





Theoretical (and numerical) study of pad roll instability in a three fluid-layers system

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Context

lssue:

Need for a reliable energy storage system for a stationary application

Possibility: Liquid Metal Battery

Composition: A molten salt (the electrolyte E) between 2 Liquid Metals (the anode LMA and the cathode LMC) Objective:

Stability analysis of a LMB model to prevent short circuits



Figure 1: Sketch of the LMB model

Literature review

Sneyd, A. D., J. Fluid Mech. (1985):

Linear stability analysis of two systems close to LMB (Hall-Héroult Cell, HHC and Electric Arc Furnace, EAF) taking into account the far magnetic field.



HHC: the local magnetic field has only a stabilizing effect. EAF: the local magnetic field can destabilize the system. LMB: Our study.

Herreman, W., J. & al. Fluid Mech. (2019): Metal pad roll instability with a perturbative method taking into account only the top two layers.

Assumptions and method

For the fluids:

- Incompressible fluids
- Inviscid fluids
- Infinite depth for extreme layers
- Isothermal conditions



For the electric and the magnetic fields:

- Slowly variable regime (quasistatic approximation)
- Coulomb force disregarded
- Magnetic field not bounded at the interfaces

Method:

• Solve base state and disturbed state (linearized) for volume equations and their jump conditions

Volume equations

Mass and momentum conservation:

$$\vec{\nabla} \cdot \vec{u} = 0$$

$$\rho_i \left(\vec{u}_{,t} + (\vec{u} \cdot \vec{\nabla}) \vec{u} \right) = -\vec{\nabla} p + \vec{f}_L + \rho \vec{g}$$

With $\vec{f_L} = \vec{j} \times \vec{B}$, the Lorentz force

Maxwell equations and Ohm's law:

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{j}$$
$$\vec{\nabla} \times \vec{E} = \vec{0}$$
$$\vec{\nabla} \cdot \vec{B} = 0$$
$$\vec{j} = \sigma \vec{E}$$

Equations valid for all the layers

No coupling between
$$\vec{u}, \vec{B}, \vec{E}$$

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Jump conditions

For mass and momentum :

$$\vec{u}_i \cdot \vec{n}_i = z_{ii+1,t} = \vec{u}_{i+1} \cdot \vec{n}_i$$
$$p_{i+1} - p_i = 0$$



For the electric and the magnetic fields :

$$\vec{B}_i \cdot \vec{n}_i = \vec{B}_{i+1} \cdot \vec{n}_i$$
$$\vec{B}_i \times \vec{n}_i = \vec{B}_{i+1} \times \vec{n}_i$$
$$\vec{j}_i \cdot \vec{n}_i = \vec{j}_{i+1} \cdot \vec{n}_i$$
$$\vec{E}_i \times \vec{n}_i = \vec{E}_{i+1} \times \vec{n}_i$$
With $i = \{1, 2\}$ and $\vec{n}_i = {}^t(-z_{ii+1,x}, -z_{ii+1,y}, 1)$

Conditions valid at
$$z = z_{ii+1}$$

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Base state

Assumptions :

Equations:

$\vec{u}_i^* = \vec{0}$	$-ec abla(p_i^*+ ho_i gz)+j_0ec e_z imesec B_{i0}=ec 0$
$z_{12}^* = 0$	$p_2^* - p_1^* = 0$ at $z = 0$

$$z_{23}^* = h$$
 $p_3^* - p_2^* = 0$ at $z = h$

Admissible fields:

$$\vec{B}_i^* = \vec{B}_{C_i} + \alpha_{ij}x_j \text{ with}$$

$$\alpha = \mu_0 j_0 \begin{pmatrix} Q & R - \frac{1}{2} & 0\\ R + \frac{1}{2} & -Q & 0\\ 0 & 0 & 0 \end{pmatrix} = \alpha_{\textit{local}} + \alpha_{\textit{far}}$$

Q and R refers to the far magnetic field

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Disturbed state

 $\begin{aligned} &z_{ii+1} = \eta_{ii+1}(x, y, z, t) \text{ with } \eta_{ii+1} \text{ perturbation of the interfaces} \\ &\vec{u}_i = \vec{u}'_i(x, y, z, t) : \text{ with } \vec{u}'_i \text{ perturbation of the velocities} \\ &p_i = p^*_i(z) + p'_i(x, y, z, t) : \text{ with } p'_i \text{ perturbation of the pressures} \\ &\vec{E}_i = \vec{E}^*_i + \vec{E}'_i(x, y, z, t) : \text{ with } \vec{E}'_i \text{ perturbation of the electric field} \\ &\vec{B}_i = \vec{B}^*_i(x, y, z) + \vec{B}'_i(x, y, z, t) : \text{ with } \vec{B}'_i \text{ perturbation of the magnetic field} \end{aligned}$

Linearized volume equations :

$$\vec{\nabla} \cdot \vec{u'_i} = 0$$

$$\rho_i \frac{\partial \vec{u'_i}}{\partial t} = -\vec{\nabla} p'_i + \vec{f'_{Li}}$$
With $\vec{f'_{L_i}} = j_o \vec{e_z} \times \vec{B'_i} + \vec{j'_i} \times \vec{B^*_i}$, the disturbed Lorentz force
With $i \in \llbracket 1; 3 \rrbracket$

For mass and momentum:

$$u_{iz} = z_{ii+1,t} = u_{i+1z}$$

$$p'_{i+1} - p'_i - (\rho_{i+1} - \rho_i)gz_{ii+1} = 0$$

For the electric and the magnetic fields :

$$\vec{B}'_{i} \cdot \vec{n}_{i} = \vec{B}'_{i+1} \cdot \vec{n}_{i}$$
$$\vec{B}'_{i} \times \vec{n}_{i} = \vec{B}'_{i+1} \times \vec{n}_{i}$$
$$\vec{j}'_{i} \cdot \vec{n}_{i} = \vec{j}'_{i+1} \cdot \vec{n}_{i}$$
$$\vec{E}'_{i} \times \vec{n}_{i} = \vec{E}'_{i+1} \times \vec{n}_{i}$$

With $\vec{n_i} = t(0, 0, 1)$

Conditions valid at
$$z = (i - 1)h$$

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Dispersion relationship

Analysing the disturbance into normal modes \Rightarrow

$$\Omega^4 f_4(K, \rho_{r12}, \rho_{r13}) + \Omega^2 f_2(K, \rho_{r12}, \rho_{r13}, J) + f_0(K, \rho_{r12}, \rho_{r13}, J) = 0$$

With:

$$\begin{split} f_4 &= \rho_{r12}(\rho_{r12}\sinh(K) + \cosh(K)) + \rho_{r13}(\rho_{r12}\cosh(K) + \sinh(K)) \\ f_2 &= \rho_{r12}(1 - \rho_{r13})(\sinh(K) + \cosh(K)) - (1 + \rho_{r13})J\sinh(K)^{-1} \\ f_0 &= (\rho_{r12} + \rho_{r13})(1 - \rho_{r12})\sinh(K) - (1 + \rho_{r13})J\sinh(K)^{-1} - J^2\sinh(K)^{-1} \end{split}$$

Dimensionless numbers:

- $\Omega = \omega / \sqrt{gk}$: pulsation
- *K* = *kh* : wave number
- $\rho_{r12} = \rho_2/\rho_1$ and $\rho_{r13} = \rho_3/\rho_1$: densities

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$$J = J_{local} + J_{far}$$
: magnetic field
With $J_{local} = -\mu_0 j_0^2 / \rho_1 g$ and $J_{far} = J_{far}(Q, R)$

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Conditions of stability

For $\rho_{r12} = 0.27$ and $\rho_{r13} = \{0; 0.25\}$ (values of Herreman & al.)



Figure 2: Stability diagram for an EAF model where $\rho_{r13} = 0$ (left) and the present LMB model (right)

An unstable region appears in the middle of the stable one \Rightarrow making difficult the conception of such a battery.

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Visualization of the interfaces

For the 2 cases of Figure 2 right:



Figure 3: Coupling between the interfaces for K = 0.2 (left) and K = 1.2 (right)

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When K increases the interfaces become uncoupled.

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Conclusion :

- Inviscid model for liquid metal batteries taking into account the coupling between the two interfaces.
- Find a liquid metal as light as possible for the third layer.

Perspectives :

- Cross-validate the theoretical results with OpenFoam.
- Viscid model for LMB.
- Develop a weakly non linear theory to extend the time of validity of the model.