

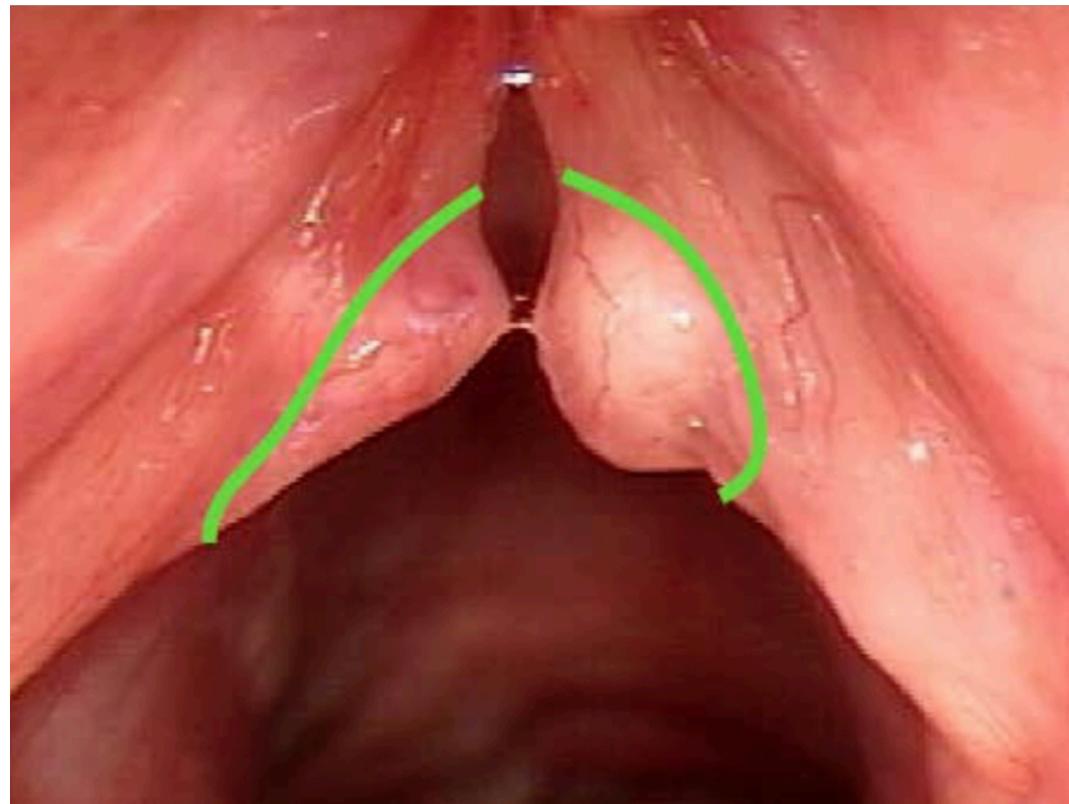
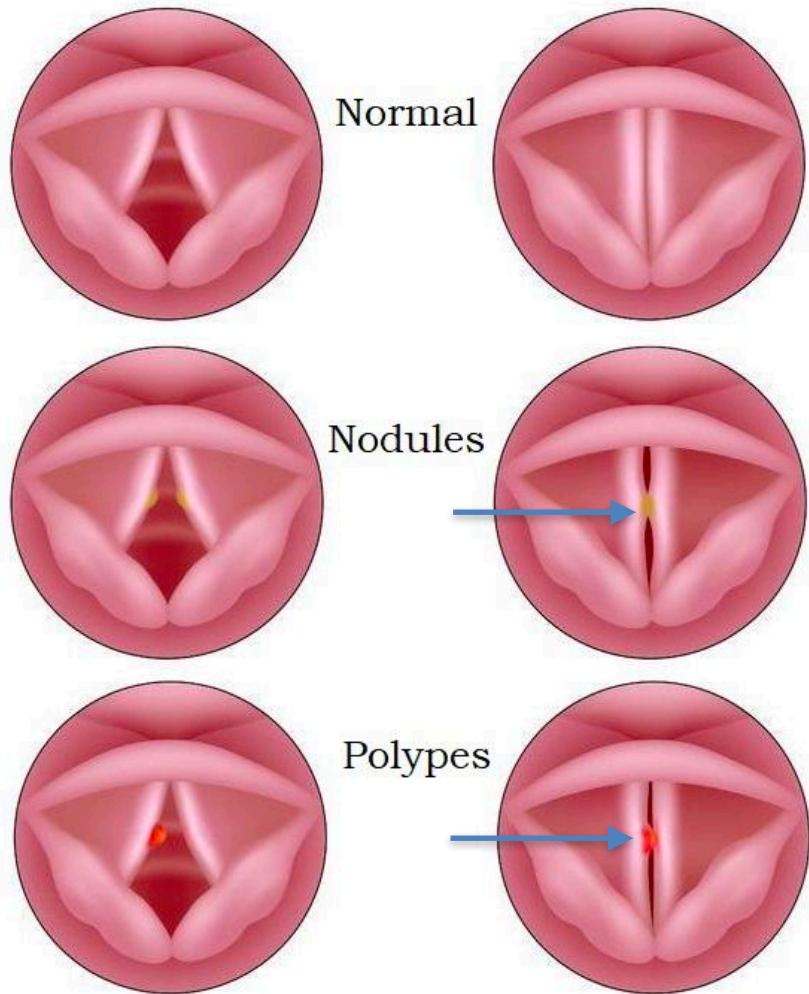


Laser surgery devices and control schemes

Brahim TAMADAZTE, FEMTO-ST/CNRS

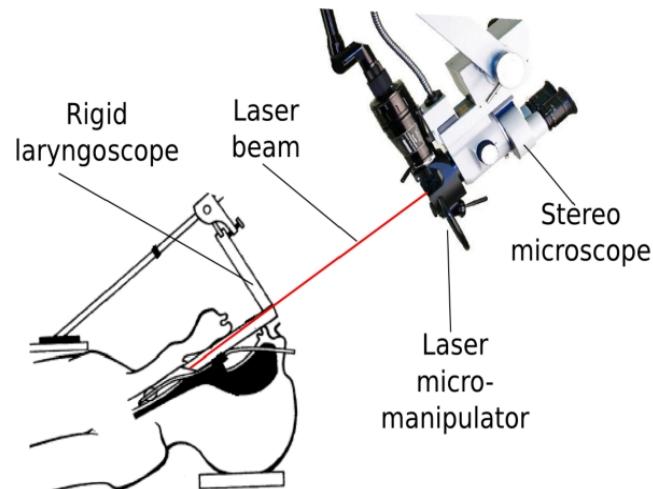
Helsinki, July, 1-5th, 2019

Clinical context





The AcuBlade system



Designed system

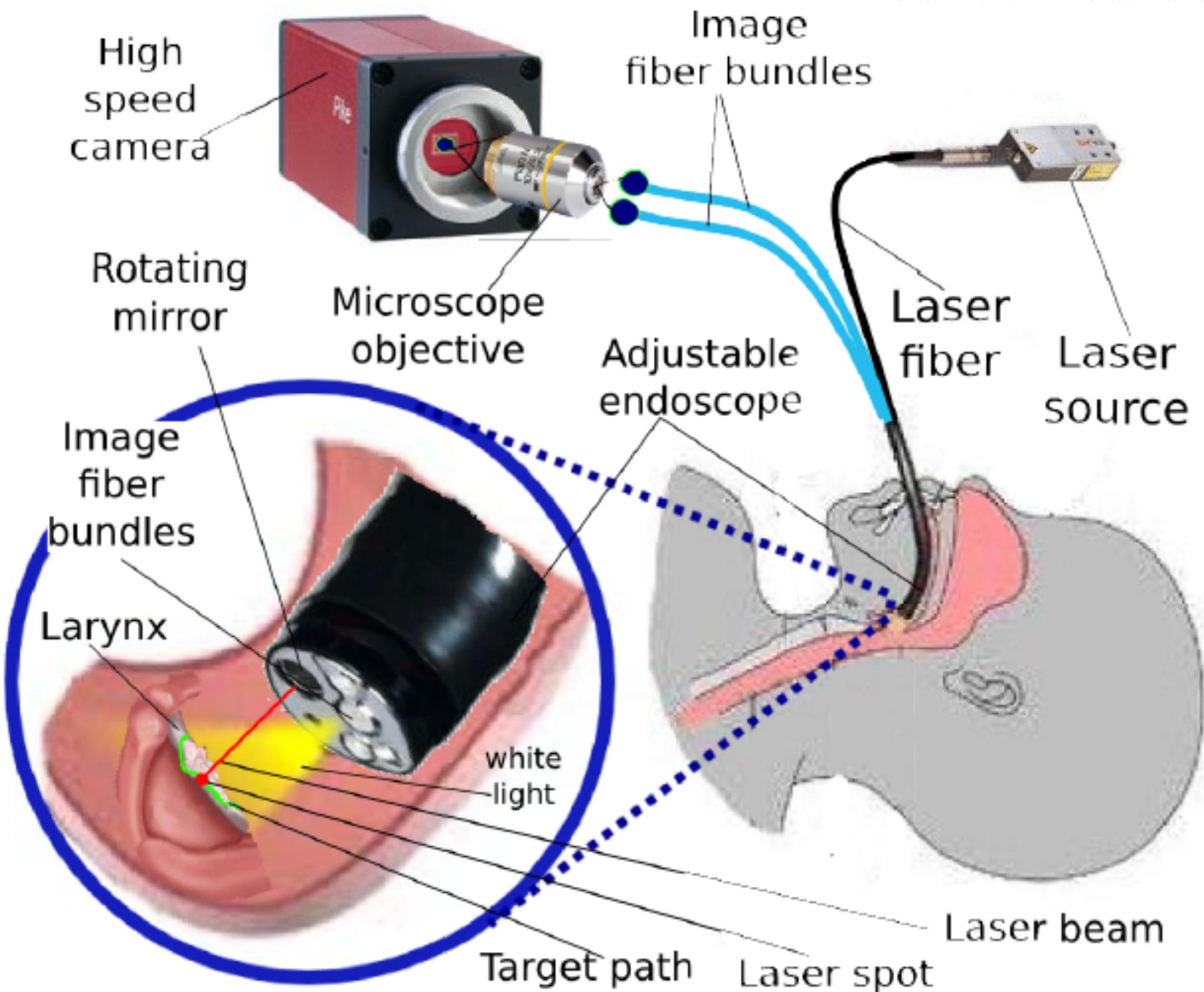


uRALP - EU-project (2012-2015)

- IIT Genova (IT),
- FEMTO-ST (FR),
- LUH Hannover (GE),
- CHRUB (FR),
- UNIGE (IT)



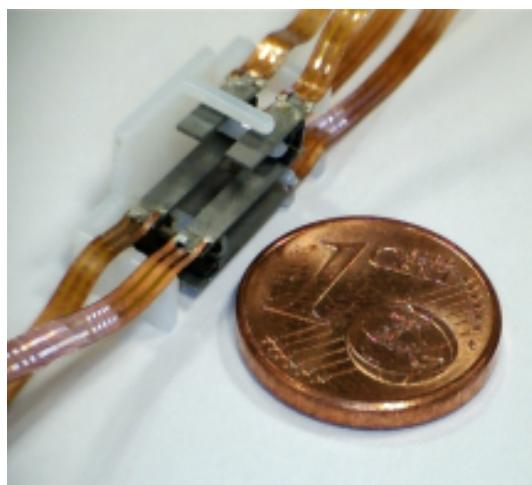
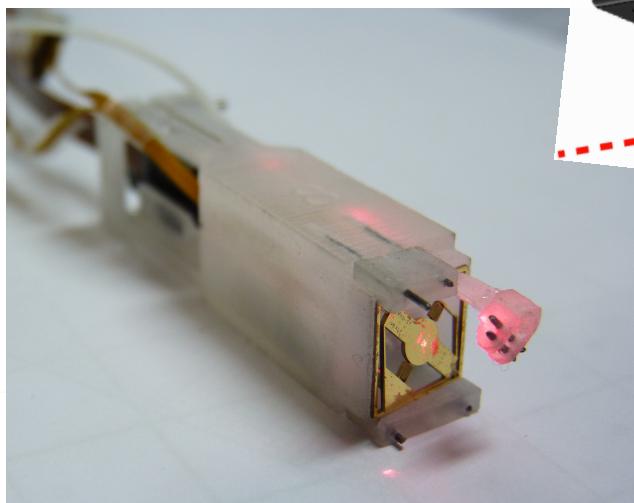
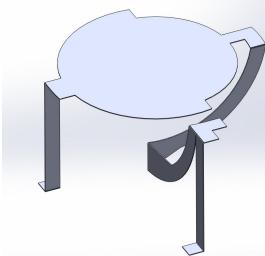
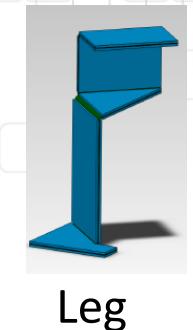
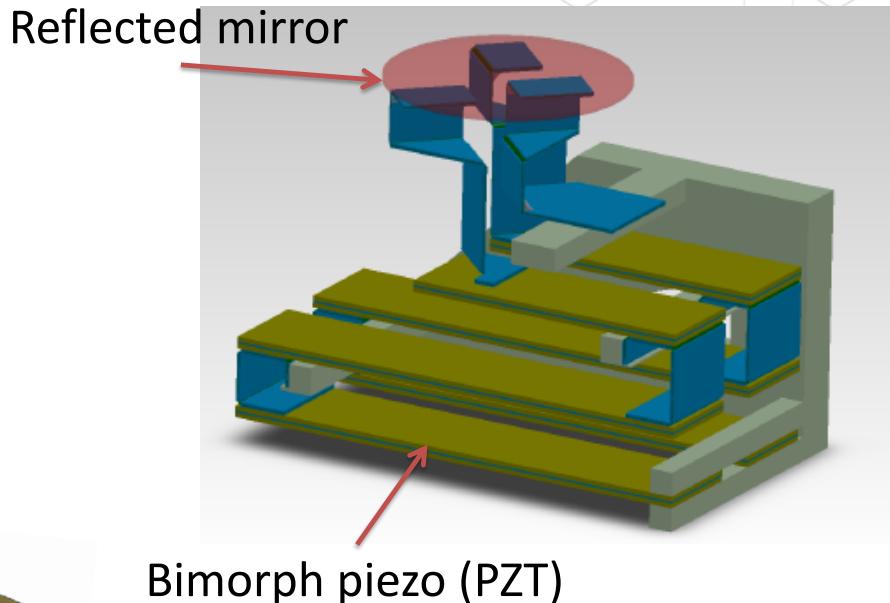
Designed system



laser beam steering mirror (microrobot)

Requirements:

- High precision and repeatability
- High speed (>400 Hz)
- Low Hysteresis
- Only few millimeters of size
- High deformation range
- Ergonomic, user-friendly

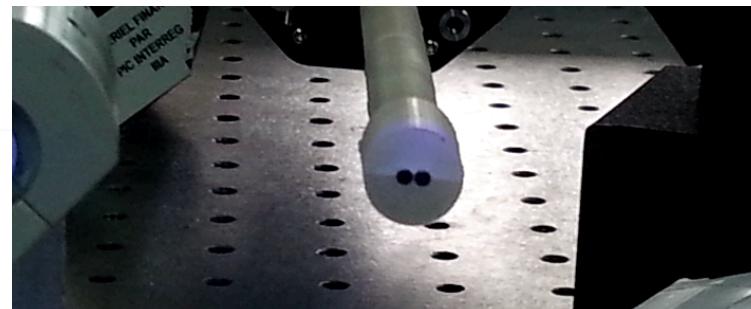
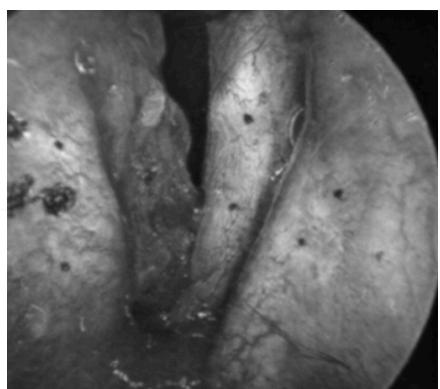
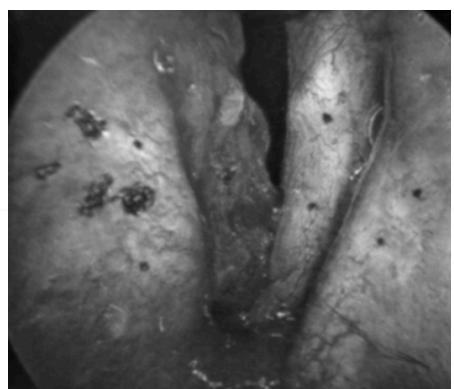
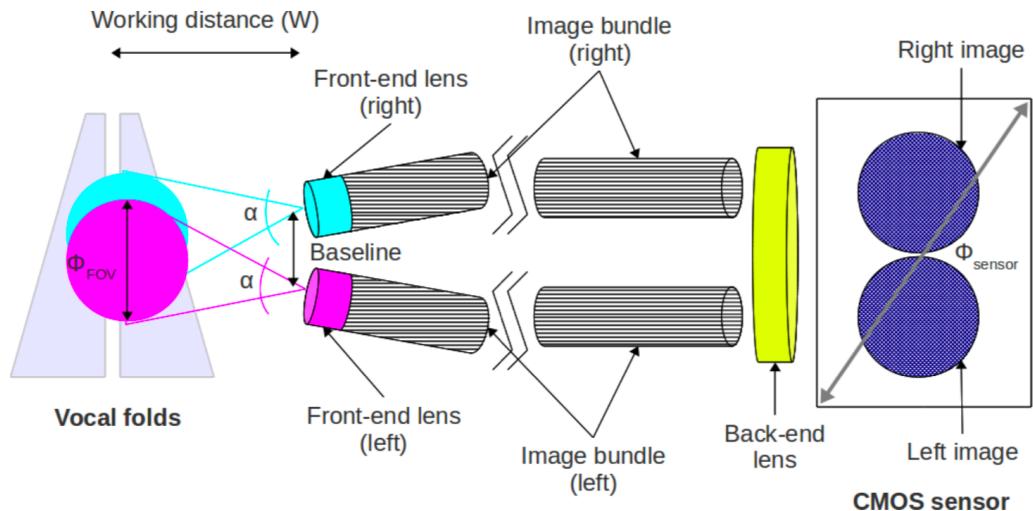


high-speed stereo vision system



Requirements:

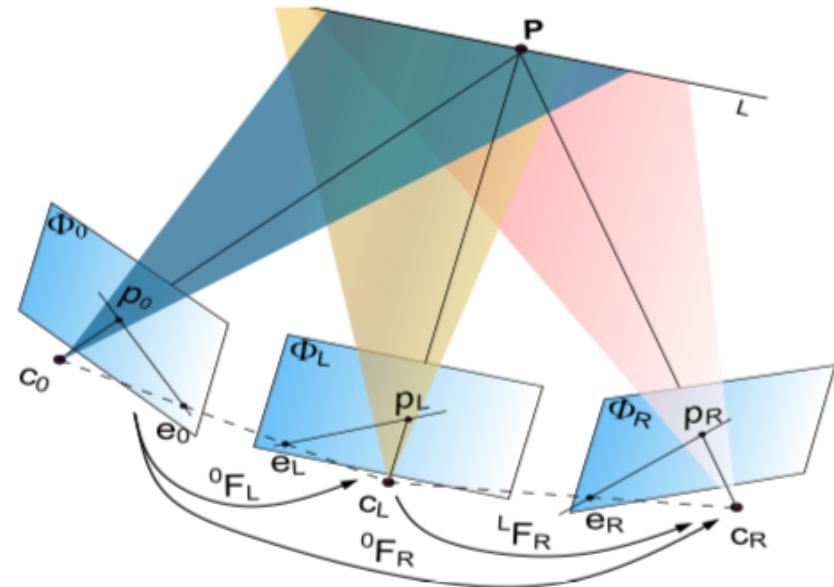
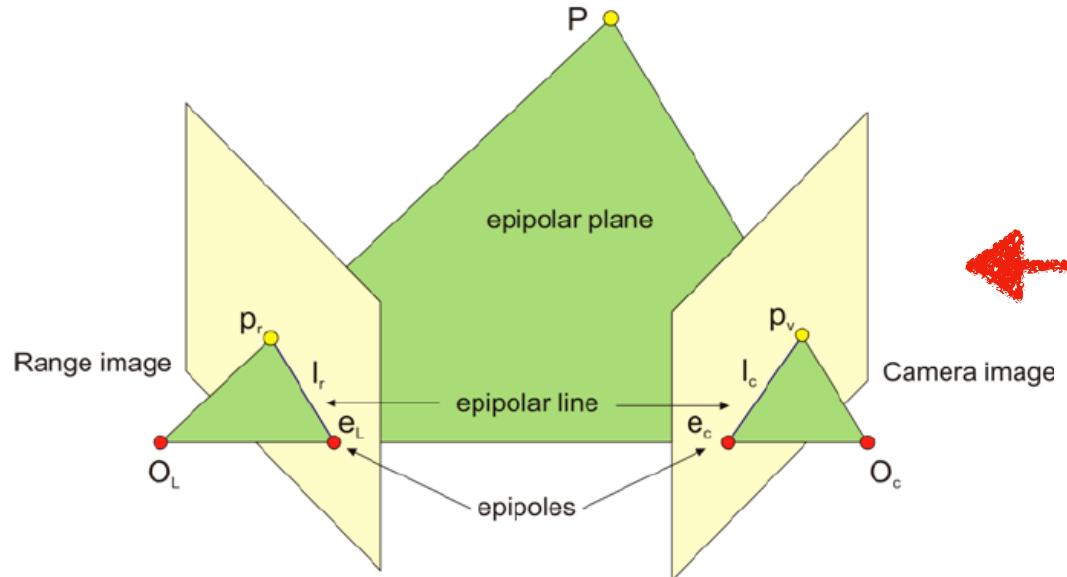
- High speed (>400 Hz)
- High sensitivity and good signal noise ratio
- 2 ou 3 millimeters of diameter



Designed system



Laser beam steering (vision-based control)



Duality between points and lines

$$\tilde{p}_L^\top {}^L \mathbf{F}_R \tilde{p}_R = 0$$

- fundamental matrix
- epipolar points
- epipolar plane

Relationship between different image-points

$$\tilde{p}_0^\top {}^0 \mathbf{F}_L \tilde{p}_L = 0$$

$$\tilde{p}_L^\top {}^L \mathbf{F}_R \tilde{p}_R = 0$$

$$\tilde{p}_0^\top {}^0 \mathbf{F}_R \tilde{p}_R^\top = 0$$

Traditional trifocal constraint

$$[\tilde{p}_L] \times \left(\sum_{i=1}^3 \tilde{p}_i \mathbf{T}_i \right) [\tilde{p}_R] \times = 0_{3 \times 3}$$

(Hartley & Zisserman, 2004)

Laser beam steering (vision-based control)

- The laser beam direction ${}^0\underline{z}$
is geometrically equivalent to the point \tilde{p}_0

$$\tilde{p}_0^\top {}^0\mathbf{F}_L \tilde{p}_L = 0$$

$$\tilde{p}_L^\top {}^L\mathbf{F}_R \tilde{p}_R = 0$$

$$\tilde{p}_L^\top {}^L\mathbf{F}_R \tilde{p}_R = 0$$

$${}^0\underline{z}^\top {}^0\mathbf{F}_R \tilde{p}_R = 0$$

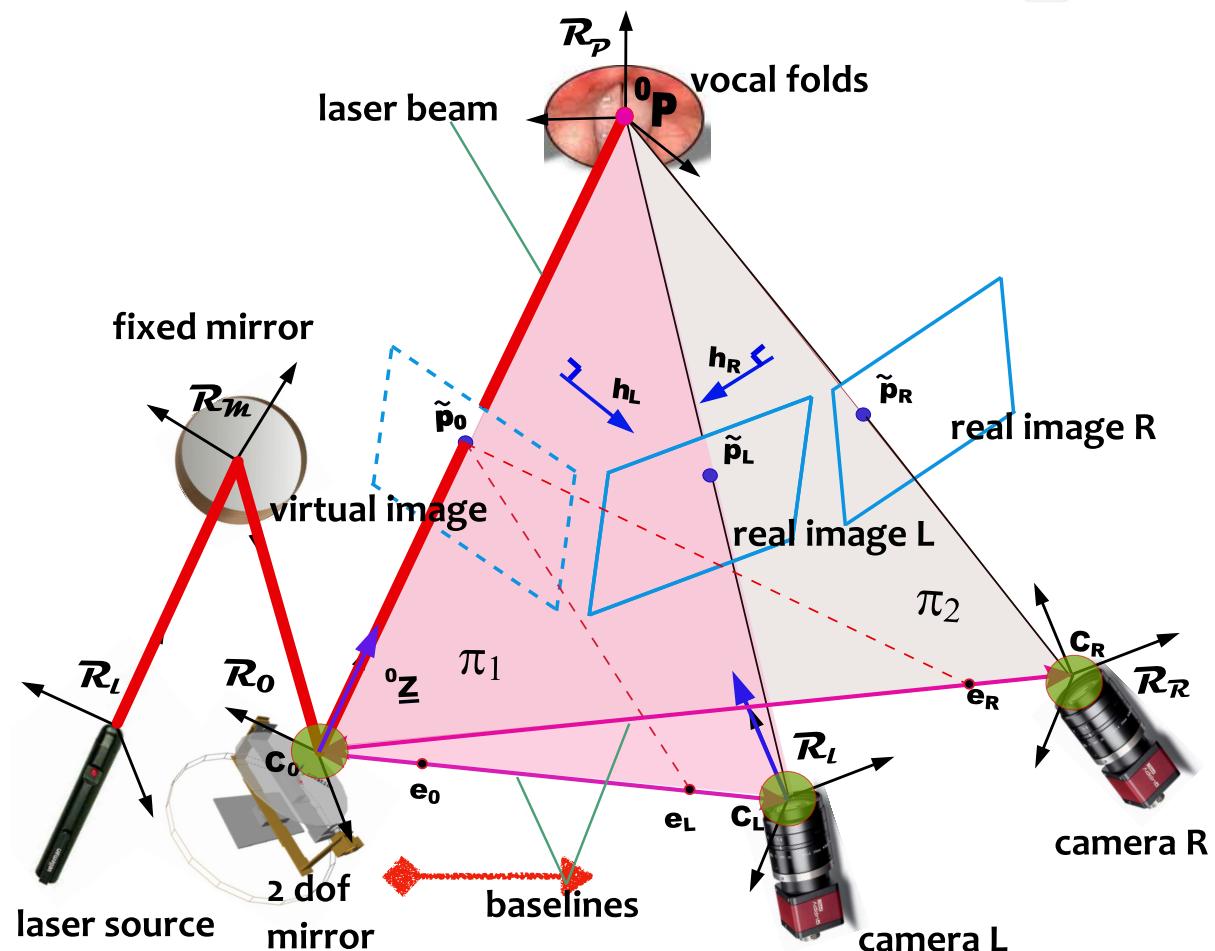
$$\tilde{p}_0^\top {}^0\mathbf{F}_R \tilde{p}_R^\top = 0$$

$${}^0\underline{z}^\top {}^0\mathbf{F}_L \tilde{p}_L = 0$$

$${}^0\underline{z} \times (h_R \times h_L) = 0$$

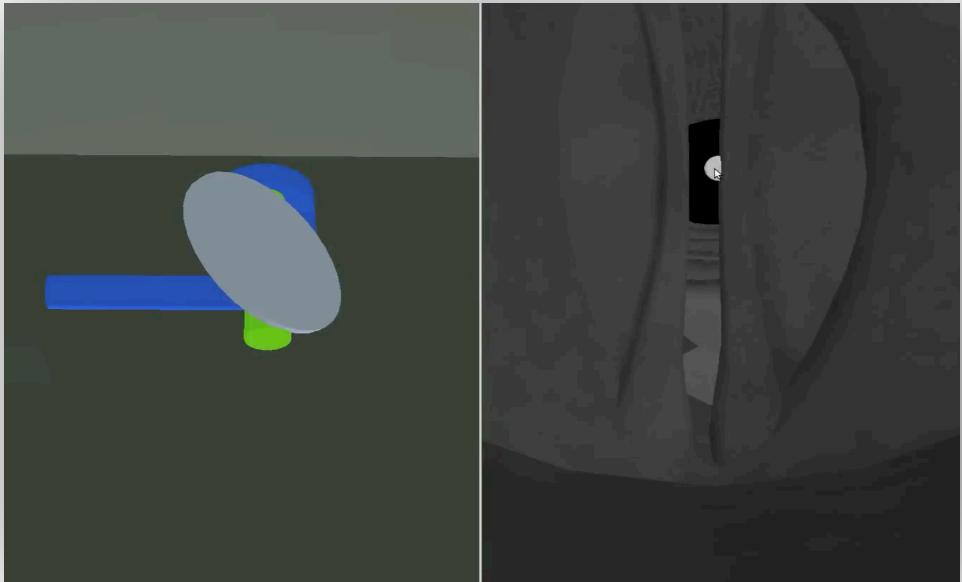
$${}^0\underline{z} \times ({}^0\mathbf{F}_R \tilde{p}_R \times {}^0\mathbf{F}_L \tilde{p}_L) = 0$$

$$\begin{cases} h_L = {}^0\mathbf{F}_L \tilde{p}_L \\ h_R = {}^0\mathbf{F}_R \tilde{p}_R \end{cases}$$



Control law: $\omega = \lambda \frac{\mathbf{h}_R \times \mathbf{h}_L}{\|\mathbf{h}_R \times \mathbf{h}_L\|^2} \times \left(\mathbf{h}_L \times ({}^0\mathbf{F}_R(\tilde{p}_r - \tilde{p}_R^*)) - \mathbf{h}_R \times ({}^0\mathbf{F}_L(\tilde{p}_l - \tilde{p}_L^*)) \right)$

Laser beam steering (vision-based control)



- No precise calibration (e.g., mirror/camera)
- High accuracy (<50 micrometers)
- High frequency
- Easy to implement (20 lines of code (C++))
- Implicit depth estimation



Laser Steering using Virtual Trifocal Visual Servoing

N. Andreff and B. Tamadazte

FEMTO-ST Institute, 25000, Besançon, France

"Validation on a 2D target"

Multimedia Extension #2

International Journal of Robotics Research

Laser Steering using Virtual Trifocal Visual Servoing

N. Andreff and B. Tamadazte

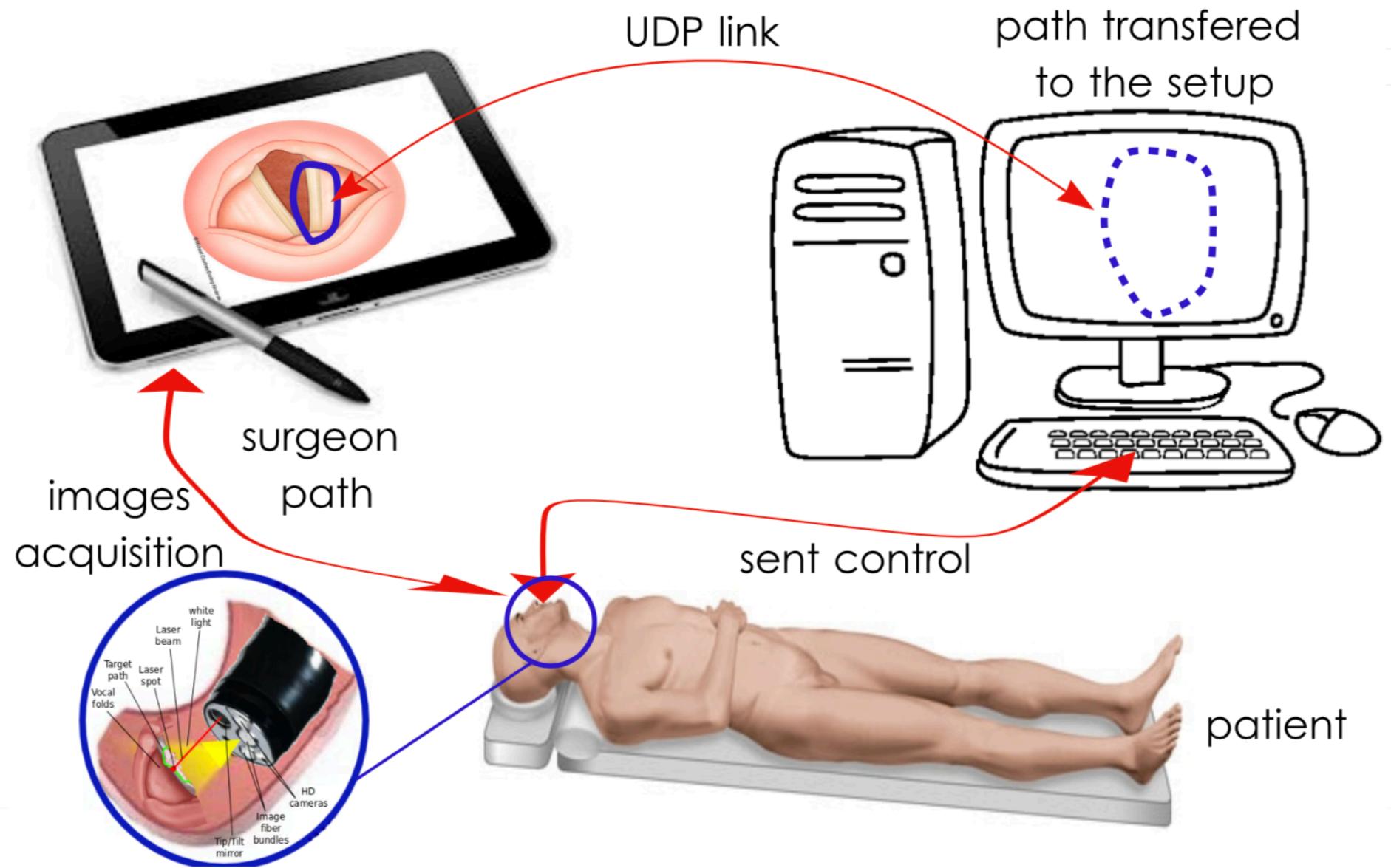
FEMTO-ST Institute, 25000, Besançon, France

"Validation on a 3D target"

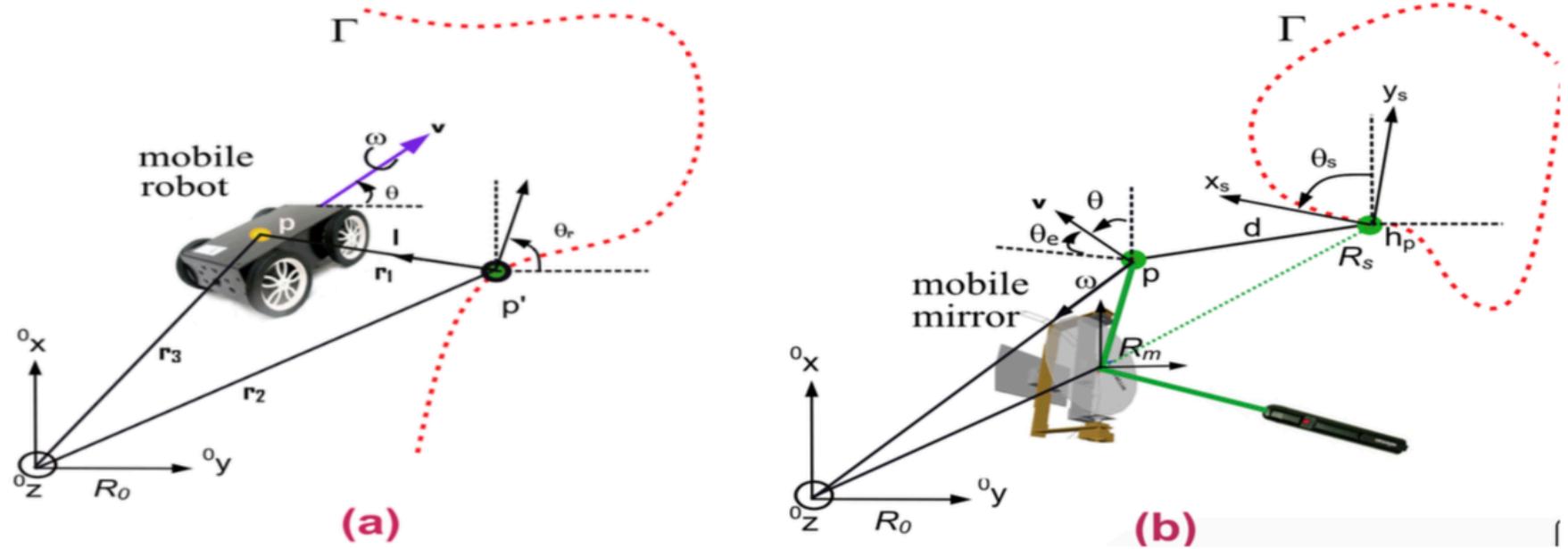
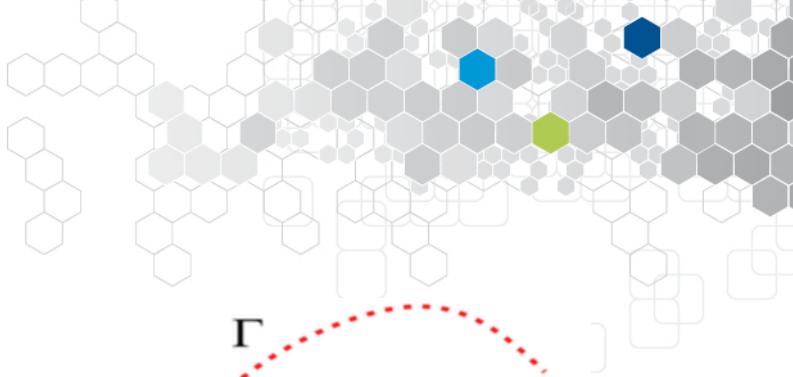
Multimedia Extension #3

International Journal of Robotics Research

Laser beam steering (vision-based control)



Laser beam steering (vision-based control)



(Morin & Samson, 2006)

$$\dot{x} = v \cos \theta$$

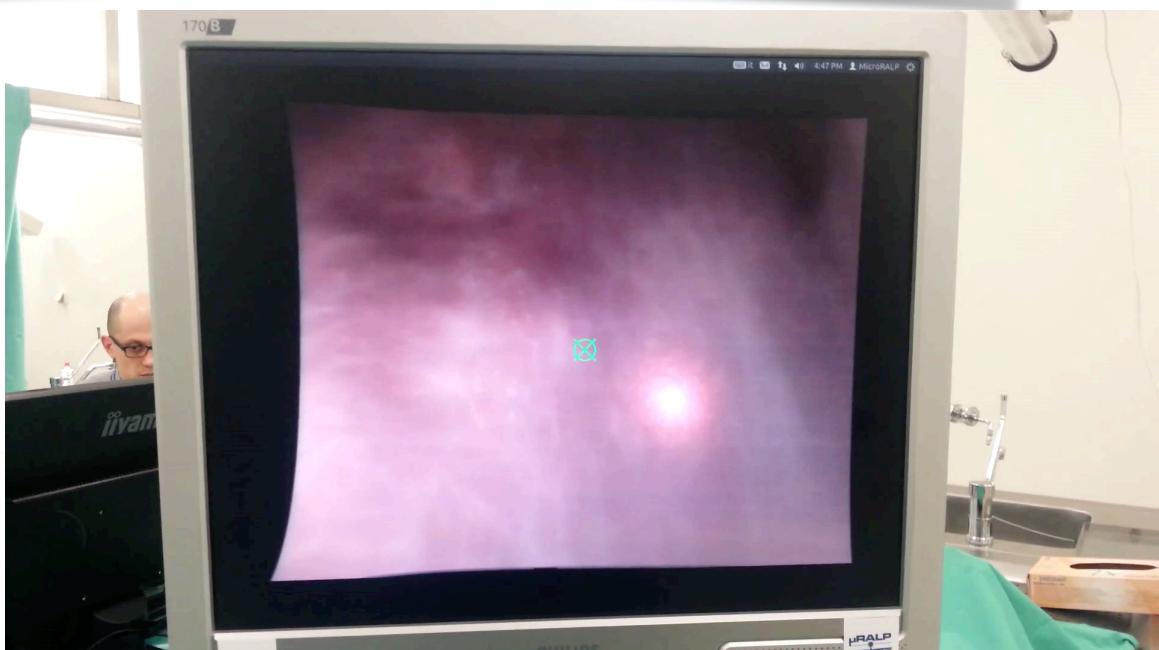
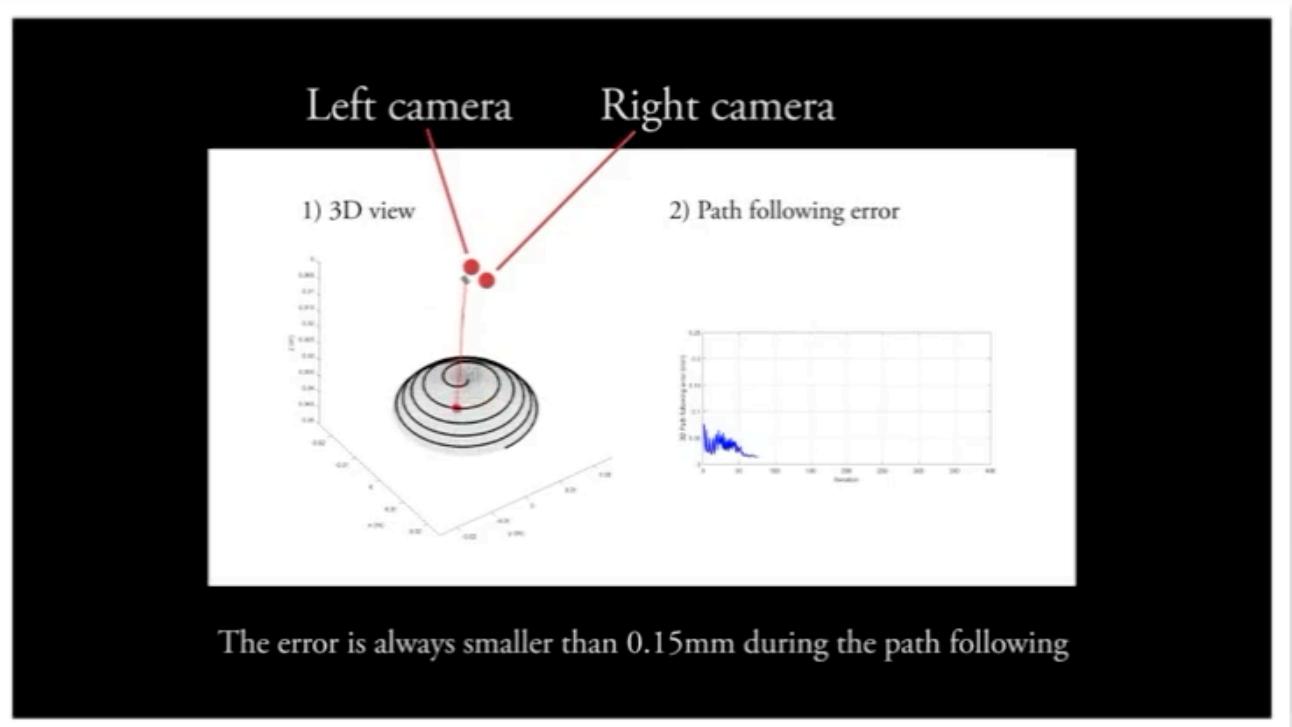
$$\dot{y} = v \sin \theta$$

$$\dot{\theta} = \omega$$

$$\omega = \frac{u_2 + \left(dC(s) + d\frac{\partial C(s)}{\partial s} \dot{s} \right) \tan \theta_e}{\left(1 - dC(s) \right) \left(1 + \tan^2 \theta_e \right)} + \dot{s}C(s)$$

$$\underline{\mathbf{v}}_{k+1} = \frac{\underline{\mathbf{v}}_k + \omega^0 \underline{\mathbf{z}} \times \underline{\mathbf{v}}_k}{\| \underline{\mathbf{v}}_k + \omega^0 \underline{\mathbf{z}} \times \underline{\mathbf{v}}_k \|}$$

Laser beam steering (vision-based control)





Besançon



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