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# Fatigue Design 2021, 9th Edition of the International Conference on Fatigue Design Ti-6Al-4V lattices obtained by SLM : characterisation of the heterogeneous high cycle fatigue behaviour of thin walls.

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## Abstract

Architected materials are attracting increasing interest since a few years, achieving numerous excellent specific properties compared to fully dense materials. The transport industry sector see periodic assemblies of elementary cells, called lattices, as a solution to lighten structures. This is made possible by the development of Additive Manufacturing technologies (AM). Among the numerous advantages of AM, these processes allow to create a wide range of porous cell topologies, and to tailor their complex geometry with the desired properties. However, understanding their fatigue properties is essential to validate their long-term use in load-bearing parts.

The FA process plays an important role in fatigue life, as it generates residual stresses, heterogeneous microstructure, as well as surface and volume defects (roughness, gaz porosities, lack of fusion porosities), which are preferred sites for fatigue crack initiation. The fatigue life of these structures also depends strongly on their geometry, which, due to their complexity, induces scale and stress gradient effects.

Recent studies have recognize thin-walls TPMS (Triply Periodic Minimal Surfaces) structures as the most promising structures for fatigue resistance, especially the gyroid geometry, compared to conventional strut-lattices.

The first aim of this work is to characterise the major parameters influencing fatigue life at the lattice scale. Roughness, microstructure will be discribed on a lattice specimen, and topology effect on stress distribution will be numerically quantified. In order to understand the influence of these parameters, and identify the critical region for fatigue life, this work focuses on the local thin-wall scale. Here, the aim is to characterise the high cycle (HCF) fatigue heterogeneous response of Ti-6Al-4V thin-walls manufactured, characterising locally the HCF behaviour of a TPMS lattice structure ( $R=0.1$ ; uniaxial tension loading,  $N=1.10^6$ ,  $f=40\text{Hz}$ ).

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**Keywords:** Selective Laser Metling; Ti-6Al-4V; Lattices; HCF; roughness; microstructure; thin-wall

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## 1. Introduction

AM technology allows a considerable gain in part mass, in production costs, in functional performance and in realization compared to classical subtractive processes. The acquisition of knowledge on the mechanical properties of AM parts will allow to rethink the design and the manufacture of generic parts in the fields of medicine, automobile, aeronautics and space industry (Hannibal et al. , 2018).

Among the AM processes, Selective Laser Melting (SLM) allows to reach the special resolution requested for small scale structures, with high geometry quality manufacturing and of superior mechanical properties parts (Yuan et al. , 2019). However, a number of technological drawbacks limit the use of AM parts in a fatigue context. Although applying a Hot Isostatic Pression treatment limits the presence of pores, unmelted particules and residual stresses (Masuo et al. , 2017; Tammam-Williams et al. , 2017), surface roughness and geometrical imperfections, inherent to the process (Stef et al. , 2018), behave like notches where the stress concentration leads to an early crack initiation (Vayssette , 2020). The printing quality depends on many parameters such as heat density, laser path strategy (Speirs et al., 2017) and misorientation between normal to surface and BD (downskin/up-skin effect). Therefore, the characterisation of parameters influencing the fatigue behaviour is essential to validate their long-term use in load-bearing parts.

The development of light 3D-periodic structures named lattices, is directly linked with the AM booming. These architected structures are attracting increasing interest since a few years, achieving numerous excellent specific properties compared to fully dense materials. Their development opens up new perspectives of complex and multi-scale parts, introducing new material properties domains. Such structures are developed for biomedical implants (Yuan et al. , 2019; Attaran et al. , 2017; Dallogo et al. , 2019), lightweight structures for the transport (Gu et al. , 2021), heat exangers (Kaur et al. , 2021), catalyst for chemical use (Innocentini et al. , 2019), or energy absorption parts (Xiang et al. , 2019). Therefore, lattices are the subject of particular attention in the recent litterature.

Among all lattices, the gyroid sheet-lattice has recently been experimentally identified as the best candidate for high HCF resistance, showing a better HCF behaviour compared to conventional strut-lattices (Speirs et al., 2017; Bobbert et al., 2017; Refai et al., 2019). This behaviour is explain by its particular topology, allowing a good manufacturing quality (Bobbert et al., 2017), minimizing stress concentrations (Yang et al. , 2019; Bobbert et al., 2017; Refai , 2020; Yang et al. , 2019).

This work investigates at first the parameters causing an heterogeneous HCF behaviour within the Ti-6Al-4V gyroid thin-wall (TWL) lattice, manufactured by Selective Laser Melting, and post-treated by HIP. Besides, a FEM numerical approach is developed to predict the multiaxial stress field of the structure under loading. A fatigue post-computation of these result allows to predict fatigue critical areas using a local multi-axial fatigue criterion. Having HCF influence parameters indentified at the lattice scale, this work aims as a second step to characterize the HCF behaviour heterogeneity of non-architected thin-walls specimens (TWS) describing the local behaviour over the lattice unit cell, and thus demonstrating the anisotropy of TWL.

## 2. Material and Method

### 2.1. Samples conception

#### 2.1.1. Gyroid thin-wall lattices

The mathematical approximation (eq. 1) describes the gyroid TPMS, with  $x, y, z$  the coordinate points,  $A$  the scale factor to control cell periodicity defined as  $A = \frac{2*\pi}{L}$  and  $L$  the dimension of the unit cell. Its deviation from the exact formulation is minimal compared to the SLM printing quality. No classical computer-aided design software allow to generate the parametric surfaces defined by an implicit equation. Hence, the cells were created by generating two surfaces with the contour3D function of the pyhton's mayavi2 package. Therefore, equation 1 is modified adding a thickness parameter  $e$  equals to 300 $\mu$ m (eq. 2). Surfaces are created over  $(n_x.L, n_y.L, n_z.L)$  domain with  $(n_x, n_y$

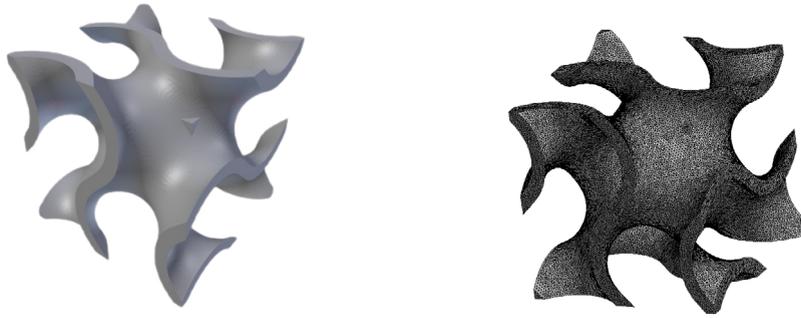


Fig. 1: Gyroid sheet lattice unit cell (4\*4\*4mm) and its mesh.

,  $n_z$ ) = (1, 1, 1) for a gyroid TWL unit cell. Finally, the closure of volume is carried out with Materialize MAGICS (fig. 1).

$$\cos(A.x).sin(A.y) + \cos(A.y).sin(A.z) + \cos(A.z).sin(A.x) = 0 \tag{1}$$

$$\cos(A.x).sin(A.y) + \cos(A.y).sin(A.z) + \cos(A.z).sin(A.x) \pm \frac{e}{2} = 0 \tag{2}$$

2.1.2. Thin-wall specimens

Tubular thin-wall specimens are manufactured to characterize the local anisotropic behaviour of the gyroid TWL. Because of their tubular geometry, the TWS do not follow the classical standards HCF samples geometry (fig. 2). The stress concentration coefficient  $K_t$  is estimated by FEA. In this study, two parameters of influence are investigated : thickness ( $e=\{300, 500\}\mu\text{m}$ ) and TWS orientation with respect to the SLM plate ( $\theta=\{90, 45\}^\circ$ ).

2.2. Additive manufacturing and post-processing

TWL and TWS are manufactured by SLM on the SLM-280-HL machine (titanium plate, argon atmosphere, Ti-6Al-4V standard strategy), using Ti-6Al-4V ELI (grade 23) powder with a particle diameter of 20-63 $\mu\text{m}$  (SLM Solution) and a chemistry according to ASTM B348/F136 (tab. 1). The SLM as-build (AB) surface aspect is conserved.

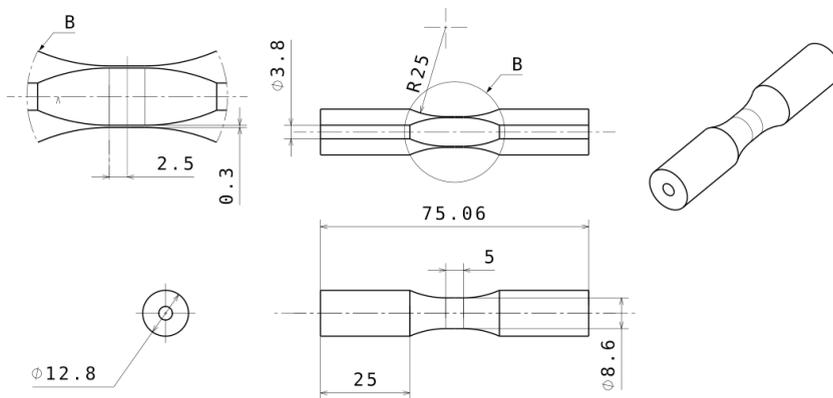


Fig. 2: Geometry and dimension of thin-wall specimens.

Table 1: Ti-6Al-4V ELI chemical composition.

Element	Al	V	Fe	C	N	O	H	Ti	Total Other
wt[%]	6,47	3,9	0,22	0,02	0,01	0,09	0,0017	Base	<0,4

All samples were post-processed by Hot Isostatic Pressing (HIP) at 920°C, under 1020MPa, during 2 hours (argon atmosphere) to enhance mechanical properties (microstructure, internal pores closure, release of residual stress). The effectiveness of HIP on thin-wall lattices has been verified by micro-tomography RX.

### 2.3. HCF testing

TWS were tested in uniaxial tension (R=0,1) up to failure. Fatigue tests were conducted on hydraulic fatigue machine (MTS), with load control, using a sinusoidal waveframe at a frequency of 40Hz, at room temperature and air. Short staircase tests were performed before completing the Whöler curve. For confidentiality reasons, all results are normalised by an arbitrary value

### 2.4. HCF numerical simulations

To characterise the stress field, a FEM calculation is conducted using Zebulon code (ONERA-Mines Paris) considering a gyroid TWL unit cell (2 249 392 elements). Its behaviour is assumed to be strictly elastic isotrop with  $E = 110$  GPA and  $\nu = 0.34$ . Periodic limit conditions are imposed, and the uniaxial tension load along Z equals to the experimental fatigue life of gyroid lattices (uniaxial tension, R=0.1, N=1.10<sup>6</sup> cycles,  $\sigma_d = 23.4$ MPa). A fatigue post-computation of these result allows to predict critical areas. A local multi-axial fatigue criterion (Crossland) is chosen to consider the fatigue stress field heterogeneity (eq. 3). Fatigue coefficients result from a previous work on as-build bulk Ti-6Al-4V SLM HIPed specimens Vayssette (2020), and are from HCF fully reverse traction/compression and torsion experiments ( $\alpha = 0.707$  and  $\beta = 195.2$ MPa). As HCF results, numerical results are normalised by the same arbitrary value.

$$FIP_{CR} = \tau_{oct,a}(M) + \sigma_{H,max}(M) \leq \beta \quad (3)$$

$$\sqrt{J_{2,a}} = \max_{t \in T} \|\underline{S}(t) - \underline{S}_m\| = \max_{t \in T} \sqrt{\frac{1}{2} [\underline{S}(t) - \underline{S}_m] : [\underline{S}(t) - \underline{S}_m]} \quad (4)$$

$$\underline{S}_m = \min_{t \in T} \left( \max_{t \in T} \|\underline{S}(t) - \underline{S}'\| \right) \quad (5)$$

$$\sigma_{H,max} = \max_{t \in T} \left[ \frac{1}{3} tr(\underline{\sigma}(M, t)) \right] \quad (6)$$

## 3. HCF influence parameters for lattice structures

### 3.1. Surface roughness

Surface roughness is observed with 2D optical analysis on the X-BD section of embedded TWL lattice samples (fig. 3). Although the gyroid TWL topology allows a good printing quality (well self-supported), a high variability in printing quality is still observed. Here, 90° and of 45°-oriented wall presents two rugosity severities. Considering a lattice thickness of 310-330µm, the down-skin effet on 45°-oriented walls creates highly severe surface defects of 70µm depth and 30µm large wheareas the up-skin effet creates a very good surface aspect on these same walls . Walls oriented at  $\theta=90^\circ$  present some partially melted particules but no large surface defects.

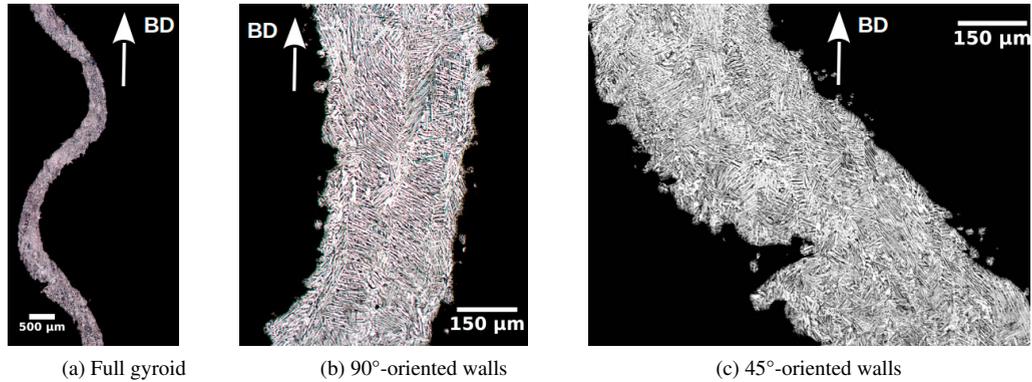


Fig. 3: Surface roughness observation on a vertical (X-BD) gyroid lattice slice (Ti-6Al-4V, SLM, HIP). Zoom in (b) vertical and (c) 45°-oriented thin-walls.

### 3.2. Microstructure

Image post-processing using OrientationJ analysis plugin (ImageJ) are undertaken to distinguish the microstructures features (fig. 4). TWL presents a Widmanstätten microstructure, typical for HIPed Ti-6Al-4V manufactured by SLM, as shown figure 3. The latter presents colonar lamellar colonies oriented along the BD. Walls close to the 90° orientation present large elongated colonies, up to 120μm large and 300μm high, oriented along the wall plane (long axis parallel to the local surface). In comparison, walls oriented around 45° present thinner (~50μm) and smaller (~100μm) columnar colonies. In this configuration, thermal gradients grain growth oriented along BD results in smaller lamellar colonies which long axis is no longer align with the wall plane. This elongated shape and the strong difference in colony size between surface volume and core volume are created with high thermal gradient along the BD direction, resulting in epitaxial growth.

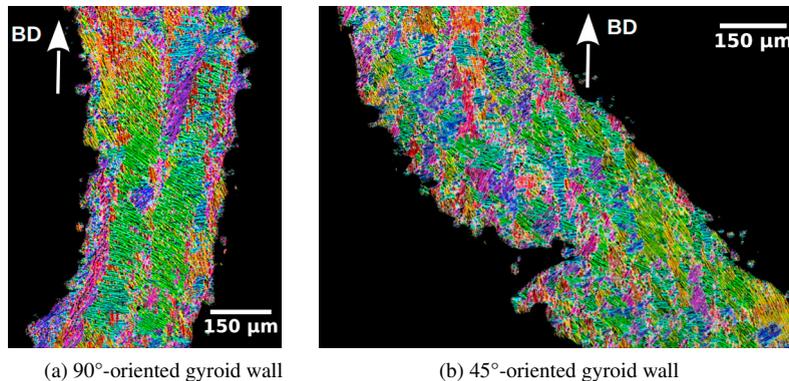


Fig. 4: Microstructure observation on a vertical (X-BD) gyroid lattice slice (Ti-6Al-4V, SLM, HIP). The applied colourisation is based on lamelas orientation Zoom in (a) vertical and (b) 45°-oriented thin-walls.

### 3.3. Topology and stress field heterogeneity

The gyroid FEM results show an important structure effect as normalised Crossland FIP  $FIP_{CR,norm}$  (eq. 3) presents an important heterogeneous stress distribution. Highly Stressed Volumes (HSV) allow a better understanding of FIP distribution (tab. 2). For instance, V90 correspond to the volume of elements where  $FIP_{CR,norm} \geq 0.9 \times FIP_{CR,norm}^{max}$ ,  $FIP_{CR,norm}^{max}$  corresponding to the maximal normalised FIP over the TWF. Therefore, a large

part of the TWL volume undertake a load lower than V30 (37.39%), whereas a smaller volume undertake high loads (V70=11.43%, V90 = 0.64%).

Table 2: Highly Stressed Volumes (HSV) and their associated normalised stress. V90 correspond to the volume of elements where  $FIP_{CR,norm} \geq 0.9 \times FIP_{CR,norm}^{max}$ .

HSV	V90	V80	V70	V60	V50	V40	V30	V20	V10	V00
$FIP_{CR,norm}$	1.808	1.608	1.405	1.205	1.004	0.803	0.603	0.402	0.201	0.0
Volume[%]	0.64	3.88	11.43	24.46	36.45	48.09	62.61	75.48	90.30	100.0

The  $FIP_{CR,norm}$  distribution analysis is completed with  $FIP_{CR,norm}$  fields description. HSV is localised on lattice walls orientated along the loading axis (Z). Low stressed volumes are larger compared to high stressed volumes (V00-V60=75.54%), and localised in horizontal walls ( $0^\circ$ -oriented walls).

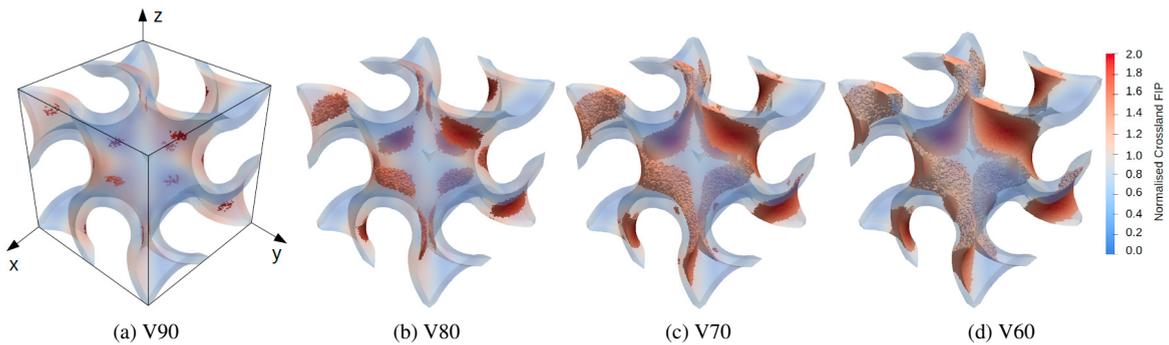


Fig. 5: Decomposition of the normalised Crossland FIP field in a gyroid thin-wall-lattice unit cell loaded along Z axis.

### 3.4. Discussion

We expect microstructure and surface roughness variation in gyroid TWL to present an important mechanical heterogeneity and anisotropy of HCF behaviour. Regarding the rugosity effect only, low fatigue resistance regions have been identified in misoriented walls regarding the BD. Nevertheless, the complex topology of lattices induces a highly heterogeneous loading of the TWL structure resulting in high stressed volumes localised in  $90^\circ$ -oriented walls along the load direction. Hence, the fatigue behaviour at the local scale is driven by the competition between surface roughness and microstructure, both having an anisotropic and heterogeneous character at the scale of the lattice VER. Therefore, it is difficult to fully understand HCF crack initiation mechanisms at the scale of the TWL. Consequently, this work investigates the heterogeneity of non-architected thin-wall specimens describing local behaviour over the gyroid structure.

## 4. HCF of thin-walls

### 4.1. Effect of thickness

The thickness effect on TWS fatigue resistance is revealed comparing TWS HCF life (uniaxial tension,  $1.10^6$ ,  $R=0.1$ ) for one orientation ( $90^\circ$ ) and one surface state (as-build) (tab. 3). Increasing the thickness of  $90^\circ$ -oriented TWS results in a decrease (-22%) of the HCF limit. In addition, while  $500\mu\text{m}-90^\circ\text{-AB}$  TWS presents a behaviour comparable to bulk behaviour,  $300\mu\text{m}-90^\circ\text{-AB}$  TWS shows a different behaviour displaying two sets of points (fig. 6): one set of sample without failure ( $N=1.0^6$  cycles) and the other set of samples which rupture occurred around 100 000 cycles, on a wide range of normalised stresses [2,80 - 3,27].

Table 3: Thin-wall high cycle fatigue limits ( $R=0.1$ ,  $N=1.10^6$  cycles).

Thickness	$\theta=90^\circ$	$\theta=45^\circ$
300 $\mu\text{m}$	$\beta_{norm} = 2.884$	$\beta_{norm} = 1.770$
500 $\mu\text{m}$	$\beta_{norm} = 2.397$	-
Bulk	$\beta_{norm} = 2.050$	-

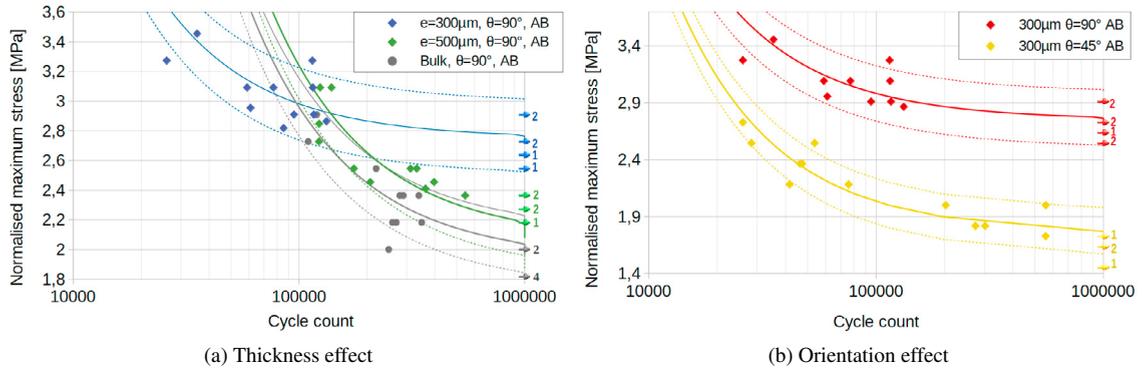


Fig. 6: Thin-wall samples whöler curves (Ti-6Al-4V, SLM, HIP, as-built).

#### 4.2. Effet of orientation

The effect of TWS orientation on their fatigue resistance is highlighted comparing HCF behaviour with one thicknesses (300 $\mu\text{m}$ ) and one surface state (as-built) (fig. 6). The 45 $^\circ$ -misorientation between TWS axis and BD results in a decrease of HCF life limit (-39%). Although the whöler curve for TWS with  $\theta=45^\circ$  keep the same tendency as 90 $^\circ$ -oriented TWS, the gap between 100 000 cycles  $1.10^6$  cycles in 300 $\mu\text{m}$ -90 $^\circ$ -AB results is no longer observed.

### 5. Discussion

- The drastic difference in HCF behaviour between 90 $^\circ$ -oriented 300 $\mu\text{m}$  and 500 $\mu\text{m}$  TWS can be explained by understanding crack initiation and propagation mechanisms in Ti-6Al-4V TWS. It is known that crack initiation in lamellar Ti-6Al-4V occurs preferentially in between lamellas or at colonies boundaries. Moreover, crack initiation in bulk materials takes places at the specimen surface or sub-surface. Later, the specimen microstructure influences the very first steps of crack propagation : fine microstructure corresponding to numerous propagation obstacles results in a slower crack propagation. Considering the microstructures highlighted in figure 7, the 300 $\mu\text{m}$  TWS presents large colonies compared to its wall thickness, locally reaching over 200 $\mu\text{m}$  width. At variance, the 500 $\mu\text{m}$  TWS exhibits thinner colonies under 60 $\mu\text{m}$  width, imposing a higher amount of structural barriers on crack propagation. Consequently, the fatigue behaviour of the 500 $\mu\text{m}$ -90 $^\circ$ -AB TWS approaches the one of bulk behaviour. On the contrary, the 300 $\mu\text{m}$ -90 $^\circ$ -AB TWS might present a colony that locally cross over the wall thickness, without important structural barrier, explaining its particular HCF behaviour.
- Fatigue life is highly dependent on the presence of defects. High stress concentration at large surface defects causes a severe drop of HCF limit. This is emphasised by the TWS scale effect : the introduction of large defects compared to the low thickness can have an important detrimental influence on the FIP field distribution across the wall, resulting in a premature crack initiation.
- Although numerical simulations identified 90 $^\circ$ -oriented regions as the most detrimental areas for HCF behaviour in TWL, the FEM calculation only takes one set of parameters into account, applying on the entire structure those of bulk material vertically manufactured. Thus, to complete the analysis, the calculated nor-

malised fatigue limits  $\beta_{norm}$  (tab. 3) are compared to Crossland FIP average  $\overline{FIP}_{(CR,norm)}$ , calculated on 90° and 45°-oriented walls in the TWS over 10% volume of the unit cell. The calculated ratios  $\frac{\overline{FIP}_{(CR,norm)}^{90}}{\beta_{norm}^{90}} = 1.81$  and  $\frac{\overline{FIP}_{(CR,norm)}^{45}}{\beta_{norm}^{45}} = 1.91$  present a very low difference, indicating that both 90° and 45°-orientated walls in TWL can be defined as critical region for fatigue behaviour.

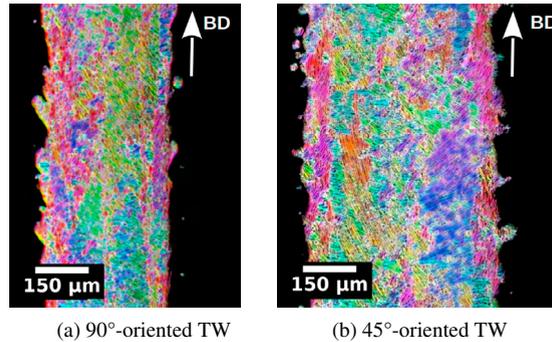


Fig. 7: Microstructure observation of vertical thin-walls (a) 300µm and (b) 500µm (Ti-6Al-4V, HIP, as-built).

## 6. Conclusion and prospects

HCF tests conducted on non-architected thin-walls specimens highlight a very specific fatigue behaviour strongly influenced by wall thickness as well as wall orientation regarding the build direction, resulting in a variation up to 30% of the fatigue limit. The comparison between the distribution of Crossland fatigue indicator parameter within the lattice and the non-architected thin-walls fatigue limits ( $\theta=90,45^\circ$ ,  $e=300\mu\text{m}$ ) clearly demonstrated that roughness and FIP distribution effects are in real competition. This results in a large critical volume for fatigue resistance covering 90° and 45° oriented regions (case of uniaxial loading along BD).

Surface roughness is probably the strongest material parameter of influence on fatigue life behaviour. Consequently, notch defect shadows all other effects. To minimise stress concentration sites, a surface treatment will be applied to suppress high  $K_t$  sites, and hence evaluate the microstructure effect and gradient effect only. Machining is not possible on complex structures, neither on tubular thin-wall specimens. Therefore, a chemical polishing will be applied.

Also, it has been demonstrated that stress gradient enhances fatigue life resistance. The complex topology of thin-wall lattices introduces by nature a high stress gradient within the small thickness of its walls. Gradient localisation and the characterisation of their effect on HCF allow a better description of the loading complexity and fatigue response.

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