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Pollutants emission scenarios for residential ventilation

performance assessment. A review

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Abstract

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assessment.

- Performance-based approaches for energy consumption in new buildings are increasingly used in codes and standards. Similarly, there is ongoing research on performance-based approaches for ventilation systems. The aim is to assess indoor air quality (IAQ) performance in low-energy houses at the design stage. In this context, the whole-building IAQ performance modelling process raises a very important question: What are the emission scenarios and occupancy schedules to be used as entry data to calculate the selected performance indicators? We focus on this issue through a literature review: firstly oriented toward the occupancy considerations so as to define the emission rates for CO₂, moisture, formaldehyde and PM_{2.5} to be use as input for ventilation performance
- Based on this review, we propose daily schedules for the occupants and their associated moisture and CO_2 emissions. We completed them with emission rate values for the main pollutant sources from indoor activities regarding moisture emissions from laundry, showering and cooking; $PM_{2.5}$ emissions from cooking and formaldehyde from building materials and furniture. Finally, from these values we built three emission rates classified for $PM_{2.5}$ and formaldehyde: high, medium and low.
- 22 **Keywords:** Ventilation, indoor air quality, performance, residential buildings, scenarios, review

1 Introduction

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Net zero-energy residential buildings are in increasing demand in Europe because of the energy performance building directive [1]. Ventilation strategies have a large impact on the heat balance and the associated air conditioning energy need. Improving ventilation strategies also has great potential to reduce the contribution of residential buildings to total energy consumption. Ventilation systems and strategies play another important role in buildings' indoor air quality (IAQ), significantly affecting public health [2–6]. People spend 60–90% of their life in indoor environments (homes, offices, schools, etc.). The current damage to public health estimated by Logue et al. [7] in disability-adjusted life years (µDALY) per person per year from all sources attributable to IAQ, excluding second-hand smoke (SHS) and radon, ranged between the health effects of road traffic accidents (4,000 µDALY.pers⁻¹.year⁻¹) and heart disease from all causes (11,000 µDALY.(pers⁻¹.year⁻¹). Health gains in Europe (EU-26) attributed to effective implementation of the energy performance building directive, which includes indoor air quality issues, have been estimated at more than 300,000 DALYs per year. In this context, in new certifications and future building regulations, building performance should be extended to indoor environment quality, beyond simply energy performance. In the energy performance field, successive regulations encouraged a performance-based approach, based on an energy consumption requirement for heating and/or cooling at the design stage [8]. In the building ventilation field, regulations throughout the world are mainly still based on prescriptive approaches, with airflow or air change rate requirements [9]. There is ongoing research on performance-based approaches for residential building ventilation; aiming to replace prescriptive approaches. Indeed, the latter methods, with prescribed ventilation rates only, are an imperfect way to achieve a given IAQ. On the opposite, a performance-based approach, using for example IAQ performance indicators instead of ventilation rates, should be more appropriate.

Given the lack of relevant performance evaluation method for ventilation systems, we previously developed a performance-based approach for assessing ventilation performance at the building scale, at the end of the design stage, much like the regulatory energy performance calculation. This would ensure that ventilation is designed to avoid risks for occupants' health. We should also keep in mind, that Indoor Air Quality relies on two main principles: reduction of indoor pollution sources and efficient ventilation. Indeed, the ventilation system can not ensure the all pollutant dilution without a significant impact on the building energy performances. The need to reduce sources of indoor pollution is also a key element in ensuring good IAQ, for example by avoiding smoking cigarettes indoors, burning candles etc... Sources reduction is out of the frame of the developed method, which is focussing exclusively on the ventilation performance assessment. The following scheme gives an overview of the whole building IAQ modelling process for this performance-based approach, the inputs and outputs needed, and identifies the scope of the present paper (Figure 1).

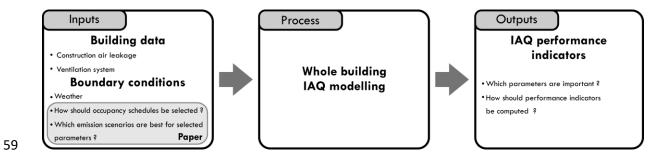


Figure 1. Performance-based approach for ventilation.

- To develop this type of performance-based approach, the following two scientific barriers had to be considered:
 - What are the relevant parameters, including pollutants, to use for calculating performance indicators and what indicators should be used?
 - What are the corresponding relevant input data to use regarding occupancy and emission scenario parameters?
- Relevant pollutants and performance indicators have been investigated and are often based on at least moisture, CO₂, formaldehyde and particle matter PM_{2.5} [10,11]. Indeed, formaldehyde and

PM_{2.5} are considered as two pollutants of concern in residential indoor air and were identified among the five pollutants with the highest median DALY loss estimates [13, 7]. In detail, the indoor sources contributing to elevated indoor particle matter levels are mainly related to human activities that generate peak emissions [14]. On the contrary, the sources of formaldehyde emissions are more uniformly distributed, both in space and time, and related to building construction materials, furniture and decorative materials [12,7,13–17]. This makes PM_{2.5} and formaldehyde interesting for their complementarity. Moisture and CO₂ where selected as historical parameters widely used in the standards and in ventilation systems controls [10,18]. Indoor humidity level should be controlled in order to avoid problems related to condensation, mould growth and material durability. CO₂ concentration is related to human presence and is recognised as a marker for other bioeffluents. Several other pollutants could have been selected, but for the performance-based method to be applied in practice, it is important to promote a low number of pollutants in order to build calculable and useful IAQ indicators.

To calculate IAQ performance indicators as cumulative exposures, we also need the occupancy schedules and parameters emission rates at the design stage of a building. In this paper, we focus on this second barrier aspect through an extensive literature review on the occupancy schedule considerations in a building and CO₂, humidity, PM_{2.5} and formaldehyde emission rate scenarios.

2 Methodology

- We reviewed the available literature (Standards, Research reports, Scopus, Elsevier, AIVC database)
 using the following terms:
- First: "ventilation performance", "smart ventilation performance", "ventilation assessment",

 "ventilation IAQ performance".
- 91 Second: "occupancy patterns", "occupancy schedules", "occupancy IAQ" and "occupant 92 IAQ".

- Last: "IAQ emission", "IAQ rate", "IAQ sources", "emission rate", "cooking emission rate", combined with "CO₂ "a", "moisture", "humidity", "formaldehyde", "fine particle matter", "PM_{2.5}", "pollutant", "occupant".

The first important point we have to consider in this review is the accuracy of the emission rates. These data are not directly measured but are calculated using mass balance equations, combining airflows or air change rate measurements and parameter concentration measurements. As a result, several sources of uncertainty exist: measurement uncertainties on airflows and air change rates, measurement uncertainties on parameter concentrations, and modelling uncertainties (mass balance includes assumptions on occupancy, room configuration, weather data, etc.). Measurement uncertainties include the precision and bias of the measurement device, the impact of the user, the impact of the weather data (for air change rates and airflows), and is well documented in the ISO guide [19]. Air change rates [20–23], ventilation airflows [24,25] and pollutant concentration measurement accuracy, notably sensor accuracy [26–31], are a broad area of research for *in-situ* and laboratory measurements. We selected only research papers and literature with consistent data on emission rates, with sufficient description of calculation methodology and of measurement uncertainties.

In addition, at the design stage of a residential building, it is difficult to fully describe occupancy for the entire life span of a building: number and age of the occupants, activities, schedules, etc. It is also impossible to precisely describe all the parameter emission rates for the occupants, their activities, the building materials and furnishings. In a performance-based approach at the design stage of a building, the standards and regulations dealing with this issue must also be considered. We therefore preferred using cyclic schedules (fixed schedules which are reiterated every week), differentiating metabolic emissions, building and occupants' activity emissions, as proposed for humidity and CO₂ in several standards and regulations [10,32–37]. The approach aims to provide a relative comparison of the performance of several ventilation systems, configurations and airflow

rates, building design choices related to ventilation, IAQ labelling products, and even several 118 119 occupant IAQ awareness levels. 120 Then we selected references allowing us to build a scenario to be used as entry data to calculate the 121 performance indicators, in order to assess the ventilation performance of a building at its design 122 stage. 123 This paper describes a detailed daily life required to calculate IAQ performance indicators. CO₂ and 124 moisture performance indicators use occupants' metabolism and activity (only for humidity) 125 emissions, combined with occupancy schedules, as input data. To calculate the cumulative exposure indicators (for instance, for formaldehyde and PM_{2.5}), we also need detailed occupancy schedules for 126 127 each occupant. In this literature review, the duration of occupation by room throughout the day and the type of occupant (adult/child) were sought because they could influence the emission rates. In 128 129 this section, we reviewed 10 papers. 130 Then the rates and scenarios for moisture, CO₂ and HCHO, PM_{2.5} emissions were studied. CO₂ and 131 moisture emissions from human metabolism and activities are quite well documented. We reviewed 132 12 papers and then built and proposed a scenario based on this analysis. 133 In contrast, formaldehyde and PM_{2.5} emission rates remain exploratory, especially in a design 134 approach for ventilation performance assessment. These pollutant emission and concentration 135 measurements and modelling are complex, because of the physics of phenomena involved (e.g. 136 diffusion, resuspension for PM, combined effects for formaldehyde) and available measurement 137 techniques. In addition, formaldehyde emissions are highly dependent on building and furnishing 138 materials. Consequently, we attempted to build low-, medium- and high-polluting emission rate 139 scenarios and chiefly focus on measured pollutant emission rates stemming from the building, the furnishings and the occupants' activities. However, multiple types of data are available and cannot 140

be directly used together for scenario proposals, so they were categorised in the formaldehyde and

PM_{2.5} sub-sections in three measurement types:

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- Chamber-tested loads: Pollutant emissions due to specific activities, products and building materials obtained using test chambers under standardised conditions as described for VOC in ISO 16000-9 [38]. We found more data on formaldehyde than PM_{2.5} emission rates.
 - Lab kitchen: PM_{2.5} emissions due to specific activities measured in unoccupied homes or in experimental setups.
 - *In-situ loads*: Emission rates measured at the dwelling scale in occupied or unoccupied buildings, resulting from the combination of pollutant concentration and air change rate measurements in dwellings. We found few data on formaldehyde and PM_{2.5} emission rates.

For $PM_{2.5}$ emissions, of the first 29 references analysed on emission sources and particle exposure in indoor environments, we selected eight published articles to build and propose a scenario based on this analysis. For formaldehyde emissions, we reviewed 22 references to build a scenario.

At the end, based on 73 articles reviewed, we provide a summary of the occupancy and emission rate scenarios selected. For emission rates, we conducted a review of the international literature, then we selected the rates and built the scenarios for a European, or even French application.

3 Occupancy considerations

3.1 Residential occupancy schedules in the literature

Precisely described data fitting our purposes are rarely found in the literature. Energy performance calculation methods use global occupancy schedules at a whole building scale (indoor/outdoor), whereas a multizone approach requires assuming an occupancy scenario in each room of the house, at each time step, both for the emission rates and exposure aspects.

In energy performance calculations, [39] proposed seven discrete occupancy profiles based on a time survey on more than 3000 Belgian dwellings. They differentiated outside, inside awake and inside asleep contexts.

A French IAQ national campaign based on a representative sample of the population included 567 homes and 1612 occupants [5]. A total of 1375 occupants provided precise information on their schedules and occupation in the rooms (25% of the sample) so that a database of 1,386,000 tenminute time steps with precise information on occupant location was available and analysed in this study. The results show that people spend on average 67.3% of their time in their homes. This is consistent with results of other surveys in Europe (EXPOLIS, 56–66%) and in the United States (NHAPS: 68.7%). Other interesting results are available in this study:

- The differences between weekend days and week days are minimal: the 3 days with the highest occupancy duration are Sunday (16.6 h), Wednesday (16.5 h) and Saturday (16.3 h), followed by Thursday (16.1 h). Friday is the least occupied day (15.7 h).
- There is no statistical difference between working periods and holidays.

- Occupants are more likely to be at home between 12.00 pm and 2 pm and between 7 pm and 7 am.
 - Time spent at home is divided, on average, into 9 h 16 min spent in bedrooms, 2 h 49 min spent in the living room, 2 h 40 min spent in the kitchen and 38 min spent in the bathroom.

To achieve the occupancy consideration in a building this schedule information needs to be completed by a description of the occupants. Human emissions stem from the metabolic functions such as respiration, transpiration and perspiration, depending on different factors such as age [40] (contradicted by [41]) and activity level. Because of the development and growth of the organs of a child, its basic metabolism can reach twice the adult rate. The basic metabolism is defined as the minimum energy expenditure of an organism to ensure daily functions at rest. It decreases between 6 years and 18 years: from 19% for boys to 27% for girls [42]. As a result, as explained by [43], even if their body surface area is lower, children's CO₂ and humidity emission rates are as high as those of adults and may even be higher. Measures taken in 20 occupied apartments showed that children's emissions were often under-estimated in the literature and were closer to adults' emissions [44], with emissions measured at 13 L.h⁻¹. for a child and 16 L.h⁻¹ for an adult. The ECA guidelines for

- ventilation requirements in buildings [41] compiles data from three studies [45–47], giving emission
- rates for adults and children (Table 1).

	CO₂ emissions [L.h ⁻¹ .occupant ⁻¹]	Water vapour [g.h ⁻¹ .occupant ⁻¹]
Sedentary adult	19	50
Low physical exercise	50	200
Medium physical exercise	100	430
High physical exercise	170	750
Children, 3-6 years	18	90
Children, 14–16 years	19	50

Table 1. Pollutant load caused by occupants. Source: [41]

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3.2 Occupancy schedule proposal

For our purposes, we used the detailed data from the French IAQ national campaign [5]. The following daily occupancy duration (rounded for a 10-min time step simulation) was retained:

- 200 9 h 20 min in bedrooms,
- 201 2 h 50 min in the living room,
- 202 2 h 40 min in the kitchen,
- 203 40 min in the bathrooms,
- For a total of 9 h 20 min asleep, 14 h 40 min awake, 9 h outside and 15 h inside.

These occupancy schedules should be carefully adapted depending on countries and their habits (meal times, school times, work times, etc.).

The number of occupants must be assumed, taking into account the size of the house, to avoid under-estimating the ventilation airflow rates. We would suggest setting the number of occupants based on the number of bedrooms, assuming two occupants in one bedroom and one in each of the others. At the design stage of a building, we could also assume that all occupants are adults, based on the data reported in Table 1.

In the next section, emissions due to occupants will occur where and when occupants are assumed to be present.

4 Emission rate scenarios for a ventilation performance assessment at the design stage of a residential building

4.1 Moisture

4.1.1 Moisture emission rates in the literature

In a building the main moisture sources are linked to the occupants' activities such as showering, cooking, dish washing and laundry drying. In addition, the building envelope helps to regulate indoor humidity by exchanging moisture flows with the indoor air. This phenomenon must be represented in the model in order to provide realistic results. We consider this phenomenon of moisture exchange as a buffer (part of the model) and not as an emission source.

In most of the references analysed, mainly including standards, related production is given for a precise activity with a duration per day, sometimes depending on the number of occupants [32–35,37] (Table 2). Note that two normative documents [34,48] proposing the schedule approach also alternatively suggest using an average constant moisture emission rate, depending on the overall moisture production and the number of occupants. Alternative approaches based on experimental

Table 2: Moisture emission rates of activities

measurements are also proposed [49,50] (Table 2).

Activities	Emission rate	Duration	Reference
Cooking /person			
- Breakfast	100 g.h ⁻¹	0.5 h	
- Lunch (weekend)	75 g.h ⁻¹ (150 g.h ⁻¹)	1 h	CCFAT [37]
- Dinner	300 g.h ⁻¹	1 h	EN 15665 [35]
Shower (a) CCFAT / EN 15665	300 g	0.5 h / 6 min	TM 12002 [22]
Laundry ^(b)	100g.h ⁻¹	2 h	
Laundry drying ^(b)	50g.h ⁻¹	20 h	
Electric cooking device	2000 g.day ⁻¹ 3000		
Gas cooking device	g.day ⁻¹		British standard,
Hand dish washing	400 g.day ⁻¹		1991 [48] &
WC/shower/dish washing	200 g.day ⁻¹ .person ⁻¹		TR-14788 [34]
Laundry	500 g.day ⁻¹		(called A)
Inside drying ^(c)	1500 g.day ⁻¹ .person ⁻¹		
Cooking			TD 14 00 [24]
- Breakfast	0.6 l.s ⁻¹	10 min	TR-14-88 [34]
- Lunch	1 l.s ⁻¹	10 min	(called B)

- Dinner	1.5 l.s ⁻¹	10 min	
Shower/person	0.5 l.s ⁻¹	10 min	
Laundry drying	0.06 l.s ⁻¹	12 h	
Moisture generation rate	Low/medium/high		
- 1 person	3.5/6/9 kg.day ⁻¹		British standard,
- 2 persons	4/8/11 kg.day ⁻¹		1991 [48] &
- 3 persons	4/9/12 kg.day ⁻¹		TR-14-788 [34]
- 4 persons	5/10/14 kg.day ⁻¹		(called C)
- 5 persons	6/11/15 kg.day ⁻¹		
Cooking meals			
- Breakfast	109 ± 20 g	15 ± 5 min	
- Lunch	288 ± 68 g	30 ± 2 min	
- Dinner	518 ± 152 g	40 ± 10 min	Evacrimental data
Dish washing			Experimental data
- Breakfast	25 ± 3 g	29 ± 3 min	[49,50] cited in [52]
- Lunch	20 ± 3 g	29 ± 3 min	[49,50] Citeu iii [52]
- Dinner	240 ± 9 g	29 ± 3 min	
Showering	250 ± 50 g	10 min	
Laundry drying ^(d)	1850 ± 670 g	11 ± 2 h	

⁽a) With 1 shower.day⁻¹.person⁻¹

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The occupants' metabolism is also a source of humidity. The most frequent distinction between activity levels is when occupants are asleep or awake. For a household of three people, a study used a value of 2.4 kg.day⁻¹ of water production in each room [51]. Experimental studies also give useful information with confidence intervals comparable to [49,50] (Table 3).

						234	Tabl
M	etabolism emission data	Awake	Asleep	At rest	Sources		
-	3–6 years			90 g.h ⁻¹	ECA guidelines	for 235	e 3:
-	14–16 years			50 g.h ⁻¹	ventilation require		N/a+
-	Adult			50 g.h ⁻¹	in buildings [4:	1] ²³⁶	Met
_	<2 years	30 g.h ⁻¹	10 g.h ⁻¹			237	- abol
-	10–13 years	45 g.h ⁻¹	15 g.h ⁻¹		[40]	237	aboi
-	>15 years	55 g.h ⁻¹	30 g.h ⁻¹			238	_ ism
-	per person	55 g.h ⁻¹	38.5 g.h ⁻¹		[37] & [53]		
-	per person	55 g.h ⁻¹	40 g.h ⁻¹		[35]	239	mois
		55 g.h ⁻¹	40 g.h ⁻¹				
	commended duration of 	Living room	Bedroom		[34] &[48]	240	ture
en	nissions	4 h	10 h			241	emis
		1			Experimental do		-
-	Active people	70 ± 5 g.h ⁻¹	$30 \pm 2 \text{ g.h}^{-1}$	50 ± 5 g.h ⁻¹	[49,50] cited in [sion
-	for 3 people		2.4 kg.day ⁻¹		[54]		_
		(averag	ge 33 g.h ⁻¹ per	person)	[51]	243	rate

⁽b) With x laundry.week $^{-1}$ (CCFAT, 2015) (x = 1–4 depending on the number of inhabitants) EN 15 665 (CEN, 2009) (x = 1)

⁽c) Naturally or with dryer without vent

⁽d) 20% of the total emissions during the first 2 h

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Finally, a review on the indoor moisture also showed sources ranging from very simplified to more realistic sources [54]. The simplest is an average constant emission based on [55] which reviewed nine studies, suggesting the average emission of 270 g.h⁻¹ to be used for a 1-year simulation. This review [54] also showed that several experimental and numerical studies preferred using typical cyclic schedules. Lastly, stochastic scenarios could also be used, as demonstrated by [56,57] in office buildings. For a one-zone experimental building, [54] showed how constant emission rates could result in increasing the comfort range by 10–20%, compared to the use of stochastic scenarios.

4.1.2 Analysis and scenario proposals

First of all, all the metabolism moisture emission rates in the literature reviewed are within the same range, so we suggest using the moisture generation rates for the metabolism emission of 55/40 g.h⁻¹ (awake/asleep). Next step is to quantify the dispersion of moisture emissions rates due to activities, given in Table 2. In order to compared them, we calculated for each reference ([34]-A, [34]-B,[35],[37],[50]) the related daily moisture emissions, assuming one or five occupants, taking into account metabolism, cooking, showering, laundry and clothes drying. We assumed one laundry, one clothes drying per person and per week, and we calculated an average weighted emission rate per day. Lastly, we compared the calculated results expressed as an average emission rate in kg per day to the thresholds given in TR 14 788-C [34] (Table 4,Table 5). From these tables, we can observe that no standard gives high emission rates, and that these are in most cases low, and become medium if we consider five occupants.

	Reference	Calculated daily emissions [kg.day ⁻¹]	Low 3.5 kg.day ⁻¹	Medium 6 kg.day ⁻¹	High 9 kg.day ⁻¹
	TR 14-788-A [34]	4.1	-	Х	-
occupant	TR 14-788-B [34]	2.6	X	-	-
0001	EN-15-665 [35]	1.4	X	-	-
	CCFAT, 2015 [37]	1.6	X	-	-

	Experimental Data [501	2.0	Χ	-	-
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Table 4. Comparing calculated daily moisture emissions with thresholds given in TR 14-788-C (CEN, 2006a), one occupant.

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Table 5. Comparing calculated daily moisture emissions with thresholds given in TR 14-788-C [34], five occupants.

	Reference	Calculated daily emissions [kg.day ⁻¹]	Low 6 kg.day ⁻¹	Medium 11 kg.day ⁻¹	High 15 kg.day ⁻¹
	TR 14-788-A [34]	8.4	-	Х	-
ant	TR 14-788-B [34]	7.2	-	Χ	-
occupants	EN-15-665 [35]	4.9	X	-	-
_	CCFAT, 2015 [37]	7.9	-	Χ	-
-CO	Experimental Data [50]	5.2	Χ	-	-

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Consequently, for our analysis, for the activity emissions, we suggest using the TR 14-788-A [34] data, because it is the most handicapping reference. We combined them with the emission duration given by [49,50] because these data came from in-situ measurements, published in an IEA Annex and cited in [52]. The following moisture generation scenarios could be used:

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- One shower per person per day, with an emission of 1440 g.h⁻¹ for 10 min per shower;
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- Cooking periods per day: 1512 g.h⁻¹ for breakfast for 15 min; 2268 g.h⁻¹ for lunch for 30 min;
- 276
 - 2844 g.h⁻¹ for dinner for 40 min;
- 277
- One laundry per person per week: 252 g.h⁻¹ for 2 h;
- 278
- One laundry drying per person per week (same days): 136.8 g.h⁻¹ for 11 h.
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- This results in an average production of 6 kg.day⁻¹ for five occupants, which is a rather low emission 280 scenario.

4.2 Carbon dioxide

4.2.1 Emission rates in the literature: analysis and proposal

CO₂ emission rates are due to occupant metabolism and depend on the occupants' size and activity. The literature gives the same order of magnitude and generally proposes making a difference between asleep and awake times, adults and children, as summarised in Table 6, which shows a quite good consensus around the value of 18 L.h⁻¹ for an awake adult with a low level of activity. For a sleeping adult, the emission rates vary between 10 and 16 L.h⁻¹.

Table 6: CO₂ metabolism emission rates

Emission rates	[L.(h.person) ⁻¹]	Sources
Sedentary		
- 3–6 years	18	[44]
- 14–16 years	19	[41]
- Adult	19	
Awake	16	[25], [27]
Asleep	10	[35]+ [37]
Awake/asleep		
- <2 year-old	8/4	Annex 27 IEA [40]
- 10- to 13-year-old	12/8	AIIIIEX 27 ILA [40]
- >15-year-old	18/12	
Asleep, measured in occupied apartments		
- Child	13	[44]
- Adult	16	
Child (medium exercise)	10	<u> </u>
Adult (office work)	18	[58]
Adult (asleep)	15	

Given this data, and as we are at the design stage of a building with generally no idea of occupant age, we considered that all occupants are adults, as explained in the above section. Finally, we used the emission rates proposed by Persily [58]: 18 L.h⁻¹ and 15 L.h⁻¹ for an "awake" or "asleep" occupant of a residential building. The first value shows quite good consensus and the second allows one to avoid over-estimating ventilation performance.

4.3 Formaldehyde

4.3.1 Formaldehyde emission rates

4.3.1.1 General considerations

For formaldehyde, several authors have highlighted the correlation of concentrations and emissions with temperature, relative humidity and air exchange rates [59]. Using a multivariate model fit on observational data testing temperature, humidity, the air change rate and outdoor concentration, [60] considered temperature to be the best correlated with the increase in the formaldehyde concentration. A chamber test study proposed a semi-empirical correlation law between the initial material's emittable concentration and the combined effect of humidity and temperature [61]. Moreover, the formaldehyde emissions of new houses from construction materials, such as wood products, are known to be constant for approximately nine months and then start to decrease [62], to reach a steady state emission rate after a few years [59].

4.3.1.2 Rates obtained in chamber-tested loads

The study reported by Plaisance et al. [63] used a passive flux sampler for 6 h to define a linear equation between the formaldehyde mass collected and the emission rate of the tested material in a test chamber, according the ISO 16000-9 standard [38]. Depending on the surface tested, they calculated emission rates within the range [11.2; 682] μ g.h⁻¹.m⁻².

Several databases have been developed to verify such chamber-tested data. Pandora is a very large free-access database for indoor pollutant emission rates [64], with more than 8000 emission rates from the literature classified by sources, including formaldehyde and PM_{2.5}. Other databases were found such as the one developed in the EPEHCT project [65] and the NIST Database [66], including formaldehyde. In these databases, formaldehyde emission rates for common materials can be found with a large spread, as for example for gypsum board (Pandora: in range [0.3; 42] μ g.h⁻¹.m⁻²) or fibreboard medium (NIST: in range [14; 640] μ g.h⁻¹.m⁻², Pandora: [237 – 320] μ g.h⁻¹.m⁻²). As a

conclusion, the range of emission values is quite different from one database to another and the relationship with the in situ rates obtained in houses is complex.

4.3.1.3 In-situ rates obtained in houses

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The EN-15251 standard [67] provides two emission rates for formaldehyde: 50 μg.h⁻¹.m⁻² for lowpolluting buildings (glass, steel, rock) and 20 µg.h⁻¹.m⁻² for very-low-polluting buildings (without tobacco), considering the material surface areas. EN-16798-1 [68] updates these emission rates to 100 and 50 μg.h⁻¹.m⁻², respectively, based on the results calculated for the European Reference Room as specified in CEN/TS-16516. A test conducted by [62,69] was repeated three times on seven unoccupied prefabricated houses and on seven unoccupied site-built houses, located in eastern and southern USA, under two different climates, hot-humid and mixed-humid. The formaldehyde concentration was measured using two active samplers, inside and outside. The indoor sampler was located in the living/dining room 1.5 m above the floor. In addition, SF₆ was used as a tracer gas to measure the air change rates. The average constant emission rate was calculated from the average concentrations measured and the air change rate measured, using the mass conservation equation on the whole house considered as one zone. The result was an average emission rate of 44.17 (± 36%) µg.h⁻¹.m⁻², considering the houses floor surface areas. The study conducted by [60] took measurements of 24 student residence rooms with five different surfaces (flooring, ceiling and walls, doors, bed and other furniture), for three construction ages. Formaldehyde concentrations were measured over 6 h with both conventional active samplers and passive samplers. Thirteen to 15 passive samplers were used per student room, with measurements taken in the room, in the common corridor adjacent to the room, and outside. Air change rates were measured using a CO₂ (tracer gas) injection method. Depending on the age of the building and the type of surface, the resulting average emission rates were within the range [1.4; 87.3] µg.h⁻¹.m⁻²,

considering the material surface areas. Table 7 summarises all the emission rates reviewed.

Materials Emission rates [μg.h ⁻¹ m ⁻²] per m ² of material surface area unless specified otherwise		Reference
Low-polluting building (glass, steel, rock) Very-low-polluting	50	EN-15-251 [67] In-situ loads
building (without tobacco)	20	
Low-polluting building (stone, glass, ceramics and non-treated metal)	100	EN-16798-1 [68] In-situ loads
Very-low-polluting building	30	
7 Unoccupied and 7 Occupied houses	[per m² of floor surface area] average: 44.17 ± 36% median: 41.72	[62,70] In-situ loads
H1 (built in 1998) - Flooring - Ceiling and wall - Door - Bed - Other furniture H2 (built in 1975, renovated in 2003) - Flooring - Ceiling and wall - Door - Bed - Other furniture H3 (built in 1991) - Flooring - Ceiling and wall - Door - Bed - Other furniture H3 (built in 1991) - Flooring - Ceiling and wall - Door - Bed - Other furniture	[Average \pm std dev (range)] $2.3 \pm (1.2-5.5)$ $3.6 \pm 1.7 (1.2-6.3)$ $4.0 \pm 2.0 (1.2-6.4)$ $3.3 \pm 1.8 (1.2-6.7)$ $2.8 \pm 0.9 (1.2-3.6)$ $1.4 \pm 0.7 (1.2-2.4)$ $3.2 \pm 2.0 (1.2-7.1)$ $2.6 \pm 1.6 (1.2-5.5)$ $2.8 \pm 1.7 (1.2-5.8)$ $3.4 \pm 0.6 (2.8-4.4)$ $5.3\pm 3.5 (2.5-13.0)$ $8.8\pm 2.8 (4.1-12.1)$ $7.0\pm 4.2 (1.2-14.7)$ $87.3\pm 37.5 (21.3-131.3)$ $2.9\pm 1.9 (1.2-7.0)$	[60] In-situ loads
Fibreboard medium 1 Fibreboard medium 2 Fibreboard medium 3 Sealing plaster Finishing plaster OSB Chipboard	92.5 135.5 133.3 43.4 682 11.2 244.4	[63] Chamber-tested loads
More than 8000 emission rates from cor	nsumer products and building materials	Pandora Database [71] EPEHCT project [65] NIST Database [72] Chamber-tested loads

Table 7: Overview of formaldehyde emission rates found in the literature

4.3.2 Analysis and scenario proposals

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Few of these formaldehyde data are fully useful for a performance-based approach to ventilation.

We found either few or no data on average in-situ loads directly measured at the dwelling scale, and

especially in low-energy dwellings considered as representative. Consequently, the available data pose two problems:

- Firstly, it is difficult to extrapolate emission rate behaviours from test chamber conditions to *in-situ* conditions, notably because of the complex physical phenomena (combined effects, resuspension, etc.). As illustrated in Table 7, the order of magnitude of emission rates between chamber-tested loads in [63] and in-situ loads in [60] varies by a factor of a 10 to 100.
- Secondly, it is difficult to build robust scenarios from the material, product and activity scale to the dwelling scale, as highlighted in [73]. Indeed, due to the wide variety of materials available, the emission per m² of floor area varies from one building to another. In addition, the type of building materials and furniture and the quantities used (floor coverings, wall paintings, etc.) depend on the purpose of the buildings as well as on the design or construction methods used. Precise data are not yet described in scientific studies. In addition, emission rates for common materials are available with a high variability and even within the same type of material emission properties can vary considerably, as shown by the diversity of values presented in the databases [64], [66] or as illustrated in [63] for the Fibreboard medium 1,2,3. Consequently, arbitrary choices must be made to establish input data (using databases such as Pandora) for a detailed IAQ modelling at the scale of a residential building, as shown by [74].

We accordingly suggest using the simplified calculation method in [75] and applying it to unpublished data gathered on French low-energy homes to calculate average *in-situ* loads at the dwelling scale.

Based on these measurements, we define three classes of formaldehyde emissions to be used as input data for IAQ modelling, and for ventilation performance-based approaches at the design stage of low-energy houses:

- The low-emission class: 4.5 μg.h⁻¹.m⁻², per m² of floor surface area, defined by the minimum calculated value;
- The medium-emission class: 12.0 μg.h⁻¹.m⁻², per m² of floor surface area, defined by the
 median calculated value;
- The high-emission class: 23.6 μg.h⁻¹.m⁻², per m² of floor surface area, defined by the
 maximum calculated value.

4.4 PM_{2.5} particles

4.4.1 PM_{2.5} emission rates in the literature

4.4.1.1 General considerations

The most widely studied PM_{2.5} indoor emission sources are principally candle combustion, smoking and cooking activities. The emission values of hairspray [76] are usually occasional and relatively low, in comparison with candle combustion [77] or incense [78,79], cooking activities [80] and smoking emissions. As described in the introduction, this work focuses on the assessment of ventilation performance, which should be seen as complementary to the reduction of indoor pollution sources. Smoking is a significant indoor emission source but it is not included in this review because it is more relative to the performance of occupants than to ventilation system performance. The source of the emissions can easily be reduced by influencing the habits of the occupants. From this perspective, Borsboom et al. [17] propose that tobacco smoke should not be considered in setting ventilation standards. A similar choice is made for candles and incense: they are related to habits and are excluded from our study.

Several studies showed that cooking is one of the most PM_{2.5}-emitting activities [13,81–83]. Ji et al. [80] corroborated this, providing measurements in an experimental house to quantify occupant exposure to ultrafine particles. They directly calculated this indicator from concentration measurements using occupancy schedules, without calculating emission rates. Each source was

tested at least three times, and the concentration was measured in three different spaces to quantify the impact of the pollutant on the entire dwelling. We could thus classify the source into four categories depending on its global impact intensity (high, medium, limited, low). This study highlighted that the largest sources were: cooking and extra-heating for the high-impact sources, the toaster for the medium-impact sources, and incense, cigarettes, and candles for the limited-impact sources.

PM_{2.5} concentrations and emissions were also strongly correlated with outdoor conditions, intensity and type of ventilation, air leakage level and deposition and resuspension conditions [81,82,84,85]. Given their mass, particle matter is deposited on surfaces by gravity and various common actions can resuspend these particles. Moreover, particle matter can be formed by a chemical gaseous reaction such as between ozone and terpene [86].

Based on this first literature analysis, we retained only emissions from cooking activities to build the PM_{2.5} emission rate scenarios. Two review papers on the chemical components of particle matters [87] and their impact on cooking emission rates [88] have recently been published.

4.4.1.2 Rates obtained in test chambers

A study was carried out in a 32-m³ test chamber in a research laboratory to characterise emissions from various activities (frying, gas stove, smoking, vacuuming, heater, radiator, scented candle, pure wax candle) [78]. The PM_{2.5} concentration was measured by two different particle counters: a condensation particle counter and an optical particle counter. The concentration was continuously monitored before, during and after all the emission tests. A tracer gas decay method was used to determine the air change rate, based on concentration measurements made continuously over 2h with a photo-acoustic spectroscopy device. Emission rates were lastly calculated through air change rate concentration measurements and expressed as particles per minute. Unfortunately, these emission rates in particles per minute cannot be used in cooking emission rate research, because conversion into mg.min⁻¹ is impossible.

Finally, the recent study conducted by O'Leary et al. [89] used a test-chamber protocol with controlled ventilation to very precisely measure the PM_{2.5} emission rate throughout the cooking processes. The four meals selected for this experiment were based on typical European portions and food types from representative data, like the panel method [90] or the Western cooking type survey conducted by [91,92].

4.4.1.3 Rates obtained in a lab kitchen

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Firstly, the study of [93] characterised the particle emissions of several foods (cheese, chips, bacon) by testing the impact of the oil used (sunflower, peanut, olive), the cooking method (frying/grilling) and temperature. These cooking tests were conducted in laboratory conditions in an 82-m² kitchen using electric and gas stoves. The results show that the higher the cooking temperature, the higher the particle emission rate is, as shown with the 50-g bacon experiment; 0.52 mg.min⁻¹ emitted with minimum power (171°C ± 17°C) versus 13 mg.min⁻¹ with maximum power (242°C ± 5.2°C). Oil type may also influence the emission rate (chips, sunflower oil, 1.20 mg.min⁻¹; chips, olive oil, 2.80 mg.min⁻¹) and this confirms that grilling activities are the highest emission sources, especially with gas stove cooking. Other in-situ studies focused on cooking only one food, e.g. [94] for the PM_{2.5} emitted during the cooking of ground beef in a dwelling. In this study, the test conditions were set up to limit other indoor and outdoor emission sources, for example, by closing all the doors during the test period and ventilating before the experiment. The resulting measurements were divided into four rate ranges [3.3 μ m >2.1 μ m >1.1 μ m >0.65 μ m >0.43 μ m] and the value retained was the total average emission rate equal to 44.9 mg.min⁻¹. Recently, [95] also measured the PM_{2.5} and PM₁₀ generation rate in situ for cooking in an experimental building based on grilling and frying activities (fish, meat, egg). Measurements were taken for 30 min including the time for cooking the ingredients (fish broiling: 13 min; meat frying: 6 min; egg frying: 4 min; meat broiling, 3 min). The comparison of experimental building results [95] between frying (deep frying meat, 2.14 mg.min⁻¹) and grilling (meat broiling, 16.08 mg.min⁻¹) confirmed that higher particle emissions come from grilling/broiling activities.

In greater detail, [91,92] tested 25 typical Chinese dishes in a domestic kitchen based on an online survey of 309 families to determine common cooking behaviours in China. A professional cook performed five cooking methods with gas stoves (stir-frying, pan-frying, deep-frying, steaming and boiling), varying the weight of the ingredients, the type of meat, the meat/vegetable ratio and the type of oil. Measuring the emission generation rate includes the use of cooking tools during the process, with doors and windows closed and ventilation systems turned off. They found that water cooking methods such as boiling [0.08 mg.min⁻¹] and steaming [0.05 mg.min⁻¹] produce fewer emissions compared to other frying cooking methods (stir-frying [2.56 mg.min⁻¹], pan-frying[1.61 mg.min⁻¹].

4.4.1.4 In-situ rates obtained

The oldest *in-situ* study was conducted by [96] in the 1990s on a panel of 178 residents in Riverside, CA (USA). The PM $_{10}$ measurements were taken with personal exposure devices; at the same time the PM $_{2.5}$ rates were measured in each house using indoor and outdoor stationary monitors for two consecutive 12-h periods. The monitors used were based on a PM $_{10}$ filter behind an impactor plate. The PM $_{10}$ emission rate of cooking activities was estimated at 4.1 ± 1.6 mg.min $^{-1}$ with 40% of the particles smaller than 2.5 μ m, with 1.7 ± 0.6 mg.min $^{-1}$ as the PM $_{2.5}$ cooking emission rate. Other sources excluding cooking and smoking were estimated to emit 0.093 mg.min $^{-1}$ for the PM $_{10}$ fraction, with 20% smaller than 2.5 μ m (approximately 0.018 mg.min $^{-1}$) as PM $_{2.5}$. This study identified smoking and cooking as the two main indoor particle sources and provides an estimation of cooking emission rates but without distinguishing cooking methods.

In Australia, PM_{2.5} measurements were conducted on 16 houses [13]. The concentration was estimated simultaneously with a condensation particle counter and a photometer (sampling time 10 and 30 s) over more than 48 h in the kitchen. Air change rates were measured with a tracer gas

method using CO₂ during the unoccupied period. The emission rate was then calculated using concentration, air change rate, volume, and penetration efficiency and deposition rate. The authors published data on cooking, frying, grilling, toasting, smoking, vacuuming and other emission rates within the range [0.07; 2.78] mg.min⁻¹. The results confirm that cooking activities are the main PM_{2.5} sources in dwellings, with high emission levels during frying and grilling activities. The concentration increased more than 30 times the normal background concentration level during frying and up to 90 times during grilling.

A study in the USA also took PM_{2.5} measurements on 37 residential homes over 7 consecutive days for each of four seasons [90]. Concentrations were monitored for 24 h inside and outside using a filter-based monitor. The air change rate was measured with a tracer gas method, using perfluorocarbon. The air change rate was calculated with a mass balance. At the same time, each occupant carried a passive sample monitor, collecting the personal PM_{2.5} data every minute, and had to fill in a 15-min time-step schedule. This provided the occupants' location and activities so that emission rates of specific cooking actions (frying, grilling, toast, stovetop, burned) could be calculated with 36 mg.min⁻¹ as the average value within the range of [10; 470] mg.min⁻¹.

Recently, an *in-situ* campaign was conducted on 30 residential buildings and one experimental building to characterise PM₁₀ and PM_{2.5} generated by Korean cooking activities over 1 month [95]. In the residential buildings the emissions of soup cooking, broiling and frying activities were measured for a total of 30 min including both cooking time limited to 15 min to prevent over-cooking and preparation time. The results were compared with Western cooking types [13] [96]: Asian cooking gave slightly higher emission rate values within the range [0.39 mg.min⁻¹; 20.54 mg.min⁻¹] (Table 8).

Table 8: Overview of PM_{2.5} emission rates

Cooking activities	Emission rate [mg.min ⁻¹]	Duration [min]	Reference
Cooking (any food preparation using stove, no frying or grilling)	0.11		[13]
Frying (any food preparation using frying)	2.68	10	נבזן In-situ loads
Grilling (any food preparation using grilling)	2.78		III-SILU IUUUS
Frying		8-10	[93]

	Mozzarella 50 g (sunflower oil) electric pan, 190°C	0.03		Lab kitchen
	hips 50 g (sunflower oil) electric pan, 190°C	0.03		
	thips 50 g (sunflower oil) gas stove, max power	1.20		
	hips 50 g (peanut oil) electric frying pan, 190°C	0.06		
	hips 50 g (peanut oil) gas stove, max power	1.80		
	hips 50 g (olive oil) electric frying pan, 190°C	0.20		
	hips 50 g (olive oil) gas stove, max power	2.80		
Grillin	_			
	ubergine 30 g, gas stove, max power	0.52		
	heese 70 g, gas stove, max power	9.5		
	Vurstel 130 g, gas stove, max power	10		
	acon 50 g electric stove	1.5		
	acon 50 g gas stove, min power	0.52		
- B	acon 50 g gas stove, max power	13		
Cookii	=			
- R	esidential building, minimum value	0.39		
- R	esidential building, maximum value	20.54		
Boilin	g			
- R	esidential building, soup	2.01		[95]
Frying	7			Lab kitchen &
- R	esidential building	3.80	13	In-situ loads
- E	xperimental building, deep frying meat	2.14		
- E	xperiment building, frying 4 eggs	10.85		
Grillin	ng			
- R	esidential building	12,02		
- E	xperimental building, fish broiling	22.84		
	xperimental building, meat broiling	16.08		
Grillin	ng		20	[94]
	Ground beef	44.90	20	Lab kitchen
Cookii	ng			
	II cooking events	36		
	Aultiple events	29		
	tove top	17		[90]
	ven	10	11	In-situ loads
	urned	470		
Frying		60		
Grillin		173		
Boilin				
	У Леаl 2, chicken (oil), potatoes, green beans (water)	0.80		
	Neal 1, chicken, potatoes (oil), green beans (water)	0.62		[89]
Frying		0.02	28	Chamber-
	/ // // // // // // // // // // // // //	1.90	20	tested loads
				testeu 1000S
	Meal 4, stir-fry, chicken, prechopped vegetable, noodles	3.20		
	oil)			
Boilin		0.05		
	teaming	0.05		
	oiling	0.08	3-33	[91,92]
Frying			mean: 13	Lab kitchen
	Deep-frying	0.32		
	an to the state of	1 61		
	an-frying tir-frying	1.61 2.56		

4.4.2 Analysis and scenario proposals

We grouped cooking emission sources in four cooking types: boiling, frying, grilling and a total cooking category taking into account any food preparation (Table 9). As expected in the articles and confirmed by the minimum, mean, maximum and median values, grilling is the highest and boiling is the lowest PM_{2.5} emission cooking type.

Cooking type		Emission ra	te [mg.min ⁻¹]	
	min	mean	max	median
Boiling	0.05	0.74	2.01	0.44
Frying activities	0.03	5.32	60.00	1.85
Grilling activities	0.52	25.56	173.00	11.01
Total cooking	0.03	12.65	173.00	2.56

Table 9. Emission rate values

Finally, a few studies took into account the entire cooking process with several food types for a complete meal and the associated duration, especially for a representative French cooking scenario context.

Assessing ventilation systems and kitchen hood performance, the O'Leary study [89] is particularly relevant and fits our overall performance evaluation approach for ventilation systems. It took into account all the cooking steps in a European context. The authors proposed meal 1, with the lowest emissions, with chicken and potatoes fried in oil and green beans boiled in water [0.62 mg.min⁻¹]. Meal 3 with pasta bolognaise had an intermediary emission rate [1.9 mg.min⁻¹]. Meal 4 had the highest emissions with fried chicken and vegetable noodle wok cooking [3.2 mg.min⁻¹]. This gave three combinations of meal 1, 3 and 4 to propose three realistic cooking scenarios for 1 week:

- Low-emission cooking practices, with the hypothesis of 50% of the meals a week, emit fewer emissions, like meal 1, and the other 50% of the meals have medium emissions, like meal 3.
- Intermediate-emission cooking practices use diversified cooking methods, where the meal types are equally distributed over a week [1/3 meal 1; 1/3 meal 3; 1/3 meal 4].

High-emission cooking practices, with the hypothesis that 50% of the meals a week emit a high level of emissions, such as meal 4, and the other 50% meals emit a medium range of emissions, such as meal 3.

These three scenarios are summarised in Table 10 as mean values repeated twice a day with a cooking duration of 28 min.

Scenario	Emission rate [mg.min ⁻¹]	Duration [min]
Low-emission cooking practice (mainly boiling)	1.26	28
Intermediate-emission cooking practice	1.91	28
High-emission cooking practice (mainly grilling)	2.55	28

Table 10. PM_{2.5} emission rate scenarios

5 Synthesis of selected occupancy and emission input scenarios

Figure 2 summarises the input data for assessing ventilation performance at the design stage of a building, classified into pollutant scenario data, moisture scenario data, and inhabitant occupancy data. For PM_{2.5} and formaldehyde emission rates, we propose three classes of emissions: high, medium and low, to be selected depending on the available data at the design stage.

For formaldehyde for instance:

- If only A-class IAQ-labelled materials [97] are used and occupants are aware of this, the low-emission formaldehyde rate can be used in the IAQ calculation. To achieve a low emission rate, it is necessary to increase the occupants' awareness and help them become low-emitting occupants in all their activities and furnishings. Tools have been developed for occupants for this purpose [98]. An *in-situ* measurement campaign could also be required once the building is occupied to encourage the low emission rate.
- If no information is given, or only D-class IAQ-labelling materials are used, a high-emission formaldehyde rate must be used.

- In other cases, a medium-emission formaldehyde rate can be used.

538 For PM_{2.5}:

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- If the occupants are aware of IAQ, and their habits confirm they rarely use grilling, and if they agree with an *in-situ* measurement campaign once the building is occupied, a lowemission PM_{2.5} rate can be used in the IAQ calculation.
- If no information is given, a high-emission PM_{2.5} rate must be used.
- If the occupants are aware of IAQ, and their habits confirm they rarely use grilling, a medium-emission PM_{2.5} rate can be used.

Scenarios for ventilation performance assessement in residential building

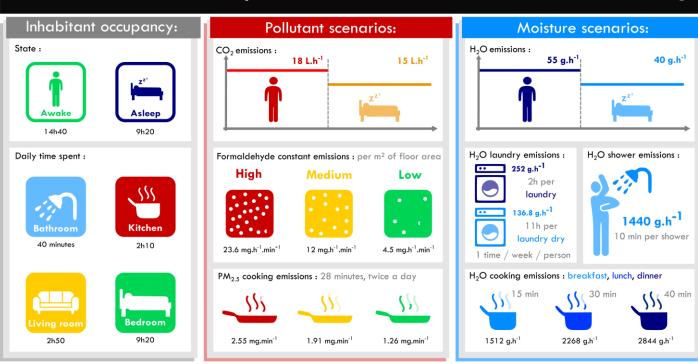


Figure 2. Selected input data to be used in a performance-based approach for ventilation.

6 Conclusion and perspectives

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applications in other countries.

We need a performance-based approach for assessing ventilation performance at the building scale, at the design stage, like the regulatory energy performance calculation to ensure energy performance. Ventilation performance assessment is often based on CO2, moisture, as they are commonly used, and on formaldehyde and PM_{2.5} as they would be complementary. To calculate such IAQ performance indicators, few occupancy schedules and emission rate parameters are available today. This paper provides an extensive literature review of 73 articles covering detailed occupancy schedules throughout the day and the year in a house, with emission rates reflecting occupants and activities (e.g. showering, cooking), as well as building material and furniture emission rates. We found relevant data on occupancy schedules, even if most of them were not precise enough to provide information on occupancy in all the rooms in a house. Substantial relevant data on CO2 and humidity emissions due to inhabitants' metabolism and activities are available in the literature and we selected those that could be used in a performance-based approach at the design stage. We noted a lack of exploitable data that could be used to model PM_{2.5} and formaldehyde average and peak emissions at the dwelling scale. As a result, we proposed using three levels of constant emission rates for formaldehyde: the low-emission rate: 4.5 μg.h⁻¹.m⁻²; the medium-emission rate: 12.0 μ g.h⁻¹.m⁻²; and the high-emission rate: 23.6 μ g.h⁻¹.m⁻². For PM_{2.5}, we also proposed three classes of emissions for cooking activities associated with a 28-min period twice a day: the low-emission rate: 1.26 mg.min⁻¹; the medium-emission rate: 1.91 mg.min⁻¹; and the high-emission rate: 2.55 mg.min⁻¹. Our objective was to build emission scenarios for a European, or even French, application. Nevertheless, the data gathered in the present review, as well as the way of analysing them and constructing scenarios are sufficiently described and referenced here and can be easily adapted for We focused on long-term exposure but this approach should also be adapted to consider acute exposure, another topic of interest and a health concern.

As for the study's limitations, there is a lack of consistent emission data on both formaldehyde and PM_{2.5} emissions at a building scale; consequently, the scenario proposals must be considered as a preliminary suggestion for overall ventilation performance assessment, which could be improved with further studies. The main objective of this work was to build a first baseline, directly usable in a method for assessing ventilation performance. Obviously, the proposed scenarios can evolve and be completed and improved in the future, as and when they are published, and according to the context of application in different regions or countries. One of the tracks would be to add relevant behaviours with other pollutant emissions, such as toasting toast for breakfast, for example, for PM_{2.5}. Another would be to link formaldehyde emissions to a series of scenarios for materials and furniture depending on the type of building and occupants, when consistent data are available. In addition, it is also possible to extend the IAQ indicators by adding other pollutants, although this then adds to the knowledge of emissions data and complicates the indication of IAQ levels and the operational aspect of the performance-based approach.

Nevertheless, it is now possible to assess the ventilation performance at the design stage of a residential building from an IAQ point of view, using the proposed occupancy schedules and emission scenarios as input data. In future work, these scenarios will be applied in a standardised approach, by modelling ventilation systems and strategies, air inlets and outlets configurations, airflow rates, etc. Such a standardised approach will allow for example a relative comparison of the performance of classic ventilation strategies and innovative ones, as smart ventilation strategies. In order to help at the design stage, the method can be used to select a ventilation system that targets a level of energy and IAQ performance, to comply with an overall performance requirement, but also to achieve IAQ labelled products and even improve IAQ awareness among occupants.

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