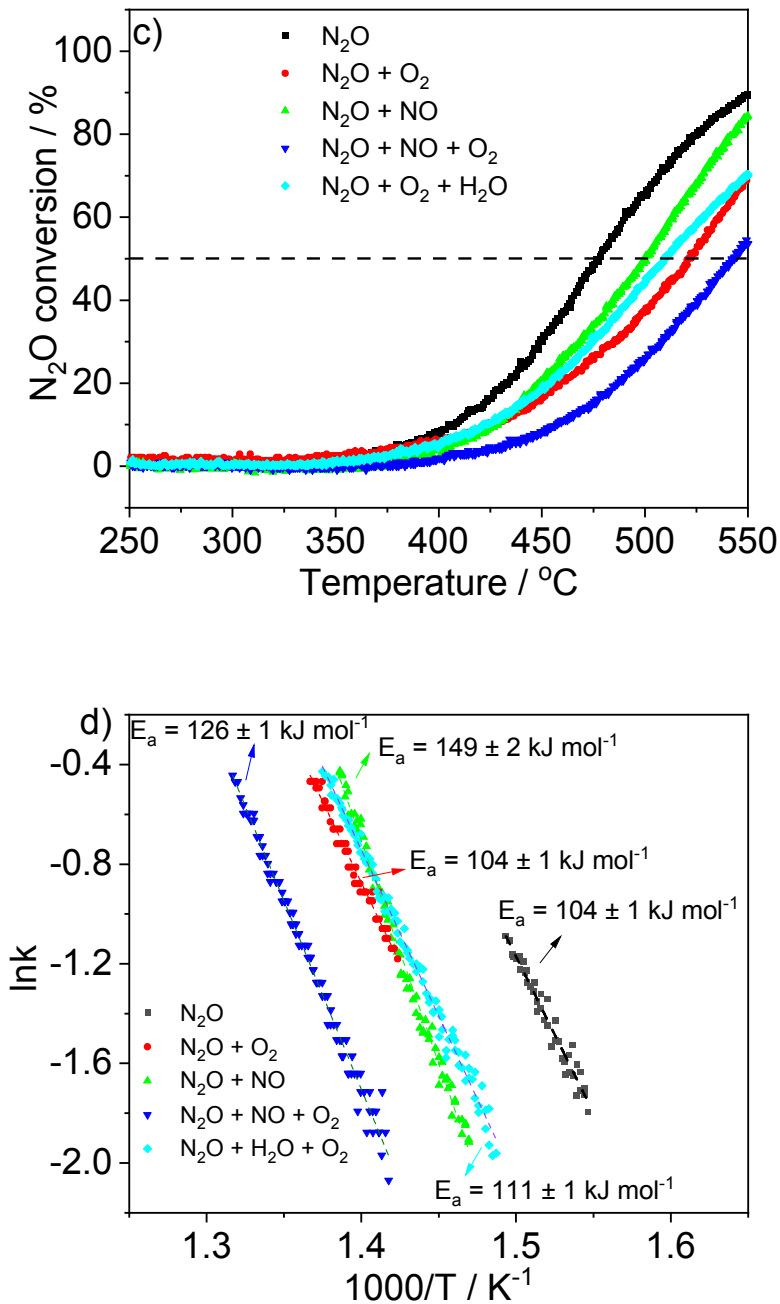
Preparation method	$S_{\text{BET}}$ ( $\text{m}^2 \text{g}^{-1}$ )	$T_{\text{max}}$ $\text{H}_2$ - TPR ( $^{\circ}\text{C}$ )	TOR ( $\text{nmol N}_2\text{O m}^{-2} \text{s}^{-1}$ )	Reference
Combustion	4	ca. 410, 480	24.3 (550 $^{\circ}\text{C}$ )	[41]
Commercial product	16*	ca. 415	135.0 (400 $^{\circ}\text{C}$ )	[43]
Precipitation	10	-	ca. 30.0 (500 $^{\circ}\text{C}$ )	[42]
Electrodeposition	23	ca. 350, 415	16.0 (450 $^{\circ}\text{C}$ ) 39.0 (490 $^{\circ}\text{C}$ )	This work
Wet impregnation coating SiC foam	18	388, 436	11.8 (450 $^{\circ}\text{C}$ )	[18]
Suspension coating SiC foam	18	341, 448	18.3 (450 $^{\circ}\text{C}$ )	[18]

- from supplier

Apparent activation energies of Co-0.06 and Co-0.15 catalysts determined from the slope of linear regression fit of Arrhenius plots were displayed in Figure 8b. Both catalysts showed similar apparent activation energy of 90-93  $\text{kJ mol}^{-1}$ . Interestingly, this value is almost the same as the raw value for  $\text{Co}_3\text{O}_4$  precipitated catalysts calculated by Yu and co-workers. However, the authors corrected this value to a lower one, taking into account the change of active phase with increasing temperature [48]. In addition, this apparent activation energy value was also similar to the one reported for  $\text{Co}_3\text{O}_4$  coated on  $\alpha\text{-Al}_2\text{O}_3$ -cordierite honeycomb monolith by combustion or impregnation method ( $\sim 83 - 88 \text{ kJ mol}^{-1}$ ) [14]. Moreover, Stelmachowski and co-workers have reported that octahedral  $\text{Co}^{3+}$  ions are more active than tetrahedral  $\text{Co}^{2+}$  ions, since the former showed apparent activation energy around 15-17  $\text{kcal mol}^{-1}$  ( $63 - 71 \text{ kJ mol}^{-1}$ ) while for the latter it was 27 - 28  $\text{kcal mol}^{-1}$  ( $113 - 117 \text{ kJ mol}^{-1}$ ) [24]. The apparent activation energy of the electrosynthesis catalysts was between these values, which suggests that they may contain both types of active sites.







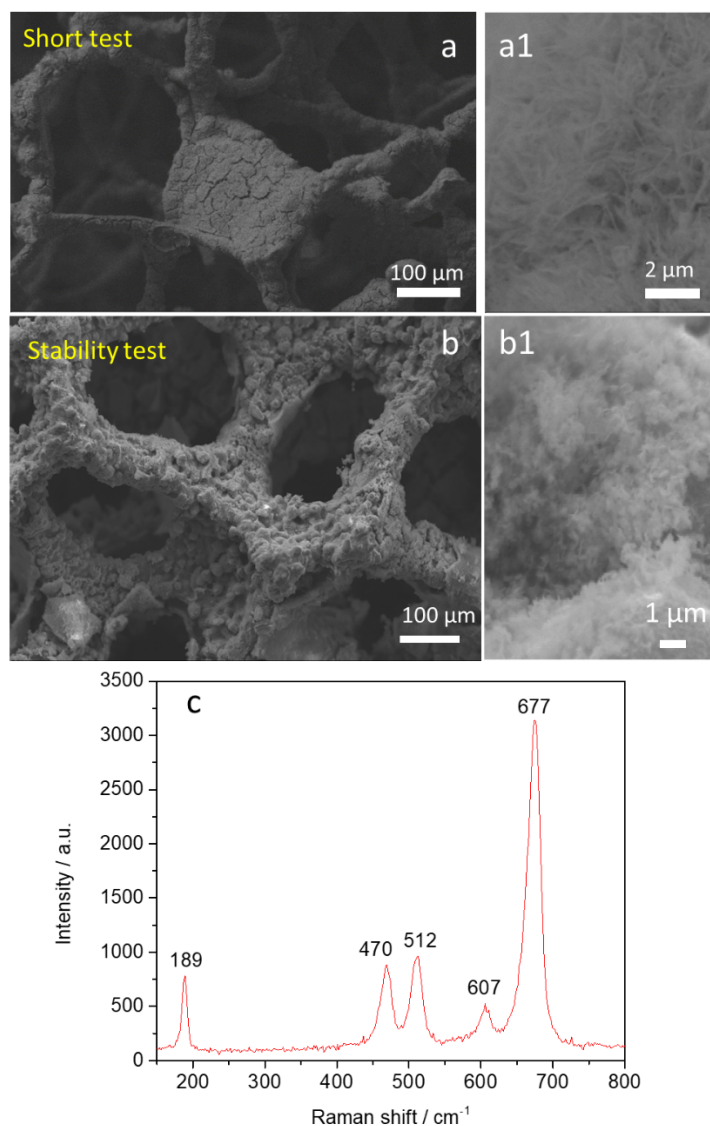
**Figure 9.** N<sub>2</sub>O catalytic decomposition on Co-based structured catalysts (foam type II): a) cycle tests with TRSR; and b) stability test; c) effect of inhibitors; and d) Arrhenius plots for apparent activation energy calculation. Reaction conditions: five coated foams (total mass of coating 24 mg), GHSV = 3500 h<sup>-1</sup> and WHSV = 75,000 mL h<sup>-1</sup>g<sup>-1</sup> under 30 mL min<sup>-1</sup> of 2500 ppm N<sub>2</sub>O/N<sub>2</sub>. The inhibitors were used with different concentrations including 500 ppm NO, 2% O<sub>2</sub>, and 3.6

vol% H<sub>2</sub>O. Arrhenius plots used data points with conversion lower than 20% N<sub>2</sub>O conversion. The error of the activation energy was calculated from the standard deviation value of the slope of the fitting curve.

The structured catalyst using type II of FeCrAlloy foam was tested for N<sub>2</sub>O decomposition with sequential experiments listed in Figure S1. Fig. 9A shows the conversion profiles of N<sub>2</sub>O during three cycles of heating/cooling at a temperature range of 250 – 550 °C. The profiles of the second and the third cycle were almost identical and slightly lower than the profile of the first cycle in the temperature range from 450 to 550 °C. The T<sub>50</sub> values of three cycles were in the range of 460 – 465 °C. Such a small difference in T<sub>50</sub> values suggested that the activity of the catalyst was stable during the cycle tests. After the third cycle, the catalyst was tested at 500 °C for 24 h and the result is presented in Fig. 9b. The N<sub>2</sub>O conversion decreased from 65% to 58% in the first five hours and was then almost stable at the plateau of 58% till the end of the test. The activity tests were subsequently performed in the presence of NO, O<sub>2</sub>, and H<sub>2</sub>O to investigate the effect of inhibitors. As shown in Figure 9c, the T<sub>50</sub> values were ranked in an increasing order of N<sub>2</sub>O (477 °C) < N<sub>2</sub>O + NO (500 °C) < N<sub>2</sub>O + O<sub>2</sub> + H<sub>2</sub>O (509 °C) < N<sub>2</sub>O + O<sub>2</sub> (521 °C) < N<sub>2</sub>O + NO + O<sub>2</sub> (543 °C). The inhibitors such as NO, O<sub>2</sub>, and H<sub>2</sub>O have competitive adsorption on the active sites with N<sub>2</sub>O and consequently inhibit the activity of the deN<sub>2</sub>O catalysts [49, 50]. To gain more information on the impact of the inhibitors, the apparent activation energy was calculated (Figure 9d). The presence of O<sub>2</sub> exhibited a similar E<sub>a</sub> value to N<sub>2</sub>O alone, suggesting that O<sub>2</sub> may not alter the reaction pathway. In contrast, the presence of NO resulted in the activation energy of 149 kJ mol<sup>-1</sup>, which is approximately 1.4 times higher than that of N<sub>2</sub>O alone. Such a significant increase in the value of apparent activation energy indicated that NO strongly inhibited the studied reaction due to its substantially competitive adsorption with N<sub>2</sub>O. The mixture of NO+O<sub>2</sub>+N<sub>2</sub>O and H<sub>2</sub>O+O<sub>2</sub>+N<sub>2</sub>O resulted in the E<sub>a</sub> of 126 and 111 kJ mol<sup>-1</sup>, respectively. A higher E<sub>a</sub> of the former than the latter suggests that NO inhibited the N<sub>2</sub>O decomposition stronger than H<sub>2</sub>O in the window temperature of around 500 °C in this study.

### 3.3 Characterizations of the spent catalysts

After catalytic tests, SEM images revealed that both the adherence and morphology of the layers on two types of foams were almost the same as in the calcined catalyst, without any expansion of the cracks (Figure 10a, a1, b, and b1). To verify whether there was a phase change after the reaction, the catalyst was additionally examined by the micro-Raman. Only the five peaks at 188 (F<sub>2g</sub>), 468 (F<sub>g</sub>), 510 (F<sub>2g</sub>), 604 (F<sub>2g</sub>), and 670 (A<sub>1g</sub>) cm<sup>-1</sup> associated with cubic Co<sub>3</sub>O<sub>4</sub> structure were observed in the Raman spectrum of the calcined samples (Figure 10c).



**Figure 10.** Characterization of the used Co-0.15M structured catalysts after the catalytic test: a and a1) SEM images of foam type I; b and b1) SEM images of foam type II, and c) Raman spectrum of foam type I.

#### 4. Conclusions

Co<sub>3</sub>O<sub>4</sub> structured catalysts based on FeCrAlloy open-cell foams were prepared by the facile electrodeposition method, followed by calcination at 600 °C. The loading of coating can be adjusted by tailoring the synthesis parameters such as time and concentration. Stable Co<sub>3</sub>O<sub>4</sub> layers were obtained on small pore foams without any pore blockage on different types of FeCrAlloy foams (7 mm x 8mm cylinder of 80 PPI and 1.6 mm x 9 mm of 450 μm cell size). The catalysts showed satisfactory performance for catalytic decomposition of N<sub>2</sub>O with T<sub>50</sub> around 490 °C and a reaction rate of 39 nmol N<sub>2</sub>O m<sup>-2</sup> s<sup>-1</sup> at 450 °C. The structured catalyst showed a higher reaction rate than Co<sub>3</sub>O<sub>4</sub> powder prepared by precipitation or combustion

method. The catalyst also performed a stable conversion of  $\text{N}_2\text{O}$  during a stability test of 24 h. The presence of inhibitors such as  $\text{O}_2$ ,  $\text{NO}$ , and  $\text{H}_2\text{O}$  hindered partially the conversion of  $\text{N}_2\text{O}$ , causing a shift of  $T_{50}$  toward higher temperatures. The wide range of applications of  $\text{Co}_3\text{O}_4$  catalysts as well as the possibility of improving the activity by further doping the  $\text{Co}_3\text{O}_4$  structure, also during the electrodeposition method, may increase the applicability of the structured catalysts developed here.

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### **CRedit authorship contribution statement**

**Phuoc Hoang Ho**: Methodology, Investigation, Writing – original draft, Visualization. **Katarzyna Świrk**: Investigation, Writing – review & editing. **Magdalena Jabłońska**: Writing – review & editing, Supervision. **Giancosimo Sanghez de Luna**: Investigation, Writing – review & editing. **Francesca Ospitali**: Resources. **Francesco Di Renzo**: Writing – review, Supervision. **Gérard Delahay**: Conceptualization, Writing – review, Supervision. **Giuseppe Fornasari**: Writing – review & editing. **Angelo Vaccari**: Writing – review & editing. **Regina Palkovits**: Writing – review, Supervision. **Patricia Benito**: Conceptualization, Writing – review, Supervision.

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