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# Soft-wall induced structure and dynamics of partially confined supercritical fluids

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### ABSTRACT

The interplay between the structure and dynamics of partially confined Lennard Jones (LJ) fluids, deep into the supercritical phase, is studied over a wide range of densities in the context of the Frenkel line (FL), which separates rigid liquidlike and non-rigid gaslike regimes in the phase diagram of the supercritical fluids. Extensive molecular dynamics simulations carried out at the two ends of the FL (P = 5000 bars, T = 300 K, and T = 1500 K) reveal intriguing features in supercritical fluids as a function of stiffness of the partially confining atomistic walls. The liquidlike regime of a LJ fluid (P = 5000 bars, T = 300 K), mimicking argon, partially confined between walls separated by 10 Å along the z-axis, and otherwise unconstrained, reveals amorphous and liquidlike structural signatures in the radial distribution function parallel to the walls and enhanced self-diffusion as the wall stiffness is decreased. In sharp contrast, in the gas-like regime (P = 5000 bars, T = 1500 K), soft walls lead to increasing structural order hindering self-diffusion. Furthermore, the correlations between the structure and self-diffusion are found to be well captured by excess entropy. The rich behaviour shown by supercritical fluids under partial confinement, even with simple interatomic potentials, is found to be fairly independent of hydrophilicity and hydrophobicity. The study identifies persisting sub-diffusive features over intermediate time scales, emerging from the strong interplay between density and confinement, to dictate the evolution and stabilization of structures. It is anticipated that these results may help gain a better understanding of the behaviour of partially confined complex fluids found in nature.

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Walls that are soft and flexible play a crucial role in modifying the dynamics of the fluids and its flow behavior. The experimental evidence of the occurrence of flow instability due to fluid flow past a soft surface has been reported.<sup>1</sup> Linear stability analyses have been performed for flow behavior through soft-gel coated walls.<sup>2</sup> Furthermore, soft wall generated turbulence in the flow has also been studied thoroughly.<sup>3</sup> These results suggest an interesting physics happening under the soft wall confinements. Furthermore, MD simulations had been carried out for water-like core-softened fluids under both fixed and flexible boundaries.<sup>4</sup> Diffusion coefficients have been found to vary non-monotonically for core-softened fluids under fixed walls, while monotonic trend is observed for fluctuating walls.<sup>4</sup> The structural properties of core-softened fluid are also changed while making walls fluctuating. The thermodynamic behavior of water-like anomalous fluids, modeled using core-softened potential, show very different dependencies on the rigidity or the flexibility of the walls.5

In sufficiently thin spacings, where separation between the two confining walls are of the order of few atomic diameters of the fluid particles, interesting and anomalous behavior of fluid has been found to exist.<sup>6-15</sup> Besides, these model systems mimic a plethora of real systems, implying a wide range of applicability from physics, chemistry, and biology.<sup>16-18</sup> Typically, dense fluids under confinement act quite abnormally compared to its bulk counterpart as wallfluid interactions in a confined domain produce layer like structural patterns, which in turn significantly modify the dynamics of the fluid. Even at room temperature, extremely dilute gas under partial confinement shows appreciable changes in dynamics with a pronounced suppression of density fluctuations with respect to the bulk gaseous systems.<sup>19</sup>

Our recent study<sup>20</sup> on the effect of confinement on the structural behavior of supercritical fluids (SCFs) indicates the possibility of unusual dynamic behavior of supercritical fluids under confinement. Though the dynamics of supercritical fluids across the Frenkel line (FL) in bulk phase have been studied for the last few years,<sup>21–23</sup> the domain of confined fluids in supercritical phase is vastly unexplored.

For the confinement, we employ a model for an atomistic wall that is aimed at capturing the thermal motion of the wall particles and ensure that the wall presents a "rough" surface that is dynamic. The particles are arranged in a lattice as in a solid and interact with each other through a well-defined inter-atomic potential. The motion of wall atoms is coupled to a thermostat of Nose-Hoover type to maintain the same temperature as that of the supercritical fluid to avoid unnecessary heat flow through the fluid.

10<sup>5</sup> atoms interacting with truncated and shifted Lennard Jones (LJ) potential mimicking argon ( $\varepsilon/k_B = 120$  K,  $\sigma = 3.4$  Å, cutoff = 20 Å ~  $6\sigma$ ) have been simulated considering a set of thermodynamics states in the supercritical regime (P = 5000 bars, 240 K  $\leqslant$  T  $\leqslant$  1500 K) of the bulk phase. The FL crossover has been determined through velocity autocorrelation function (VACF) and radial distribution function (RDF) calculations to be at around T ~ 600-700 K. We explore the changes in the dynamic and structural features across the FL through a series of MD simulations of the supercritical fluid (SCF) under partial confinement using atomistic walls. To determine the FL and consistency checks in bulk, constant pressure temperature (NPT) ensembles are used while NVT ensembles are used to simulate fluids under atomistic boundaries. Walls are simulated along z, while periodic boundary conditions are applied along other two directions (x, y). Throughout the study, a fixed value of 10 Å (~3 $\sigma$ ) has been chosen as a representative spacing to understand the interplay between the density and confinement on the dynamics and strong packing structures. After an energy minimization, a standard velocity-verlet algorithm with a time step ( $\Delta t$ ) of 0.0001 ps has been used to equilibrate the system up to 50 ps followed by a 1000 ps production run to calculate and analyze the properties of interests.

The solid, atomistic walls are made of three layers of the facecentered cubic (fcc) lattice. The number of wall atoms are 583 444 for T = 300 K and 1 076 404 for T = 1500 K. Each of these wall atoms are attached to the lattice sites by harmonic springs. For our study, we chose a fixed spacing (H) of 10 Å (~3 $\sigma$ ) between the walls at both side of FL (T = 300 K and T = 1500 K) and vary the spring constant (k) for these springs from a higher value 5000 eV/Å<sup>2</sup> to a very low value of 0.005 eV/Å<sup>2</sup> to investigate the effect of wall softness on the structure and dynamics of the supercritical fluid. Higher spring constants (k = 5000 eV/Å<sup>2</sup>) mimic rigid walls, by restricting the mean squared displacement (MSD) of the wall atoms with respect to their lattice sites to a very low value, while lower spring constants (k = 0.005 eV/Å<sup>2</sup>) mimic soft walls, by increasing the MSD of the wall atoms with respect to their lattice sites. To define rigid wall, we allow the root mean squared displacement (RMSD) of wall particles to be 40 times and 100 times smaller than a typical distance traversed by a fluid particle between two collisions<sup>21</sup> (~1 Å), at 1500 K and 300 K, respectively. Further details on parameters used for wall-wall, wallfluid interactions, and complete computational exercises to locate FL can be found in our previous work.<sup>20</sup> Figure 1 shows a typical snapshot of the systems with rigid and soft walls. All MD simulations have been carried out using the Large-scale Atomic/Molecular Massively Parallel Simulator (LAMMPS) software package.<sup>26,27</sup>

Figure 2 presents the mean squared displacement (MSD) components, parallel and perpendicular to the walls, for the liquid-like (T = 300 K) and gas-like (T = 1500 K) regimes of the partially confined SCF. The main results, shown for rigid (k = 5000 eV/Å<sup>2</sup>) and soft (k = 0.005 eV/Å<sup>2</sup>) atomistic wall conditions, feature a ballistic regime (~t<sup>2</sup>) and a diffusive (~t) or sub-diffusive (~t<sup> $\alpha$ </sup>;  $\alpha$  = 0) regime separated by an intermediate regime displaying a variety of crossover characteristics. Figure 2 includes the bulk MSD for purposes of comparison.

On short time scales, the fluid particles appear to be largely unaffected by the confinement. While in the bulk, particles undergo thermal collisions resulting in diffusive motion, under partial confinement, particles undergo wall-mediated collisions in addition to thermal collisions resulting in diffusive or sub-diffusive motion. These wall-mediated collisions, being governed by the fluid density, temperature, spacing between the walls and the stiffness of the walls, are seen to produce significant changes in the MSD over intermediate and long-time scales.

The wall-mediated collisions are seen to constrain the z-component of the particle motion completely in the gas-like regime at T = 1500 K [Fig. 2(d)] over long time scales. The constraint arises due to frequent velocity reversals produced by wall-mediated collisions reinforced by the strong confinement [see the Velocity autocorrelation function (VACF) in Fig. S1(c) in the supplementary material where such velocity reversals produce minima in the VACF] that lead to progressively smaller changes in the z-component of the particle position. The effect of the wall stiffness manifests on intermediate time scales influencing the details of the crossover from ballistic to diffusive or sub-diffusive motion. Onset of corrections to ballistic motion due to wall-mediated collisions is earlier for the soft wall than for the rigid wall [green and red curves in Fig. 2(d)] due to the larger amplitude of thermal motion of wall particles in the former.

The motion parallel to the walls in the gas-like regime (T = 1500 K) is diffusive over long time scales. Since the particles of the soft wall have a much larger root mean squared displacement









than those of the rigid wall at T = 1500 K, the wall-mediated collisions from the soft wall are significantly more non-specular in nature. Consequently, the in-plane scattering due to wall-mediated collisions induce faster decay in velocity autocorrelation function when the wall is soft than when the wall is rigid [see VACF in Fig. S1(d) in the supplementary material]. It may indeed be noted from Fig. S1(d) of the supplementary material that partial confinement induces faster decay than what is possible through purely thermal collisions. What is more interesting is that as the wall stiffness decreases, the non-specular nature of the wall-mediated collisions increases and results in the VACF<sub>||</sub> developing almost a shallow minimum and vanishing much earlier. The diffusion coefficients parallel to the walls in the gas-like and liquid-like regimes evaluated over a range of wall stiffness are shown in Table I.

As can be seen from Table I, at 1500 K, the diffusion coefficients parallel to the walls ( $D_{\parallel}$ ) are reduced by about 20% and 70% from the bulk when the wall is rigid and soft, respectively. While in-plane scattering could contribute to a lowering of the diffusion coefficient, it will be seen later that an increased structural order also plays a role in the net reduction of the diffusion coefficient.

In the liquidlike regime (T = 300 K), we note surprising trends in both parallel and perpendicular components of the motion particularly over intermediate time scales. From Table I, we note that bulk diffusion coefficient is significantly lowered with respect to that in the gas-like regime (T = 1500 K) due to the higher fluid density. The velocity reversals, along the z-axis, produced by wall-mediated collisions acting as it does at liquid-like densities lead to caging effects over intermediate time scales and vanishes soon after for both rigid and soft walls. It is important to note that while the caging effect exists even in the bulk SCF due to the high densities, it is more pronounced when the wall is rigid than when the wall is soft [see

**TABLE I**. Variation of diffusion coefficients parallel to the walls (D<sub>||</sub>) with different wallstiffnesses (k values) for a fixed confined spacing (H = 10 Å) at 300 K and 1500 K. For reference, corresponding bulk diffusion coefficients are also shown in column 4 for these two phase space points.

	$k (eV/Å^2)$	$D_{\parallel}$ (Å <sup>2</sup> /ps)	$D_{bulk}$ (Å <sup>2</sup> /ps)	
T = 300 K	5000	0.076		
(liquidlike regime) H = 10 Å	1000	0.077		
	10	0.129	0.74	
	0.5	0.234	0.74	
	0.05	0.358		
	0.005	0.509		
T = 1500 K	5000	7.191		
(gaslike regime)	1000	7.118		
0 0	10	6.489	9.117	
H = 10 Å	0.5	5.861		
	0.05	4.366		
	0.005	2.656		

VACF Fig. S1(a) in the supplementary material]. This pronounced caging effect seems to arise from a nearly specular nature of wallmediated collisions induced by the rigid wall and compounded by the strong confinement at such high densities. The surprising aspect of this pronounced caging effect is that it manifests as a sub-diffusive feature in the MSD<sub>⊥</sub> resembling that of a glassy phase and persists over a fairly wide intermediate time scale suggestive of the characteristic slowing down encountered in the glass forming liquids.<sup>13</sup> The sub-diffusive feature exhibited by MSD<sub>⊥</sub> for the soft wall confinement which develops more gradually over time is distinctly different from that for the rigid wall although persisting over almost as wide an intermediate time scale. Over long time scales, however, the z-component motion is constrained for both rigid and soft wall conditions.

Motion parallel to the walls exhibits surprising features as well. At T = 300 K, while the particles of the soft wall and the rigid wall would both have relatively smaller root mean squared displacements than at T = 1500 K, the relatively smaller root mean squared displacement associated with the rigid wall would induce wall-mediated collisions that are almost specular in nature. With strong confinement compounding the nearly specular scattering, the VACF<sub>II</sub> exhibits deeper minima as wall stiffness is increased at such high densities [see VACF Fig. S1(b) in the supplementary material]. The existence of a well-defined minimum, followed by the vanishing of the VACF $_{\parallel}$  soon after, manifests as a sub-diffusive feature in the MSD<sub>||</sub> when the wall is rigid. From Table I, we note that the diffusion coefficient is nearly 90% lower than that in the bulk, under rigid wall confinement, while the diffusion coefficient is only 30% lower than that in the bulk, under soft wall confinement. Such a large reduction of the diffusion coefficient appears possible only if in-plane scattering produced by wall-mediated collisions combines with an increased structural order imposing restrictions to particle motion.

The constraints on  $MSD_{\perp}$  at T = 300 K as well as at T = 1500 K, have important structural implications—at long time, the fluid particles have root mean squared displacements of 2.9 Å and 3.7 Å at T = 300 K, and 2.8 Å and 3.3 Å at T = 1500 K, for the rigid and soft wall confinements, respectively, along z. Although the separation between the walls is 10 Å, these constraints on the root mean squared displacements of fluid particles force them to adopt non-uniform but symmetric spatial distributions with respect to the z-axis. Figures 3(a) and 3(b) show the normalized particle counts along the z-axis at T = 300 K and T = 1500 K for rigid and soft wall confinements. At T = 300 K, the higher fluid density imposes further packing restrictions resulting in a finer layering across the z-axis. The scale over which local number density varies is about 3 Å consistent with the average displacement of fluid particles in both the gas-like regime as well as the liquid-like regime of the SCF. As mentioned in our previous work,<sup>20</sup> the number of layers formed due to confinement scales linearly with the ratio of spacing to the atomic diameter ( $\frac{H}{\sigma} = 10/3.4 \sim 3$ ) in the liquidlike regime of SCF.

It is intriguing to see how motion parallel to the walls influences the lateral structure. This structure-dynamics interrelationship is examined using the radial distribution function parallel to the walls,  $g_{\parallel}(r)$ , and the excess entropy associated with it.

The radial distribution function parallel to the walls  $(g_{\parallel}(r))$  is computed for specified intervals along the z-axis from

$$g_{\parallel}(r) \equiv \frac{1}{\rho^2 V} \sum_{i \neq j} \delta(r - r_{ij}) \left[ \theta \left( |z_i - z_j| + \frac{\delta z}{2} \right) - \theta \left( |z_i - z_j| - \frac{\delta z}{2} \right) \right],$$
(1)

where *V* is the volume,  $\rho$  is the density,  $r_{ij}$  is the distance parallel to the walls between molecules i and j,  $z_i$  is the *z* coordinate of the molecule *i*, and  $\delta(x)$  is the Dirac  $\delta$  function. The Heaviside function  $\theta(x)$  restricts the sum to a pair of particles located in the same slab of thickness  $\delta z$ . We have considered  $\delta z$  to be same as the width of each layer. We use a uniform bin width and bin number of 80 to calculate  $g_{\parallel}(r)$  for all the cases. Figures 4 and 5 show  $g_{\parallel}(r)$  for soft and rigid wall confinements at the two temperatures, 1500 K and 300 K, respectively. For purposes of comparison, the g(r) for the bulk phases are also included.

The two-body excess entropy, parallel to the walls, is defined as  $^{28,29}$ 

$$s^{(2)} = -2\pi\rho k_B \int [g_{\parallel}(r)\ln g_{\parallel}(r) - g_{\parallel}(r) + 1]r^2 dr.$$
(2)



FIG. 3. Distributions of argon particles in the supercritical state, averaged over several time steps, at 300 K (a) and at 1500 K (b) are calculated for two extreme k values, normal to the walls for 10 Å confined spacing. For comparison, the bulk density distribution is shown.



**FIG. 4**. (a) shows  $g_{\parallel}(r)$  of the central region in the number distribution of SCF (argon) particles at 1500 K, with H = 10 Å, for two extreme stiffness coefficients (k). (b) shows  $g_{\parallel}(r)$  of the region close to the left wall (wall at z = -5 Å) for two extreme k values. For comparison, bulk g(r) has also been shown.

Table II shows the two-body excess entropy evaluated as a function of wall stiffness (k) for T = 300 K and T = 1500 K for the same spatial regions considered in the computation of  $g_{\parallel}(r)$ . The bulk values of  $s^{(2)}$  are negative since the reference is an ideal gas. The values for the confined systems are more negative due to the more ordered structures formed. As the density is kept constant representing a particular phase space point for both bulk and confined systems, the quantity  $\frac{s^{(2)}}{2\pi\rho k_B}$  is used for the study.

Although Figs. 4(a) and 4(b) show that  $g_{\parallel}(r)$  appears not to be influenced significantly by the cross-sectional density variation under rigid wall confinement at 1500 K, compared to the bulk, the excess entropy values from Table II clearly indicate that there is some degree of ordering in the central region and even more ordering in the higher density region of the cross-section [see Fig. 3(b)]. It may be recalled that at T = 1500 K, under rigid wall confinement, the perpendicular component of the wall-mediated collisions is seen to (a)



**FIG. 5**. Shows  $g_{\parallel}(r)$  of the layer close to the left wall (wall at z = -5 Å) in the number distribution of SCF (argon) particles at 300 K, with H = 10 Å, for two extreme stiffness coefficients (k). For comparison, bulk g(r) has also been shown.

bring about deviations from the ballistic regime a little earlier than that in the bulk, and (b) limit the values of  $MSD_{\perp}$  soon after, within a short time. This rapid change in the nature of motion is seen to produce cross-sectional density variations early on. In other words, the long-time scale density variations shown in Fig. 3(b) appear to set in much earlier. The increase in structural order, captured by the lowering of the excess entropy, leads to restricted particle motion contributing to the overall reduction of 20% in the diffusion coefficient with respect to the bulk. The enhanced non-specular wall mediated collisions along with an increased structural order (seen in Fig. 4 and Table II) parallel to the soft walls at 1500 K, play a crucial role in the decrement of the diffusion coefficient to 70% compared to the bulk.

At T = 300 K, the persistence of sub-diffusive features over a wide intermediate time scale seen in the  $MSD_{\perp}$  appears to be the key to the formation of spatial structures and signal the mutual influence between particle motion and structure as time evolves. The "slowing down" of the dynamics implies the emergence of spatially ordered structures which in-turn restricts the dynamics and this in turn reinforces the ordering and so on until  $MSD_{\perp}$  no longer changes. As can be seen from Fig. 3(a), the cross-sectional density variations are stronger when the wall is rigid due to the combined effect of high fluid density and strong confinement.

The onset of the sub-diffusive features can be seen in the parallel component of MSD (MSD<sub>||</sub>) as well when the wall is rigid. The large reduction in the excess entropy indicates significant structural ordering and is indeed evident from g<sub>||</sub>(r) shown in Fig. 5. The appearance of several peaks in g<sub>||</sub>(r) and the distorted features of these successive maxima and minima suggest that the structure is more amorphous than liquid-like. The 90% reduction in the diffusion coefficient appears to be largely due to the higher degree of structural order.

When the wall is soft, the features in  $g_{\parallel}(r)$  appear relatively smoother with fewer peaks resembling a more liquid-like phase. Table II indicates that there is considerable structural ordering even when the wall is soft and appears to play a major role in reducing the diffusion coefficient by 30% with respect to the bulk. This again seems to be an outcome of the combined effect of high fluid density and strong confinement.

	k (eV/Ų)	$s^{(2)}/2\pi\rho k_B$ (central region)	$s^{(2)}/2\pi ho k_B$ (region near left wall)	$s^{(2)}/2\pi\rho k_B$ (region near right wall)	$s^{(2)}/2\pi ho k_B$ (bulk)
T = 300 K	5000	-63.82	-53.48	-52.54	-9.39
(liquidlike regime)	1000	-65.31	-53.41	-54.31	
	10	-61.94	-57.64	-56.86	
H = 10 Å	0.5	-43.11	-58.32	-56.29	
	0.05	-20.16	-23.11	-23.03	
	0.005	-13.68	-16.64	-17.75	
T = 1500 K	5000	-4.86	-7.71	-6.70	
(gaslike regime)	1000	-5.43	-5.85	-5.56	
	10	-5.05	-6.77	-6.38	-3.27
H = 10 Å	0.5	-6.11	-5.26	-6.98	
	0.05	-4.67	-6.35	-6.13	
	0.005	-7.62	-11.27	-11.50	

**TABLE II.** Variation of Pair-excess entropy ( $s^{(2)}/2\pi\rho k_B$ ), parallel to the walls, with different wall-stiffnesses (k values) for a fixed confined spacing (H = 10 Å) at 300 K and 1500 K. For reference, corresponding bulk values are also shown in column 6 for these two phase space points.

We note that all the results described in the article have been obtained with the ratio of fluid-wall  $(\varepsilon_{w-f})$  and fluid-fluid  $(\varepsilon_{f-f})$  interaction strengths  $\frac{\varepsilon_{w-f}}{\varepsilon_{f-f}} = 1$ . A value  $\geq 1$  for this ratio represents hydrophilic boundary conditions.<sup>30,31</sup> Studies were undertaken explicitly varying the ratios of fluid-wall and fluid-fluid interaction strengths, mimicking both hydrophobic  $(\frac{\varepsilon_{w-f}}{\varepsilon_{f-f}} < 1)$  and hydrophilic  $(\frac{\varepsilon_{w-f}}{\varepsilon_{f-f}} \geq 1)$  boundary conditions. It is observed that the key findings regarding the structure and dynamics remain unaltered, thus making the results presented here quite generic and fairly independent of the affinity between the fluid and the wall particles.

In summary, soon after the ballistic regime, the highly dense SCF at T = 300 K exhibits persisting in-plane sub-diffusive features under rigid-wall confinement enabling amorphous-like structural features to emerge. Over long-time scales, the structure stabilizes as evidenced by the appearance of multiple distorted peaks in the radial distribution function and the associated large negative excess entropy denoting ordering. The structure causes a nearly 90% reduction in the diffusion coefficient from the bulk. Perhaps not surprisingly, soft-wall confinement leads to a more liquid-like structure to emerge with only a 30% reduction in the diffusion coefficient from the bulk.

At T = 1500 K, the gas-like SCF, although still dense, exhibits mild in-plane sub-diffusive features which are influenced significantly by the soft-wall confinement in sharp contrast with the behaviour at T = 300 K. The diffusion coefficient under soft-wall confinement is reduced by nearly 70% from the bulk, while that for rigid-wall confinement is reduced only by 20% from the bulk.

The dynamics and structure of SCF under rigid and soft walls at two phase space points lying on either side of the FL emerges as a unique system, showcasing features of almost all types of fluids: (a) liquid-like packing with prominent layering across the confined width before crossing FL, (b) gas-like diffusion dominated motion after crossing FL, (c) glass-like slowdown in dynamics at intermediate time scale, and (d) amorphous-like structural features for rigid wall confinement in the liquid-like regime.

In the supplementary material, detailed descriptions of velocity autocorrelation function (VACF) have been discussed for supercritical LJ fluid under both rigid and soft walls at two ends of the FL (300 K and 1500 K).

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