## Microscopic foundation of the $\mu(I)$ rheology for dense granular flows on inclined planes - Supplementary Information -

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## FRICTION

We carry out additional simulations and change the value of the microscopic sliding friction coefficient  $\mu_s$ , from 0.3 to 1. As shown in Fig S1, we note that it only shifts the threshold values  $\mu_c(\mu_s)$  and  $\phi_c(\mu_s)$  but has no impact on the scaling laws. By simply subtracting the threshold value, we obtain a collapse of all our data on a single master curve.



FIG. S1. a) Shifted effective friction coefficient,  $\mu - \mu_c$  as a function of the inertial number  $I = \dot{\gamma} d \sqrt{\rho_{\rm p}/P}$ , obtained for a layer of grains with an initial layer thicknesses  $H_{\rm i} = 20d$  and various microscopic sliding frictions  $\mu_s$  as indicated. The solid line indicates a linear fit of the small I values as provided in legend. b) Shifted volume fraction  $\phi_c - \phi$  as a function of the inertial number I. The solid line indicates a linear fit as provided in legend.



FIG. S2. Evolution of the rescaled local velocity (a), volume fraction  $\phi$  (b) and inertial number I (c) as functions of rescaled normal coordinate z/d for a layer of frictional grains initially characterized by  $H_i = 30d$  and various inclination angles  $\theta$  as indicated. The curves in (a) corresponds to the best fit of the Bagnold profile expression.

## **BAGNOLD-LIKE FLOWS**

In order to check the validity of our DEM simulations of granular flows on inclined planes, we study in details the properties of the flow. We observe that the local time-averaged velocity profile is well described by a Bagnold profile  $\langle v(z) - v(0) \rangle \sim H^{3/2} - (H - z)^{3/2}$  (see Fig. S2a). Besides, the inertial number *I* (see Fig. S2b) and the volume fraction  $\phi$  (see Fig. S2c) remain mostly constant throughout the layer (except at both boundaries) for all the studied inclination angles. These observations are in good agreement with previously reported observations [1–5].

## VELOCITY CORRELATIONS AND DIFFUSION

As shown in Fig. S3a, we calculate the mean square displacement ( $\Delta_z$ , MSD) along the *z* coordinate averaged over all the grains for various inclination angles. From those MSD, the thickness-averaged diffusion coefficient,  $\overline{D_z}$  is evaluated by fitting the data in the diffusive regime, *i.e.* where  $\Delta_z = 2\overline{D_z t}$ . In addition, we also evaluate the time correlation of the *z*-component of the velocity *w*, averaged over the layer thickness, for various inclination angles. The thickness averaged correlation times,  $\overline{\tau}$  were obtained by fitting the correlation curves with decreasing exponentials of the type  $\sim e^{-t/\overline{\tau}}$ .



FIG. S3. (a) Mean square displacement  $\Delta_z$  along the z coordinate averaged over all the grains and (b) time correlations of the velocity following z for a layer of frictional grains initially characterized by  $H_i = 30d$  and various inclination angles as indicated. Inset: Log-lin plot of the velocity correlations.

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