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# **Microwave-Assisted Pyrolysis of Biomass with and without Use of Catalyst in a Fluidised Bed Reactor: A Review**

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Abstract: Lignocellulosic biomass and waste, such as plastics, represent an abundant resource today, and they can be converted thermo-chemically into energy in a refinery. Existing research works on catalytic and non-catalytic pyrolysis performed in thermally-heated reactors have been reviewed in this text, along with those performed in microwave-heated ones. Thermally-heated reactors, albeit being the most commonly used, present various drawbacks such as superficial heating, high thermal inertia and slow response times. That is why microwave-assisted pyrolysis (MAP) appears to be a very promising technology, even if the process does present some technical drawbacks as well such as the formation of hot spots. The different types of catalysts used during the process and their impacts have also been examined in the text. More specifically, studies conducted in fluidised bed reactors (FBR) have been detailed and their advantages and drawbacks discussed. Finally, future prospects of MAP have been briefly presented.

Keywords: microwave pyrolysis; MAP; catalytic pyrolysis; HDO; biomass; plastics

#### 1. Introduction

Since the start of the twenty-first century, rapid population and technological growth have put relentless pressure on already ever-dwindling fossil fuel resources. The peak in energy demand is not expected to diminish in the coming years. More people existing on the planet translates into more waste, and so, more biomass being produced. Hence, biomass as an energy source could be a viable replacement for fossil sources in the coming years. Various products such as biodiesel, bioethanol and biohydrogen have successfully been produced from biomass, supporting its potential as a reliable and clean energy source. Biofuels can be classified into three broad categories: first, second and third generations. Table 1 catalogues the different known biomass resources.



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First-Generation Sources	Virgin resources	Forest resources	Wood such as pine, woody and forest biomass such as willow, poplar, aspen
		Oil crops	Wheat, barley, corn, canola, rapeseed, palm oil, soybean, sugarcane, flax, oat, straw, pasture grasses
		Wood residues	Bark, branches, leftover treetop, leaves from harvest, sawdust, shavings from pulp and sawmills
Second-Generation Sources	Residues Municipal solid waste (MSW)	Agricultural residues and waste	Residual fraction from oil crop harvest, waste oil/fat
-		Livestock residues	Livestock excrement and carcass
		Residential	Cardboard and mixed paper, glass, various metals, electronics, plastics, tyres, organics
		Non-residential	Sewage sludge
Third-Generation Sources	Algae	-	Macroalgae, microalgae

Table 1. Biofuel resource classification (Adapted from [1]).

A plethora of conversion processes—physical, thermal, biochemical, microbial or chemical—have been used to transform biomass into fuels [2,3]. Among all the processes, thermochemical ones present a better choice so as to convert biomass feedstock more rapidly at a lesser cost [3]. Interesting thermochemical transformation processes include combustion or incineration, catalytic liquefaction, gasification and pyrolysis, which is the main focus of this review.

#### 2. Pyrolysis and Catalytic Pyrolysis

Pyrolysis is a thermal conversion process that heats and decomposes a substance in an oxygen-inert atmosphere. This process is classified into three distinct technologies, and forms three main products, as illustrated in Figures 1 and 2, respectively. The process has largely been examined in literature and can be optimised to maximise the production of any of its product constituents by altering process parameters such as the operational temperature and residence time, among others [4–8].



Figure 1. Pyrolysis technologies classification (Adapted from [9]).



Figure 2. Biomass pyrolysis products (Adapted from [10]).

Different types of reactors have been used to conduct pyrolysis reactions over time [11]. The more common ones are: ablative, conical spouted bed, rotating cone, Auger and fluidised bed (bubbling and circulating) reactors [12–14]. Lam et al. [15] state that most studies pertaining to biomass pyrolysis at the laboratory scale are performed in batch reactors as the latter are simple to use, no high-pressure pump or compressor is needed, all types of biomass can be used and no complex separation means needs to be applied to recover the remaining bio-char. However, the drawbacks presented by this technology, extended reaction, heating and cooling times, product inconsistency and difficulty of large-scale production, have geared more recent research towards semi-continuous and continuous processes [16].

Now, it should be noted that the bio-oil produced from biomass pyrolysis has a high oxygen content, which translates to it also having high acidity, high viscosity, low calorific value and thermal instability [17]. The latter characteristics present a challenge for bio-oil to be used as a substitute for conventional fuels. Therefore, the main objective of most pyrolysis systems is to maximise the yield of bio-oil and improve the selectivity of the compounds within the bio-oil. Various methods have been studied in literature to enhance the properties of these bio-oils. One method commonly used in literature is catalytic fast pyrolysis (CFP). Different upgrading methods have also been researched in the literature; one of the most studied methods is catalytic hydrodeoxygenation (HDO).

Some studies have shown that catalytic HDO presents an increase in liquid hydrocarbons, gaseous olefin yields and a decrease in coke yield with respect to untreated bio-oil [18]. On the other hand, it does exhibit some drawbacks such as its need for rare metals and high-pressure hydrogen, and its rather expensive cost. Most research studies on catalytic HDO have been conducted on model compounds such as guaiacol, phenol or cresol; Ambursa et al. [19] and Wang et al. [20] present an exhaustive summary of these studies in their respective publications. Some of the most notable research works concerning catalytic HDO have been summarised in Table 2.

As for CFP, only the research performed on the upgrading of pyrolytic vapours, that is, ex situ CFP, have been considered. The most commonly used catalysts in literature are zeolite-based. Their efficiency in deoxygenating bio-oils and increasing their hydrocarbon content has been widely researched and proven, as shown in Table 3.

		Reactio	n Conditions		Results		
Feed	Catalyst Used	Reactor Used	Temperature (°C), Pressure (bar), H <sub>2</sub> Percentage	WHSV * (g feed/g cat. h), Contact Time (s) or F/C * Ratio	Bio-Oil Yield (wt. %)	Products and Conclusions	Ref.
	MoS <sub>2</sub>					HDO transformation of guaiacol was significantly	
-	CoMoS	- T 11 1	300 °C, 40 bar, 100% H <sub>2</sub>	0.3–1 s	-	enhanced by promoting MoS <sub>2</sub> -based catalysts with Co. However, the use of Al <sub>2</sub> O <sub>3</sub> as support gave rise to demethylation and production of methyl-substituted products, which render de-oxygenation more difficult.	[21]
Guaiacol	$MoS_2/Al_2O_3$	Fixed bed					
	CoMoS/Al <sub>2</sub> O <sub>3</sub>						
	$MoS_2/\gamma$ - $Al_2O_3$	_				Out of Mass based establists the TiOs supported and	[22]
-	$MoS_2/TiO_2$	Fixed bed	300 °C, 40 bar, 100% H <sub>2</sub>	0.3–1 s	-	gave the most interesting improvements. As for CoMoS, ZrO <sub>2</sub> proved to have the most significant catalytic activities. The CoMoS/ZrO <sub>2</sub> system was very selective towards aromatic (C-O) hydrogenolysis as demethoxylation and direct de-oxygenation were both observed.	
	$MoS_2/ZrO_2$						
Guaiacol	$CoMo/\gamma$ - $Al_2O_3$						
	CoMo/TiO <sub>2</sub>						
	CoMo/ZrO <sub>2</sub>						
	NiCu/ CeO <sub>2</sub> -ZrO <sub>2</sub>						
	NiCu/Al <sub>2</sub> O <sub>3</sub>	_		337.5:1	-	NiCu/SiO <sub>2</sub> -ZrO <sub>2</sub> -La <sub>2</sub> O <sub>3</sub> was the most efficient catalyst. Deoxygenation degree increased with temperature, while guaiacol conversion decreased due to catalyst coking at higher temperatures.	[23]
Guaiacol	NiCu/SiO <sub>2</sub>	Batch	280–360 °C, 170 bar,				
Gualacol	NiCu/SiO <sub>2</sub> -ZrO <sub>2</sub> - La <sub>2</sub> O <sub>3</sub>	Dutch	100% H <sub>2</sub>				
	Ni/SiO <sub>2</sub>	_					
	Ni-Cu-MgO	_					

**Table 2.** Notable research works on catalytic HDO.

Table 2. Cont.

		Reactio	on Conditions		Results		
Feed	Catalyst Used	Reactor Used	Temperature (°C), Pressure (bar), H <sub>2</sub> Percentage	WHSV * (g feed/g cat. h), Contact Time (s) or F/C * Ratio	Bio-Oil Yield (wt. %)	Products and Conclusions	Ref.
Ni/C					63.8	The mesoporous silica supports (SBA-15 and	
Yellow poplar bio-oil	Ni/SBA-15	Autoclave	300 °C, 30 bar, 100% H <sub>2</sub>	25:1	76.0	<ul> <li>Al-SDA-D) showed greater catalytic activity that</li> <li>Ni/C. this could be correlated to a higher surface area</li> <li>and pore size, which caused uniform dispersion of</li> <li>NI particles.</li> </ul>	[24]
	Ni/Al-SBA-15	-			74.8		
	NiMo/C					NiMo/Al <sub>2</sub> O <sub>3</sub> and NiMo/ASA showed the highest	
Methyl oleate (as model compound for green diesel)	NiMo/SiO <sub>2</sub>	Fixed bed	260 $^\circ \rm C$ , 30 bar, 90% $\rm H_2$ and 10% $\rm H_2 S$	6.5 g feed/g cat. h -	_	during the run—owing to Lewis acidity of Al surface active in methyl oleate hydrolysis. NiMo/SiO <sub>2</sub> had	[25]
	NiMo/ASA					similar overall activity than the two previous, but did not de-activate. NiMo/C did not de-activate either, and was more active than the others at the end of the run.	[20]
	NiMo/Al <sub>2</sub> O <sub>3</sub>	-					
	Ni-Cu/HZSM-5			bar, 12:1	33.9	<ul> <li>Addition of CeO<sub>2</sub> to Ni-Cu/HZSM-5 improved the performance of the catalyst. It caused an improvement in the Ni dispersion, redox ability and the Bronsted</li> <li>acidity ratio. It also decreased the particle size of the catalyst and diminished coke deposition on the</li> <li>catalyst surface, which causes catalyst deactivation. In total, 15% CeO<sub>2</sub>-Ni-Cu/HZSM-5 was the best in terms of catalyst efficiency.</li> </ul>	[26]
	5% CeO <sub>2</sub> -Ni-Cu/ HZSM-5		270 °C, 20 bar, 100% H <sub>2</sub>		37.4		
bio-oil	15% CeO <sub>2</sub> -Ni-Cu/ HZSM-5	- Autoclave			47.6		
	20 % CeO <sub>2</sub> -Ni-Cu/ HZSM-5	-			35.3		
Anisole, m-cresol and phenol	5% Pd/C		250–350 °C, 50 bar, 100% H <sub>2</sub>		-	Residence time of 4 h allowed the formation of high yields of deoxygenated compounds. $Pt/Al_2O_3$ promoted hydrogenation (ring saturation) and	
	5% Pt/Al <sub>2</sub> O <sub>3</sub>	Parr batch				removal of the pendant groups, and a significant pathway shift was observed as temperature increased. Pd/C showed ring saturation followed by methanol abstraction.	[27]

Table 2. Cont.

**Reaction Conditions** Results WHSV \* Temperature (°C), Feed Ref. **Bio-Oil Yield** (g feed/g cat. h), Catalyst Used **Reactor Used** Pressure (bar), **Products and Conclusions** Contact Time (s) or (wt. %) H<sub>2</sub> Percentage F/C \* Ratio 80.4 HZSM-5 Pressures of 3 to 15 bar were tested and 15 bar provided the highest bio-oil yield; all catalytic tests 77.6  $Co/\gamma - Al_2O_3$ were hence performed at 15 bar. HHV\* of HDO-upgraded bio-oils improved with use of Saccharina 82.1 350 °C, 3–15 bar,  $Fe//\gamma$ -Al<sub>2</sub>O<sub>3</sub>  $Co/\gamma$ -Al<sub>2</sub>O<sub>3</sub>, but decreased with use of metal [28] Autoclave 10:1 *Japonica* bio-oil 100% H<sub>2</sub> phosphide catalysts. The latter promoted 82.7  $CoP//\gamma$ -Al<sub>2</sub>O<sub>3</sub> decarboxylation while metal catalysts elevated demethylation. An increase in kerosene fraction of 78.8  $Fe_2P//\gamma-Al_2O_3$ bio-oil was also observed with the use of  $CoMoP//\gamma - Al_2O_3$ 68.0 catalytic HDO. Zeolite Y Conversion over catalysts with low Si/Al ratios gave (Si/Al: 5.1:1) rise to the production of aromatics (benzene, toluene, xylene and phenol). Highest benzene yield was 19.5 Zeolite Y (Si/Al: 30:1) wt. % over zeolite Y (30:1). Trend of overall BTX yield Pyroprobe 500 °C, 1.01 bar, [29] Guaiacol and 1:10 was: Zeolite Y (30:1), 30.5% > Zeolite Y (5.1:1), 28.1% > (Pv-GC/MS)100% H<sub>2</sub> Zeolite Y furfural Zeolite Y (80:1), 12.0% > Zeolite Y (60:1), 6.4%. It was (Si/Al: 60:1) also shown that zeolite acidity played an important Zeolite Y role in the deoxygenation of guaiacol, but not in that (Si/Al: 80:1) of, furfural, 275 or 300 °C, Catalyst with a 50:50 Al/Si ratio after calcination at 450 Guaiacol γ-Al<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub> Fixed bed 6.50 g guaiacol/g cat. h [30] 1.01 bar, 25% H<sub>2</sub> <sup>o</sup>C exhibited the highest guaiacol conversion (81.79%).

\* WHSV: Weight hourly space velocity. F/C ratio: Feed to catalyst ratio. HHV: Higher heating value.

		Reaction	Conditions	Results			
Feed	Catalyst Used	Reactor Used	Temperature (°C)	WHSV (g feed/g cat. h) or F/C Ratio	Bio-Oil Yield (wt. %)	Product Quality, Oxygen Content and Conclusions	Ref.
	HZSM-5		500–550		28.8	Good aromatics yield (15.9 wt. %)	
	Na-ZSM-5	-			24.3	Higher aromatics yield (21.3 wt. %)	-
Waste wood shavings	Y-Zeolite	Fluidised bed		1.05–1.14 g biomass/g cat. h	28.6	Average aromatics yield (14.0 wt. %)	[31]
	Activated alumina	-			31.2	Lowest aromatics yield (8.0 wt. %)	
Radiata pine sawdust	HZSM-5	Bubbling	475–625	4 g biomass/g cat. h	43.7	Formation of mainly aromatic hydrocarbons	[32,33]
	Н-Ү			8 g biomass/g cat. h	45.7	Almost no formation of aromatics	
	Ga/HZSM-5	fluidised bed		4 g biomass/g cat. h	51.3	Higher selectivity for aromatics (as compared to HZSM-5)	
	HZSM-5				46.6	Reduction of non-phenolic oxygenates	_
Radiata pine sawdust	MMZ <sub>HZSM-5</sub> (mesoporous material from HZSM-5)					50.6	No change in phenols; reduction in other oxygenates
	MFI zeolite	Fixed bed	500	10:1	45.9	High aromatics yield; reduction in non-phenolic oxygenates and	[34]
	1% Ga/MFI	-				in phenols	
	5% Ga/MFI	-				Similar to HZSM-5; less efficient than 1% Ga/MFI	-

**Table 3.** Notable research works on CFP using zeolite-based catalysts.

Pine wood

Table 3. Cont.

H-Y

HZSM-5

Auger

**Reaction Conditions** Results WHSV Feed Ref. Product Quality, Oxygen Content **Bio-Oil Yield** Catalyst Used **Reactor Used** (g feed/g cat. h) or Temperature (°C) (wt. %) and Conclusions F/C Ratio Η-β 37.8 Fe-H-β 37.0  $\beta$ -zeolite was the most efficient for H-Y 39.7 Dual [35] 450 8.33:1 Pine sawdust deoxygenation, followed by Y and fluidised bed Fe-H-Y 34.3 ferrierite zeolites **H-Ferrierite** 43.8 44.5 Fe-H-Ferrierite ZSM-5 [36] Fluidised bed 0.35 g biomass/g cat. h Increase in selectivity of aromatics Pine wood 450-600 -Conversion of 76.7-91.6% found; HZSM-5 Fixed bed 550 2:1 4.1-8.7 [37] Jatropha wastes production of mainly aromatics Reduction in oxygenates and increase HZSM-5 42.5 in aromatics and phenolics Larger reduction in oxygenates and higher increase in aromatics 500 [38] Particle board Batch 10:1 Ga/HZSM-5 46.3 (compared to HZSM-5); lower phenolic content Η-β 44.6 Similar to HZSM-5, but less efficient  $\beta/Al_2O_3$ Si/Al and  $\beta$ -zeolite contributed to 52.0 increase of liquid product while Si/Al 51.0 HZSM-5 and H-Y led to formation of

450

12 g biomass/g cat. h

43.0

41.0

[39]

aromatics and higher gas percentage.

HZSM-5 reduced oxygen content of

46.4 wt. % to 30 wt. %.

**Reaction Conditions** Results WHSV Feed Ref. Product Quality, Oxygen Content **Bio-Oil Yield** Catalyst Used **Reactor Used** (g feed/g cat. h) or Temperature (°C) (wt. %) and Conclusions F/C Ratio High selectivity in monoaromatic HZSM-5 compounds (4.4 wt. %); CO<sub>2</sub>:CO = 0.5 Micro 8.3-10.1 fluidised bed Higher selectivity in monoaromatic Desilicated HZSM-5 compounds (6.2 wt. %); same CO<sub>2</sub>:CO Oak wood High selectivity in monoaromatics 500 0.85:1 [40] HZSM-5 (4.1 wt. %), but less efficient cylinder particles than FBR \* Fixed bed Higher selectivity than parent HZSM-5 Desilicated HZSM-5 (5.1 wt. %), but less efficient than FBR \* HZSM-5 50.0 Fe-HZSM-5 58.8 H-Y 49.0 Fe-HZSM-5 was the most efficient in Beech wood (BW) deoxygenation (33.82 to 17.50% for Fe-H-Y 61.0 BW and 34.76 to 17.31% for FS).  $Pt/Al_2O_3$ 60.0 Zeolites were found to cause decomposition of carboxylic acids to Semi-CoMo/Al<sub>2</sub>O<sub>3</sub> 54.0 [17] 500 4:1 form phenols, H<sub>2</sub>, H<sub>2</sub>O, CO<sub>2</sub> and CO, continuous HZSM-5 50.0 mostly. Pt and CoMo-based catalysts Fe-HZSM-5 58.8 did not show high efficiencies; these catalysts might be better suited for H-Y 41.0 HDO applications. Flax shives (FS) Fe-H-Y 51.0  $Pt/Al_2O_3$ 52.0  $CoMo/Al_2O_3$ 47.0

\* FBR: Fluidised bed reactor.

Table 3. Cont.

Nowadays, research is tending more and more towards a cleaner way of disposing of plastic waste, which has been increasing at an alarming rate in recent years. Pyrolysis, and hence, microwave pyrolysis, has emerged as a very promising technology to this end. Kaminsky [41] performed the chemical recycling of different types of plastics in an FBR. His results have been summarised in Table 4.

Feed	Temperature (°C)	Fluidising Gas	Products
Polyethylene (PE), Polypropylene (PP)	400–550	Nitrogen, steam and pyrolysis gas	70–90% waxy products, oil, 2–9% gas
Polymethylmethacrylate (PMMA), Polystyrene (PS)	400–500	Pyrolysis gas	70–95% monomers, 5–30% gas, oil
Polyethylene terephthalate (PET)	400–550	Steam	45–60% monomers, 40–45% gas, oil
PE, PP	700-800	Nitrogen, steam	70–80% gas (olefins), 20–30% oil
PE, PP, polyamide (PA)	700-800	Pyrolysis gas	30–50% aromatics, 30–40% oil, gas, 1–10% soot

Table 4. Results of pyrolysis of different plastics by Kaminsky [Adapted from 41].

The authors found that PE and PP formed mostly waxy products around temperatures of 400–550 °C and gas and oil around 700 °C. By using pyrolysis gas as a fluidising agent, aromatics were produced. It was also observed that up to 98 wt. % of MMA could be recovered from the pyrolysis of pure PMMA wastes. As for styrene recovery from PS, it was limited to about 77 wt. % and the remainder was oligomers. PET was hydrolysed through this process with steam as a fluidising agent and PA, at low temperatures, produced aromatics and gas; soot formation was found to be low. Finally, PTFE was pyrolysed into high amounts of TFE and HEP, its monomers. Hence, it was concluded that the pyrolysis of plastics in a fluidised bed reactor was a real option for an industrial application.

Now, conventional pyrolysis systems making use of electrical heating have by far been the most-studied types of systems in the literature. However, these systems are energyintensive, which compromises their economic viability on an industrial scale. Over recent years, research has been focusing on new, innovative ways to build energy-efficient systems for pyrolysis. One of the most promising routes found is microwave-assisted pyrolysis. It should also be noted that the addition of proper catalysts to a microwave pyrolysis process can dramatically influence the process' product selectivity; gas and liquid yields, as well as heating performance, can be importantly promoted through this addition of catalysts [42]. The distinction between the effects of the two (microwave heating and catalyst use) will try to be made throughout the text.

#### 3. Fundamentals on Microwaves

Microwaves are electromagnetic irradiation with a wavelength range of 0.01 to 1 m, and a frequency range of 0.3 to 300 GHz, correspondingly [43]. Most microwave reactors used for chemical syntheses, as well as all domestic microwave ovens, function at a frequency of 2.45 GHz, correlating to a 12.25 cm wavelength. This is conducted in order to prevent any interference with telecommunications and cellular phone frequencies [44]. Microwaves are typically defined as electromagnetic waves having two perpendicular components, electric and magnetic fields, as shown in Figure 3.



Figure 3. Electric (E) and magnetic (H) field components in microwaves [45].

Microwave dielectrics are known as materials able to absorb microwave irradiation, and thus, microwave heating is called dielectric heating [46]. Dielectric heating generally functions by transforming electromagnetic energy into thermal energy; it is more of an energy conversion than direct heating. The microwaves penetrate materials and deposit energy; thus, the heat can be diffused throughout the volume of the material. In this case, the centre of the material is at a higher temperature than its surroundings [1]. On the other hand, during conventional heating, heat is transferred from the surface to the core of the material via conduction driven by temperature gradients [47]. This difference is illustrated in Figure 4.



Figure 4. Microwave and conventional heating systems (Adapted from [1]).

Some advantages of microwave heating over conventional heating are presented in Table 5 [48].

Microwave-Assisted Heating	<b>Conventional Heating</b>
Conversion of energy	Transfer of energy
Uniform heating at a molecular level from core	Superficial heating through conduction, convection and radiation
Frequent hot spot formation	Rarer hot spot formation
Rapid	Slow
Higher electricity conversion efficiency	Low electricity conversion efficiency
Selective	Non-selective
Dependent on material properties	Less dependent
Precise heating	Less precise
Lower thermal inertia and faster response	Higher thermal inertia and slower response

Table 5. Microwave-assisted heating compared to conventional heating.

Now, according to the dielectric properties of a material, it may be categorised in three possible ways [2,39]:

- 1. Insulators or microwave-transparent materials, through which microwaves may pass without any losses (e.g., quartz, Teflon and so on), commonly possess low dielectric loss factors and have very large penetration depths;
- 2. Conductors or reflectors, which microwaves cannot penetrate and are reflected, are generally materials with high conductance and low capacitance (e.g., metals) that have high dielectric loss factors and hence, near-zero penetration depth for microwaves, and;
- 3. Absorbers, where microwave irradiation may be absorbed most effectively (e.g., water, oils and so on), have dielectric loss factors in the middle of the conductivity range.

According to the literature [49,50], there are three ways of enhancing a chemical reaction using the microwave irradiation technology:

- 1. Thermal effects (the influence of a high reaction temperature rapidly attained when irradiating polar materials in a microwave field);
- 2. Specific effects (caused by the unique nature of the heating mechanism of microwave irradiation in a microwave field; this cannot be achieved using conventional heating) and;
- 3. Non-thermal, non-specific effects (chemical transformation accelerations that have not been attributed to either thermal or specific microwave effects).

Indeed, as a result of rapid heating within the material due to the use of microwaves, reaction times of many microwave-assisted organic reactions are shortened and allow higher yields and selectivity to be obtained. Another good reason to use microwave heating is that there is no direct contact between the energy source and the reactor walls as microwaves pass through the vessel walls, which are almost transparent to them, directly to interact with the reactants [50].

#### 4. Microwave-Assisted Pyrolysis (MAP)

As mentioned previously, when compared to conventional heating, microwave heating presents various advantages, which influence significantly the yield and characteristics of the resulting products. Products from microwave pyrolysis obtained by using appropriate power levels may have high heating values; they may also yield higher gas and solid fractions, but lower liquid products than conventional pyrolysis. Indeed, through the use of microwave pyrolysis, almost half of the lignocellulosic biomass can be converted to gaseous products, mainly consisting of H<sub>2</sub>, CH<sub>4</sub>, CO and CO<sub>2</sub> and this gas product will possess a higher energetic value because of its high H<sub>2</sub> and CO yields [42].

Many researchers have devoted time and resources to microwave-assisted pyrolysis of biomass since recent years due to its advantages [2,6,7,51–58]. These studies have mostly

focused on what the use of microwaves can bring to the pyrolysis process when compared to the use of conventional heating. This review will endeavour to group together significant research works performed in recent years concerning microwave-assisted catalytic pyrolysis while focusing mainly on the reactions carried out in fluidised bed reactors.

Setups used at the laboratory scale are typically fixed beds utilising continuous gas flow ones [59]. Microwave reactors may be differentiated based on applicator design, wavelength, flow and power source type [59]. Firstly, the applicator, also known as the cavity, is the structure where the dielectric material to be heated is placed. There are three types of applicators [59]:

- 1. Multimode applicators: the most commonly used types of applicators for domestic and laboratory purposes, where a large number of resonant modes for operational frequency are hosted.
- 2. Single-mode applicators: most widely used for heterogeneous gas-phase reactions; capacity to attain high temperatures at low powers. These applicators are able to deliver a highly concentrated energy field, leading to faster heating rates.
- 3. Travelling-wave applicators: microwaves travel in only one direction, ensuring no back-reflection of waves and hence, no non-uniform interference in the waveguide (channel through which microwave energy propagates from transmitter to receiver) and no standing wave formation.

Secondly, the type of waveguide used is important as each type can only support specific modes of wave propagation [59]. Rectangular ones are the most commonly used types owing to their compatibility with the operational modes needed and their ease of being fabricated [59]. Next to be considered are the generator types. Microwave reactors are typically powered by magnetron tubes. However, magnetrons function at a unique frequency and have short lifetimes (2000–10,000 h). New emerging technologies include solid-state amplifiers which can vary frequency during their operation. The advantage of changing frequency is to mitigate hot spot formation and random wave interactions [59]. Finally, a microwave system can be dimensioned and optimised for specified reaction flow conditions. Depending on various cases, fixed bed, batch or fluidised bed reactors may be used.

Lab-scale microwave setups include a microwave power generator, waveguides, a cavity withholding the reactor, an autotuner, sliding short, temperature and flow controllers, gas supply units and a cooling system [59]. Figure 5 illustrates an example of a common type of microwave setup used for the pyrolysis of biomass waste. The setup presented here was used by Mokhtar et al. [60].



Figure 5. Schematic of microwave reactor as used by Mokhtar et al. (Adapted from [60]).

#### 4.1. Effect of MAP on Pyrolysis Product Distribution

Based on the literature, MAP is reported to be much better than conventional pyrolysis in terms of product distribution, yield and quality. Indeed, Ge et al. [55] found by comparing the effects of different heating sources (direct thermal, solar, infrared and microwave heating) on liquid yield obtained from pyrolysis under the same operational conditions that microwave heating was the most efficient heating method in order to achieve the highest bio-oil yield. Several studies have been performed on the effect of the intensity of power used for microwave heating on the products [61–65]. These have shown that the minimum power required to initiate the pyrolysis process is 300 W. However, powers less than 480 W yielded low bio-oil quantities. Increasing the microwave power used resulted in enhancing gas and bio-oil formation while diminishing char formation. It can also be noted that maximum gas yield is obtained at the maximum wattage used.

Domínguez et al. [65] studied the MAP and conventional pyrolysis of sewage sludge using graphite as a microwave absorber at temperatures ranging from 800 to 1000 °C. They used a multimode microwave cavity oven with a flow of 10 mL/min in a quartz reactor, maintaining a constant power input of 1000 W and microwave frequency of 2450 MHz. The temperature of the sample was monitored throughout the experiment through an infrared optical pyrometer. They found that a higher amount of bio-oil was obtained from MAP and these oils were found to contain virtually no polycyclic aromatic hydrocarbons (PAHs), which are undesirable since they are carcinogenic (present in significant amounts in oil obtained from conventional pyrolysis). Moreover, Fernández and Menéndez [66] examined the conventional pyrolysis and MAP of a series of biomass wastes: sewage sludges, coffee hulls and glycerol using the same reactor and conditions as Domínguez et al. [65]. They found higher quantities of syngas and less  $CO_2$  in the gaseous components from MAP as compared to those from conventional pyrolysis. They also observed that glycerol gave the highest concentration of syngas out of all the feedstock, but it also gave the lowest H<sub>2</sub>/CO ratio. Sewage sludges exhibited the opposite tendency while coffee hulls showed an intermediate behaviour.

Liu et al. [67] investigated the MAP and conventional pyrolysis of sewage sludge over a range of temperatures of 600 to 900 °C. The reactor used for conventional pyrolysis was a horizontal fixed-bed quartz tubular one, having a 60 mm internal diameter (i.d.)  $\times$  900 mm length. It was heated in a 2200 W electrical furnace. The power used for MAP was 1400 W, the reactor a 2.45 GHz multimode tubular quartz one with a 45 mm i.d. and 750 mm length. A flow of 300 mL/min of N<sub>2</sub> was used to ensure an inert atmosphere. Despite the two setups not being identical, the authors found that when the temperature was increased, the product yields for conventional pyrolysis varied significantly, while those for microwave pyrolysis showed only a slight change. For instance, during conventional pyrolysis, H<sub>2</sub> yield went from 1.26 mmol/g at 600 °C to 9.07 mmol/g at 900 °C whereas the yield during MAP changed from 1.84 mmol/g to 3.67 mmol/g at the same temperatures. This difference was attributed to the fact that more hydrogen atoms were converted to tar compounds instead of being released into the syngas under MAP, as observed by a higher H/C ratio under MAP.

Furthermore, microwave-induced pyrolysis of palm oil biomass using char as a microwave absorber was carried out by Salema and Ani [68]. The authors used a 1 kW modified domestic microwave system with a 2450 MHz frequency. The microwave cavity was modified to accommodate a fluidised bed quartz reactor (0.1 m i.d.  $\times$  0.15 m height). Their setup is illustrated in Figure 6. They used a microwave power of 450 W and an exposure time of 25 min for each experiment. Different ratios of biomass to microwave absorber (1:0.25, 1:0.5 and 1:1) and an N<sub>2</sub> flow rate of 20 L/min were used in the experiment series. They found the maximum bio-oil yield and lowest char yield at a biomass to microwave absorber ratio of 1:0.5, showing that the quantity of microwave absorbers or catalysts used did affect the pyrolysis product yields. They also concluded that the use of an eco-friendly microwave absorber (bio-char, in this case) can help operate the microwave reactor at a lower power input, thus reducing the need for high power MAP.



Figure 6. MAP setup used by Salema and Ani (Adapted from [68]).

#### 4.2. MAP in Fluidised Bed Reactors

Besides the study led by Salema and Ani [68] mentioned earlier, other researchers have also tried out MAP experiments in FBRs. One such example is Adam et al. [69], who developed a methodology for a microwave fluidised bed system based on processing raw biomass, without adding any microwave absorbents (Figure 7). The authors determined the minimum fluidisation velocity ( $u_{mf}$ ) of the biomass used, sycamore, through cold fluidisation tests in a 50 mm i.d. and 70 cm height acrylic column. They found  $u_{mf}$  values of 0.06–0.81 m/s corresponding to 45–2360 µm particle sizes, respectively.



Figure 7. MAP FBR used by Adam et al. (Adapted from [69]).

The authors found that particle sizes <600  $\mu$ m exhibited homogeneous fluidisation, with no channel formation, contrary to bigger particle sizes. It was also found that a minimum power density of 54 W/m<sup>3</sup> was needed to reach 400 °C; a higher power density value would enable reaching the temperature more quickly. According to the simulations run by Adam et al. [66], the optimum dimensions and operating conditions of the microwave cavity would be a height of 30 cm, a width of 24 cm, waveguide position of 20.10 mm  $\times$  162.50 mm (Y and Z positions, respectively), an input power of 6 kW and a microwave frequency of 2450 MHz. However, the authors noted that a compromise would be needed on the input power when designing an actual experimental setup.

#### 4.3. Catalytic MAP

It was found that through the use of catalysts during MAP, the yield and quality of biooil may be enhanced [70]. However, depending on the type of catalyst used, the production of bio-char or syngas may be favoured at the expense of that of bio-oil. Ge et al. [71] and Morgan et al. [57] have made an exhaustive list of relevant studies having been performed on different catalysts and process parameters used during MAP of biomass in recent years. The most significant and pertinent ones to the aim of this review have been detailed further down this text.

As with conventional pyrolysis, MAP also includes two processes for the use of catalysts: in situ and ex situ catalytic MAP [57]. The difference between the two is that during ex situ MAP, the biomass and catalyst are not in contact with one another; the volatiles generally pass through a packed-bed catalyst reactor after they leave the quartz reactor where pyrolysis takes place under microwaves.

The most common type of catalysts used in MAP, as with conventional catalytic pyrolysis, are zeolites such as HZSM-5, H-Ferrierite, H-Modernite and H-Y. These catalysts, as mentioned earlier, are very effective in enhancing the properties of bio-oil through cracking [72]. One noteworthy article written by Muley et al. [73] deals with the ex situ catalytic upgrading of pine sawdust pyrolysis vapours using a zeolite catalyst in a travelling wave microwave reactor. The authors then compared the results obtained with those from conventional pyrolysis. A catalyst:biomass ratio of 1:2 was used and it was noticed that when catalyst temperature increased, liquid yield slightly decreased. The latter amount was also found to be comparable to that obtained from conventional pyrolysis (25–35%). The use of catalysts resulted in higher amounts of aromatic and aliphatic hydrocarbons while the non-upgraded bio-oil mostly consisted of ketones, phenols, alcohols and aldehydes. The gas yield, on the other hand, increased as the catalyst bed temperature increased. Gas composition went from CO (the highest) to  $CO_2$  to  $CH_4$  to finally,  $C_2$ - $C_5$  gases (the lowest). No mention of  $H_2$  was made. As for coke, a high C/H ratio was observed for coke that was deposited on the catalyst surface, making it aromatic in nature. This ratio increased with temperature when MAP was used.

A selective summary of recent notable research works published on microwave pyrolysis using zeolites as a catalyst has been presented in Table 6. It should also be noted that the table also contains those performed on pyrolysis or co-pyrolysis of plastic wastes since, as mentioned earlier, more recent research studies have been focusing on this type of feedstock.

Other types of catalysts used in the catalytic MAP of biomass are metal oxides, most commonly NiO, CaO, CuO and MgO [57]. Wu et al. [72] performed the catalytic MAP of waste cooking oil under temperatures ranging from 350 to 550 °C, using CoO, NiO, ZrO<sub>2</sub>, SrO, CeO<sub>2</sub> and CaO as catalysts, both in- and ex situ. They also studied the reaction using a mixture of different ratios of HZSM-5 and metal oxides. The reactor used was a catalytic MAP system with a frequency of 2450 MHz and a power input of 0–800 W. The microwave-absorber used was 300 g of 5 mm diameter SiC beads.

Their results showed that using higher pyrolytic temperatures increased monocyclic aromatic hydrocarbon formation despite diminishing overall bio-oil yield. However, increasing the temperature from 500 to 500 °C only resulted in a 1.16% increase in benzene-toluene-xylene (BTX) production. Using metal oxides, especially CaO, as a catalyst, promoted the formation of polycyclic aromatic hydrocarbons, which were produced in significantly less proportions when only HZSM-5 was used as a catalyst. The authors also found that an ex situ configuration suited co-catalysis of metal oxides and HZSM-5 more than an in situ one. The highest BTX yield found by the authors (702.20 mg/mL) was produced at 500 °C, using an HZSM-5:CaO ratio of 2:1 in an ex situ configuration. Other researchers have also used metal oxides during their catalytic MAP experimental works. Some significant findings have been summarised in Table 7.

Feed	Reaction Conditions					Results			
	Catalyst Used	Reactor Used (Power and Frequency)	Temperature (°C)	WHSV (g feed/g cat. h) or F/C Ratio	Bio-Oil Yield (wt. %)	Products and Conclusions	ixei.		
	HZSM-5					WCO:LDPE used was 1:1. Reaction			
Waste cooking oil - (WCO) and	Η-β	_	550	2:1	-	conditions used produced maximum yield of BTX and minimum yield of polyaromatic			
low-density	Н-Ү	Fixed bed (-)				hydrocarbons. Efficiency of catalysts on	[74]		
polyethylene (LDPE) –	SAPO-34	_				SAPO-34 < H- $\beta$ < H-Y < HZSM-5.			
Corn straw	MCM-41 mixed with ZSM-5	Fixed bed (750 W and 2450 MHz)	450–650	1:2	-	Carbon outputs of aromatics and olefins peaked at 550 °C. Addition of MCM-41 inhibited formation of coke on ZSM-5 surface.	[75]		
Rice straw				44.4. 14.7. 11.1 g	21.5	Catalytic upgradation of pyrolytic vapours of biomass and polymer mixtures produced de-oxygenated bio-oils with properties	[76]		
Bagasse		Fixed bed			22.4				
PP	HZSM-5	(3.2 kW and 2.45 GHz)	500	feed/g cat. h	h 74.2 similar to conventional fuel oil. WHSP of 11 violed diabar selectivity to uncerture	similar to conventional fuel oil. WHSP of			
PS					92.3	aliphatics and aromatic hydrocarbons.			
LDPE	NiO 2 stage fixed bed (1.8 kW and 2.45 GHz) H-Y	450 (00	20:1, 15:1, 10:1, 5:1	20.1 15.1 10.1 5.1	20.1 15.1 10.1 5.1	201 151 101 51	22 57	Optimum conditions were found to be 500 °C pyrolysis temperature, 450 °C catalytic temperature and LDPE:H-Y of 10:1. Results	[52]
		430-000		32-37	obtained at these conditions were 56.53 wt. % oil and 93.80% gasoline-range fraction. Addition of catalysts favoured formation of aromatics and inhibited that of aliphatics.	[33]			

**Table 6.** Summary of recent works on catalytic MAP using zeolites as catalyst.

Configuration	Catalyst	Feedstock	Microwave Power (W)	Feedstock:Catalyst Ratio	Pyrolytic Temperature (°C)	Findings	Ref.
In situ	NiO, CuO, CaO, MgO	Corn stover	500	10:1–33:1	450–520	The authors found that pyrolysis under an $N_2$ atmosphere was more efficient than one under a $CO_2$ atmosphere due to the fact that $CO_2$ possesses better heat absorbability and so, its use reduced heat for pyrolysis. The catalysts were found to increase maximum temperature and mass reduction ratio, but they also decreased the solids' calorific values. Moreover, use of catalysts diminished PAHs formation, making the bio-oil less toxic.	[77]
In situ	NiO, CuO, CaO, MgO	Sugarcane bagasse	500	10:1–33:1	490–532	Addition of catalysts resulted in an increase in mass reduction ratio and reaction rate, but in a decrease in maximum temperature. Use of NiO and CaO enhanced H <sub>2</sub> production while use of NiO and CuO lessened it. Addition of CaO and MgO improved gas production while NiO and CuO favoured liquid production.	[78]
In situ	CaO, CaCO <sub>3</sub> , NiO, Ni <sub>2</sub> O <sub>3</sub> , γ-Al <sub>2</sub> O <sub>3</sub> , TiO <sub>2</sub>	Sewage sludge	700	10:1	-	Addition of catalysts was found to affect temperature evolution of sludge, product distribution and gas composition. The temperature rise rate was found to be highest with CaCO <sub>3</sub> , followed by, respectively, NiO, TiO <sub>2</sub> , Ni <sub>2</sub> O <sub>3</sub> $\approx \gamma$ -Al <sub>2</sub> O <sub>3</sub> and CaO, which caused virtually no temperature rise. Ni-based catalysts used favoured decomposition of organic matters in sludge and highly increased bio-oil and CO-rich syngas yields. CaO gave rise to a H <sub>2</sub> -rich syngas while $\gamma$ -Al <sub>2</sub> O <sub>3</sub> and TiO <sub>2</sub> showed no impact on gas percentage or H <sub>2</sub> :CO ratio.	[79]
In situ	CaO, Fe <sub>2</sub> O <sub>3</sub>	Sludge	-	10:1	500–900	$Fe_2O_3$ was found to favour bio-oil production while CaO improved gas formation. The best quality of bio-oil was obtained at 800 °C while using CaO. It was also observed that CaO privileged H <sub>2</sub> formation while $Fe_2O_3$ enhanced CH <sub>4</sub> production.	[80]
Ex situ	HZSM-5, MgO	Low-density polyethylene (LDPE)	750	0, 1:2, 1:1 and 2:1	450-600	LDPE was found to be a good $H_2$ donor to improve bio-oil properties; methoxy phenols were converted to phenols and alkylated phenols. HZSM-5 favoured aromatics production while MgO improved alkylation of phenols. Optimum parameters were found to be 500 °C and feedstock to catalyst ratio of 1:1.	[81]

**Table 7.** Notable works on MAP using metal oxides as catalyst.

Apart from zeolites and metal oxides, carbon-based catalysts have also been considered good candidates for catalytic MAP studies as they can act as both catalysts and microwave absorbers [58]. One important research work was led by Omoriyekomwan et al. [82]. The latter studied phenol production from palm kernel shell pyrolysis at 400, 500 and 600 °C using a 2000 W microwave generator. The authors used 10% activated carbon or 20% lignite char as a catalyst. It was found that the addition of the catalysts enabled pyrolysis temperature to increase as biomass alone is a poor microwave absorber. Bio-oil yield also improved with the presence of the catalysts. The highest concentration of total phenolics was 71.24%, with the highest concentration of phenol of 64.58% in bio-oil, was obtained at 500 °C using activated carbon. Other research works performed using carbon-based catalysts for MAP include those made by Zhang et al. [83] and Chen et al. [84]. All in all, significant results included that carbon-based catalysts gave rise to higher heating rates. When these catalysts are doped with metal precursors, syngas yield increased importantly, while bio-oil yield was mostly impacted positively by the use of activated carbon as catalyst.

#### 5. Conclusions

Even though conventional and microwave pyrolysis technologies are difficult to put on par because of the presence of microwave irradiation, a comparison between their respective products is helpful to shed some light on their efficiency. Recent research works performed on microwave pyrolysis of different feedstocks with and without the use of catalysts were reviewed in this work. This technology presents very favourable odds of being successfully scaled up to an industrial scale, given its practicality and interesting results. Indeed, given the fact that MAP has proven to have a more rapid volumetric heating, have more precise control and be more energy saving, it can be established to be more interesting than the conventional means of performing pyrolysis. However, as of today, the most common type of reactor used for industrial pyrolysis applications is the fluidised bed reactor [85]. MAP being a fairly recent technology, most of the research was conducted on fixed bed reactors. Few studies have been performed in FBR and they have mostly shown that these reactors need a fair microwave power for efficient pyrolysis to take place. So as to find a valid compromise, the use of an eco-friendly microwave absorber such as bio-char may be warranted. However, more detailed studies such as studying the reaction kinetics and numerical simulation of the overall process need to be performed in this direction so as to prove this technology's worth in being used in upcoming industrial applications.

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