

# **Reservoir depressurization driven by passive gas emissions at Ambrym volcano**

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#### Abstract



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## 1 Introduction



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 ical of the 'classic volcano deformation cycle' (Biggs & Pritchard, 2017), eruptions may be counterintuitively preceded by periods of reservoir depressurization (Girona et al., 2014,  $2015$ .



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#### 2 Data and Methods

## 2.1 2015–2017 Subsidence Episode and 2018 Eruption





 brym's caldera subsided by up to 3 meters, and the lava lakes were completely drained 109 (Shreve et al., 2019; Hamling et al., 2019). Although  $> 0.4 \text{ km}^3$  of magma was intruded into the rift zone (Shreve et al., 2019; Hamling et al., 2019), causing drastic changes to the activity at Ambrym (e.g., lava lake drainage), less than 5 cm of precursory deforma- tion occurred in the year before the event (Figure 1b). Despite a lack of pre-eruptive up- lift, two primary observations indicate an increase in magma and gas supply to the sys- tem, which may have been precursors to the 2018 eruption. First, a new thermal anomaly  $\sim$ 1 km to the south of the main lava lake hosted in Marum crater is detected using Sentinel- 2 images sometime between 23 June 2016 and 10 March 2018 (Video S1). This indicates either a new vent for gas emissions or the presence of magma close to the surface, although discriminating between the two is ambiguous without additional observations. While the new vent may be a redirection of gas or magma that was already present at depth, its surface manifestation indicates a deviation from background activity. Second, the lava lake level rose rapidly in the weeks before the 2018 eruption, as documented by Moussallam

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 et al. (2021), which can indicate an increase in magma influx to the system, according to Patrick et al. (2019); Burgi et al. (2020); Global Volcanism Program (2017c).

## 2.2 2015–2018  $SO_2$  Gas Emissions





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#### 2.3 Geodetic Inversion

 To estimate magma reservoir depressurization, we invert surface displacements mea- surements spanning March 2015 to October 2017 measured by ALOS-2 and S1. Inter- ferograms were processed using the Interferometric SAR scientific computing environ- ment (ISCE) (Rosen et al., 2012). We multilook ascending S1 interferograms (Track 81) 36 times in range and 12 times in azimuth, filter with a power spectrum filtering strength of 0.3 and unwrap with SNAPHU (Chen & Zebker, 2001). The ascending ALOS-2 in-terferograms (Track 101) are multilooked 8 times in range and 16 times in azimuth, fil-

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ious locations at Ambrym from 30 October 2015 to 13 December 2018. Subsidence is mea-

–9–



## 2.4 Model Coupling Gas Emissions and Reservoir Depressurization





Figure 1: Time series of InSAR LOS displacement, thermal anomalies, and SO<sup>2</sup> emissions. a. A tectonic map showing the location of Ambrym island (from Shreve et al. (2019)) and a zoom on Ambrym's caldera, showing the velocity map of the Sentinel-1 ascending time series, assuming deformation spans 30 October 2015–31 October 2017. The caldera is outlined in black, and the extent of the lava flows emplaced in 2015 and 2018 are shown in pink and purple, respectively. The points plotted in the LOS displacement time series are identified with the colored circles (magenta measures displacement inside the deforming caldera, while green and blue measure background displacement near the borders or outside the caldera). The reference point is the black square. b. Top figure: The colored dots correspond to the cumulative LOS displacement calculated from a Sentinel-1 ascending time series in three different locations. The triangles outlined in black indicate the cumulative LOS displacement of an ALOS-2 interferogram.

Figure 1: (cont.) The three triangles plotted on 21 March 2015 overlap at 0 m. At each location, the mean of a 3 × 3 pixel box (∼0.6×0.6 km) is calculated. The black dotted lines indicate the (at least partly) cloud-free Sentinel-2 images available during this time period (see Video S1). The orange dots are the excess radiation of thermal anomalies detected within Benbow and Marum craters by the Moderate Resolution Imaging Spectroradiometer (MODIS), which has a pixel size of ∼1×1 km at nadir (Wright et al., 2004; Wright, 2016), and processed using the MODVOLC algorithm. The grey line shows temporal averages calculated using a sliding window of 30 days. Bottom figure: Empty grey dots represent the time-series of raw  $SO<sub>2</sub>$  mass burden integrated in an 150 km radius disk around Ambrym from OMI data (TRL product). Red-filled dots represent selected SO<sup>2</sup> mass burden estimates, after removing measurements affected by emissions from the nearby Ambae volcano. The period of elevated volcanic activity at Ambae is indicated by the grey area. Figure adapted from Shreve (2020).









Table 2: A description of the symbols used in Cases 1–3, as well as the ranges chosen for the parameters in this study. Symbols with no range presented are calculated from the defined parameters.



Figure 2: Inversion results. a. Geodetic observations (top row), synthetic displacements (middle row) and residuals (bottom row) of an ellipsoid at ∼1.9 km b.s.l (2.8 km beneath the vents). Left column is the Sentinel-1 velocity map, and right column is the ALOS-2 interferogram scaled to obtain displacement in centimeters year<sup>−</sup><sup>1</sup> . The caldera and craters are outlined in black, and the 2015 and 2018 lava flows are shown in pink and purple, respectively. b. A map and aerial view of the geometry of the depressurized ellipsoid estimated using Defvolc. Plot created with PyVista (Sullivan & Kaszynski, 2019).





<sup>240</sup> Based on the first assumption above, the pressure change at the base of the con- $241$  duit at time t can be written as

$$
1 - \frac{1}{2}
$$

$$
\Delta P(t) = P(t) - P(t_0) = \frac{g(m_{m,c}(t) + m_{g,c}(t))}{\pi R_c(t)^2} - P(t_0),\tag{1}
$$

242 where  $P(t)$  and  $P(t_0)$  are the pressure within the reservoir at time t and  $t_0$ ,  $m_{m,c}(t)$ <sup>243</sup> is the melt mass within the conduit of constant length L (Figure 3a),  $m_{g,c}(t)$  is the gas 244 mass within the conduit,  $R_c(t)$  is the conduit radius, and g is gravity. Equation 1 de-<sup>245</sup> scribes a pressurized reservoir which is sustaining the weight of the magma-filled cylin-246 drical conduit, which acts on a surface area of  $\pi R_c(t)^2$  (Girona et al., 2014).

<sup>247</sup> Taking the time derivative of this equation, we can obtain the rate of pressure change:

$$
\frac{\mathrm{d}\Delta P(t)}{\mathrm{d}t} = \frac{g\hat{\rho}_{m,c}(t)V_{m,c}(t)}{\pi R_c(t)^2} \left\{ \frac{1}{\hat{\rho}_{m,c}(t)V_{m,c}(t)} \left[ \hat{\rho}_{g,c}(t) \frac{\mathrm{d}V_{g,c}(t)}{\mathrm{d}t} + V_{g,c}(t) \frac{\mathrm{d}\hat{\rho}_{g,c}(t)}{\mathrm{d}t} + V_{g,c}(t) \frac{\mathrm{d}\hat{\rho}_{m,c}(t)}{\mathrm{d}t} \right] - \frac{2}{R_c(t)} \frac{\mathrm{d}R_c(t)}{\mathrm{d}t} \right\}.
$$
\n(2)

<sup>248</sup> We have substituted  $m_{m,c}(t) = \hat{\rho}_{m,c}(t)V_{m,c}(t)$  and  $m_{g,c}(t) = \hat{\rho}_{g,c}(t)V_{g,c}(t)$ , where <sup>249</sup>  $\hat{\rho}_{m,c}(t)$ ,  $V_{m,c}(t)$ ,  $\hat{\rho}_{g,c}(t)$ ,  $V_{g,c}(t)$  are the mean melt and gas density and volume in the con-<sup>250</sup> duit, respectively.

<sup>251</sup> We further simplify Equation 2 by assuming an elastic host rock, a constant gas **and melt density in the conduit**  $\left(\frac{d\hat{\rho}_{g,c}(t)}{dt} = 0\right)$  and  $\frac{d\hat{\rho}_{m,c}(t)}{dt} = 0$ , a conduit radius that does not change significantly over time  $\left(\frac{dR_c(t)}{dt} = 0\right)$ , and that the mean gas density <sup>254</sup> in the conduit is significantly smaller than the mean melt density  $(\hat{\rho}_{g,c}(t) \ll \hat{\rho}_{m,c}(t)).$ <sup>255</sup> We then obtain:

$$
\frac{\mathrm{d}\Delta P(t)}{\mathrm{d}t} = \frac{g\hat{\rho}_{m,c}(t)}{\pi R_c(t)^2} \frac{\mathrm{d}V_{m,c}(t)}{\mathrm{d}t}.
$$
\n(3)

<sup>256</sup> After considering the relationship between the volume of magma in the reservoir 257 and the partial density of water in a silicate melt,  $\rho_w$ , we can rewrite the above equa-<sup>258</sup> tion as:

$$
\frac{\mathrm{d}\Delta P(t)}{\mathrm{d}t}\left(\frac{\pi R_c(t)^2}{g\hat{\rho}_{m,c}(t)} + \frac{V_r(t)}{k_r}\right) = -\frac{\hat{Q}}{\rho_w},\tag{4}
$$

**259** which yields, by integration, assuming  $\hat{Q}$  is constant, Equation 45 from Girona et 260 al.  $(2014)$ :

$$
\Delta P(t) = -\frac{g\hat{\rho}_{m,c}(t_0)k_r\hat{Q}t}{\pi R_c(t_0)^2 \rho_w k + g\rho_w \hat{\rho}_{m,c}(t_0)V_r(t_0)}.
$$
\n(5)





3 Results

### 3.1 Geodetic Source Estimation





- timated in Section 2.2, we investigate whether a model coupling mass loss by passive de-
- gassing and reservoir depressurization reasonably explains these estimates. We acknowl-



3.2 Reservoir Depressurization Rate With No Magma Replenishment

 We explore various cases to investigate the effect of the fixed model parameters on reservoir depressurization rate. This includes fixing whether the host-rock is either elas- tic or viscoelastic, or if gas exsolution occurs in the conduit or reservoir. Finally, we dis-cuss the effect of magma replenishment on the reservoir depressurization rate.

#### 3.2.1 Elastic Rheology (Case 1)

 We calculate the theoretical reservoir depressurization rate at Ambrym in an elas-317 tic halfspace, for a range of reservoir volumes  $V_r(t_0)$  and conduit radii  $R_c(t_0)$ , given a water vapor flux of  $\hat{Q} \approx 110$  kt day<sup>-1</sup>. The higher the gas flux  $\hat{Q}$ , the higher the depres- surization rate. We also explore a range of reasonable values for the free parameters. For example, the reservoir bulk modulus  $k_r$  may realistically vary from  $5 \times 10^8$  to  $1 \times 10^{10}$   $MPa.$  As  $k_r$  increases, the host rock becomes more rigid. On the contrary, if the reser-



For larger reservoirs  $(V_r > 12 \text{ km}^3)$ , the conduit radius connecting the lava lakes to the <sup>345</sup> reservoir may be as low as 10 m.

#### <sup>346</sup> 3.2.2 Viscoelastic Rheology, Gas Exsolves in Conduit (Case 2)

 Case 1 assumes an elastic half-space, and we wish to investigate how viscoelastic- ity affects the response of the host rock to mass loss by degassing. We still assume that there is no exsolved gas in the reservoir and introduce a host rock with a Maxwell vis- $\frac{356}{200}$  coelastic rheology. Gas is exsolved in and degassed from the conduit of length L, which 351 has an initial gas volume fraction  $\beta_c = 0.1$ . As in Case 1, we impose steady-state magma convection in the conduit.

**353** Despite the addition of viscoelasticity, for the range of parameters of interest  $(V_r =$  $1-35 \text{ km}^3$  and  $R_c = 10-700 \text{ m}$ , no meaningful difference is noted between Case 1 and 355 Case 2 (Figure S7). For larger values of  $V_r$ , the solutions begin to diverge when the host 356 rock becomes less viscous ( $\mu \approx 10^{17}$  Pa s, Figure S7c). Aside from the minimum vis-<sup>357</sup> cosity necessary to maintain topography, we have no constraints on this parameter for <sup>358</sup> the host rock at Ambrym. Therefore, we proceed with Case 3 by setting the effective vis-<sup>359</sup> cosity of the crust to  $\mu = 10^{18}$  Pa s (Table S1) and allowing for gas exsolution in the <sup>360</sup> reservoir.

#### <sup>361</sup> 3.2.3 Viscoelastic Rheology, Gas Exsolves in Reservoir (Case 3)

<sup>362</sup> We assume that gases may exsolve within the reservoir according to Henry's Law 363  $(n_r(t) = \alpha - S[P(t_0) - \Delta P(t)]^{\frac{1}{2}}$  when  $\alpha > S[P(t_0) + \Delta P(t)]^{\frac{1}{2}}$ ) (e.g., Huppert & Woods,





# 3.3 Reservoir Depressurization Rate With Magma Replenishment (Case

4)

 In Section 3.2, depressurization rates estimated at Ambrym from geodetic observations can be obtained using the theoretical model for reservoir volumes  $> 12 \text{ km}^3$ . Us- ing an end member scenario that is consistent with the best-fit mean depressurization 381 rate of -2.15 MPa year<sup>-1</sup>, we investigate the change in depressurization rate that occurred 382 in October 2017. Between October 2017  $(t_0)$  and December 2018  $(t_1)$ , we assume no net depressurization of the magmatic system  $\left(\frac{d\Delta P(t_1 - t_0)}{dt} = 0\right)$  because the time series displacements are within the data uncertainty (∼1 cm),.



Figure 3: Degassing-induced depressurization theoretical model. a. A schematic showing the parameters included in the theoretical model. Modified after Girona et al. (2014). b. The pressurization rate change in MPa year-1 for a variety of conduit radii and reservoir volumes. The heavy black lines show the upper and lower bounds of the pressure change estimated in the geodetic inversion, and the heavy blue line shows the pressure change of the best-fit model. The dotted contour lines show pressure changes of -32, -16, -8, and -4 MPa year-1 . c. The reservoir pressure change evolution over time (black and blue corresponding to the upper and lower bounds and best-fit pressure change, respectively), as estimated from geodetic inversions. The vertical dotted line indicates the end of the subsidence episode. The dotted lines show the total reservoir pressure change if no change in the depressurization rate occurred in October 2017.



Both scenarios will consider a viscoelastic behavior of the host rock. Therefore, we can no longer use the simplified Equation 5 to calculate the reservoir pressure change. Without the simplifications of Equation 2 outlined in Section 2.4,  $\frac{d\Delta P(t)}{dt}$  is instead expressed as

$$
\frac{\mathrm{d}\Delta P(t)}{\mathrm{d}t} = \frac{C_1(t) + C_2(t)\Delta P(t)}{C_3(t)},\tag{6}
$$

400 where the constants  $C_1(t)$ ,  $C_2(t)$ , and  $C_3(t)$  are functions of the parameters in Equation <sup>401</sup> 2 (See also Equation 34 in Girona et al. (2014), which includes the rate of magma re-

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- <sup>402</sup> plenishment). The full expansion of these constants and a table of parameters used in
- <sup>403</sup> this study can be found in Table 2, Text S5, and Table S1.

Following Girona et al. (2014), the pressure change in the shallow reservoir can be expressed with an equation of the form

$$
\Delta P(t) = -\Delta P_{\infty} (1 - e^{-\Gamma t}),\tag{7}
$$

where  $\Delta P_{\infty} = \frac{C_1(t_0)}{C_2(t_0)}$  $\frac{C_1(t_0)}{C_2(t_0)}$  and  $\Gamma = -\frac{C_2(t_0)}{C_3(t_0)}$ where  $\Delta P_{\infty} = \frac{C_1(t_0)}{C_2(t_0)}$  and  $\Gamma = -\frac{C_2(t_0)}{C_3(t_0)}$ , assuming  $C_1(t)$ ,  $C_2(t)$  and  $C_3(t)$  do not vary

<sup>405</sup> significantly with time from their initial values.

The volumetric rate of magma replenishment is

$$
\frac{\mathrm{d}V_{\text{rep}}}{\mathrm{d}t} = \lambda(t)(\Delta P_s(t) - \Delta P(t)),\tag{8}
$$

 $\Delta P(t)$  is the pressure change in the shallow reservoir,  $\Delta P_s(t)$  is the deep source  $\frac{407}{407}$  overpressure, and  $\lambda(t)$  is, as defined by Girona et al. (2014), the hydraulic strength (or <sup>408</sup> strength of connectivity between the shallow and deep reservoirs), as derived from the <sup>409</sup> Hagen-Poiseuille law for the volumetric flow rate, given laminar fluid flow in a conduit <sup>410</sup> (Anderson & Segall, 2011; Le Mével et al., 2016).

$$
\lambda(t) = \frac{\pi R_d(t)^4}{8M\mu_{nd}},\tag{9}
$$

 $\mathbf{A}_{411}$  where  $R_d(t)$  is the radius of the dike connecting the deeper magma source to the shallow reservoir, M is the length of the dike, and  $\mu_{nd}$  is the viscosity of the replenished, undegassed magma. The maximum Reynold's number  $Re = \frac{\rho_m MV_{\rm rep}}{\pi R_d^2 \mu_m}$ , given  $\rho_m < 2700$ 414 kg m<sup>-3</sup>,  $V_{\text{rep}} < 5 \text{ m}^3 \text{s}^{-1}$ ,  $M < 15 \text{ km}$ ,  $\mu_m > 10^4 \text{ Pa s}$  and  $R_d > 2 \text{ m}$ , is ∼1600. This is



421 the model of active replenishment, considering instead an overpressured deep source  $(\Delta P_s(t) >$ 

422 0).



As stated in Equation 8, the volume of replenished magma (Figure 4a), is a function of the deep reservoir overpressure  $\Delta P_s(t)$ , the dike radius and length, and the magma viscosity. Because we have no constraints on these parameters, we instead explore the tradeoff between the lumped parameter  $\lambda(t_0)$  (hydraulic strength) and the deep source overpressure  $\Delta P_s(t_0)$  (Figure 4c, assuming a  $V_r = 29 \text{ km}^3$  and  $R_c = 10 \text{ m}$ , resulting in a shallow reservoir pressure change of ∼2.15 MPa year-1). A pressure balance occurs for a wide range of  $\Delta P_s(t_0)$  and  $\lambda(t_0)$ . However, the volume of replenished magma does not vary based on the depressurization rate measured, because the melt volume decrease in the conduit-reservoir system when  $\Delta P(t_n) = \Delta P(t_{n+1})$  (i.e., no net pressure change) is also constant and defined by  $\frac{dV_m(t)}{dt} = \frac{dV_d(t)}{dt}$  $\frac{d}{dt}(t) + \frac{dV_{\text{rep}}(t)}{dt}$  $\frac{\dot{\epsilon}_{\rm rep}(t)}{\mathrm{d}t} = \frac{-\hat{Q}}{\rho_w}$  $\frac{Q}{\rho_w} + \lambda(t_0)(\Delta P_s(t_0) \Delta P(t)$ ) (Figure 4a). In the case of no net pressure change, Equation 6 can be simplified

to

$$
\frac{d\Delta P(t)}{dt} = 0 \Longrightarrow \frac{\hat{Q}}{\rho_w} - \lambda(t_0)(\Delta P_s(t_0) - \Delta P(t)) - \frac{\Delta P(t)}{\mu}(V_r(t_0) + V_{m,c}(t_0)) = 0, \quad (10)
$$

<sup>437</sup> where volume change is determined by the balance between volume loss due to de-<sup>438</sup> gassing, volume increase due to magma influx, and the viscous response of the conduit <sup>439</sup> and reservoir. As shown in Figure 4a, the total replenished volume necessary to create a pressure balance  $\Delta P(t_{n+1})-\Delta P(t_n)=0$  within the shallow reservoir is  $\sim\!\!0.16~{\rm km}^3$ 440 over 14 months, or a magma supply rate into the shallow reservoir of  $\sim$ 4.3 m<sup>3</sup> s<sup>-1</sup>.



0) are indicated by the black and deep reservoir overpressure  $\Delta P_s(t_0)$ . The parameters that lead to a pressure balance in the shallow reservoir  $(\Delta P = 0)$  are indicated by the black Figure 4: Effect of magma replenishment. a. The replenishment volume over time for three cases: an overpressurized and underpressurized reser-Figure 4: Effect of magma replenishment. a. The replenishment volume over time for three cases: an overpressurized and underpressurized reserfor reasonable  $V_r$  and  $R_c$  that correspond to these values). The vertical dotted line represents when the deeper reservoir becomes instantaneously overfor reasonable  $V_r$  and  $R_c$  that correspond to these values). The vertical dotted line represents when the deeper reservoir becomes instantaneously overvoir (pink and blue lines, respectively) at  $t_1$  (December 2018) and a reservoir with a pressure balance (grey line). **b.** The lower and upper bounds and voir (pink and blue lines, respectively) at t1 (December 2018) and a reservoir with a pressure balance (grey line). b. The lower and upper bounds and pressurized. c. The relationship between shallow reservoir pressure difference between  $t_0$  (October 2017) and  $t_1$  (December 2018), hydraulic strength, best-fit shallow reservoir pressurization bounds (thin and thick black lines, respectively) over time as estimated from the theoretical model (Figure 3b best-fit shallow reservoir pressurization bounds (thin and thick black lines, respectively) over time as estimated from the theoretical model (Figure 3b pressurized. **c.** The relationship between shallow reservoir pressure difference between  $t_0$  (October 2017) and  $t_1$  (December 2018), hydraulic strength, line, and an overpressurized  $(\Delta P > 0)$  and underpressurized  $(\Delta P < 0)$  shallow reservoir by the pink and blue dotted lines, respectively. line, and an overpressurized (∆P > 0) and underpressurized (∆P < 0) shallow reservoir by the pink and blue dotted lines, respectively.  $\parallel$ and deep reservoir overpressure  $\Delta P_s(t_0)$ . The parameters that lead to a pressure balance in the shallow reservoir ( $\Delta P$ 

## 4 Discussion

## 4.1 Volume of Ambrym's Reservoir





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ization rate is based on the assumption of a constant  $\frac{H_2O}{SO_2}$  ratio, as well as a  $SO_2$  CMA  $\frac{1}{500}$  at 3 km. If these assumptions are incorrect, the H<sub>2</sub>O flux used as input for the theoret- $\frac{1}{501}$  ical model would be biased. Therefore, we run the model for H<sub>2</sub>O fluxes  $\pm 50\%$  (55 or **502** 165 kt; Figure S10). The estimated reservoir volume is >5 km<sup>3</sup> for a conduit radius  $R_c \sim$ 503 10 m, and the total replenished volume is  $V_{rep} = 0.077 \text{ km}^3$  when  $\hat{Q} = 55 \text{ kt}$  and 0.232  $\sin^3$  when  $\hat{Q} = 165$  kt.

## 4.1.2 Underestimation of Reservoir Volume Estimates



#### <sup>523</sup> 4.2 Magma Replenishment Prior to the 2018 Eruption

#### $\mu$ <sub>524</sub> 4.2.1 Magma Supply Rate

 $\epsilon_{\text{25}}$  According to our study, approximately 0.16 km<sup>3</sup> of magma would have been needed <sup>526</sup> to replenish the shallow reservoir to counteract the subsidence from degassing, equivs27 alent to a magma supply rate into the shallow reservoir  $\frac{dV_{rep}}{dt} \approx 4.3 \text{ m}^3 \text{ s}^{-1}$ . In a pres28 vious study, Allard et al. (2015) estimates that  $25 \text{ m}^3 \text{ s}^{-1}$  of magma is necessary to sus- $\frac{1}{229}$  tain the SO<sub>2</sub> flux released at the surface. However, the estimate from Allard et al. (2015) <sup>530</sup> corresponds to the volume of the magma batch that loses its gas and is recycled deeper <sup>531</sup> in the system per unit time. On the other hand, our estimate corresponds to the volume <sup>532</sup> lost in this recycling process, due to density changes during degassing, hence represent-<sup>533</sup> ing a fraction of the recycled volume of Allard et al. (2015). The ratio between the two estimates is approximately equal to a "shrinkage ratio"  $\beta = \frac{\rho_c - \rho_{nd}}{\rho_{nd}} = \frac{\Delta \rho}{\rho_{nd}} \approx 10\%,$  de-<sup>535</sup> fined as the density increase of the magma due to degassing (see Text S6 for a detailed <sup>536</sup> derivation).

 $\sigma$ <sub>537</sub> The magma supply rate estimated in this study  $(4.3 \text{ m}^3 \text{ s}^{-1})$  is on the same order 538 of magnitude as the mantle-driven surge in magma supply rate at Kīlauea in 2006, during the eruption from the Pu'u ' $\overline{O}$ ' $\overline{O}$ -Kupaianaha vent system which began in 1983 (Poland  $\epsilon_{\text{40}}$  et al., 2012). The supply rate was estimated to range between 6–7 m<sup>3</sup> s<sup>-1</sup>, depending on <sup>541</sup> the assumed magma compressibility (Poland et al., 2012). This estimate was made us- $\frac{1}{542}$  ing a calculation similar to Allard et al. (2015), with SO<sub>2</sub> flux used as a proxy for lava <sup>543</sup> effusion rates and consequently magma supply rate (Poland et al. (2012) also includes <sup>544</sup> volume change due to geodetic modeling of uplift that occurred in 2006). However, at

545 Kīlauea, the degassed magma is assumed to have erupted from the Pu'u  $\bar{O}$ ' $\bar{O}$  vent (as opposed to being recycled) and been replenished at the same rate with magma from depth. Therefore, these calculations are more comparable to our estimate than the supply rate estimated by Allard et al. (2015).

#### 4.2.2 Stealth Magma Replenishment

 Recent conceptual models describe volcanic unrest and eruption (in particular ini- tial conduit formation) in three phases. The first is "staging", which can occur either at the end of a previous eruption, during intereruptive time periods, or immediately pre- ceding an eruption (Roman & Cashman, 2018). In the case of replenishment at Ambrym, the latter seems the most likely. Earthquakes detected in mid-2017 were the first indi- cation of magma replenishment to shallower levels (Global Volcanism Program, 2017a), possibly indicating the shear failure of host rocks due to a magma intrusion. Further anal- ysis of seismic data is necessary to discriminate between the processes causing seismic-ity in August 2017.

 Around the same time, the number of active vents increased, also indicating a magma influx into the system (Video S1). After an increase in lava lake level (Moussallam et al., 2021), the shallow reservoir destabilized, causing the initial intra-caldera eruption of 14 December 2018, and eventually tapped the deeper magmatic system the following day (Shreve et al., 2019). The deeper portion of the magmatic system (>6.5 km b.s.l.) fed the rift zone intrusion and submarine eruption, according to melt inclusion entrapment pressures (Moussallam et al., 2021).



## 5 Conclusion





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